

POOL ENGINEERING
DOTT. ING. VIRGILIO M. CHIONO

Progettazione civile e impiantistica - Architettura - Consulenza - Certificazioni - Formazione - Qualità - Sicurezza - Ambiente

STUDIO DI INGEGNERIA
GEOM. ANDREA ZANUSSO

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Regione Piemonte
Città Metropolitana di Torino
Città di Moncalieri

Progetto

SCUOLA ELEMENTARE MONTESSORI (ex MAINA)

**Interventi di Manutenzione Straordinaria
dell'edificio scolastico ai fini dell'adeguamento
alle norme di prevenzione incendi
ed adeguamento impiantistico**

Localizzazione

Strada Vignotto, 22 - Moncalieri (To)

Fase Progettuale

Progetto ESECUTIVO

Titolo Tavola

**RELAZIONE ILLUSTRATIVA e DI CALCOLO
delle OPERE STRUTTURALI**

Committenza



Città di Moncalieri
P.zza Vittorio
Emanuele II
10024 Moncalieri (To)

Per validazione
Dirigente Settore gestione
Infrastrutture e Servizi Ambientali
arch. Teresa Pochettino

Professionisti



R.U.P.
arch. Teresa Pochettino

Coordinatore del Servizio
Edifici ed Impianti
geom. Dario Viola

Riferimenti

Rev. n° 000	Data	Ott 2015	Dis.	M.F.	Descr. Emissione definitiva
Rev. n° 001	Data		Dis.		Descr.
Rev. n° 002	Data		Dis.		Descr.
Rev. n° 003	Data		Dis.		Descr.

Tavola

Scala -
Cod. Comm. 150286
Cod. Tavola --
N° Tavola

RT STR

Pool Engineering S.A.
P. IVA 08926970016
Pool Engineering S.n.c.
P. IVA 09266390013



Cert. UNI EN ISO 9001
n° 10-Q-10121-TIC

Mod 760-00 08-2010 (Rev 002)
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SOMMARIO

<i>Sommario</i>	<i>1</i>
1 Premessa Generale	3
1.1 Assunti Progettuali	3
2 Relazione illustrativa	3
3 Relazione di calcolo	5
3.1 Report di calcolo	5
3.2 Report Grafico	133

1 PREMESSA GENERALE

1.1 Assunti Progettuali

Non essendo stato tutt'ora identificato da parte dell'amministrazione competente il tecnico incaricato per le indagini geologiche finalizzate all'identificazione dei parametri geotecnici di dettaglio, si è fatto riferimento a quanto noto alla geologia dell'area e si sono stimati i parametri geotecnici, proponendo una soluzione strutturale compatibile con le condizioni geotecniche mediocri. Tali parametri dovranno essere confermati da campagna analitica in sito prevista dall'amministrazione competente.

2 RELAZIONE ILLUSTRATIVA

TITOLO DEL PROGETTO

Realizzazione Scala esterna di sicurezza

COMMITTENTE

Città di Moncalieri
P.zza Vittorio Emanuele II
10024 Moncalieri (To)

PROGETTISTA

Dott. Ing. Virgilio M. CHIONO - Studio Associato POOL ENGINEERING
Vicolo Cugiano 4 - San Giorgio Can.se (To)
Ordine degli Ingegneri di Torino e Provincia al n° 8645 F

1. INDIVIDUAZIONE DEL MODELLO DI CALCOLO

1.1 DESCRIZIONE GENERALE DELL'OPERA

Oggetto della presente relazione e' l'analisi delle sollecitazioni ed il calcolo della struttura in cemento armato ordinario da realizzarsi in:

Lotto: Strada Vignotto, 21- 10024 Moncalieri (To)
Comune di: Moncalieri (To)
Proprieta

Città di Moncalieri
P.zza Vittorio Emanuele II
10024 Moncalieri (To)

Destinazione e tipologia dell'opera:

Il sito oggetto dell'intervento presenta i seguenti caratteri morfologico-geotecnici generali:

Realizzazione Scala esterna di sicurezza con opere in cemento armato normale e acciaio strutturale

La struttura e' composta dai seguenti elementi, previsti in calcestruzzo gettato in opera:

FONDAZIONI: soletta piena di fondazione in c.a.

Tale soluzione strutturale si e' adottata per diminuire i cedimenti, ed assicurare la funzionalità della struttura.

TRAVI: Profili in acciaio strutturale S235, sezioni tipo HE ed UPN

PILASTRI: Pilastri a sezione rettangolare e Profili in acciaio strutturale S235, sezioni tipo HE

1.2 NORMATIVE DI RIFERIMENTO

L'analisi della struttura in oggetto e' stata fatta utilizzando i metodi usuali della Scienza delle Costruzioni ed in conformità alle normative e leggi vigenti:

- Legge 5/11/1971 n. 1086: Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

- D.P.R. 6/6/2001 n. 380: Testo unico delle disposizioni legislative e regolamentari in materia edilizia.

- D.M. 14/1/2008: Norme tecniche per le costruzioni.

1.3 CRITERI DI ANALISI DELLA SICUREZZA

Con riferimento alle normative precedentemente citate, le strutture in oggetto sono verificate per quanto riguarda:

- verifica di resistenza;

- verifica a deformazione e fessurazione.

Calcestruzzo per le strutture in elevazione: classe C25/30

Acciaio in barre : B450C

Acciaio in Profili: S235/FE360

1.4 SCHEMATIZZAZIONE DELLA STRUTTURA E DEI VINCOLI

La struttura e' stata schematizzata escludendo il contributo degli elementi aventi rigidità e resistenza trascurabili a fronte dei principali. E' quindi stata considerata l'orditura a telaio tridimensionale, i solai ed i setti verticali ad elevata rigidità (vano ascensore, setti in cls).

Le opere di fondazione vengono assimilate a vincoli elastici di cui e' fornita la costante di rigidità. Le travi di fondazione sono schematizzate come poggianti su vincoli elastici distribuiti.

1.5 MODELLAZIONE DELLA STRUTTURA E DEI VINCOLI

La struttura e' modellata con il metodo degli elementi finiti, applicato a sistemi tridimensionali. Gli elementi utilizzati sono sia monodimensionali (trave con eventuali sconnessioni interne), che bidimensionali (piastre e membrane triangolari e quadrangolari). I vincoli sono considerati puntuali ed inseriti tramite le sei costanti di rigidità elastica, oppure come elementi asta poggianti su suolo elastico. Le sezioni oggetto di verifica nelle travi sono stampate a passo costante; dei gusci si conoscono le sollecitazioni nel baricentro dell'elemento stesso.

1.6 SCHEMATIZZAZIONE DELLE AZIONI

In accordo con le sopracitate normative, sono state considerate nei calcoli le seguenti azioni:

- pesi propri strutturali
- carichi permanenti portati dalla struttura
- carichi variabili sui solai, neve, vento.
- forze di piano simulanti il sisma, ricavate tramite analisi statica semplificata
- distorsioni termiche

Le condizioni ed i casi di carico prese in conto nei calcoli sono specificate nella stampa dei dati di input.

1.7 MODELLAZIONE DELLE AZIONI

Sono stati adottati i valori di carico come riportato in relazione e confacenti ai dettati normativi.

Carico Variabile Luoghi soggetti ad affollamento:

- 1) -400 - daN/m²

Le azioni sono state modellate tramite opportuni carichi concentrati e distribuiti su nodi ed aste.

1.8 MODELLAZIONE DEI MATERIALI

I materiali costituenti la struttura sono considerati elastici e con comportamento lineare. Le loro caratteristiche sono specificate nella stampa dei dati di input.

1.9 TIPO DI ANALISI

Le analisi strutturali condotte sono statiche in regime lineare. Il metodo di calcolo è ad elementi finiti. Il calcolo sismico è stato effettuato tramite analisi statica semplificata. La verifica delle membrature in cemento armato viene eseguita considerando tutte le caratteristiche di sollecitazione.

2 CODICE DI CALCOLO

2.1 INDIVIDUAZIONE DEL CODICE DI CALCOLO

Per il calcolo delle sollecitazioni e per la verifica di travi e pilastri in cemento armato si è fatto ricorso all'elaboratore elettronico utilizzando il seguente programma di calcolo:

DOLMEN WIN (R), versione 15.0 del 2015 prodotto, distribuito ed assistito dalla CDM DOLMEN srl, con sede in Torino, Via Drovetti 9/F.

Questa procedura è sviluppata in ambiente Windows, ed è stata scritta utilizzando i linguaggi Fortran e C. DOLMEN WIN permette l'analisi elastica lineare di strutture tridimensionali con nodi a sei gradi di libertà utilizzando un solutore ad elementi finiti. Gli elementi considerati sono la trave, con eventuali svincoli interni o rotazione attorno al proprio asse, ed il guscio, sia rettangolare che triangolare, avente comportamento di membrana e di piastra. I carichi possono essere applicati sia ai nodi, come forze o coppie concentrate, sia sulle travi, come forze distribuite, trapezie, concentrate, come coppie e come distorsioni termiche. I vincoli sono forniti tramite le sei costanti di rigidità elastica.

A supporto del programma è fornito un ampio manuale d'uso contenente fra l'altro una vasta serie di test di validazione sia su esempi classici di Scienza delle Costruzioni, sia su strutture particolarmente impegnative e reperibili nella bibliografia specializzata.

2.2 GRADO DI AFFIDABILITÀ DEL CODICE

L'affidabilità del codice di calcolo è garantita dall'esistenza di un'ampia documentazione di supporto, come indicato nel paragrafo precedente. La presenza di un modulo CAD per l'introduzione di dati permette la visualizzazione dettagliata degli elementi introdotti. È possibile inoltre ottenere rappresentazioni grafiche di deformate e sollecitazioni della struttura. Al termine dell'elaborazione viene inoltre valutata la qualità della soluzione, in base all'uguaglianza del lavoro esterno e dell'energia di deformazione.

2.3 MOTIVAZIONE DELLA SCELTA DEL CODICE

DOLMEN WIN permette in campo elastico lineare un'analisi dettagliata del comportamento dell'intera struttura, tenendo conto del comportamento irrigidente di setti anche complessi e solai considerati con la loro effettiva rigidità. È possibile inoltre scegliere il grado di affinamento dell'analisi di elementi complessi utilizzando mesh via via più dettagliate.

3. ESAME DEI RISULTATI E CONTROLLI

3.1 VALUTAZIONE DELLA CORRETTEZZA DEL MODELLO

Il modello di calcolo adottato è da ritenersi appropriato in quanto non sono state riscontrate labilità, le reazioni vincolari equilibrano i carichi applicati, la simmetria di carichi e struttura dà origine a sollecitazioni simmetriche.

4. GIUDIZIO MOTIVATO DI ACCETTABILITÀ DEI RISULTATI

L'analisi critica dei risultati e dei parametri di controllo nonché il confronto con calcolazioni di massima eseguite manualmente porta ad confermare la validità dei risultati.

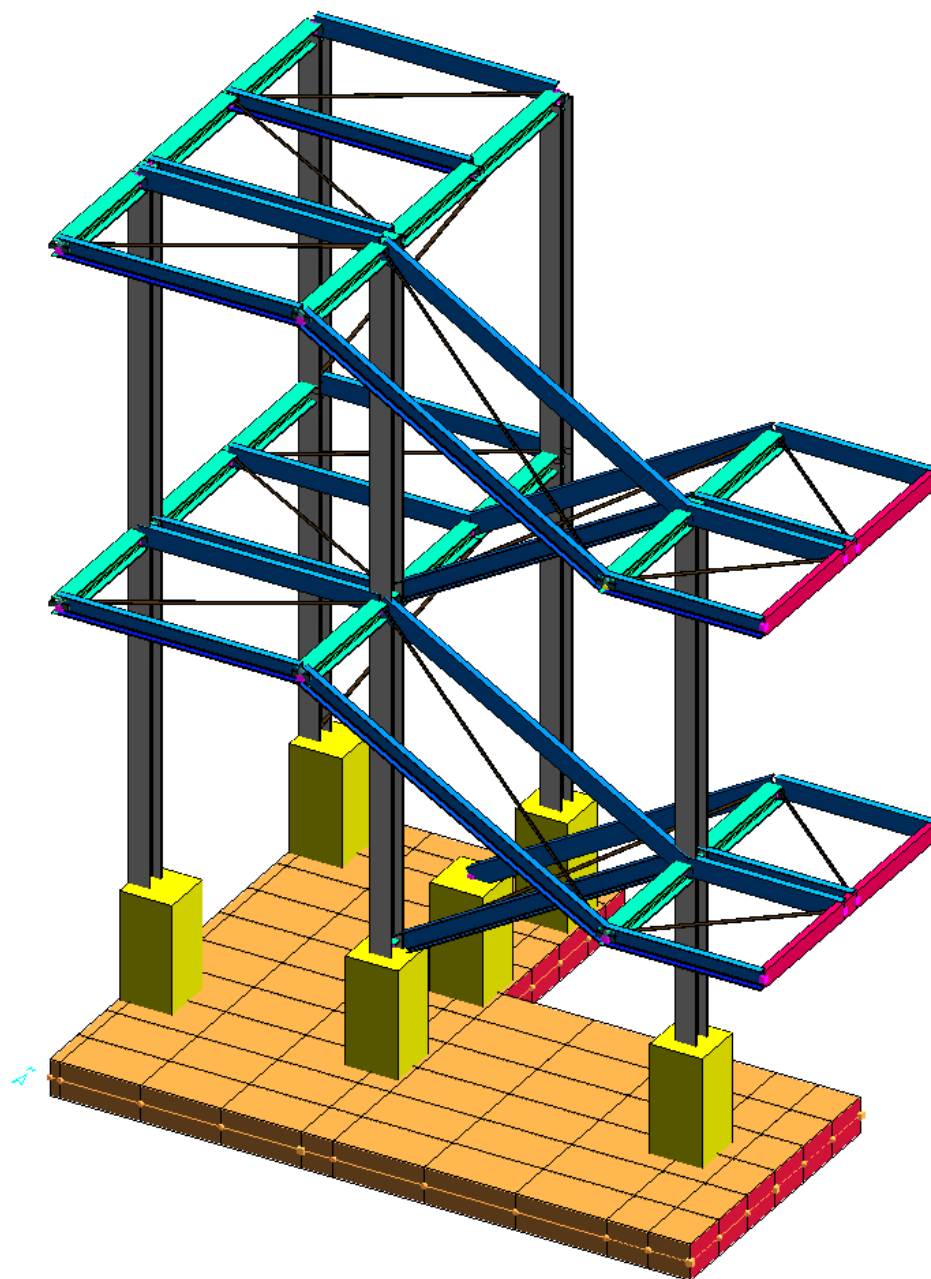
5. ALLEGATI

Alla presente relazione si allegano le seguenti stampe:

- dati di ingresso;
- sollecitazioni nelle aste e nei gusci;
- reazioni vincolari;
- verifiche di resistenza di travi e pilastri;
- diagrammi di sollecitazioni e deformazioni.

3 RELAZIONE DI CALCOLO

3.1 Report di calcolo




```
494      1      778      779      780      781
495      1      781      780      782      783
496      1      782      782      958      784
497      1      784      958      785      786
498      1      786      785      787      788
499      1      788      787      789      790

PROPRIETA' ASTE-----|-----|-----|-----|num.= 6
Nome Materiale Base Altezza Area Area tag. Y Area tag. Z
1 2 Kw vertic. 7.00 Kw orizz. 18.00 2.8000E+01 1.4400E+01 1.5400E+01
2 2 0.000000 0.000000 9.28333E+00 1.14000E+02 1.15400E+03
3 2 20.00 0.000000 5.93000E+01 2.00300E+03 5.69600E+03
4 2 36.00 0.000000 8.12000E+01 8.89000E+02 2.49200E+03
5 2 6.50 0.000000 6.20000E+01 1.20000E+01 1.36500E+01
6 2 3.00 0.000000 7.26558E+03 8.51000E+01 9.2500E+02
5 2 3.00 0.000000 3.00 2.3000E+00 1.2000E+00 1.2000E+00
6 1 50.00 0.000000 6.4000E+02 1.8000E+00 1.8000E+00
0.000000 2.000000 5.20833E+03 2.0833E+03 5.20833E+03

PROPRIETA' GUSCI-----|-----|-----|-----|num.= 1
Nome Materiale Sp. piastra Kw
1 1 35.00 35.00 5.000000

MATERIALI-----|-----|-----|-----|num.= 2
Nome Mod. elast. Coeff. nu Mod. tang. Peso spec. D11. te.
1 3.0000E+05 1.5000E-01 1.3000E+05 2.5000E-03 1.0000E-05
2 2.1000E+06 3.0000E-01 8.5000E+05 7.8500E-03 1.0000E-05

VINCOLI-----|-----|-----|-----|num.= 6
Nodo Rigid. X Rigid. Y Rigid. Z Rigid. RX Rigid. RY Rigid. RZ
958 bloccato bloccato libero libero libero libero
960 bloccato bloccato libero libero libero libero
964 bloccato bloccato libero libero libero libero
967 bloccato bloccato libero libero libero libero
969 bloccato bloccato libero libero libero libero
40 bloccato bloccato libero libero libero libero

CARICHI NODI-----|-----|-----|-----|num.= 308
Nome Nodo Direzione Intensita
1 154 : Forze Statiche (Analisi Semplificata)
155 308 : Momenti Torcenti Additionali

CARICHI ASTE-----|-----|-----|-----|num.= 200
Nome Asta Dir Tip REF Parametro 1 Parametro 2 Parametro 3 Parametro 4
309 PERM 4 2 Z RD glo -2.000
310 PERM 7 2 Z RD glo -2.000
311 PERM 31 2 Z RD glo -2.000
312 PERM 23 2 Z RD glo -2.000
313 PERM 15 2 Z RD glo -2.000
314 PERM 32 2 Z RD glo -2.000
315 PERM 24 2 Z RD glo -2.000
316 PERM 16 2 Z RD glo -2.000
317 PERM 8 2 Z RD glo -2.000
318 PERM 25 2 Z RD glo -2.000
319 PERM 17 2 Z RD glo -2.000
320 PERM 10 2 Z RD glo -2.000
321 PERM 2 2 Z RD glo -2.000
322 PERM 19 2 Z RD glo -2.000
323 PERM 27 2 Z RD glo -2.000
324 PERM 12 2 Z RD glo -2.000
325 PERM 130 2 Z RD glo -2.000
326 PERM 132 2 Z RD glo -2.000
327 PERM 134 2 Z RD glo -2.000
328 PERM 136 2 Z RD glo -2.000
329 PERM 145 2 Z RD glo -2.000
330 PERM 141 2 Z RD glo -2.000
331 PERM 142 2 Z RD glo -2.000
332 PERM 119 2 Z RD glo -2.000
333 PERM 122 2 Z RD glo -2.000
334 PERM 154 2 Z RD glo -2.000
335 PERM 156 2 Z RD glo -2.000
336 PERM 165 2 Z RD glo -2.000
337 PERM 138 2 Z RD glo -2.000
338 PERM 137 2 Z RD glo -2.000
339 ACC 4 2 Z RD glo -3.500
340 ACC 7 2 Z RD glo -3.500
341 ACC 31 2 Z RD glo -3.500
342 ACC 23 2 Z RD glo -3.500
343 ACC 15 2 Z RD glo -3.500
344 ACC 32 2 Z RD glo -3.500
345 ACC 24 2 Z RD glo -3.500
346 ACC 16 2 Z RD glo -3.500
347 ACC 8 2 Z RD glo -3.500
348 ACC 25 2 Z RD glo -3.500
349 ACC 17 2 Z RD glo -3.500
350 ACC 10 2 Z RD glo -3.500
351 ACC 2 2 Z RD glo -3.500
352 ACC 19 2 Z RD glo -3.500
353 ACC 27 2 Z RD glo -3.500
354 ACC 12 2 Z RD glo -3.500
355 ACC 130 2 Z RD glo -3.500
356 ACC 132 2 Z RD glo -3.500
357 ACC 134 2 Z RD glo -3.500
358 ACC 136 2 Z RD glo -3.500
359 ACC 145 2 Z RD glo -3.500
360 ACC 122 2 Z RD glo -3.500
361 ACC 119 2 Z RD glo -3.500
362 ACC 141 2 Z RD glo -3.500
363 ACC 142 2 Z RD glo -3.500
364 ACC 154 2 Z RD glo -3.500
365 ACC 156 2 Z RD glo -3.500
366 ACC 165 2 Z RD glo -3.500
367 ACC 138 2 Z RD glo -3.500
368 ACC 137 2 Z RD glo -3.500
369 NEVE 4 2 Z RD glo -1.200
370 NEVE 7 2 Z RD glo -1.200
371 NEVE 31 2 Z RD glo -1.200
372 NEVE 23 2 Z RD glo -1.200
373 NEVE 15 2 Z RD glo -1.200
374 NEVE 32 2 Z RD glo -1.200
375 NEVE 24 2 Z RD glo -1.200
376 NEVE 16 2 Z RD glo -1.200
377 NEVE 8 2 Z RD glo -1.200
378 NEVE 25 2 Z RD glo -1.200
379 NEVE 17 2 Z RD glo -1.200
380 NEVE 10 2 Z RD glo -1.200
381 NEVE 2 2 Z RD glo -1.200
382 NEVE 19 2 Z RD glo -1.200
383 NEVE 27 2 Z RD glo -1.200
384 NEVE 12 2 Z RD glo -1.200
385 NEVE 130 2 Z RD glo -1.200
386 NEVE 132 2 Z RD glo -1.200
387 NEVE 134 2 Z RD glo -1.200
388 NEVE 136 2 Z RD glo -1.200
389 NEVE 145 2 Z RD glo -1.200
390 NEVE 141 2 Z RD glo -1.200
391 NEVE 142 2 Z RD glo -1.200
392 NEVE 154 2 Z RD glo -1.200
393 NEVE 156 2 Z RD glo -1.200
394 NEVE 165 2 Z RD glo -1.200
395 NEVE 138 2 Z RD glo -1.200
396 NEVE 137 2 Z RD glo -1.200
397 Vento_Y 137 Y RD glo -1.800
398 Vento_Y 138 Y RD glo -1.800
399 Vento_Y 27 Y RD glo -0.400
400 Vento_Y 25 Y RD glo -0.400
401 Vento_Y 10 Y RD glo -0.400
402 Vento_Y 12 Y RD glo -0.400
403 Vento_Y 31 Y RD glo -0.400
404 Vento_Y 32 Y RD glo -0.400

PESTI PROPRIETA' ASTE-----|-----|-----|-----|
Cond. Nome Carichi Asta
1 405-506 2 4 7-8, 10, 12, 15-17, 19, 23-25, 27, 31-36,
38-59, 91-94, 99-102, 104-112, 116-117, 119-128,
130, 132, 134, 136-138, 141-143, 145-149, 154,
156-163, 165-166, 170-176, 178

CARICHI DI LINEA-----|-----|-----|-----|num.= 0
Nome numero coordinata
inizio Fine Cond. Diraz. inizio Fine Descrizione
1 405-506 2 4 7-8, 10, 12, 15-17, 19, 23-25, 27, 31-36,
38-59, 91-94, 99-102, 104-112, 116-117, 119-128,
130, 132, 134, 136-138, 141-143, 145-149, 154,
156-163, 165-166, 170-176, 178

CONDIZIONE DI CARICO-----|-----|-----|-----|num.= 9
Nome
1 Peso proprio N. carichi: 104
Lista carichi: 405-506
2 Permanente N. carichi: 30
Lista carichi: 309-338
3 A:Var_abitazione N. carichi: 30
Lista carichi: 339-368
4 Neve_(c000n_s_m) N. carichi: 28
Lista carichi: 369-396
5 Vento_Y N. carichi: 8
Lista carichi: 397-404
6 Sigma_X N. carichi: 77
Lista carichi: 1-77
7 Sigma_Y N. carichi: 77
Lista carichi: 78-154
8 Torcente_add_X N. carichi: 77
Lista carichi: 155-231
9 Torcente_add_Y N. carichi: 77
Lista carichi: 232-308

RISULTANTI DEI CARICHI (punto di applicazione nell'origine degli assi):
cond. FX FY FZ MX MY MZ
1 0.00000E+00 0.00000E+00 -8.152057E+03 -7.291865E+05 -7.030302E+04 0.000000E+00
2 0.00000E+00 0.00000E+00 -1.348847E+04 -4.915020E+05 9.962628E+05 0.000000E+00
3 0.00000E+00 0.00000E+00 -2.360483E+04 -8.637126E+05 1.744100E+06 0.000000E+00
4 0.00000E+00 0.00000E+00 -7.757864E+02 -2.255701E+05 6.752571E+05 0.000000E+00
5 0.00000E+00 -1.484847E+03 0.00000E+00 8.177556E+05 0.000000E+00 -2.642286E+04
6 2.106702E+03 0.00000E+00 0.00000E+00 0.00000E+00 1.254815E+06 -8.433983E+04
7 0.00000E+00 2.106702E+03 0.00000E+00 -1.254815E+06 0.00000E+00 8.103990E+04
8 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 -1.533155E+02 -3.926788E+04
9 0.00000E+00 0.00000E+00 0.00000E+00 -4.875793E+01 0.000000E+00 2.260460E+04
```


DATI ANALISI SISMICA:

Analisi sismica - Statica lineare - (NTC 2008)

DATI PROGETTO

Edificio sito in località MONCALIERE (long. 7,702 lat. 45,000100)

Categoria del suolo di fondazione = C

Coeff. di amplificazione stratigrafica Ss = 1,500

Coeff. di amplificazione topografica ST = 1,000

S = 1,500

Vita nominale dell'opera VN = 50 anni

Coefficiente d'uso CU = 1,5

Periodo di riferimento VR = 75,0

PMR : probabilità di superamento in VR = 10 %

Tempo di ritorno = 712

Coeff. di smorzamento viscoso = 5,0

Valori risultanti per :

ag 0,599 [g/10]

Tc 2,796

Tc 0,281

Edificio con struttura in acciaio :

Fattore di struttura q = 3,200

q = q0 * KR dove :

q0 = 4,00 2,00 + -1,0

KR = 0,8 (edifici non regolari in altezza)

Rapporto spettro di esercizio / spettro di progetto = 1,648

Coeff. lambda = 1,0000

Sd = 0,078 per T1 = 0,36

Numero condizioni generanti carichi sismici : 3

Cond. 001 : Peso,proprio con coeff. 1,000

Cond. 002 : Permanente con coeff. 1,000

Cond. 003 : Avar.abitazione con coeff. 0,300

Condizioni di carico sisma generate:

Cond. 005 : Sisma X

Cond. 007 : Sisma Y

Cond. 008 : Torcente add. X

Cond. 009 : Torcente add. Y

Carichi sismici :

[Baric. Y]	PlanI	Resi	C. distr.	Forze di piano	Torc. di piano	Baric. X]
cm]	cm]	dani	I	dani]	dancm]	cm]
[0,1,7]	120,0]	3434]	0,0192]	66]	923]	1713]
0,1]	285,0]	4482]	0,0456]	204]	2860]	1532]
66,5]	450,0]	7996]	0,0720]	575]	12085]	6618]
60,0]	620,0]	4439]	0,0992]	440]	6163]	3302]
60,1]	790,0]	6496]	0,1264]	821]	17237]	9439]

ANALISI DINAMICA lavoro : \1504..

PARAMETRI DI CALCOLO:

Calcolo secondo NTC 2008

Modello generale

Asci di vibrazione: X Y

Combinazione quadratica completa (CQC)

DATI PROGETTO

Edificio sito in località MONCALIERE (long. 7,702 lat. 45,000100)

Categoria del suolo di fondazione = C

Coeff. di amplificazione stratigrafica Ss = 1,500

Coeff. di amplificazione topografica ST = 1,000

S = 1,500

Vita nominale dell'opera VN = 50 anni

Coefficiente d'uso CU = 1,5

Periodo di riferimento VR = 75,0

PMR : probabilità di superamento in VR = 10 %

Tempo di ritorno = 712

Coeff. di smorzamento viscoso = 5,0

Valori risultanti per :

ag 0,599 [g/10]

Tc 2,796

Tc 0,281

Edificio con struttura in acciaio :

Fattore di struttura q = 3,200

q = q0 * KR dove :

q0 = 4,00 2,00 + -1,0

KR = 0,8 (edifici non regolari in altezza)

Rapporto spettro di esercizio / spettro di progetto = 1,648

CONDIZIONI DI RIFERIMENTO COEFFICIENTE

PESO RISULTANTE

1. 1,000

2. 1,000

3.*** TABELLA AUTORETTORE ***

n	PERIODO	MASSA ATTIVATA	COEFFICIENTI DI CORRELAZIONE
[sec]	%	SV	SV
1	0,436440	0,532	71,273
2	0,322633	0,335	1,762

3 | 0,220435 | 76,743 | 0,155 | 0,000 | 0,041 | 0,022 | 0,017 | 0,009 | 0,008 | 0,006 | 0,004

4 | 0,137223 | 0,001 | 0,010 | 0,000 | 0,270 | 0,141 | 0,038 | 0,036 | 0,018 | 0,018 | 0,012

5 | 0,116474 | 0,003 | 9,394 | 0,000 | 0,602 | 0,304 | 0,084 | 0,077 | 0,032 | 0,018

6 | 0,107385 | 0,022 | 5,740 | 0,000 | 0,141 | 0,126 | 0,045 | 0,034

7 | 0,084024 | 3,055 | 0,696 | 0,000 | 0,975 | 0,392 | 0,067

8 | 0,086277 | 0,285 | 0,558 | 0,000 | 0,249 | 0,073

9 | 0,068499 | 1,447 | 0,058 | 0,000 | 0,269

10 | 0,058310 | 6,104 | 0,031 | 0,000

MASSA TOTALE 88,537 89,497 0,000 |

***** AUTORETTORE N. 1 - periodo: 0,4164398

percentuale di massa attivata:

X Y Z

71,773 0,000

NDOO SX SY SZ

2 0,7938E-02 0,3904E-01 0,0000E+00

3 0,1753E-01 0,8209E-01 0,0000E+00

5 0,2875E-01 0,1524E+00 0,0000E+00

11 0,6245E-02 0,2909E-01 0,0000E+00

12 0,9728E-02 0,8269E-01 0,0000E+00

14 0,1662E-01 0,1524E+00 0,0000E+00

19 0,5984E-02 0,4995E-02 0,0000E+00

20 0,6230E-02 0,3909E-01 0,0000E+00

21 0,7698E-02 0,8269E-01 0,0000E+00

23 0,1475E-01 0,1524E+00 0,0000E+00

28 0,0946E-03 0,4995E-02 0,0000E+00

29 0,1393E-01 0,3913E-01 0,0000E+00

30 0,4796E-02 0,8270E-01 0,0000E+00

32 0,4938E-02 0,1524E+00 0,0000E+00

37 0,9617E-03 0,4995E-02 0,0000E+00

38 0,4894E-02 0,8269E-01 0,0000E+00

39 0,1569E-01 0,1524E+00 0,0000E+00

41 0,6149E-02 0,3909E-01 0,0000E+00

42 0,1461E-01 0,1683E+00 0,0000E+00

210 0,2874E-01 0,1527E+00 0,0000E+00

111 0,1702E-01 0,1525E+00 0,0000E+00

212 0,1486E-01 0,1525E+00 0,0000E+00

213 0,5698E-02 0,1527E+00 0,0000E+00

139 0,3914E-01 0,1692E+00 0,0000E+00

340 0,1618E-01 0,1698E+00 0,0000E+00

341 0,1534E-01 0,1697E+00 0,0000E+00

342 0,5271E-02 0,1692E+00 0,0000E+00

466 0,1638E-01 0,8411E-01 0,0000E+00

467 0,9471E-02 0,8411E-01 0,0000E+00

468 0,8286E-02 0,8313E-01 0,0000E+00

469 0,4825E-02 0,8311E-01 0,0000E+00

470 0,9378E-02 0,4008E-01 0,0000E+00

471 0,7014E-02 0,4045E-01 0,0000E+00

472 0,5857E-02 0,4043E-01 0,0000E+00

473 0,5139E-01 0,4001E-01 0,0000E+00

726 0,3813E-01 0,1894E+00 0,0000E+00

727 0,5258E-02 0,1894E+00 0,0000E+00

728 0,1362E-02 0,1893E+00 0,0000E+00

729 0,1636E-01 0,1894E+00 0,0000E+00

730 0,5138E-01 0,3662E-01 0,0000E+00

731 0,6276E-02 0,3662E-01 0,0000E+00

732 0,7094E-02 0,3665E-01 0,0000E+00

733 0,9578E-02 0,3666E-01 0,0000E+00

734 0,9622E-03 0,4423E-02 0,0000E+00

735 0,7692E-02 0,6218E-01 0,0000E+00

737 0,1233E-01 0,6202E-01 0,0000E+00

738 0,1112E-01 0,1309E+00 0,0000E+00

739 0,1233E-01 0,8257E-01 0,0000E+00

740 0,1111E-01 0,1524E+00 0,0000E+00

741 0,5588E-03 0,4423E-02 0,0000E+00

742 0,2929E-03 0,4995E-02 0,0000E+00

745 0,2127E-01 0,6227E-01 0,0000E+00

746 0,8590E-02 0,6218E-01 0,0000E+00

747 0,6799E-02 0,6218E-01 0,0000E+00

748 0,9472E-02 0,6216E-01 0,0000E+00

749 0,4474E-02 0,6208E-01 0,0000E+00

750 0,7846E-02 0,6294E-01 0,0000E+00

751 0,9157E-02 0,6310E-01 0,0000E+00

752 0,1672E-01 0,6331E-01 0,0000E+00

753 0,2416E-01 0,6310E-01 0,0000E+00

754 0,1243E-01 0,8333E-01 0,0000E+00

760 0,6994E-02 0,1307E+00 0,0000E+00

951 0,1568E-01 0,1310E+00 0,0000E+00

953 0,1104E-01 0,1525E+00 0,0000E+00

961 0,1591E-01 0,1683E+00 0,0000E+00

962 0,1339E-01 0,1683E+00 0,0000E+00

963 0,3698E-02 0,1310E+00 0,0000E+00

964 0,3756E-01 0,1682E+00 0,0000E+00

967 0,1662E-01 0,1310E+00 0,0000E+00

968 0,1664E-01 0,1310E+00 0,0000E+00

969 0,1473E-01 0,1310E+00 0,0000E+00

970 0,2398E-02 0,1309E+00 0,0000E+00

972 0,1694E-01 0,1316E+00 0,0000E+00

973 0,1486E-01 0,1315E+00 0,0000E+00

975 0,1395E-01 0,1316E+00 0,0000E+00

976 0,2876E-01 0,1316E+00 0,0000E+00

978 0,9615E-02 0,5723E-02 0,0000E+00

***** AUTORETTORE N. 2 - periodo: 0,3226327

percentuale di massa attivata:

X Y Z

0,335 1,762 0,000

NDOO SX SY SZ

2 0,4640E-01 0,2849E-01 0,0000E+00

3 0,3598E-01 0,2524E-01 0,0000E+00

5 0,1020E+00 0,6165E-01 0,0000E+00

11 0,1336E-01 0,2861E-01 0,0000E+00

12 0,1802E-01 0,2524E-01 0,0000E+00

14 0,3411E-01 0,6165E-01 0,0000E+00

19 0,6208E-02 0,1715E-02 0,0000E+00

20 0,8936E-02 0,2864E-01 0,0000E+00

21 0,2590E-01 0,2524E-01 0,0000E+00

23 0,3364E-01 0,6165E-01 0,0000E+00

28 0,1871E-02 0,1717E-02 0,0000E+00

29 0,4466E-02 0,2876E-01 0,0000E+00

30 0,2843E-01 0,2524E-01 0,0000E+00

32 0,4575E-02 0,6165E-01 0,0000E+00

37 0,8646E-03 0,1715E-02 0,0000E+00

38 0,1640E-01 0,2524E-01 0,0000E+00

39 0,2887E-01 0,6165E-01 0,0000E+00

41 0,1102E-01 0,2862E-01 0,0000E+00

42 0,2499E-01 0,1172E+00 0,0000E+00

210 0,1019E+00 0,6165E-01 0,0000E+00

211 0,3525E-01 0,6175E-01 0,0000E+00

212 0,2775E-01 0,6173E-01 0,0000E+00

213 0,4428E-01 0,6177E-01 0,0000E+00

139 0,1078E+00 0,1172E+00 0,0000E+00

340 0,3164E-01 0,1178E+00 0,0000E+00

341 0,1862E-01 0,1178E+00 0,0000E+00

342 0,4946E-02 0,1172E+00 0,0000E+00

466 0,5156E-01 0,2494E-01 0,0000E+00

467 0,1815E-01 0,2494E-01 0,0000E+00

468 0,1226E-01 0,2508E-01 0,0000E+00

469 0,4948E-01 0,2506E-01 0,0000E+00

964 -0.9882E-01 -0.2535E-01 0.0000E+00
967 -0.6033E-01 0.1248E-01 0.0000E+00
968 -0.3803E-01 0.2105E-01 0.0000E+00
969 -0.3607E-01 0.1245E-01 0.0000E+00
970 -0.1396E-01 0.1245E-01 0.0000E+00
971 -0.3874E-01 0.1245E-01 0.0000E+00
972 -0.3727E-01 0.1275E-01 0.0000E+00
973 -0.3317E-01 0.1267E-01 0.0000E+00
974 -0.3941E-01 0.1294E-01 0.0000E+00
975 -0.6001E-01 0.1294E-01 0.0000E+00
976 -0.6001E-01 0.2521E-01 0.0000E+00
977 -0.3447E-01 0.1645E+00 0.0000E+00
***** AUTOTETTORE N. 6 - periodo: 0.037850
percentuale di massa attivata :
X
0.022 Y
5.710 Z
0.000

NDO SX SZ
2 -0.5689E-01 0.1733E-01 0.0000E+00
3 -0.4158E-01 0.1645E+00 0.0000E+00
4 -0.3429E-01 0.8838E-01 0.0000E+00
11 -0.7856E-02 0.1715E-01 0.0000E+00
12 -0.6520E-02 0.1645E+00 0.0000E+00
13 -0.1307E-01 0.8941E-01 0.0000E+00
14 -0.1587E-01 0.8840E-01 0.0000E+00
19 -0.8528E-03 0.9882E-02 0.0000E+00
20 -0.1133E-02 0.1715E-01 0.0000E+00
21 -0.3830E-02 0.1645E+00 0.0000E+00
23 -0.1307E-01 0.8941E-01 0.0000E+00
28 -0.3956E-02 0.9878E-02 0.0000E+00
29 -0.3410E-01 0.1696E-01 0.0000E+00
30 -0.1420E-01 0.1645E+00 0.0000E+00
32 -0.4313E-02 0.8847E-01 0.0000E+00
37 -0.1063E-02 0.9882E-02 0.0000E+00
38 -0.5249E-02 0.1645E+00 0.0000E+00
39 -0.1447E-01 0.8840E-01 0.0000E+00
41 -0.4441E-02 0.1714E-01 0.0000E+00
42 -0.5783E-02 0.1857E-01 0.0000E+00
210 -0.3432E-02 0.8884E-01 0.0000E+00
211 -0.1439E-02 0.8850E-01 0.0000E+00
212 -0.1344E-02 0.8849E-01 0.0000E+00
213 -0.5208E-02 0.8868E-01 0.0000E+00
339 -0.8940E-01 0.1838E-01 0.0000E+00
340 -0.3030E-01 0.1674E-01 0.0000E+00
341 -0.1886E-02 0.1978E-01 0.0000E+00
342 -0.1543E-02 0.1307E-01 0.0000E+00
466 -0.4628E-01 0.1652E+00 0.0000E+00
467 -0.6965E-02 0.1652E+00 0.0000E+00
468 -0.4000E-02 0.1644E+00 0.0000E+00
469 -0.1420E-01 0.1644E+00 0.0000E+00
470 -0.3805E-01 0.1743E-01 0.0000E+00
471 -0.8390E-02 0.1736E-01 0.0000E+00
472 -0.8412E-02 0.1645E+00 0.0000E+00
473 -0.3182E-01 0.1897E-01 0.0000E+00
726 -0.2648E-01 0.8888E-02 0.0000E+00
727 -0.1581E-02 0.8828E-02 0.0000E+00
728 -0.2658E-02 0.8890E-02 0.0000E+00
729 -0.9940E-02 0.8880E-02 0.0000E+00
730 -0.1319E-01 0.3560E-01 0.0000E+00
731 -0.1401E-02 0.3553E-01 0.0000E+00
732 -0.8501E-02 0.3557E-01 0.0000E+00
733 -0.5818E-01 0.3566E-01 0.0000E+00
734 -0.1066E-02 0.1487E-01 0.0000E+00
735 -0.2755E-02 0.1924E+00 0.0000E+00
737 -0.2250E-01 0.1934E+00 0.0000E+00
738 -0.1734E-01 0.1924E+00 0.0000E+00
739 -0.2291E-01 0.1639E+00 0.0000E+00
740 -0.1708E-01 0.8849E-01 0.0000E+00
741 -0.4989E-01 0.1487E-01 0.0000E+00
742 -0.4983E-02 0.9881E-02 0.0000E+00
745 -0.2263E-01 0.1931E+00 0.0000E+00
746 -0.3978E-02 0.1924E+00 0.0000E+00
747 -0.1545E-02 0.1924E+00 0.0000E+00
748 -0.1383E-01 0.1921E+00 0.0000E+00
749 -0.1370E-01 0.1924E+00 0.0000E+00
750 -0.3284E-02 0.1932E+00 0.0000E+00
751 -0.6589E-02 0.1932E+00 0.0000E+00
752 -0.4471E-01 0.1934E+00 0.0000E+00
753 -0.2247E-01 0.1936E+00 0.0000E+00
754 -0.2288E-01 0.1639E+00 0.0000E+00
760 -0.4851E-02 0.1196E+00 0.0000E+00
951 -0.1446E-01 0.1173E-01 0.0000E+00
953 -0.1794E-01 0.8847E-01 0.0000E+00
961 -0.7463E-02 0.1859E-01 0.0000E+00
962 -0.4313E-02 0.1853E-01 0.0000E+00
963 -0.3129E-02 0.1828E-01 0.0000E+00
964 -0.2133E-01 0.1874E-01 0.0000E+00
967 -0.3497E-01 0.1212E+00 0.0000E+00
968 -0.1572E-01 0.1210E+00 0.0000E+00
969 -0.1310E-01 0.1210E+00 0.0000E+00
970 -0.3881E-02 0.1209E+00 0.0000E+00
971 -0.1403E-01 0.1247E+00 0.0000E+00
973 -0.1347E-01 0.1240E+00 0.0000E+00
975 -0.1809E-01 0.1244E+00 0.0000E+00
976 -0.3413E-01 0.1248E+00 0.0000E+00
978 -0.1064E-02 0.3617E-02 0.0000E+00
***** AUTOTETTORE N. 7 - periodo: 0.084045
percentuale di massa attivata :
X
3.065 Y
0.636 Z
0.000

NDO SX SZ
2 -0.1406E+00 0.1039E+00 0.0000E+00
3 -0.1101E+00 -0.1122E-01 0.0000E+00
4 -0.6946E-01 0.2834E-02 0.0000E+00
11 -0.5333E-01 0.1036E+00 0.0000E+00
12 -0.8172E-01 -0.1128E-01 0.0000E+00
14 -0.7803E-01 0.2823E-02 0.0000E+00
19 -0.3867E-02 0.4750E-02 0.0000E+00
20 -0.3301E-01 0.1036E+00 0.0000E+00
21 -0.8262E-01 -0.1123E-01 0.0000E+00
23 -0.8241E-01 0.2801E-02 0.0000E+00
24 -0.6977E-02 0.4753E-02 0.0000E+00
29 -0.4067E-01 0.1040E+00 0.0000E+00
30 -0.9501E-01 0.1123E-01 0.0000E+00
32 -0.1044E+00 0.2784E-02 0.0000E+00
37 -0.3605E-02 0.4750E-02 0.0000E+00
38 -0.8202E-01 0.1123E-01 0.0000E+00
39 -0.8705E-01 0.2810E-02 0.0000E+00
41 -0.4534E-01 0.1035E+00 0.0000E+00
42 -0.2262E-01 0.8752E-01 0.0000E+00
210 -0.6235E-01 0.1735E-01 0.0000E+00
211 -0.6239E-01 0.2584E-02 0.0000E+00
212 -0.8605E-01 0.2584E-02 0.0000E+00
213 -0.8608E-01 0.2501E-02 0.0000E+00
339 -0.1372E+00 -0.8002E-01 0.0000E+00
340 -0.3533E-01 0.3504E-01 0.0000E+00
341 -0.5911E-01 0.5084E-01 0.0000E+00
342 -0.4653E+00 -0.9595E-01 0.0000E+00
466 -0.1166E+00 -0.1116E-01 0.0000E+00
467 -0.5165E-01 0.1116E-01 0.0000E+00
468 -0.8240E-01 0.1074E-01 0.0000E+00
469 -0.9576E-01 0.1070E-01 0.0000E+00
470 -0.1410E+00 0.1018E+00 0.0000E+00
471 -0.6760E-01 0.1066E+00 0.0000E+00
472 -0.2344E-01 0.1053E+00 0.0000E+00
473 -0.3620E-01 0.1078E+00 0.0000E+00
726 -0.1380E+00 0.1487E+00 0.0000E+00
727 -0.2664E+00 0.1489E+00 0.0000E+00
728 -0.5541E-01 0.1484E+00 0.0000E+00
729 -0.1004E-01 0.1482E+00 0.0000E+00
730 -0.3677E-01 0.1518E-01 0.0000E+00

731 -0.2655E-01 0.3093E-01 0.0000E+00
732 -0.6548E-01 0.3089E-01 0.0000E+00
733 -0.2401E-01 0.3105E-01 0.0000E+00
734 -0.3618E-02 0.7245E-03 0.0000E+00
735 -0.9082E-01 0.1903E-01 0.0000E+00
737 -0.3625E-01 0.1828E-01 0.0000E+00
738 -0.1340E+00 0.3016E-01 0.0000E+00
739 -0.3941E-01 0.1154E-01 0.0000E+00
740 -0.1321E+00 0.2598E-02 0.0000E+00
741 -0.1028E-01 0.7230E-03 0.0000E+00
742 -0.6203E-01 0.4762E-02 0.0000E+00
745 -0.7766E-01 0.1839E-01 0.0000E+00
746 -0.3048E-01 0.1904E-01 0.0000E+00
747 -0.9122E-01 0.1904E-01 0.0000E+00
748 -0.3971E-01 0.1878E-01 0.0000E+00
749 -0.9440E-01 0.1872E-01 0.0000E+00
750 -0.8534E-01 0.1878E-01 0.0000E+00
751 -0.3638E-01 0.1873E-01 0.0000E+00
752 -0.1142E+00 0.1759E-01 0.0000E+00
753 -0.6206E-01 0.1858E-01 0.0000E+00
754 -0.6398E-01 0.1192E-01 0.0000E+00
760 -0.5927E-01 0.3009E-01 0.0000E+00
951 -0.7985E-01 0.2974E-01 0.0000E+00
953 -0.1360E+00 0.3002E-02 0.0000E+00
961 -0.3545E-02 0.8749E-01 0.0000E+00
962 -0.4238E-01 0.8757E-01 0.0000E+00
963 -0.2763E+00 0.8778E-01 0.0000E+00
964 -0.1478E+00 0.8651E-01 0.0000E+00
967 -0.6408E-01 0.2963E-01 0.0000E+00
968 -0.1493E-01 0.2974E-01 0.0000E+00
969 -0.8287E-01 0.2978E-01 0.0000E+00
730 -0.1098E+00 0.3011E-01 0.0000E+00
972 -0.6793E-01 0.3005E-01 0.0000E+00
973 -0.8623E-01 0.3007E-01 0.0000E+00
975 -0.1378E+00 0.3883E-01 0.0000E+00
976 -0.6248E-01 0.2946E-01 0.0000E+00
978 -0.1591E-02 0.1178E-01 0.0000E+00
***** AUTOTETTORE N. 8 - periodo: 0.082678
percentuale di massa attivata :
X
0.285 Y
0.558 Z
0.000

NDO SX SZ
2 -0.1213E+00 -0.1157E+00 0.0000E+00
3 -0.2687E-01 0.1186E+00 0.0000E+00
5 -0.8807E-01 0.6407E-01 0.0000E+00
11 -0.1806E-01 0.1153E+00 0.0000E+00
12 -0.1478E-01 0.1186E+00 0.0000E+00
14 -0.1656E-01 0.6409E-01 0.0000E+00
740 -0.1578E-02 0.6216E-02 0.0000E+00
20 -0.6845E-03 0.1159E+00 0.0000E+00
21 -0.8636E-02 0.1186E+00 0.0000E+00
23 -0.1581E-02 0.6411E-01 0.0000E+00
28 -0.3580E-02 0.6231E-02 0.0000E+00
729 -0.1404E+00 0.1164E+00 0.0000E+00
730 -0.1112E+00 0.1186E+00 0.0000E+00
32 -0.6539E-01 0.6403E-01 0.0000E+00
37 -0.5886E-02 0.6223E-02 0.0000E+00
38 -0.1828E-01 0.1186E+00 0.0000E+00
39 -0.3001E-01 0.6405E-01 0.0000E+00
41 -0.8674E-02 0.1158E+00 0.0000E+00
42 -0.1481E-02 0.2543E-01 0.0000E+00
210 -0.8787E-01 0.6477E-01 0.0000E+00
211 -0.1809E-01 0.6444E-01 0.0000E+00
212 -0.5821E-01 0.6442E-01 0.0000E+00
213 -0.6647E-01 0.6481E-01 0.0000E+00
219 -0.1037E-01 0.2028E-01 0.0000E+00
340 -0.8313E-03 0.2175E-01 0.0000E+00
341 -0.8312E-04 0.2214E-01 0.0000E+00
342 -0.7916E-01 0.2210E-01 0.0000E+00
466 -0.1643E+00 0.1215E+00 0.0000E+00
467 -0.5646E-01 0.1215E+00 0.0000E+00
468 -0.9315E-02 0.1182E+00 0.0000E+00
469 -0.1112E+00 0.1181E+00 0.0000E+00
730 -0.1193E+00 0.1144E+00 0.0000E+00
471 -0.2867E-01 0.1185E+00 0.0000E+00
472 -0.8642E-01 0.1196E+00 0.0000E+00
473 -0.1013E+00 0.1225E+00 0.0000E+00
21 -0.6976E-01 0.1196E-01 0.0000E+00
727 -0.5809E-01 0.4193E-01 0.0000E+00
728 -0.7641E-03 0.4177E-01 0.0000E+00
729 -0.5240E-02 0.4171E-01 0.0000E+00
730 -0.1023E+00 0.8286E-02 0.0000E+00
731 -0.7123E-01 0.7123E-02 0.0000E+00
732 -0.2278E-01 0.8278E-02 0.0000E+00
733 -0.1198E+00 0.8275E-02 0.0000E+00
734 -0.3576E-02 0.6371E-02 0.0000E+00
735 -0.2139E-01 0.9918E-01 0.0000E+00
737 -0.1993E+00 0.9886E-01 0.0000E+00
738 -0.1096E+00 0.6242E-01 0.0000E+00
739 -0.4012E+00 0.1178E+00 0.0000E+00
740 -0.1090E+00 0.6425E-01 0.0000E+00
741 -0.3674E-02 0.6394E-02 0.0000E+00
742 -0.5646E-02 0.6238E-02 0.0000E+00
745 -0.1533E+00 -0.9989E-01 0.0000E+00
746 -0.3801E-01 0.9903E-01 0.0000E+00
747 -0.1189E+00 0.9902E-01 0.0000E+00
748 -0.1113E+00 0.9905E-01 0.0000E+00
749 -0.1103E+00 0.9905E-01 0.0000E+00
750 -0.1018E-01 0.9917E-01 0.0000E+00
751 -0.2823E-01 0.9908E-01 0.0000E+00
752 -0.1646E+00 0.9980E-01 0.0000E+00
753 -0.1996E+00 0.9881E-01 0.0000E+00
754 -0.2015E+00 0.1177E+00 0.0000E+00
760 -0.6581E-01 0.6152E-01 0.0000E+00
951 -0.1195E-01 0.6246E-01 0.0000E+00
953 -0.1159E+00 0.6439E-01 0.0000E+00
961 -0.2403E-02 0.2544E-01 0.0000E+00
962 -0.4588E-02 0.2538E-01 0.0000E+00
963 -0.5614E-01 0.2480E-01 0.0000E+00
964 -0.5893E-01 0.1545E-01 0.0000E+00
967 -0.9013E-01 0.6246E-01 0.0000E+00
969 -0.1701E-01 0.6246E-01 0.0000E+00
970 -0.6540E-01 0.6246E-01 0.0000E+00
972 -0.1877E-01 0.6411E-01 0.0000E+00
973 -0.1847E-01 0.6383E-01 0.0000E+00
975 -0.1415E+00 0.6405E-01 0.0000E+00
976 -0.8888E-01 0.6375E-01 0.0000E+00
978 -0.3610E-02 0.6235E-02 0.0000E+00
***** AUTOTETTORE N. 9 - periodo: 0.068489
percentuale di massa attivata :
X
1.447 Y
0.058 Z
0.000

NDO SX SZ
2 -0.1484E+00 0.1107E+00 0.0000E+00
3 -0.5164E-01 0.3266E-01 0.0000E+00
5 -0.7625E-01 0.1201E-01 0.0000E+00
11 -0.1395E-01 0.1115E+00 0.0000E+00
12 -0.3013E-01 0.3270E-01 0.0000E+00
14 -0.9566E-01 0.1202E-01 0.0000E+00
19 -0.1234E-01 0.3116E-02 0.0000E+00
20 -0.8295E-01 0.1116E+00 0.0000E+00
21 -0.3270E-01 0.3270E-01 0.0000E+00
22 -0.3338E-01 0.1199E-01 0.0000E+00
28 -0.6198E-02 0.3120E-02 0.0000E+00
29 -0.2714E+00 0.1120E+00 0.0000E+00
30 -0.5849E-01 0.3583E-01 0.0000E+00

32 -0.4156E-01 -0.1199E-01 0.0000E+00
37 -0.1258E-01 0.3116E-02 0.0000E+00
38 -0.2401E-01 0.3105E-01 0.0000E+00
39 -0.3156E-01 0.1199E-01 0.0000E+00
41 -0.2623E-01 0.1115E+00 0.0000E+00
42 -0.2859E-01 0.3178E-01 0.0000E+00
210 -0.2027E-01 0.1106E-01 0.0000E+00
211 -0.3308E-01 0.1154E-01 0.0000E+00
212 -0.3405E-01 0.1182E-01 0.0000E+00
213 -0.4220E-01 0.1145E-01 0.0000E+00
214 -0.1152E+00 0.2894E-01 0.0000E+00
340 -0.1554E-01 0.3900E-01 0.0000E+00
341 -0.3727E-01 0.3834E-01 0.0000E+00
342 -0.1387E+00 0.4654E-01 0.0000E+00
466 -0.3672E+00 0.3685E-01 0.0000E+00
467 -0.9440E-01 0.3683E-01 0.0000E+00
468 -0.2072E-01 0.3177E-01 0.0000E+00
469 -0.3848E-01 0.3172E-01 0.0000E+00
470 -0.1351E+00 0.1022E+00 0.0000E+00
728 -0.1629E-01 0.1134E+00 0.0000E+00
472 -0.4061E-01 0.1172E+00 0.0000E+00
473 -0.2713E-01 0.1205E+00 0.0000E+00
728 -0.1157E+00 0.1675E+00 0.0000E+00
727 -0.1395E+00 0.1673E+00 0.0000E+00
730 -0.3489E-01 0.1664E+00 0.0000E+00
739 -0.1665E-01 0.1665E+00 0.0000E+00
730 -0.2726E+00 0.1782E+00 0.0000E+00
731 -0.4070E-01 0.1772E+00 0.0000E+00
732 -0.1848E-01 0.1770E+00 0.0000E+00
733 -0.1788E-01 0.1788E+00 0.0000E+00
734 -0.1258E-01 0.7492E-02 0.0000E+00
735 -0.3623E-01 0.9008E-01 0.0000E+00
737 -0.1453E+00 0.9135E-01 0.0000E+00
738 -0.1571E-01 0.5533E-02 0.0000E+00
975 -0.1378E+00 0.3883E-01 0.0000E+00
740 -0.1542E-01 0.1186E-01 0.0000E+00
741 -0.1344E-02 0.7495E-01 0.0000E+00
742 -0.2918E-03 0.3115E-02 0.0000E+00
745 -0.9913E-01 0.8861E-01 0.0000E+00
746 -0.4127E-01 0.8806E-01 0.0000E+00
747 -0.3094E-01 0.9101E-01 0.0000E+00
748 -0.4639E-01 0.9106E-01 0.0000E+00
749 -0.4136E-01 0.9129E-01 0.0000E+00
750 -0.2687E-01 0.9106E-01 0.0000E+00
751 -0.3128E-01 0.9000E-01 0.0000E+00
752 -0.4186E-01 0.8817E-01 0.0000E+00
730 -0.1457E+00 0.1140E+00 0.0000E+00
754 -0.1449E+00 0.1361E-01 0.0000E+00
760 -0.4127E+00 0.1516E-02 0.0000E+00
973 -0.3134E-01 0.6215E-02 0.0000E+00
953 -0.1915E-01 0.1184E-01 0.0000E+00
962 -0.3053E-01 0.6222E-02 0.0000E+00
963 -0.3662E-01 0.3725E-01 0.0000E+00
964 -0.1478E+00 0.1164E+00 0.0000E+00
967 -0.1881E-01 0.6270E-02 0.0000E+00
968 -0.3053E-01 0.6222E-02 0.0000E+00
969 -0.3235E-01 0.6186E-02 0.0000E+00
970 -0.3001E-01 0.6274E-02 0.0000E+00
972 -0.3323E-01 0.7728E-02 0.0000E+00
973 -0.3385E-01 0.7596E-02 0.0000E+00

[illegible]

409	0.000000	0.000000	-0.011572	-0.003660	0.000031	0.000000
410	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
420	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
430	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
440	0.156093	0.025045	0.019595	-0.002599	0.000036	0.000342
451	0.149591	0.025122	0.010306	0.000000	0.000046	0.000528
461	0.150842	0.025182	0.000000	0.000000	0.000000	0.000000
471	0.147719	0.025208	0.001568	-0.000044	0.000322	0.000331
481	0.150368	0.025268	0.000000	0.000000	0.000000	0.000000
491	0.150368	0.025268	0.000000	0.000000	0.000000	0.000000
500	0.128239	0.033364	-0.016439	0.001328	0.000180	-0.000768
511	0.112656	0.043124	-0.018821	-0.009309	0.000128	-0.000848
521	0.110261	0.043124	-0.018821	-0.009309	0.000128	-0.000848
531	0.096209	0.050277	0.015940	-0.005050	0.000088	0.000104
541	0.096209	0.050277	0.015940	-0.005050	0.000088	0.000104
550	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
560	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
570	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
580	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
590	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
600	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
610	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
620	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
630	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
640	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
650	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
660	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
670	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
680	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
690	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
700	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
710	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
720	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
730	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
740	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
750	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
760	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
770	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
780	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
790	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
800	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
810	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
820	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
830	0.087865	0.050277	0.015940	-0.005050	0.000088	0.000104
840	0.087865	0.050277	0.015940	-0.005050	0.000088	0.0001

[illegible]

42	-0.005064	-0.01864	0.000407	-0.000028	-0.000063	0.000122
43	0.000000	0.000000	0.000379	0.000004	-0.000017	0.000000
44	0.000000	0.000000	0.000000	0.000000	-0.000002	0.000000
168	0.000000	0.000000	0.000063	-0.000002	-0.000002	0.000000
169	-0.019921	-0.002377	-0.000000	-0.000000	-0.000000	0.000000
211	-0.007310	-0.002233	-0.000549	0.000073	-0.000000	0.000094
212	-0.005632	-0.002323	-0.000552	-0.000000	0.000033	-0.000100
213	-0.00424	-0.002423	-0.000664	-0.000000	-0.000004	0.000000
339	-0.019951	-0.018729	-0.002140	0.000537	-0.000095	-0.000094
340	-0.005425	-0.015742	-0.000664	-0.000000	-0.000000	0.000000
431	-0.003787	-0.018174	-0.000618	-0.000000	0.000015	-0.000079
434	0.006517	-0.015844	-0.000618	-0.000000	-0.000000	0.000000
466	-0.010319	-0.010518	-0.000401	0.000071	0.000014	-0.000536
467	-0.003593	-0.011598	-0.000626	-0.000078	0.000017	-0.000554
468	-0.003554	-0.014045	-0.000626	-0.000078	0.000017	-0.000554
469	-0.00041	-0.000485	0.000397	-0.000002	0.000050	-0.000564
470	-0.000831	-0.000957	-0.000626	-0.000078	0.000017	-0.000554
471	-0.000358	-0.000390	0.000126	-0.000083	-0.000049	-0.000147
472	-0.000337	-0.003013	-0.000626	-0.000078	0.000017	-0.000554
473	-0.000789	-0.004851	-0.000331	-0.000029	-0.000000	0.000000
476	-0.019966	-0.012347	-0.000003	-0.000002	-0.000045	-0.000094
477	-0.000000	-0.002536	-0.000626	-0.000078	0.000017	-0.000554
478	-0.003912	-0.003255	-0.000521	-0.000004	0.000077	0.000155
479	-0.006498	-0.002545	-0.000617	-0.000077	0.000016	-0.000554
730	0.000081	-0.000000	-0.000050	-0.000004	-0.000023	-0.000138
731	-0.001448	-0.009619	-0.000715	-0.000049	0.000000	-0.000576
732	-0.002946	-0.008628	-0.000715	-0.000049	0.000000	-0.000576
733	-0.008639	-0.000000	0.000274	-0.000000	-0.000028	-0.000333
734	-0.000089	-0.000733	0.000027	-0.000000	-0.000000	0.000000
735	-0.000734	0.011297	-0.000330	-0.000028	-0.000125	-0.000575
737	0.014943	-0.011278	-0.000589	-0.000027	0.000070	-0.000547
738	0.000000	-0.000899	-0.000715	-0.000049	0.000000	-0.000576
739	0.017212	-0.004452	-0.000729	-0.000000	0.000029	-0.000538
740	0.002251	-0.002243	-0.000796	-0.000000	-0.000000	0.000000
741	0.000075	0.000000	-0.000546	-0.000000	0.000070	-0.000547
742	0.000075	0.000000	-0.000546	-0.000000	0.000070	-0.000547
743	0.000097	-0.011282	-0.000048	-0.000000	-0.000100	-0.000504
746	-0.002390	0.011297	-0.000579	-0.000028	-0.000044	-0.000561
747	-0.000000	-0.011297	-0.000579	-0.000028	-0.000044	-0.000561
748	0.001545	-0.012920	-0.000546	-0.000018	-0.000021	-0.000539
749	-0.000000	-0.012920	-0.000546	-0.000018	-0.000021	-0.000539
750	-0.000046	-0.000140	0.000119	-0.000000	0.000045	-0.000537
751	-0.005512	-0.014121	-0.000579	-0.000028	-0.000049	-0.000572
752	-0.010094	-0.011371	-0.000579	-0.000028	-0.000049	-0.000572
753	-0.012975	-0.014020	-0.000591	-0.000028	-0.000025	-0.000537
754	-0.012862	-0.014054	-0.000579			

CONCENTRANTI NOXI		9 Torcento_add_y			
CONCENTRANTE		SU_SV_SZ [cm]; RX_RV_RZ [rad]			
UNITA di MISURA:					
Coefficiente moltiplicativo:		1.000000			
NOXI	NOXI	RX	RV	RZ	
1	0.000000	0.000000	0.000018	0.000001	0.000000
2	0.000451	0.000000	0.000000	0.000000	0.000000
3	0.000530	0.000000	0.000000	0.000000	0.000000
4	0.000907	0.000000	0.000000	0.000000	0.000000
5	0.000126	0.000000	0.000000	0.000000	0.000000
6	0.000120	0.000000	0.000000	0.000000	0.000000
7	0.000048	0.000000	0.000000	0.000000	0.000000
8	0.000043	-0.000001	0.000000	0.000000	0.000000
9	0.000000	0.000000	0.000000	0.000000	0.000000
10	0.000125	0.000000	0.000000	0.000000	0.000000
11	0.000247	0.000000	0.000000	0.000000	0.000000
12	0.000000	0.000000	0.000000	0.000000	0.000000
13	-0.000000	0.000000	0.000000	0.000000	0.000000
14	0.000000	0.000000	0.000000	0.000000	0.000000
15	-0.000000	0.000000	0.000000	0.000000	0.000000
16	0.000000	0.000000	0.000000	0.000000	0.000000
17	0.000000	0.000000	0.000000	0.000000	0.000000
18	0.000000	0.000000	0.000000	0.000000	0.000000
19	0.000000	0.000000	0.000000	0.000000	0.000000
20	0.000000	0.000000	0.000000	0.000000	0.000000
21	0.000000	0.000000	0.000000	0.000000	0.000000
22	0.000000	0.000000	0.000000	0.000000	0.000000
23	0.000000	0.000000	0.000000	0.000000	0.000000
24	0.000000	0.000000	0.000000	0.000000	0.000000
25	0.000000	0.000000	0.000000	0.000000	0.000000
26	0.000000	0.000000	0.000000	0.000000	0.000000
27	0.000000	0.000000	0.000000	0.000000	0.000000
28	0.000000	0.000000	0.000000	0.000000	0.000000
29	0.000000	0.000000	0.000000	0.000000	0.000000
30	0.000000	0.000000	0.000000	0.000000	0.000000
31	0.000000	0.000000	0.000000	0.000000	0.000000
32	0.000000	0.000000	0.000000	0.000000	0.000000
33	0.000000	0.000000	0.000000	0.000000	0.000000
34	0.000000	0.000000	0.000000	0.000000	0.000000
35	0.000000	0.000000	0.000000	0.000000	0.000000
36	0.000000	0.000000	0.000000	0.000000	0.000000
37	0.000000	0.000000	0.000000	0.000000	0.000000
38	0.000000	0.000000	0.000000	0.000000	0.000000
39	0.000000	0.000000	0.000000	0.000000	0.000000
40	0.000000	0.000000	0.000000	0.000000	0.000000
41	0.000000	0.000000	0.000000	0.000000	0.000000
42	0.000000	0.000000	0.000000	0.000000	0.000000
43	0.000000	0.000000	0.000000	0.000000	0.000000
44	0.000000	0.000000	0.000000	0.000000	0.000000
45	0.000000	0.000000	0.000000	0.000000	0.000000
46	0.000000	0.000000	0.000000	0.000000	0.000000
47	0.000000	0.000000	0.000000	0.000000	0.000000
48	0.000000	0.000000	0.000000	0.000000	0.000000
49	0.000000	0.000000	0.000000	0.000000	0.000000
50	0.000000	0.000000	0.000000	0.000000	0.000000
51	0.000000	0.000000	0.00		

870	0.018724	0.506923	-0.001334	0.000059	0.0001851	0.0000805
872	0.039585	0.008292	0.016514	-0.001283	0.000105	0.0000544
874	0.025258	0.529496	-0.007498	0.000000	0.000000	0.000000
875	0.063676	0.597487	-0.015467	-0.001027	0.000027	0.0000565
876	0.057993	0.592330	-0.007498	0.000000	0.000000	0.000000
878	0.026360	0.014540	-0.000662	-0.000320	0.0000209	0.0001303
879	0.000000	0.000000	0.011244	-0.000033	0.000021	0.000000
880	0.000000	0.000000	0.002468	0.000000	0.000023	0.000000
881	0.000000	0.000000	0.0009751	-0.0005572	0.0000134	0.000000
882	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
883	0.000000	0.000000	0.0006132	-0.000037	0.0000265	0.000000
884	0.000000	0.000000	0.004620	-0.000613	0.0000169	0.000000
885	0.000000	0.000000	0.005242	-0.000613	0.0000169	0.000000
886	0.000000	0.000000	0.000318	-0.0006639	0.0000221	0.000000
887	0.000000	0.000000	0.000005	-0.0006639	0.0000221	0.000000
888	0.000000	0.000000	0.000000	-0.0006639	0.0000221	0.000000
889	0.000000	0.000000	-0.000076	-0.0006639	0.0000221	0.000000
890	0.000000	0.000000	-0.000025	-0.0006639	0.0000221	0.000000
891	0.000000	0.000000	-0.0006639	-0.0006639	0.0000221	0.000000
892	0.000000	0.000000	-0.000040	-0.0006639	0.0000221	0.000000
893	0.000000	0.000000	0.015995	-0.000548	0.0000234	0.000000
894	0.000000	0.000000	0.015993	-0.000548	0.0000220	0.000000
895	0.000000	0.000000	0.014761	-0.000548	0.0000220	0.000000
896	0.000000	0.000000	0.012499	-0.000548	0.0000207	0.000000
897	0.000000	0.000000	0.011115	-0.000548	0.0000207	0.000000
898	0.000000	0.000000	0.010602	-0.000548	0.0000207	0.000000
899	0.000000	0.000000	0.008004	-0.000548	0.0000207	0.000000
900	0.000000	0.000000	0.007141	-0.000548	0.0000207	0.000000
1001	0.000000	0.000000	0.007479	-0.000579	0.0000106	0.000000
1002	0.000000	0.000000	0.000850	-0.000579	0.0000106	0.000000
1003	0.000000	0.000000	0.000190	-0.000579	0.0000106	0.000000
1004	0.000000	0.000000	0.0000396	-0.000579	0.0000106	0.000000
1005	0.000000	0.000000	-0.000046	-0.000579	0.0000106	0.000000
1006	0.000000	0.000000	-0.000340	-0.000815	0.0000189	0.000000
1007	0.000000	0.000000	-0.000574	-0.000815	0.0000189	0.000000
1008	0.000000	0.000000	-0.000464	-0.000815	0.0000189	0.000000
1009	0.000000	0.000000	-0.000738	-0.000815	0.0000247	0.000000
1010	0.000000	0.000000	-0.000829	-0.000815	0.0000247	0.000000
1011	0.000000	0.000000	-0.000863	-0.000893	0.0000187	0.000000
1012	0.000000	0.000000	-0.000862	-0.000893	0.0000187	0.000000
1013	0.000000	0.000000	-0.011564	-0.000946	0.0000255	0.000000
1014	0.000000	0.000000	-0.013262	-0.000978	0.0000248	0.000000
1015	0.000000	0.000000	-0.010429	-0.000986	0.0000290	0.000000
1016	0.000000	0.000000	-0.016121	-0.000986	0.0000290	0.000000
1017	0					

771	0.000000	0.000000	0.000354	-0.000004	-0.000021	0.000000
772	0.000000	0.000000	0.000496	-0.000002	-0.000028	0.000000
773	0.000000	0.000000	0.000496	-0.000002	-0.000028	0.000000
774	0.000000	0.000000	0.000495	-0.000001	-0.000025	0.000000
775	0.000000	0.000000	0.000495	-0.000001	-0.000025	0.000000
776	0.000000	0.000000	0.000548	0.000001	-0.000024	0.000000
777	0.000000	0.000000	0.000495	-0.000009	-0.000028	0.000000
778	0.000000	0.000000	0.000495	-0.000009	-0.000028	0.000000
779	0.000000	0.000000	0.000413	-0.000000	0.000032	0.000000
780	0.000000	0.000000	0.000413	-0.000000	0.000032	0.000000
781	0.000000	0.000000	0.000493	-0.000000	0.000031	0.000000
782	0.000000	0.000000	0.000560	-0.000010	0.000036	0.000000
783	0.000000	0.000000	0.000385	-0.000000	0.000032	0.000000
784	0.000000	0.000000	0.000289	-0.000002	0.000011	0.000000
785	0.000000	0.000000	0.000278	-0.000000	0.000011	0.000000
786	0.000000	0.000000	0.000243	0.000006	0.000014	0.000000
787	0.000000	0.000000	0.000291	-0.000000	0.000024	0.000000
788	0.000000	0.000000	0.000321	-0.000002	0.000024	0.000000
789	0.000000	0.000000	0.000391	0.000024	0.000034	0.000000
790	0.000000	0.000000	0.000431	0.000000	0.000034	0.000000
791	0.000000	0.000000	0.000590	-0.000004	0.000036	0.000000
792	0.000000	0.000000	0.000417	-0.000026	0.000048	0.000000
793	0.000000	0.000000	0.000247	-0.000000	0.000024	0.000000
794	0.000000	0.000000	-0.000248	-0.000000	0.000002	0.000000
795	0.000000	0.000000	-0.000232	-0.000000	0.000002	0.000000
801	0.000000	0.000000	-0.000257	-0.000002	-0.000002	0.000000
802	0.000000	0.000000	-0.000251	-0.000005	0.000006	0.000000
803	0.000000	0.000000	-0.000265	-0.000000	0.000002	0.000000
804	0.000000	0.000000	-0.000265	-0.000000	-0.000003	0.000000
805	0.000000	0.000000	-0.000261	-0.000000	0.000002	0.000000
806	0.000000	0.000000	-0.000273	-0.000006	0.000000	0.000000
807	0.000000	0.000000	-0.000255	-0.000000	0.000011	0.000000
808	0.000000	0.000000	0.000311	-0.000000	0.000000	0.000000
813	0.000000	0.000000	-0.000691	-0.000018	0.000049	0.000000
814	0.000000	0.000000	-0.000774	-0.000000	0.000000	0.000000
909	0.000000	0.000000	-0.000587	-0.000000	0.000051	0.000000
924	0.000000	0.000000	0.000444	-0.000002	0.000051	0.000000
925	0.000000	0.000000	0.000495	-0.000000	0.000051	0.000000
961	-0.005975	0.020709	0.000335	-0.000021	-0.000089	0.000012
962	0.022576	-0.022323	0.000800	0.000000	0.000025	0.000000
963	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
964	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000031
967	0.000000	0.000000	-0.000273	-0.000007	0.000021	-0.000031
968	0.000000	0.000000	0.000369	-0.000000	0.000021	0.000000
969	0.000000	0.000000	-0.000550	-0.000002	0.000053	0.000538
970	0.000000	0.000000	-0.0005			

[illegible][illegible]

972	-0.007094	0.002783	0.005652	0.0000729	0.0000567	0.0001004
973	-0.005934	0.002769	0.005623	0.0000729	0.0000567	0.0001004
974	0.002748	0.000773	0.005566	0.0000730	0.0000568	0.0001000
975	-0.005969	0.002774	0.005626	0.0000740	0.0000568	0.0001004
976	-0.004990	-0.000861	-0.005698	0.0000740	0.0000568	0.0001004
977	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
978	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
979	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
980	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
981	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
982	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
983	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
984	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
985	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
986	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
987	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
988	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
989	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
990	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
991	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
992	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
993	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
994	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
995	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
996	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
997	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
998	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
999	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000

```

771 0.000000 0.000000 -0.000192 -0.000008 0.000012 0.000000
772 0.000000 0.000000 -0.000027 -0.000007 0.000007 0.000000
773 0.000000 0.000000 -0.000027 -0.000007 0.000007 0.000000
774 0.000000 0.000000 -0.000022 -0.000005 0.000014 0.000000
775 0.000000 0.000000 -0.000022 -0.000005 0.000014 0.000000
776 0.000000 0.000000 -0.000020 -0.000005 0.000013 0.000000
777 0.000000 0.000000 -0.000020 -0.000005 0.000013 0.000000
778 0.000000 0.000000 -0.000019 -0.000005 0.000017 0.000000
779 0.000000 0.000000 -0.000019 -0.000005 0.000017 0.000000
780 0.000000 0.000000 -0.000018 -0.000004 -0.000016 0.000000
781 0.000000 0.000000 -0.000018 -0.000004 -0.000016 0.000000
782 0.000000 0.000000 -0.000019 -0.000005 0.000014 0.000000
783 0.000000 0.000000 -0.000018 -0.000004 -0.000013 0.000000
784 0.000000 0.000000 -0.000018 -0.000004 -0.000015 0.000000
785 0.000000 0.000000 -0.000019 -0.000005 -0.000008 0.000000
786 0.000000 0.000000 -0.000019 -0.000005 -0.000008 0.000000
787 0.000000 0.000000 -0.000013 -0.000010 -0.000012 0.000000
788 0.000000 0.000000 -0.000013 -0.000010 -0.000012 0.000000
789 0.000000 0.000000 -0.000012 -0.000013 -0.000018 0.000000
790 0.000000 0.000000 -0.000012 -0.000013 -0.000018 0.000000
791 0.000000 0.000000 -0.000010 -0.000014 -0.000020 0.000000
795 0.000000 0.000000 -0.000010 -0.000014 -0.000021 0.000000
797 0.000000 0.000000 -0.000012 -0.000014 -0.000016 0.000000
798 0.000000 0.000000 -0.000013 -0.000015 -0.000019 0.000000
799 0.000000 0.000000 -0.000012 -0.000015 -0.000021 0.000000
800 0.000000 0.000000 -0.000012 -0.000015 -0.000021 0.000000

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17/136

[illegible]

20/136

978	0.005043	-0.001630	-0.071794	0.000002	0.000003	-0.001044
979	0.000000	0.000000	-0.041350	-0.000000	0.000005	0.000000
980	0.000000	0.000000	-0.048584	-0.000000	0.000005	0.000000
981	0.000000	0.000000	-0.048581	-0.000000	0.000011	0.000000
982	0.000000	0.000000	-0.052573	-0.000000	0.000005	0.000000
983	0.000000	0.000000	-0.049484	-0.000000	0.000005	0.000000
984	0.000000	0.000000	-0.058021	-0.000000	0.000004	0.000000
985	0.000000	0.000000	-0.052348	-0.000000	0.000005	0.000000
986	0.000000	0.000000	-0.058984	-0.000000	0.000005	0.000000
987	0.000000	0.000000	-0.050025	-0.000000	0.000005	0.000000
988	0.000000	0.000000	-0.055329	0.000000	0.000004	0.000000
989	0.000000	0.000000	-0.047232	0.000000	0.000005	0.000000
990	0.000000	0.000000	-0.054594	0.000000	0.000005	0.000000
991	0.000000	0.000000	-0.043760	0.000008	0.000004	0.000000
992	0.000000	0.000000	-0.048689	0.000000	0.000005	0.000000
993	0.000000	0.000000	-0.035399	-0.000008	0.000000	0.000000
994	0.000000	0.000000	-0.039196	-0.000000	0.000000	0.000000
995	0.000000	0.000000	-0.036554	-0.000000	0.000000	0.000000
996	0.000000	0.000000	-0.040708	-0.000008	0.000004	0.000000
997	0.000000	0.000000	-0.042405	0.000000	0.000005	0.000000
998	0.000000	0.000000	-0.044111	0.000000	0.000005	0.000000
999	0.000000	0.000000	-0.042026	0.000001	0.000000	0.000000
1000	0.000000	0.000000	-0.045449	0.000000	0.000000	0.000000
1001	0.000000	0.000000	-0.034878	0.000005	0.000000	0.000000
1002	0.000000	0.000000	-0.043895	0.000005	0.000000	0.000000
1003	0.000000	0.000000	-0.038005	0.000000	0.000001	0.000000
1004	0.000000	0.000000	-0.044070	0.000000	0.000000	0.000000
1005	0.000000	0.000000	-0.036227	0.000005	0.000001	0.000000
1006	0.000000	0.000000	-0.038297	0.000000	0.000004	0.000000
1007	0.000000	0.000000	-0.034347	0.000003	0.000000	0.000000
1008	0.000000	0.000000	-0.034193	0.000000	0.000000	0.000000
1009	0.000000	0.000000	-0.036420	0.000000	0.000000	0.000000
1010	0.000000	0.000000	-0.039795	0.000002	0.000004	0.000000
1011	0.000000	0.000000	-0.033586	0.000001	0.000000	0.000000
1012	0.000000	0.000000	-0.033381	0.000001	0.000000	0.000000
1013	0.000000	0.000000	-0.033586	0.000000	0.000004	0.000000
1014	0.000000	0.000000	-0.034584	0.000000	0.000000	0.000000
1015	0.000000	0.000000	-0.032590	0.000002	0.000000	0.000000
1016	0.000000	0.000000	-0.034732	0.000002	0.000004	0.000000
1017	0.000000	0.000000	-0.032436	0.000004	0.000000	0.000000
1018	0.000000	0.000000	-0.034194	0.000002	0.000000	0.000000
1019	0.000000	0.000000	-0.032590	0.000000	0.000000	0.000000
1020	0.000000	0.000000	-0.033553	0.000002	0.000004	0.000000
1021	0.000000	0.000000	-0.039795	0.000005	0.000000	0.000000
1022	0.000000	0.000000	-0.040866	0.000000	0.000000	0.000000
1023	0.000000	0.000000	-0.040469	0.000000	0.000004	0.000000
1024	0.000000	0.000000	-0.034615	0.000000	0.000000	0.000000
1025	0.000000	0.000000	-0.033808	0.000000	0.000000	0.000000

POSTAMENTO NODI

UNITA DI CARICO : 30 Nera Vertov

COMBINAZIONE

1	5	SCONDAZIONATI ANALISI STATICA																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																								</
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339	-0.218003	-0.465367	-0.597343	0.003201	0.00108	-0.00311
	-0.166493	-0.445348	-0.488593	0.00099	0.00079	-0.00311
340	-0.024869	-0.450683	-0.131011	0.007676	0.00173	-0.00329
	0.004951	-0.112801	-0.122230	-0.003511	0.00178	-0.00351
341	0.004774	-0.226726	-0.114057	-0.003514	0.00176	-0.00407
	0.050309	0.118146	-0.124005	-0.00063	0.00183	-0.00402
	0.001151	-0.428709	-0.389477	0.00076	0.00182	-0.00402
	0.243169	0.138385	-0.500870	0.003153	0.00119	-0.00409
346	-0.078322	-0.352371	-0.515150	0.00078	0.00088	-0.00387
	-0.163092	0.021434	-0.353548	0.00074	0.00088	-0.00387
347	-0.005160	-0.323492	-0.102628	-0.002022	-0.00010	-0.00050
	0.012786	0.021466	-0.080446	0.006330	-0.00009	-0.00018
	-0.000132	-0.338136	-0.091301	-0.00014	0.00004	-0.00034
	0.012139	0.033864	-0.083433	-0.00009	-0.00009	-0.00025

469	0.0401094	-0.335925	-0.123650	0.00414	0.00072	-0.00047	0.00000	0.00000	0.00000	-0.042183	-0.00012	0.00004	0.00000	1014	0.000000	0.000000	0.000000	-0.030018	0.00007	0.00003	0.00000	790	0.000000	0.000000	0.000000	-0.026170	0.00002	-0.00001	0.00000
470	0.041749	0.039398	-0.148579	-0.05661	0.00090	-0.00014	0.00000	0.00000	0.00000	-0.054178	0.00005	-0.00003	0.00000	1015	0.000000	0.000000	0.000000	-0.048349	-0.00006	0.00006	0.00000	791	0.000000	0.000000	0.000000	-0.026990	0.00000	-0.00001	0.00000
471	0.045221	0.040161	-0.041162	-0.040003	0.00000	-0.040000	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1016	0.000000	0.000000	0.000000	-0.027007	-0.00005	0.00000	0.00000	792	0.000000	0.000000	0.000000	-0.026626	0.00000	-0.00001	0.00000
472	-0.040689	-0.130906	-0.113622	0.00741	0.01041	-0.00103	0.00000	0.00000	0.00000	-0.040689	0.00002	0.00000	0.00000	1017	0.000000	0.000000	0.000000	-0.024934	-0.00005	0.00002	0.00000	793	0.000000	0.000000	0.000000	-0.024576	-0.00007	0.00001	0.00000
473	0.026028	0.000000	-0.040003	-0.040003	0.00000	-0.040003	0.00000	0.00000	0.00000	-0.040003	0.00000	0.00000	0.00000	1018	0.000000	0.000000	0.000000	-0.024122	-0.00008	0.00002	0.00000	794	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
474	0.025793	-0.009714	-0.059002	0.00015	0.01214	-0.00117	0.00000	0.00000	0.00000	-0.040689	0.00003	0.00004	0.00000	1019	0.000000	0.000000	0.000000	-0.021123	-0.00009	-0.00001	0.00000	795	0.000000	0.000000	0.000000	-0.030957	-0.00006	0.00000	0.00000
475	0.041206	0.040004	-0.060000	-0.060000	0.00000	-0.060000	0.00000	0.00000	0.00000	-0.060000	0.00000	0.00000	0.00000	1020	0.000000	0.000000	0.000000	-0.040689	-0.00009	0.00000	0.00000	796	0.000000	0.000000	0.000000	-0.025301	0.00000	-0.00001	0.00000
476	0.041576	-0.079464	-0.400122	-0.06007	0.00006	-0.00017	0.00000	0.00000	0.00000	-0.040689	0.00002	0.00004	0.00000	1021	0.000000	0.000000	0.000000	-0.025170	-0.00009	0.00002	0.00000	797	0.000000	0.000000	0.000000	-0.027532	0.00000	0.00000	0.00000
477	0.277421	0.071762	-0.146627	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	-0.040689	0.00013	0.00002	0.00000	1022	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	798	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
478	0.277999	-0.450030	-0.046512	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	-0.040689	0.00013	0.00002	0.00000	1023	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	799	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
479	0.168452	-0.104857	-0.693546	0.00000	0.01044	-0.00132	0.00000	0.00000	0.00000	-0.040689	0.00011	0.00001	0.00000	1024	0.000000	0.000000	0.000000	-0.040574	-0.00004	0.00001	0.00000	800	0.000000	0.000000	0.000000	-0.029540	0.00000	0.00000	0.00000
480	0.139131	-0.040000	-0.040000	-0.040000	0.00000	-0.040000	0.00000	0.00000	0.00000	-0.040689	0.00000	0.00000	0.00000	1025	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	801	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
481	0.245170	-0.104765	-0.761935	-0.00021	0.01085	-0.00132	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00002	0.00000	1026	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	802	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
482	0.040000	-0.040000	-0.040000	-0.040000	0.00000	-0.040000	0.00000	0.00000	0.00000	-0.040689	0.00000	0.00000	0.00000	1027	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	803	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
483	0.035955	-0.104839	-0.641056	-0.00039	0.01040	-0.00132	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1028	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	804	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
484	-0.025473	-0.671130	-0.649552	0.00000	0.00395	-0.00130	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1029	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	805	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
485	0.026079	-0.104835	-0.655773	0.00000	0.00395	-0.00130	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1030	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	806	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
486	0.215753	-0.292246	-0.903498	-0.00003	0.00079	-0.00135	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1031	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	807	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
487	0.277427	-0.175238	-0.660294	-0.00001	0.00006	-0.00187	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1032	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	808	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
488	0.025870	-0.282170	-0.330121	0.00073	0.00346	-0.00148	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1033	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	809	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
489	0.041723	-0.175399	-0.559576	-0.00004	0.00359	-0.00167	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1034	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	810	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
490	0.043750	-0.282130	-0.547115	-0.00006	0.00359	-0.00167	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1035	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	811	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
491	0.009016	-0.175307	-0.570402	0.00000	0.00354	-0.00154	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1036	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	812	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
492	0.145165	-0.282116	-0.572715	-0.00009	0.00086	-0.00104	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1037	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	813	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
493	-0.104981	-0.175289	-0.626217	-0.00007	0.00095	-0.00122	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1038	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	814	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
494	0.006490	0.008103	-0.092525	-0.00008	0.00007	-0.00023	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1039	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	815	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
495	0.006634	-0.261424	-0.065248	-0.00097	-0.00004	-0.00033	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1040	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	816	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
496	0.009048	0.008459	-0.093111	0.00004	0.00001	0.00023	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1041	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	817	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
497	0.062156	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1042	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	818	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
498	0.026282	0.084188	-0.049801	-0.00002	0.00038	-0.00017	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1043	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	819	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
499	0.030787	-0.163623	-0.034278	0.00003	-0.00019	-0.00027	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1044	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	820	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
500	0.102000	0.062521	-0.053581	0.00001	-0.00004	-0.00027	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1045	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	821	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
501	0.0844725	-0.1385175	-0.0321380	0.00000	-0.00002	-0.00012	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1046	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000	822	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
502	0.054885	0.031811	-0.060900	0.00003	-0.00013	-0.00031	0.00000	0.00000	0.00000	-0.040689	0.00009	0.00003	0.00000	1047	0.000000	0.000000	0.000000	-0.024619	-0.00005	0.00007	0.00000								

466	-0.043855	-0.099033	-0.267709	0.00089	0.00052	-0.00020	1011	0.000000	0.000000	-0.024663	0.00000	-0.00001	0.00000	739	0.048502	-0.000298	-0.035039	0.00033	-0.00006	-0.00015	959	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
467	-0.001017	-0.099012	-0.062134	0.00000	-0.00007	-0.00021	1012	0.000000	0.000000	-0.025274	0.00000	-0.00001	0.00000	740	0.037215	-0.127890	-0.029433	0.00055	-0.00010	-0.00007	960	0.000000	0.000000	-0.028919	-0.00001	0.00003	-0.00012
468	-0.000779	-0.099013	-0.055600	0.00000	-0.00007	-0.00002	1013	0.000000	0.000000	-0.025987	0.00000	-0.00002	0.00000	741	0.001297	-0.000000	-0.025413	0.00000	-0.00000	0.00000	961	0.000000	0.000000	-0.029000	0.00002	0.00003	-0.00013
469	-0.023114	-0.000158	-0.085884	-0.00046	0.00049	-0.00018	1014	0.000000	0.000000	-0.027017	-0.00001	0.00002	0.00000	742	0.047383	-0.153828	-0.026378	0.00016	-0.00010	-0.00015	962	-0.010201	-0.151891	-0.080470	0.00046	-0.00007	-0.00090
470	-0.002057	-0.025495	-0.349599	0.00019	0.00013	-0.00079	1015	0.000000	0.000000	-0.024703	0.00000	-0.00001	0.00000	743	0.002413	-0.024213	-0.020178	0.00000	-0.00000	0.00000	963	0.000000	0.000000	-0.027013	0.00000	0.00000	-0.00000
471	-0.000057	-0.049495	-0.067000	0.00000	-0.00000	-0.00000	1016	0.000000	0.000000	-0.025244	0.00000	-0.00002	0.00000	744	0.001960	-0.000728	-0.026118	0.00000	-0.00002	-0.00006	964	0.000758	-0.151902	-0.073738	0.00000	-0.00006	-0.00001
472	-0.019713	-0.000165	-0.067312	-0.00014	0.00083	-0.00009	1017	0.000000	0.000000	-0.024618	0.00000	-0.00001	0.00000	745	0.001144	-0.004040	-0.025231	0.00000	-0.00000	0.00000	965	0.000000	0.000000	-0.025000	0.00000	0.00000	-0.00000
473	-0.129977	-0.000000	-0.025000	-0.00000	-0.00000	-0.00000	1018	0.000000	0.000000	-0.025015	0.00000	-0.00000	0.00000	746	0.001963	-0.001234	-0.030275	-0.00001	-0.00002	-0.00012	966	0.012963	-0.152016	-0.265049	-0.00003	0.00011	-0.00094
474	-0.119772	-0.236260	-0.478813	0.00077	0.00101	-0.00098	1019	0.000000	0.000000	-0.024438	0.00000	-0.00001	0.00000	747	-0.06330	-0.087139	-0.188902	0.00110	-0.01350	-0.00017	967	-0.137719	-0.040340	-0.287330	-0.00217	0.00026	-0.00097
475	-0.134406	-0.236011	-0.428132	0.00000	0.00106	-0.00008	1020	0.000000	0.000000	-0.024885	0.00001	0.00002	0.00000	748	0.001352	-0.000102	-0.031880	0.00000	-0.00000	0.00000	968	-0.124700	-0.040362	-0.287330	-0.00217	0.00026	-0.00097
476	-0.010565	-0.025495	-0.067000	0.00000	-0.00000	-0.00000	1021	0.000000	0.000000	-0.025788	0.00000	-0.00002	0.00000	749	-0.003952	-0.087469	-0.046412	0.00050	-0.00004	-0.00018	969	-0.114601	-0.040163	-0.324019	0.00242	0.00006	-0.00084
477	-0.007701	-0.126202	-0.389948	0.00026	0.00048	-0.00000	1022	0.000000	0.000000	-0.027413	0.00000	0.00001	0.00000	750	0.000611	-0.006370	-0.027413	0.00000	-0.00000	0.00000	970	0.000000	0.000000	-0.027394	0.00000	0.00000	-0.00000
478	-0.130869	-0.000000	-0.067000	0.00000	-0.00000	-0.00000	1023	0.000000	0.000000	-0.027413	0.00000	-0.00000	0.00000	751	-0.040875	-0.029257	-0.168513	0.00004	-0.00008	-0.00018	971	-0.003011	-0.236617	-0.049891	0.00017	0.00006	-0.00011
479	-0.013836	-0.126202	-0.340075	0.00014	0.00221	-0.00097	1024	0.000000	0.000000	-0.025252	0.00000	-0.00001	0.00000	752	-0.000442	-0.087469	-0.033854	0.00029	-0.00028	-0.00018	972	0.000000	0.000000	-0.030274	-0.00001	0.00003	0.00000
480	-0.005063	-0.42032	-0.346436	0.00000	-0.00000	-0.00000	1025	0.000000	0.000000	-0.025256	-0.00001	-0.00001	0.00000	753	0.000498	-0.003370	-0.037181	0.00000	-0.00000	0.00000	973	0.000000	0.000000	-0.032949	0.00000	0.00000	-0.00000
481	-0.020267	-0.140211	-0.425017	0.00074	0.00059	-0.00070	730	0.020282	-0.087575	-0.052737	-0.00011	0.00036	-0.00013	754	0.000000	0.000000	-0.028901	0.00000	-0.00000	0.00000	974	0.000000	0.000000	-0.028901	0.00000	-0.00001	0.00000
482	-0.002292	-0.001682	-0.031812	0.00000	0.00003	-0.00017	731	0.021250	-0.018415	-0.052622	-0.00007	0.00011	0.00015	755	-0.002028	-0.235486	-0.153662	0.00006	0.00006	0.00002	975	-0.002028	-0.235486	-0.153662	0.00006	0.00006	0.00002
483	-0.000628	-0.025202	-0.039648	0.00000	-0.00000	-0.00000	732	0.022106	-0.087574	-0.052622	-0.00007	0.00011	0.00015	756	0.016495	-0.015907	-0.032719	0.00019	0.00022	0.00004	976	0.016495	-0.015907	-0.032719	0.00019	0.00022	0.00004
484	-0.035725	-0.025293	-0.038017	0.00028	0.00002	-0.00010	733	0.022694	-0.018800	-0.052648	-0.00013	0.00038	-0.00015	757	-0.000194	-0.008917	-0.030618	0.00000	-0.00000	0.00000	977	-0.000194	-0.008917	-0.030618	0.00000	-0.00000	0.00000
485	-0.046641	-0.167912	-0.031004	0.00009	-0.00008	-0.00010	734	0.023291	-0.000000	-0.052244	0.00046	-0.00009	-0.00010	758	0.000498	-0.008917	-0.030618	0.00000	-0.00000	0.00000	978	0.000498	-0.008917	-0.030618	0.00000	-0.00000	0.00000
486	-0.037291	-0.091051	-0.032244	0.00046	-0.00009	-0.00010	735	0.046712	-0.101936	-0.033437	0.00021	0.00009	-0.00015	759	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	979	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
487	-0.046712	-0.101936	-0.033437	0.00021	0.00009	-0.00015	736	0.047154	-0.010151	-0.033437	0.00021	0.00009	-0.00015	760	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	980	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
488	-0.047154	-0.010151	-0.033437	0.00021	0.00009	-0.00015	737	0.047596	-0.010151	-0.033437	0.00021	0.00009	-0.00015	761	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	981	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
489	-0.047596	-0.010151	-0.033437	0.00021	0.00009	-0.00015	738	0.048038	-0.010151	-0.033437	0.00021	0.00009	-0.00015	762	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	982	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
490	-0.048038	-0.010151	-0.033437	0.00021	0.00009	-0.00015	739	0.048480	-0.010151	-0.033437	0.00021	0.00009	-0.00015	763	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	983	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
491	-0.048480	-0.010151	-0.033437	0.00021	0.00009	-0.00015	740	0.048922	-0.010151	-0.033437	0.00021	0.00009	-0.00015	764	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	984	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
492	-0.048922	-0.010151	-0.033437	0.00021	0.00009	-0.00015	741	0.049364	-0.010151	-0.033437	0.00021	0.00009	-0.00015	765	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	985	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
493	-0.049364	-0.010151	-0.033437	0.00021	0.00009	-0.00015	742	0.049806	-0.010151	-0.033437	0.00021	0.00009	-0.00015	766	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	986	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
494	-0.049806	-0.010151	-0.033437	0.00021	0.00009	-0.00015	743	0.050248	-0.010151	-0.033437	0.00021	0.00009	-0.00015	767	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	987	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
495	-0.050248	-0.010151	-0.033437	0.00021	0.00009	-0.00015	744	0.050690	-0.010151	-0.033437	0.00021	0.00009	-0.00015	768	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	988	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
496	-0.050690	-0.010151	-0.033437	0.00021	0.00009	-0.00015	745	0.051132	-0.010151	-0.033437	0.00021	0.00009	-0.00015	769	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	989	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
497	-0.051132	-0.010151	-0.033437	0.00021	0.00009	-0.00015	746	0.051574	-0.010151	-0.033437	0.00021	0.00009	-0.00015	770	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	990	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
498	-0.051574	-0.010151	-0.033437	0.00021	0.00009	-0.00015	747	0.052016	-0.010151	-0.033437	0.00021	0.00009	-0.00015	771	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	991	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
499	-0.052016	-0.010151	-0.033437	0.00021	0.00009	-0.00015	748	0.052458	-0.010151	-0.033437	0.00021	0.00009	-0.00015	772	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	992	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
500	-0.052458	-0.010151	-0.033437	0.00021	0.00009	-0.00015	749	0.052900	-0.010151	-0.033437	0.00021	0.00009	-0.00015	773	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	993	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
501	-0.052900	-0.010151	-0.033437	0.00021	0.00009	-0.00015	750	0.053342	-0.010151	-0.033437	0.00021	0.00009	-0.00015	774	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018	994	0.000154	-0.009953	-0.040197	0.00173	0.00054	-0.00018
502	-0.053342	-0.010151	-0.033437	0.00021	0.00009	-0.00015	751	0.053784	-0.010151	-0.033437	0.00021	0.00009	-0.00015	775	0.000154	-0.009953	-0.04019										

3 A*var_abitazione___ + 0.30

1) +1.00*c001 +1.00*c002 +0.30*c009

unità di misura: SX,SY,SZ [m]; RX,RY,RZ [rad]

Coefficiente moltiplicativo: 1.000000

Nodo SX SY SZ RX RY RZ

1 0.000000 0.000000 -0.094208 -0.000000 0.000000 0.000000
2 -0.076082 -0.008318 -0.271164 0.00215 0.00068 -0.00054
3 -0.022667 -0.069882 -0.209514 0.00241 -0.00041 -0.00028
4 -0.024724 -0.153106 -0.266700 0.00262 -0.00000 -0.00011
11 -0.000920 -0.008350 -0.053227 0.00042 -0.00008 -0.00008
12 -0.001715 -0.009939 -0.049502 0.00007 -0.00000 -0.00004
14 0.000682 -0.155223 -0.054580 0.00030 -0.00007 -0.00011
19 0.001365 -0.000400 -0.031554 0.00000 0.00005 -0.00000
20 0.013904 -0.008346 -0.050638 -0.00014 0.00020 -0.00071
21 0.000779 -0.069938 -0.044578 0.00017 -0.00040 -0.00013
23 0.001531 -0.155296 -0.090114 0.00019 0.00001 0.00011
28 0.001096 -0.000448 -0.022884 0.00000 0.00001 -0.00024
29 0.144657 -0.008257 -0.232527 -0.00078 0.00068 -0.00080
30 0.016744 -0.069929 -0.068717 -0.00007 0.00006 -0.00010
32 0.016244 -0.155279 -0.042586 0.00006 0.00006 -0.00011
37 0.001387 -0.000446 -0.072881 0.00000 0.00001 0.00000
38 0.000421 -0.069935 -0.043090 0.00034 -0.00001 -0.00013
39 0.000451 -0.155246 -0.002053 0.00004 0.00000 -0.00011
40 0.000000 0.000000 -0.037398 0.00000 0.00004 -0.00070
41 0.006812 -0.008352 -0.046384 0.00013 0.00003 -0.00070
42 0.000684 -0.072508 -0.057857 -0.00004 -0.00004 -0.00071
107 0.000000 0.000000 -0.039863 0.00000 0.00003 0.00000
109 0.000000 0.000000 -0.032544 -0.00007 0.00004 0.00000
168 0.000000 0.000000 -0.033827 0.00006 0.00004 0.00000
210 -0.043499 -0.157813 -0.126593 0.00073 0.00032 -0.00012
211 -0.001026 -0.155648 -0.054641 0.00078 -0.00008 -0.00012
212 0.001613 -0.155640 -0.049180 0.00000 -0.00052 -0.00011
213 0.016529 -0.156678 -0.042621 0.00000 0.00004 0.00002
339 0.009365 -0.082711 -0.262786 0.00139 0.00048 -0.00062
340 -0.006659 -0.074739 -0.062123 0.00000 0.00000 0.00007
341 0.007586 -0.072110 -0.059562 -0.00000 0.00000 -0.00069
342 0.014123 -0.064388 -0.217753 -0.00216 0.00052 -0.00074
466 0.024714 -0.076049 -0.209582 0.00009 0.00000 0.00015
467 0.000115 -0.075993 -0.049634 0.00077 -0.00007 -0.00016
468 0.001325 -0.069115 -0.044647 0.00000 0.00007 0.00013
469 0.017053 -0.069081 -0.068782 -0.00036 0.00037 -0.00014
470 0.007474 -0.000000 -0.271254 0.00012 -0.00002 -0.00000
471 -0.000507 -0.094063 -0.053520 0.00133 0.00074 -0.00062
472 0.014967 -0.007533 -0.050750 -0.00090 0.00066 -0.00062
473 0.117858 0.000646 -0.233041 0.00113 0.00104 0.00071
726 0.093629 -0.178862 -0.178011 0.00060 0.00081 -0.00065
727 0.104123 -0.178947 -0.138095 0.00000 0.00000 -0.00007
728 0.007489 -0.178950 -0.313242 0.00008 0.00136 -0.00072
729 0.006759 -0.178964 -0.316022 0.00020 0.00196 -0.00071
730 0.117852 -0.110336 -0.290413 -0.00025 0.00050 -0.00078
731 0.015040 -0.110335 -0.271795 0.00011 0.00175 -0.00077
732 -0.000106 -0.110303 -0.275127 0.00000 0.00022 -0.00000
733 -0.072697 -0.110295 -0.335911 0.00057 0.00049 -0.00054
734 0.001380 -0.000923 -0.026913 0.00001 0.00002 -0.00013
745 0.001194 -0.040463 -0.033279 0.00024 0.00001 -0.00013
737 0.026595 -0.040514 -0.027267 0.00022 0.00016 -0.00007
738 0.032254 -0.139358 -0.029143 0.00000 0.00031 0.00000
739 0.027808 -0.069798 -0.027286 0.00036 -0.00008 -0.00007
740 0.021540 -0.155581 -0.028275 0.00016 0.00006 -0.00011
741 0.000817 -0.000625 -0.023618 0.00001 0.00000 0.00007
742 0.000820 -0.000447 -0.023637 0.00001 0.00001 0.00007
745 0.018521 -0.040109 -0.127760 0.00078 0.00126 0.00012
746 -0.002466 -0.040461 -0.036671 0.00032 0.00027 -0.00013
747 0.000081 -0.040461 -0.031938 0.00016 0.00019 -0.00013
748 0.015578 -0.040518 -0.044395 -0.00008 0.00018 -0.00010
749 0.016494 -0.040158 -0.044416 -0.00036 0.00028 -0.00012
750 -0.000895 -0.041283 -0.033864 -0.00031 0.00142 0.00011
751 -0.000981 -0.042600 -0.036696 0.00077 0.00042 -0.00014
752 -0.033362 -0.040451 -0.127783 0.00049 0.00067 -0.00013
753 0.027423 -0.041615 -0.027307 0.00022 0.00017 -0.00010
754 0.027396 -0.071555 -0.027319 0.00035 -0.00009 -0.00009
760 0.016488 -0.129402 -0.044633 0.00001 0.00053 0.00012
761 0.000000 0.000000 -0.028804 -0.00007 0.00005 0.00000
762 0.000000 0.000000 -0.038814 -0.00007 0.00005 0.00000
763 0.000000 0.000000 -0.034165 -0.00007 0.00004 0.00000
764 0.000000 0.000000 -0.032300 -0.00007 0.00005 0.00000
765 0.000000 0.000000 -0.035818 -0.00007 0.00004 0.00000
766 0.000000 0.000000 -0.037158 -0.00005 0.00004 0.00000
767 0.000000 0.000000 -0.035111 0.00006 0.00005 0.00000
768 0.000000 0.000000 -0.038586 -0.00005 0.00004 0.00000
769 0.000000 0.000000 -0.038641 0.00000 0.00000 0.00000
770 0.000000 0.000000 -0.037564 0.00004 0.00004 0.00000
771 0.000000 0.000000 -0.039598 0.00005 0.00005 0.00000
772 0.000000 0.000000 -0.038958 0.00004 0.00004 0.00000
773 0.000000 0.000000 -0.039041 0.00006 0.00004 0.00000
774 0.000000 0.000000 -0.032773 0.00006 0.00005 0.00000
775 0.000000 0.000000 -0.036618 0.00006 0.00004 0.00000
776 0.000000 0.000000 -0.032022 0.00006 0.00004 0.00000
777 0.000000 0.000000 -0.039458 0.00006 0.00005 0.00000
778 0.000000 0.000000 -0.020659 -0.00005 -0.00002 0.00000
779 0.000000 0.000000 -0.030462 -0.00005 -0.00002 0.00000
780 0.000000 0.000000 -0.022993 -0.00005 -0.00002 0.00000
781 0.000000 0.000000 -0.023205 -0.00005 -0.00002 0.00000
782 0.000000 0.000000 -0.025264 -0.00004 -0.00002 0.00000
783 0.000000 0.000000 -0.025485 -0.00004 -0.00002 0.00000
784 0.000000 0.000000 -0.026467 0.00000 -0.00000 0.00000
785 0.000000 0.000000 -0.025370 0.00003 -0.00002 0.00000
786 0.000000 0.000000 -0.025545 0.00003 -0.00002 0.00000
787 0.000000 0.000000 -0.023779 0.00003 -0.00001 0.00000
788 0.000000 0.000000 -0.023622 0.00003 -0.00001 0.00000
789 0.000000 0.000000 -0.022615 0.00002 0.00000 0.00000
790 0.000000 0.000000 -0.022737 0.00002 -0.00001 0.00000
795 0.000000 0.000000 -0.023376 0.00000 -0.00000 0.00000
797 0.000000 0.000000 -0.023252 0.00000 -0.00001 0.00000
798 0.000000 0.000000 -0.019549 -0.00006 0.00000 0.00000
799 0.000000 0.000000 -0.023126 -0.00006 0.00000 0.00000
800 0.000000 0.000000 -0.022225 -0.00006 0.00001 0.00000
801 0.000000 0.000000 -0.034897 -0.00005 0.00000 0.00000
802 0.000000 0.000000 -0.024885 -0.00005 0.00001 0.00000
803 0.000000 0.000000 -0.026960 -0.00001 -0.00001 0.00000
804 0.000000 0.000000 -0.025599 0.00003 0.00000 0.00000
805 0.000000 0.000000 -0.025521 0.00003 0.00001 0.00000
806 0.000000 0.000000 -0.024003 0.00003 0.00000 0.00000
807 0.000000 0.000000 -0.023918 0.00003 0.00001 0.00000
808 0.000000 0.000000 -0.022568 0.00002 0.00000 0.00000
813 0.000000 0.000000 -0.023703 -0.00001 0.00001 0.00000
814 0.000000 0.000000 -0.023716 0.00000 0.00002 0.00000
909 0.000000 0.000000 -0.023269 0.00000 0.00002 0.00000
924 0.000000 0.000000 -0.023224 0.00000 -0.00001 0.00000
943 0.000000 0.000000 -0.023159 0.00000 0.00000 0.00000
951 0.000399 -0.130367 -0.036578 0.00022 0.00001 -0.00011
953 0.021863 -0.155746 -0.028322 -0.00073 -0.00059 -0.00010
954 0.000000 0.000000 -0.026534 0.00000 0.00001 0.00000
957 0.000000 0.000000 -0.022797 0.00001 0.00001 -0.00024
958 0.000000 0.000000 -0.026130 0.00000 0.00001 0.00013
959 0.000000 0.000000 -0.023271 0.00000 0.00001 -0.00007
960 0.000000 0.000000 -0.023271 0.00000 -0.00001 -0.00007
961 0.006365 -0.077526 -0.063101 0.00044 0.00006 0.00070
962 0.007784 -0.027513 -0.059456 -0.00008 -0.00004 -0.00071
963 0.101398 -0.025738 -0.115722 -0.00164 0.00014 0.00075
964 -0.094350 -0.077481 -0.262708 0.00035 0.00014 -0.00066
965 0.000000 0.000000 -0.023198 0.00000 0.00002 0.00000
966 0.000000 0.000000 -0.023107 0.00000 -0.00001 0.00000
967 -0.014440 -0.130358 -0.116973 0.00071 0.00003 -0.00010
968 -0.000744 -0.133367 -0.038672 0.00029 -0.00003 -0.00011

969 0.001543 -0.130367 -0.035659 0.00013 0.00001 -0.00011
970 0.016514 -0.130367 -0.054801 -0.00009 -0.00001 -0.00011
972 -0.000028 -0.131812 -0.039684 0.00078 0.00004 -0.00010
973 0.001603 -0.131026 -0.035691 0.00000 0.00004 -0.00011
975 0.013911 -0.131916 -0.029175 -0.00073 0.00058 -0.00010
976 -0.014395 -0.133886 -0.116993 0.00073 0.00021 -0.00010
978 0.001396 0.000162 -0.038664 0.00000 0.00000 -0.00070
979 0.000000 0.000000 -0.020449 -0.00006 0.00002 0.00000
980 0.000000 0.000000 -0.023024 -0.00005 0.00002 0.00000
981 0.000000 0.000000 -0.023986 -0.00006 0.00006 0.00000
982 0.000000 0.000000 -0.026854 -0.00006 0.00006 0.00000
983 0.000000 0.000000 -0.025106 -0.00003 0.00002 0.00000
984 0.000000 0.000000 -0.026266 -0.00004 0.00007 0.00000
985 0.000000 0.000000 -0.026151 -0.00001 0.00002 0.00000
986 0.000000 0.000000 -0.026055 0.00000 0.00007 0.00000
987 0.000000 0.000000 -0.025873 0.00002 0.00002 0.00000
988 0.000000 0.000000 -0.029867 0.00003 0.00007 0.00000
989 0.000000 0.000000 -0.026696 0.00003 0.00002 0.00000
990 0.000000 0.000000 -0.028154 0.00004 0.00006 0.00000
991 0.000000 0.000000 -0.027180 0.00003 0.00001 0.00000
992 0.000000 0.000000 -0.026022 0.00005 0.00005 0.00000
993 0.000000 0.000000 -0.019149 -0.00005 -0.00001 0.00000
994 0.000000 0.000000 -0.021527 -0.00005 -0.00001 0.00000
995 0.000000 0.000000 -0.018934 -0.00005 0.00001 0.00000
996 0.000000 0.000000 -0.021438 -0.00005 0.00001 0.00000
997 0.000000 0.000000 -0.023484 -0.00003 -0.00002 0.00000
998 0.000000 0.000000 -0.025576 -0.00004 0.00001 0.00000
999 0.000000 0.000000 -0.024371 0.00000 -0.00001 0.00000
1000 0.000000 0.000000 -0.024540 -0.00001 0.00002 0.00000
1001 0.000000 0.000000 -0.025989 0.00002 -0.00001 0.00000
1002 0.000000 0.000000 -0.024098 0.00002 0.00002 0.00000
1003 0.000000 0.000000 -0.022746 0.00002 -0.00001 0.00000
1004 0.000000 0.000000 -0.022914 0.00003 0.00001 0.00000
1005 0.000000 0.000000 -0.021743 0.00002 -0.00001 0.00000
1006 0.000000 0.000000 -0.021881 0.00002 0.00001 0.00000
1007 0.000000 0.000000 -0.021331 0.00000 -0.00001 0.00000
1008 0.000000 0.000000 -0.022212 0.00000 -0.00001 0.00000
1009 0.000000 0.000000 -0.021415 0.00000 0.00001 0.00000
1010 0.000000 0.000000 -0.022448 0.00000 0.00001 0.00000
1011 0.000000 0.000000 -0.021475 0.00001 -0.00001 0.00000
1012 0.000000 0.000000 -0.022782 -0.00002 -0.00002 0.00000
1013 0.000000 0.000000 -0.021476 0.00000 0.00001 0.00000
1014 0.000000 0.000000 -0.022772 -0.00001 0.00001 0.00000
1015 0.000000 0.000000 -0.021737 0.00000 -0.00001 0.00000
1016 0.000000 0.000000 -0.021701 0.00000 0.00001 0.00000
1017 0.000000 0.000000 -0.021805 0.00000 -0.00001 0.00000
1018 0.000000 0.000000 -0.021768 0.00000 0.00001 0.00000
1019 0.000000 0.000000 -0.021788 0.00000 -0.00001 0.00000
1020 0.000000 0.000000 -0.021764 0.00000 0.00001 0.00000
1021 0.000000 0.000000 -0.023762 0.00000 0.00002 0.00000
1022 0.000000 0.000000 -0.022737 0.00000 0.00001 0.00000
1023 0.000000 0.000000 -0.023173 -0.00001 0.00001 0.00000
1024 0.000000 0.000000 -0.022442 0.00000 -0.00001 0.00000
1025 0.000000 0.000000 -0.022929 -0.00001 -0.00001 0.00000

REAZIONI VINCOLARI:

REAZIONI VINCOLARI									
CONDIZIONE : 1 Peso proprio									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	321.4	-68.7	0.0	0.0	0.0	0.0			
954	54.7	-48.5	0.0	0.0	0.0	0.0			
957	18.8	-29.8	0.0	0.0	0.0	0.0			
958	-284.8	-48.2	0.0	0.0	0.0	0.0			
959	126.9	111.0	0.0	0.0	0.0	0.0			
960	-237.0	84.2	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 2 Permanente									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	372.1	56.5	0.0	0.0	0.0	0.0			
954	-53.5	58.8	0.0	0.0	0.0	0.0			
957	-22.0	-149.5	0.0	0.0	0.0	0.0			
958	-274.6	75.9	0.0	0.0	0.0	0.0			
959	124.7	-77.3	0.0	0.0	0.0	0.0			
960	-146.7	35.6	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 3 A:var_abitazione									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	651.2	98.9	0.0	0.0	0.0	0.0			
954	-93.6	102.9	0.0	0.0	0.0	0.0			
957	-38.5	-261.7	0.0	0.0	0.0	0.0			
958	-480.6	132.8	0.0	0.0	0.0	0.0			
959	218.2	-135.3	0.0	0.0	0.0	0.0			
960	-256.8	62.3	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 4 Neve (<1000m_slm)									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	177.8	57.2	0.0	0.0	0.0	0.0			
954	-59.4	49.4	0.0	0.0	0.0	0.0			
957	-24.3	-79.4	0.0	0.0	0.0	0.0			
958	-151.1	36.7	0.0	0.0	0.0	0.0			
959	87.7	-44.8	0.0	0.0	0.0	0.0			
960	-30.7	-19.2	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 5 Vento_Y									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	16.1	308.2	0.0	0.0	0.0	0.0			
954	-0.1	380.8	0.0	0.0	0.0	0.0			
957	12.6	708.7	0.0	0.0	0.0	0.0			
958	-40.3	274.7	0.0	0.0	0.0	0.0			
959	-80.6	-142.3	0.0	0.0	0.0	0.0			
960	112.3	-47.2	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 6 Sisma_X									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	-162.0	-168.9	0.0	0.0	0.0	0.0			
954	-696.9	-114.5	0.0	0.0	0.0	0.0			
957	539.4	264.4	0.0	0.0	0.0	0.0			
958	-538.2	-82.3	0.0	0.0	0.0	0.0			
959	-96.9	131.1	0.0	0.0	0.0	0.0			
960	-53.2	-29.7	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 7 Sisma_Y									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	13.1	-512.3	0.0	0.0	0.0	0.0			
954	-22.0	-560.5	0.0	0.0	0.0	0.0			
957	3.1	-1028.8	1.0	0.0	0.0	0.0			
958	-47.5	-365.2	0.0	0.0	0.0	0.0			
959	138.3	239.5	0.0	0.0	0.0	0.0			
960	-180.1	120.6	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 8 Torcente_add_X									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	-31.2	52.1	0.0	0.0	0.0	0.0			
954	21.0	0.0	0.0	0.0	0.0	0.0			
957	-22.3	11.0	0.0	0.0	0.0	0.0			
958	-42.3	-49.5	0.0	0.0	0.0	0.0			
959	-12.2	16.5	0.0	0.0	0.0	0.0			
960	2.3	-36.1	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 9 Torcente_add_Y									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	14.9	-29.4	0.0	0.0	0.0	0.0			
954	-13.2	1.2	0.0	0.0	0.0	0.0			
957	31.2	-6.0	0.0	0.0	0.0	0.0			
958	-23.4	23.3	0.0	0.0	0.0	0.0			
959	8.6	-8.0	0.0	0.0	0.0	0.0			
960	0.9	18.9	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CASO DI CARICO : 1 SLU									
N. 4 CONDIZIONE ANALISI STATICA									
1) 1.00°<001 +1.50°<002 +1.50°<003 +1.50°<004									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	2219.4	229.7	0.0	0.0	0.0	0.0			
954	SX	SY	SZ	RX	RY	RZ			

Nodo	SX	SY	SZ	RX	RY	RZ			
957	-102.9	-774.7	0.0	0.0	0.0	0.0			
958	-1729.6	305.4	0.0	0.0	0.0	0.0			
959	811.0	-241.8	0.0	0.0	0.0	0.0			
960	-959.5	227.6	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI

CASO DI CARICO : 2 SLU VENTOX

N. 4 CONDIZIONE ANALISI STATICA									
1) 1.00°<001 +1.50°<002 +1.50°<003 +1.50°<004									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	SX	SY	SZ	RX	RY	RZ			
40	2219.4	229.7	0.0	0.0	0.0	0.0			
954	SX	SY	SZ	RX	RY	RZ			
957	-238.5	253.7	0.0	0.0	0.0	0.0			
958	-102.9	-774.7	0.0	0.0	0.0	0.0			
959	811.0	-241.8	0.0	0.0	0.0	0.0			
960	-959.5	227.6	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CASO DI CARICO : 3 SLU VENTY									
N. 5 CONDIZIONE ANALISI STATICA									
1) +1.30°c001 +1.50°c002 +1.50°c003 +1.50°c004									
Unità di misura: SX,SY,SZ [daN];RX,RY,RZ [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	SX	SY	SZ	RX	RY	RZ			
40	2219.4	229.7	0.0	0.0	0.0	0.0			
954	SX	SY	SZ	RX	RY	RZ			
957	-238.5	253.7	0.0	0.0	0.0	0.0			
9									

Nodo	959	SX	SY	SZ	RX	RY	RZ
		378.3	-42.9	0.0	0.0	0.0	0.0
Nodo	960	SX	SY	SZ	RX	RY	RZ
		-518.3	147.1	0.0	0.0	0.0	0.0

REAZIONI VINCOLARI

CASO DI CARICO : 13 Frequente Vento

COMBINAZIONE

N. 5 CONDIZIONI ANALISI STATICA

- 1 Peso_proprio + 1.00
- 2 Permanente + 1.00
- 3 A'Var_abitazione + 0.50
- 4 NiveL(-1000n_sln) + 0.20
- 5 Vento_y +- 0.20

- 1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004 +0.20*c005
- 2) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004 -0.20*c005

Unità di misura: SX,SY,SZ [dm];RX,RY,RZ [dm/cm]

Coefficiente moltiplicativo:		1.000000					
Nodo	40	SX	SY	SZ	RX	RY	RZ
		1057.9	110.4	0.0	0.0	0.0	0.0
		1051.4	-12.9	0.0	0.0	0.0	0.0
Nodo	954	SX	SY	SZ	RX	RY	RZ
		-57.4	148.2	0.0	0.0	0.0	0.0
		-57.4	-4.9	0.0	0.0	0.0	0.0
Nodo	957	SX	SY	SZ	RX	RY	RZ
		-24.9	-184.3	0.0	0.0	0.0	0.0
		-29.9	-467.8	0.0	0.0	0.0	0.0
Nodo	958	SX	SY	SZ	RX	RY	RZ
		-842.0	156.3	0.0	0.0	0.0	0.0
		-817.8	46.5	0.0	0.0	0.0	0.0
Nodo	959	SX	SY	SZ	RX	RY	RZ
		362.2	-71.4	0.0	0.0	0.0	0.0
		394.4	-14.5	0.0	0.0	0.0	0.0
Nodo	960	SX	SY	SZ	RX	RY	RZ
		-495.8	137.7	0.0	0.0	0.0	0.0
		-540.7	156.6	0.0	0.0	0.0	0.0

REAZIONI VINCOLARI

CASO DI CARICO : 14 Quasi Perm

COMBINAZIONE

N. 3 CONDIZIONI ANALISI STATICA

- 1 Peso_proprio + 1.00
- 2 Permanente + 1.00
- 3 A'Var_abitazione + 0.30

- 1) +1.00*c001 +1.00*c002 +0.30*c003

Unità di misura: SX,SY,SZ [dm];RX,RY,RZ [dm/cm]

Coefficiente moltiplicativo:		1.000000					
Nodo	40	SX	SY	SZ	RX	RY	RZ
		888.8	17.5	0.0	0.0	0.0	0.0
		-26.8	41.2	0.0	0.0	0.0	0.0
Nodo	954	SX	SY	SZ	RX	RY	RZ
		-14.8	-257.8	0.0	0.0	0.0	0.0
		-703.6	67.5	0.0	0.0	0.0	0.0
Nodo	958	SX	SY	SZ	RX	RY	RZ
		317.1	-6.9	0.0	0.0	0.0	0.0
		-460.8	138.5	0.0	0.0	0.0	0.0

SOLLECITAZIONI ASTE:

SOLLECITAZIONI ASTE CASO DI CARICO : 1 SLU

N. 4 CONDIZIONI ANALISI STATICA

1. Pieno proprio + 1.30
2. Permanente + 1.50
3. A variazione + 1.50
4. New_Condition + 1.50

1) +1.30*001 +1.50*002 +1.50*003 +1.50*004

Unità di misura: Preg e frecce [cm] NORM, TZZ [dwn]

ASTA	2	TY	TZZ	TORS	MY	NZZ
PROGR.	0	1174.4	-1567.1	-0.8	-58.9	9.0
19.	-500.6	-1465.8	-0.7	-55.8	98.1	68891.5
42.	-713.7	-1091.1	-0.7	-55.8	128.2	15570.3
83.	306.9	-716.5	-0.7	-55.8	133.8	22124.2
125.	-1140.1	-341.8	-0.7	-55.8	188.4	41192.7
167.	-1353.3	32.9	-0.7	-55.8	218.5	50634.8
209.	-1566.4	407.5	-0.7	-55.8	248.7	41450.5
250.	-1779.6	782.2	-0.7	-55.8	278.8	15640.0
292.	-1992.8	1156.9	-0.7	-55.8	308.9	23796.6
334.	-2206.0	1531.6	-0.7	-55.8	339.0	79859.9
ASTA	4	210	399			
PROGR.	0	1174.4	-1567.1	-0.8	-58.9	9.0
19.	-500.6	-1465.8	-0.7	-55.8	98.1	68891.5
42.	-713.7	-1091.1	-0.7	-55.8	128.2	15570.3
83.	306.9	-716.5	-0.7	-55.8	133.8	22124.2
125.	-1140.1	-341.8	-0.7	-55.8	188.4	41192.7
167.	-1353.3	32.9	-0.7	-55.8	218.5	50634.8
209.	-1566.4	407.5	-0.7	-55.8	248.7	41450.5
250.	-1779.6	782.2	-0.7	-55.8	278.8	15640.0
292.	-1992.8	1156.9	-0.7	-55.8	308.9	23796.6
334.	-2206.0	1531.6	-0.7	-55.8	339.0	79859.9
ASTA	8	420	798			
PROGR.	0	1174.4	-1567.1	-0.8	-58.9	9.0
19.	-500.6	-1465.8	-0.7	-55.8	98.1	68891.5
42.	-713.7	-1091.1	-0.7	-55.8	128.2	15570.3
83.	306.9	-716.5	-0.7	-55.8	133.8	22124.2
125.	-1140.1	-341.8	-0.7	-55.8	188.4	41192.7
167.	-1353.3	32.9	-0.7	-55.8	218.5	50634.8
209.	-1566.4	407.5	-0.7	-55.8	248.7	41450.5
250.	-1779.6	782.2	-0.7	-55.8	278.8	15640.0
292.	-1992.8	1156.9	-0.7	-55.8	308.9	23796.6
334.	-2206.0	1531.6	-0.7	-55.8	339.0	79859.9

COMBINAZIONE

Comparison						
+1.50e+004						
Z [dan]						
470						
MY	NZZ					
15.8	98.1	6880.5				
15.8	188.2	15570.5				
15.8	158.3	-2212.2				
15.8	125.4	-4430.7				
15.8	218.5	-5063.8				
15.8	218.5	-4450.6				
15.8	278.8	-16640.2				
15.8	306.9	27396.6				
15.8	339.0	28803.6				
339						
MY	NZZ					
18.9	100.4	9824.5				
18.9	100.4	9824.5				
18.9	163.7	1963.9				
18.9	155.3	-2945.0				
18.9	227.0	-7018.7				
18.9	236.6	-3403.0				
18.9	281.9	3340.9				
18.9	321.9	2304.7				
18.9	353.5	75252.6				
726						
MY	NZZ					
18.9	334.8	7525.6				
18.9	289.4	5214.3				
18.9	240.1	14607.7				
18.9	198.7	10843.7				
18.9	153.4	8614.3				
18.9	108.0	1072.6				
18.9	62.7	-2862.4				
18.9	17.3	-3163.8				
18.9	-28.0	-168.5				
733						
MY	NZZ					
19.1	322.2	78959.6				
19.1	147.9	57182.0				
19.1	-26.4	3818.0				
19.1	-375.1	2277.7				
19.1	-20.5	1093.0				
19.1	-723.7	-1701.3				
19.1	-688.1	-2577.0				
19.1	-727.4	151.0				
471						
MY	NZZ					
13.3	-90.2	-5432.0				
13.3	-137.7	-14380.8				
13.3	-181.3	15093.1				
13.3	-226.8	6366.7				
13.3	-271.9	20006.0				
13.3	-317.9	2020.5				
13.3	-363.4	-1363.8				
13.3	-408.9	-6841.9				
13.3	-454.5	-15168.7				
340						
MY	NZZ					
19.1	-103.6	-5200.3				
19.1	-153.9	-10897.1				
19.1	-204.1	14665.7				
19.1	-254.4	2439.1				
19.1	-304.6	10800.0				
19.1	-354.9	3372.4				
19.1	-405.1	-4887.2				
19.1	-455.4	-9411.5				
19.1	-505.6	-16310.2				
732						
MY	NZZ					
19.1	-465.9	-16310.2				
19.1	-397.4	-12997.9				
19.1	-328.0	-10948.2				
19.1	-254.5	-7462.0				
19.1	-189.1	-5238.9				
19.1	-114.6	-1380.7				
19.1	-50.1	-1889.2				
19.1	13.3	-7524.8				
19.1	68.8	16.9				
732						
MY	NZZ					
19.1	-420.4	-15168.7				
19.1	-471.1	-10303.6				
19.1	-439.2	-9150.2				
19.1	-448.6	-6791.4				
19.1	-452.0	-6669.3				
19.1	-467.4	-2952.9				
19.1	-476.7	-10303.6				
19.1	-486.3	-6108.9				
19.1	-495.7	152.6				
472						
MY	NZZ					
19.4	-91.1	4631.9				
19.4	-24.1	30340.6				
19.4	115.8	-15332.6				
19.4	382.8	-4116.5				
19.4	233.9	-13252.9				
19.4	320.8	30400.0				
19.4	389.8	69796.4				
19.4	458.7	164936.2				
731						
MY	NZZ					
19.4	105.2	53875.6				
19.4	152.2	12257.7				
19.4	196.0	-13624.9				
19.4	245.2	-10250.0				
19.4	283.9	28118.1				
19.4	326.5	3398.8				
19.4	369.9	60294.9				
19.4	413.4	30133.8				
19.4	456.9	161713.3				
728						
MY	NZZ					
19.5	426.5	161713.3				
19.5	356.8	12876.3				
19.5	287.1	39443.3				
19.5	219.4	7757.8				
19.5	147.8	-4370.9				
19.5	78.1	32387.7				
19.5	8.4	-10250.0				
19.5	-61.3	752.2				

ASTA	24	nod	472	731	MY	NZZ
PROGR.	0	1212.8	1263.9	0.8	0.0	0.0
42.	-993.2	-889.2	0.8	0.0	-123.8	45905.6
84.	-773.5	514.6	0.8	0.0	-49.8	74731.1
126.	-553.9	139.9	0.8	0.0	-60.7	88881.5
168.	-334.3	-234.8	0.8	0.0	-130.5	86868.6
210.	-114.6	-609.4	0.8	0.0	-174.6	68752.2
252.	105.0	-984.1	0.8	0.0	-209.5	31272.4
294.	324.6	-1358.8	0.8	0.0	-244.4	13950.8
336.	544.3	-1733.4	0.8	0.0	-279.3	-78917.4
ASTA	25 <td>nod</td> <td>28</td> <td>473<td>MY<th>NZZ</th></td></td>	nod	28	473 <td>MY<th>NZZ</th></td>	MY <th>NZZ</th>	NZZ
PROGR.	0	-956.2	1565.0	0.8	72.6	-123.8
42.	-776.8	1190.3	0.8	72.6	-157.4	-39718.6
84.	-557.5	815.6	0.8	72.6	-191.1	2425.0
126.	-337.6	441.0	0.8	72.6	-224.7	28825.2
168.	-117.9	66.3	0.8	72.6	-258.4	39842.0
210.	101.7	-358.4	0.8	72.6	-292.0	34395.4
252.	321.3	-683.1	0.8	72.6	-325.6	13655.4
294.	541.0	-1027.7	0.8	72.6	-359.3	23008.0
336.	760.6	-1432.4	0.8	72.6	-392.9	-75324.8
ASTA	31 <td>nod</td> <td>342</td> <td>727</td> <td>MY<th>NZZ</th></td>	nod	342	727	MY <th>NZZ</th>	NZZ
PROGR.	0	-1276.3	1565.0	0.8	72.6	-123.8
42.	-776.8	1190.3	0.8	72.6	-157.4	-39718.6
84.	-557.5	815.6	0.8	72.6	-191.1	2425.0
126.	-337.6	441.0	0.8	72.6	-224.7	28825.2
168.	-117.9	66.3	0.8	72.6	-258.4	39842.0
210.	101.7	-358.4	0.8	72.6	-292.0	34395.4
252.	321.3	-683.1	0.8	72.6	-325.6	13655.4
294.	541.0	-1027.7	0.8	72.6	-359.3	23008.0
336.	760.6	-1432.4	0.8	72.6	-392.9	-75324.8
ASTA	36 <td>nod</td> <td>342</td> <td>727</td> <td>MY<th>NZZ</th></td>	nod	342	727	MY <th>NZZ</th>	NZZ
PROGR.	0	-1276.3	1565.0	0.8	72.6	-123.8
42.	-776.8	1190.3	0.8	72.6	-157.4	-39718.6
84.	-557.5	815.6	0.8	72.6	-191.1	2425.0
126.	-337.6	441.0	0.8	72.6	-224.7	28825.2
168.	-117.9	66.3	0.8	72.6	-258.4	39842.0
210.	101.7	-358.4	0.8	72.6	-292.0	34395.4
252.	321.3	-683.1	0.8	72.6	-325.6	13655.4
294.	541.0	-1027.7	0.8	72.6	-359.3	23008.0
336.	760.6	-1432.4	0.8	72.6	-392.9	-75324.8

PROGR.	0	-162.3	496.0	13157.8
42.	-993.2	-889.2	0.8	0.0
84.	-773.5	514.6	0.7	0.0
126.	-553.9	676.4	0.6	0.0
168.	-334.3	139.9	0.5	0.0
210.	-114.6	796.6	0.3	0.0
252.	105.0	856.3	0.2	0.0
294.	324.6	916.8	0.1	0.0
336.	544.3	916.8	0.0	-212.2
TZ2	TORS	MY	MZZ	
0.8	0.0	0.0	0.0	
0.8	0.0	-24.9	4527.3	
0.8	0.0	-69.8	74731.1	
0.8	0.0	-60.7	88881.5	
0.8	0.0	-139.6	86868.6	
0.8	0.0	-174.6	68752.2	
0.8	0.0	-209.5	31272.4	
0.8	0.0	-244.4	13950.8	
0.8	0.0	-279.3	-78917.4	
469	342	727	78917.4	
0.8	0.0	72.6	-123.8	
0.8	72.6	-123.8	-39705.6	
0.8	72.6	-157.4	-39718.6	
0.8	72.6	-191.1	2425.0	
0.8	72.6	-224.7	28825.2	
0.8	72.6	-258.4	39842.0	
0.8	72.6	-292.0	34395.4	
0.8	72.6	-325.6	13655.4	
0.8	72.6	-359.3	23008.0	
0.8	72.6	-392.9	-75324.8	
473	730	342	78917.4	
TZ2	TORS	MY	MZZ	
-3.7	-136.1	-375.2	4527.3	
-3.7	-136.1	-306.6	74731.1	
-3.7	-136.1	-236.9	88743.3	
-3.7	-136.1	-167.3	86868.6	
-3.7	-136.1	-98.2	-8473.4	
-3.7	-136.1	-29.1	2425.0	
-3.7	-136.1	40.3	28990.0	
-3.7	-136.1	109.5	34395.4	
-3.7	-136.1	178.7	39842.0	
473	730	342	78917.4	
1.3	-141.2	-240.9	-78917.4	
1.3	-141.2	-171.6	-39718.6	
1.3	-141.2	-92.4	-2425.0	
1.3	-141.2	-23.3	28825.2	
1.3	-141.2	55.9	34395.4	
1.3	-141.2	125.1	39842.0	
1.3	-141.2	194.3	23008.0	
1.3	-141.2	263.5	-75324.8	
1.3	-141.2	332.7	-158.0	
TZ2	TORS	MY	MZZ	
-6.2	-3.2	-156.8	-38285.2	
-6.2	-3.2	-156.8	-38285.2	
-6.2	-3.2	-100.3	-31522.4	
-6.2	-3.2	-100.3	-31522.4	
-6.2	-3.2	-480.2	-11273.4	
-6.2	-3.2	-218.6	-41.3	
-6.2	-3.2	-218.6	222.2	
-6.2	-3.2	304.7	9053.9	
-6.2	-3.2	304.7	9053.9	
978	41	727	1586.6	
-73.9	0.0	-7338.2	14829.0	
-73.9	0.0	-3814.3	14920.1	
-73.9	0.0	-403.2	2883.2	
-73.9	0.0	-2768.4	26275.3	
-73.9	0.0	-124.5	31272.4	
-73.9	0.0	278.1	38395.9	
-73.9	0.0	1801.4	36172.6	
-73.9	0.0	332.6	4163.7	
-73.9	0.0	4847.9	41518.8	
TZ2	TORS	MY	MZZ	
15.6	9.9	5287.6	2774.2	
15.6	9.9	4642.9	2187.2	
15.6	9.9	3990.7	1647.3	
15.6	9.9	3342.9	1107.4	
15.6	9.9	2686.4	570.5	
15.6	9.9	2034.5	21.0	
15.6	9.9	1382.2	-500.3	
15.6	9.9	730.0	-1044.7	
15.6	9.9	72.7	-1381.1	
93.6	468.1	0.0	471.3	
93.6	468.1	-151.1	-3069.3	
93.6	468.1	-304.6	-10691.3	
93.6	468.1	-453.9	-23899.4	
93.6	468.1	-603.4	-37889.4	
93.6	468.1	-760.6	-51969.5	
93.6	468.1	-916.8	-66049.6	
93.6	468.1	-1064.9	-79739.7	
93.6	468.1	-1217.0	-94352.2	
TZ2	TORS	MY	MZZ	
-40.8	-128.7	-504.9	-40963.9	
-40.8	-304.0	-619.5	-53808.1	
-40.8	-479.2	-691.6	-66653.2	
-40.8	-654.0	-493.9	-75333.5	
-40.8	-830.0	-395.1	-70437.9	
-40.8	-1005.0	-298.8	-61388.1	
-40.8	-1180.0	-197.5	-50129.0	
-40.8	-1355.0	-98.7	-38873.9	
-40.8	-1530.0	0.0	-27628.8	
-40.8	-1705.0	0.0	-16368.6	
TZ2	TORS	MY	MZZ	
12.8	-128.7	-1047.2	-46375.0	
12.8	-257.6	-1047.2	-46375.0	
12.8	-386.5	-983.2	-46375.0	
12.8	-515.4	-919.3	-44301.4	
12.8	-644.3	-855.4	-40702.2	
12.8	-773.2	-791.5	-37103.0	
12.8	-902.1	-727.6	-33503.8	
12.8	-1031.0	-663.7	-29904.6	
12.8	-1160.0	-599.8	-26305.4	
11	41	727	1586.6	
168.1	-840.7	-1217.0	-94352.2	
168.1	-840.7	-1190.2	-10105.6	
168.1	-840.7	-1163.4	-2086.2	

8,	-993.2	
9,	-993.7	
10,	-99.7	
ASTA	42	
PROGR.	0,	-147.3
0,	-147.3	
16,	-147.3	
33,	-147.3	
49,	-147.3	
65,	-147.3	
81,	-147.3	
98,	-147.3	
114,	-147.3	
130,	-147.3	
ASTA	43	
PROGR.	0,	2.0
1,	2.0	
3,	2.0	
4,	2.0	
5,	2.0	
6,	2.0	
8,	2.0	
9,	2.0	
10,	2.0	
ASTA	44	
PROGR.	0,	-115.3
1,	-115.3	
3,	-115.3	
4,	-115.3	
5,	-115.3	
6,	-115.3	
8,	-115.3	
9,	-115.3	
10,	-115.3	
ASTA	45	
PROGR.	0,	NOM
1,	25.6	
16,	25.6	
33,	25.6	
49,	25.6	
65,	25.6	
81,	25.6	
98,	25.6	
114,	25.6	
130,	25.6	
ASTA	46	
PROGR.	0,	-68.4
16,	-68.4	
33,	-68.4	
49,	-68.4	
65,	-68.4	
81,	-68.4	
98,	-68.4	
114,	-68.4	
130,	-68.4	
ASTA	47	
PROGR.	0,	-63.5
1,	-63.5	
3,	-63.5	
4,	-63.5	
5,	-63.5	
6,	-63.5	
8,	-63.5	
9,	-63.5	
10,	-63.5	
ASTA	48	
PROGR.	0,	130.1
1,	130.1	
3,	130.1	
4,	130.1	
5,	130.1	
6,	130.1	
8,	130.1	
9,	130.1	
10,	130.1	
ASTA	49	
PROGR.	0,	-187.3
16,	-187.3	
33,	-187.3	
49,	-187.3	
65,	-187.3	
81,	-187.3	
98,	-187.3	
114,	-187.3	
130,	-187.3	
ASTA	50	
PROGR.	0,	-73.2
16,	-73.2	
33,	-73.2	
49,	-73.2	
65,	-73.2	
81,	-73.2	
98,	-73.2	
114,	-73.2	
130,	-73.2	
ASTA	51	
PROGR.	0,	-611.0
1,	-611.0	
3,	-611.0	
4,	-611.0	
5,	-611.0	
6,	-611.0	
9,	-611.0	
10,	-611.0	
ASTA	52	
PROGR.	0,	-563.7
1,	-563.7	
3,	-563.7	
4,	-563.7	
5,	-563.7	
8,	-563.7	
9,	-563.7	
10,	-563.7	
ASTA	53	
PROGR.	0,	-63.7
16,	-65.7	
33,	-65.7	
49,	-65.7	
65,	-65.7	
81,	-65.7	
98,	-65.7	
114,	-65.7	

66.	-76.0	0.0	0.0	0.0	0.0	0.0	4.	-3901.7	-18.5	-4.8	0.0	-3.0	11.6	18.	329.8	-619.6	28.1	84.0	2758.0	10524.0	173.	-347.6	828.5	-0.5	0.0	94.8	-10852.1
99.	-76.0	0.0	0.0	0.0	0.0	0.0	5.	-3901.5	-18.5	-4.8	0.0	0.0	0.0	35.	329.8	-805.2	28.1	84.0	2765.5	9395.4	201.	-347.6	1125.7	-0.5	0.0	110.6	17240.2
132.	-76.0	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	35.	329.8	-805.2	28.1	84.0	2772.0	7541.2	201.	-347.6	1242.9	-0.5	0.0	126.4	53875.6
165.	-76.0	0.0	0.0	0.0	0.0	0.0	1.	-2997.2	22.3	-187.7	0.0	-936.5	-111.6	70.	329.8	-1176.4	28.1	84.0	1280.5	58378.6	ASTA	136	nodi	749	469	MY	NZZ
231.	-76.0	0.0	0.0	0.0	0.0	0.0	1.	-2997.0	22.3	-187.7	0.0	-936.5	-111.6	88.	329.8	-1261.9	28.1	84.0	788.0	36398.4	PROGR.	NORM	TY	TZ	TORS	MY	NZZ
264.	-76.0	0.0	0.0	0.0	0.0	0.0	1.	-2996.8	22.3	-187.3	0.0	-936.5	-111.6	123.	329.8	-1733.1	28.1	84.0	107.0	4747.7	29.	441.7	467.1	0.6	0.0	-17.9	17700.3
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	1.	-2996.7	22.3	-187.3	0.0	-936.5	-111.6	140.	329.8	-1918.7	28.1	84.0	-689.4	-4994.7	29.	441.7	467.1	0.6	0.0	-17.9	17700.3
0.	757.7	0.0	0.0	0.0	0.0	0.0	2.	-2996.5	22.3	-187.3	0.0	-468.3	-55.8	ASTA	120	nodi	745	746	MY	NZZ	115.	441.7	-424.4	0.6	0.0	-71.8	19542.3
33.	757.7	0.0	0.0	0.0	0.0	0.0	3.	-2996.3	22.3	-187.7	0.0	-352.1	-41.9	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	115.	441.7	-424.4	0.6	0.0	-71.8	19542.3
66.	757.7	0.0	0.0	0.0	0.0	0.0	4.	-2996.1	22.3	-187.3	0.0	-27.9	0.0	16.	-708.2	-881.8	2.4	-2026.1	-39.4	-1253.9	9.0	-15.8	-821.6	0.6	0.0	-15.8	3070.0
99.	757.7	0.0	0.0	0.0	0.0	0.0	4.	-2995.9	22.3	-187.3	0.0	-117.1	-14.0	36.	-708.2	-890.8	2.4	-2026.1	-78.7	-1031.8	0.6	-15.8	-821.6	0.6	0.0	-15.8	3070.0
132.	757.7	0.0	0.0	0.0	0.0	0.0	5.	-2995.8	22.3	-187.3	0.0	0.0	0.0	49.	-708.2	-908.8	2.4	-2026.1	-151.2	-1477.9	0.6	-15.8	-821.6	0.6	0.0	-15.8	3070.0
165.	757.7	0.0	0.0	0.0	0.0	0.0	ASTA	104	nodi	742	466	MY	NZZ	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	170.	441.7	-1018.7	0.6	0.0	-107.6	-21945.4
198.	757.7	0.0	0.0	0.0	0.0	0.0	1.	-2516.1	-95.1	5374.0	0.0	26870.2	475.6	81.	-708.2	-926.8	2.4	-2026.1	-136.9	-71608.8	230.	-15.8	-1258.5	0.6	0.0	-143.5	-9705.6
231.	757.7	0.0	0.0	0.0	0.0	0.0	1.	-2515.9	-95.1	5374.0	0.0	20352.7	416.2	98.	-708.2	-935.8	2.4	-2026.1	-236.2	-867.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ
264.	757.7	0.0	0.0	0.0	0.0	0.0	2.	-2515.7	-95.1	5374.0	0.0	13455.1	237.8	114.	-708.2	-944.8	2.4	-2026.1	-277.6	-10022.2	115.	-54.4	0.0	0.0	0.0	-15.8	3070.0
ASTA	83	nodi	467	470	473	475	2.	-2515.5	-95.1	5374.0	0.0	16793.9	297.3	130.	-708.2	-953.8	2.4	-2026.1	-315.0	-117449.9	58.	-15.8	524.4	-5.9	-15.5	-335.4	19764.2
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	3.	-2515.3	-95.1	5374.0	0.0	10076.3	178.4	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	86.	-15.8	227.3	-5.9	-15.5	-166.5	30569.6
0.	943.4	0.0	0.0	0.0	0.0	0.0	4.	-2515.0	-95.1	5374.0	0.0	6717.6	118.9	1.	-169.1	1135.0	-23.8	-237.7	-283.2	-101865.0	144.	-15.8	-367.0	-5.9	-15.5	-171.2	26551.0
45.	943.4	0.0	0.0	0.0	0.0	0.0	2.	-2514.8	-95.1	5374.0	0.0	3358.8	59.5	16.	-169.1	1126.0	-23.8	-237.7	102.9	-83491.8	173.	-15.8	-664.2	-5.9	-15.5	-171.2	26551.0
134.	943.4	0.0	0.0	0.0	0.0	0.0	3.	-2514.6	-95.1	5374.0	0.0	0.0	0.0	33.	-169.1	1117.0	-23.8	-237.7	488.9	-65266.9	230.	-15.8	-961.3	-5.9	-15.5	208.9	-11640.2
169.	943.4	0.0	0.0	0.0	0.0	0.0	ASTA	105	nodi	742	467	MY	NZZ	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	173.	-15.8	-664.2	-5.9	-15.5	208.9	-11640.2
224.	943.4	0.0	0.0	0.0	0.0	0.0	1.	-4128.4	720.0	-1842.7	0.0	-90713.7	-3600.0	65.	-169.1	1099.0	-23.8	-237.7	1261.1	-2956.1	ASTA	138	nodi	975	953	MY	NZZ
279.	943.4	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-1842.7	0.0	-79374.5	-3150.0	98.	-169.1	1106.0	-23.8	-237.7	2031.2	-11470.2	0.	-54.4	0.0	0.0	0.0	0.0	0.0
313.	943.4	0.0	0.0	0.0	0.0	0.0	1.	-4128.0	720.0	-1842.7	0.0	-68035.3	-2700.0	114.	-169.1	1072.0	-23.8	-237.7	2419.3	2366.2	29.	-54.4	891.4	0.0	0.0	-0.1	29900.7
358.	943.4	0.0	0.0	0.0	0.0	0.0	2.	-4127.9	720.0	-1842.7	0.0	-56066.1	-2250.0	130.	-169.1	1063.0	-23.8	-237.7	3805.3	41009.6	86.	-54.4	291.0	0.0	0.0	-0.1	5128.2
ASTA	86	nodi	19	473	475	477	3.	-4127.7	720.0	-1842.7	0.0	-54017.6	-1350.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	86.	-54.4	291.0	0.0	0.0	-0.1	64072.6
0.	72.8	0.0	0.0	0.0	0.0	0.0	4.	-4127.3	720.0	-1842.7	0.0	-22678.4	0.0	ASTA	122	nodi	748	737	MY	NZZ	29.	-54.4	891.4	0.0	0.0	-0.1	64072.6
45.	72.8	0.0	0.0	0.0	0.0	0.0	4.	-4127.2	720.0	-1842.7	0.0	-22678.4	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	86.	-54.4	291.0	0.0	0.0	-0.1	64072.6
90.	72.8	0.0	0.0	0.0	0.0	0.0	4.	-4127.1	720.0	-1842.7	0.0	-11339.2	-400.0	15.	-8.3	297.3	24.9	5.7	2805.3	40205.3	144.	-54.4	-294.2	0.0	0.0	-0.6	64072.6
135.	72.8	0.0	0.0	0.0	0.0	0.0	4.	-4127.0	720.0	-1842.7	0.0	-450.0	0.0	35.	-8.3	143.3	24.9	5.7	2368.9	40205.3	173.	-54.4	-294.2	0.0	0.0	-0.7	51256.9
180.	72.8	0.0	0.0	0.0	0.0	0.0	ASTA	106	nodi	741	468	MY	NZZ	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	173.	-54.4	-294.2	0.0	0.0	-0.7	51256.9
225.	72.8	0.0	0.0	0.0	0.0	0.0	0.	-9774.0	-675.0	9248.5	0.0	46242.4	3375.2	53.	-8.3	103.8	24.9	5.7	1851.9	40205.3	230.	-54.4	-1188.6	0.0	0.0	-0.9	-2.6
270.	72.8	0.0	0.0	0.0	0.0	0.0	1.	-9773.8	-675.0	9248.5	0.0	40462.1	2953.3	88.	-8.3	-47.3	24.9	5.7	623.3	3518.7	PROGR.	NORM	TY	TZ	TORS	MY	NZZ
315.	72.8	0.0	0.0	0.0	0.0	0.0	2.	-9773.6	-675.0	9248.5	0.0	28901.5	2309.5	105.	-8.3	-627.1	24.9	5.7	186.9	2289.6	0.	-768.9	798.5	1.6	-5.8	234.1	-9338.1
360.	72.8	0.0	0.0	0.0	0.0	0.0	2.	-9773.4	-675.0	9248.5	0.0	15580.6	941.8	123.	-8.3	-781.2	24.9	5.7	1851.9	40205.3	10.	-768.9	619.2	1.6	-5.8	407.0	6031.3
ASTA	88	nodi	468	442	442	442	3.	-9773.3	-675.0	9248.5	0.0	5780.8	421.9	35.	-708.2	-935.8	2.4	-2026.1	-236.2	-867.8	35.	-768.9	427.3	1.6	-5.8	179.1	12112.7
0.	210.1	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	10.	-768.9	56.2	1.6	-5.8	123.3	20574.5
45.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-9772.5	-675.0	9248.5	0.0	0.0	0.0	10.	-708.2	-935.8	2.4	-2026.1	-236.2	-867.8	105.	-768.9	-313.0	1.6	-5.8	67.5	16044.2
90.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-9772.4	-675.0	9248.5	0.0	0.0	0.0	123.	-768.9	-500.6	1.6	-5.8	39.6	8908.3	PROGR.	NORM	TY	TZ	TORS	MY	NZZ
135.	210.1	0.0	0.0	0.0	0.0	0.0	ASTA	107	nodi	740	469	MY	NZZ	10.	-708.2	-935.8	2.4	-2026.1	-236.2	-867.8	10.	-768.9	-313.0	1.6	-5.8	67.5	16044.2
180.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-2443.3	74.4	2699.1	0.0	1340.8	-372.1	5.	-70.2	-1301.5	-15.8	-2303.9	-236.1	-12218.6	10.	-768.9	-313.0	1.6	-5.8	39.6	8908.3
225.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-2443.1	74.4	2699.1	0.0	11808.6	-325.6	8.	-70.2	-1301.5	-15.8	-2303.9	-236.1	-12218.6	10.	-768.9	-313.0	1.6	-5.8	39.6	8908.3
270.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-2443.0	74.4	2699.1	0.0	10121.7	-279.1	8.	-70.2	-1301.5	-15.8	-2303.9	-236.1	-12218.6	10.	-768.9	-313.0	1.6	-5.8	39.6	8908.3
315.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-2442.8	74.4	2699.1	0.0	8647.8	-183.0	8.	-70.2	-1301.5	-15.8	-2303.9	-236.1	-12218.6	10.	-768.9	-313.0	1.6	-5.8	39.6	8908.3
360.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-2442.4	74.4	2699.1	0.0	6747.8	-93.0	ASTA	124	nodi	735	747	MY	NZZ	10.	-768.9	-313.0	1.6	-5.8	39.6	8908.3
ASTA	89	nodi	469	443	443	443	1.	-2442.4	74.4	2699.1	0.0	5780.8	421.9	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	10.	-768.9	-313.0	1.6	-5.8	39.6	8908.3
0.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-2442.4	74.4	2699.1	0.0	5780.8	421.9	1.	-69.2	2109.1	12.5	1500.4	-158.2	-122028.8	88.	-25.6	-142.7	1.2	30.6	182.0	61505.3
45.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-69.2	2109.1	12.5	1500.4	-158.2	12.	1500.4	-173.8	-12029.9	12.	1500.4	-173.8	-12029.9	18.	-25.6	-142.7	1.2	30.6	160.9	62654.2
90.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-69.2	2109.1	12.5	1500.4	-158.2	12.	1500.4	-173.8	-12029.9	12.	1500.4	-173.8	-12029.9	18.	-25.6	-142.7	1.2	30.6	160.9	62654.2
135.	210.																										

1979.6	782.2	-0.7	-55.8	278.8	-16540.2
1980.6	1156.9	-0.7	-55.8	308.9	25796.6
1981.6	-200.0	0.0	-55.8	339.6	79016.6
sta	4	nodes	230		
1982.6	1174.4	-1567.1	-58.9	100.4	92844.5
1983.6	954.5	-1182.4	-0.8	-58.9	4208.6
1984.6	73.8	-8.4	-0.8	-58.9	132.1
1985.6	116.5	-443.1	-0.8	-58.9	135.3
1986.6	206.6	116.6	-0.8	-58.9	2843.0
1987.6	230.0	76.2	306.3	-58.9	2586.6
1988.6	-143.6	105.6	-58.9	-58.9	290.9
1989.6	-363.1	105.6	-58.9	-58.9	2304.7
1990.6	-582.7	1430.3	-58.9	353.5	75252.6
1991.6	1174.4	1174.4	1174.4	1174.4	1174.4
1992.6	1174.4	1174.4	1174.4	1174.4	1174.4
1993.6	1174.4	1174.4	1174.4	1174.4	1174.4
1994.6	1174.4	1174.4	1174.4	1174.4	1174.4
1995.6	1174.4	1174.4	1174.4	1174.4	1174.4
1996.6	1174.4	1174.4	1174.4	1174.4	1174.4
1997.6	1174.4	1174.4	1174.4	1174.4	1174.4
1998.6	1174.4	1174.4	1174.4	1174.4	1174.4
1999.6	1174.4	1174.4	1174.4	1174.4	1174.4
2000.6	1174.4	1174.4	1174.4	1174.4	1174.4
2001.6	1174.4	1174.4	1174.4	1174.4	1174.4
2002.6	1174.4	1174.4	1174.4	1174.4	1174.4
2003.6	1174.4	1174.4	1174.4	1174.4	1174.4
2004.6	1174.4	1174.4	1174.4	1174.4	1174.4
2005.6	1174.4	1174.4	1174.4	1174.4	1174.4
2006.6	1174.4	1174.4	1174.4	1174.4	1174.4
2007.6	1174.4	1174.4	1174.4	1174.4	1174.4
2008.6	1174.4	1174.4	1174.4	1174.4	1174.4
2009.6	1174.4	1174.4	1174.4	1174.4	1174.4
2010.6	1174.4	1174.4	1174.4	1174.4	1174.4
2011.6	1174.4	1174.4	1174.4	1174.4	1174.4
2012.6	1174.4	1174.4	1174.4	1174.4	1174.4
2013.6	1174.4	1174.4	1174.4	1174.4	1174.4
2014.6	1174.4	1174.4	1174.4	1174.4	1174.4
2015.6	1174.4	1174.4	1174.4	1174.4	1174.4
2016.6	1174.4	1174.4	1174.4	1174.4	1174.4
2017.6	1174.4	1174.4	1174.4	1174.4	1174.4
2018.6	1174.4	1174.4	1174.4	1174.4	1174.4
2019.6	1174.4	1174.4	1174.4	1174.4	1174.4
2020.6	1174.4	1174.4	1174.4	1174.4	1174.4
2021.6	1174.4	1174.4	1174.4	1174.4	1174.4
2022.6	1174.4	1174.4	1174.4	1174.4	1174.4
2023.6	1174.4	1174.4	1174.4	1174.4	1174.4
2024.6	1174.4	1174.4	1174.4	1174.4	1174.4
2025.6	1174.4	1174.4	1174.4	1174.4	1174.4
2026.6	1174.4	1174.4	1174.4	1174.4	1174.4
2027.6	1174.4	1174.4	1174.4	1174.4	1174.4
2028.6	1174.4	1174.4	1174.4	1174.4	1174.4
2029.6	1174.4	1174.4	1174.4	1174.4	1174.4
2030.6	1174.4	1174.4	1174.4	1174.4	1174.4
2031.6	1174.4	1174.4	1174.4	1174.4	1174.4
2032.6	1174.4	1174.4	1174.4	1174.4	1174.4
2033.6	1174.4	1174.4	1174.4	1174.4	1174.4
2034.6	1174.4	1174.4	1174.4	1174.4	1174.4
2035.6	1174.4	1174.4	1174.4	1174.4	1174.4
2036.6	1174.4	1174.4	1174.4	1174.4	1174.4
20					

6.	2.0	-6240.0	716.9	3124.3	7885.7	-372206.5	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	179.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	Asta	105	nodr	12	467	MY	NZZ	
8.	2.0	-6240.7	716.9	3124.3	6989.5	-380066.9	0.	-1.3	282.1	-7.9	184.0	-587.0	-34748.6	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	
9.	2.0	-6241.0	716.9	3124.3	6989.5	-380066.9	16.	-1.3	278.2	-7.9	184.0	-458.2	-30306.3	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
10.	2.0	-6242.1	716.9	3124.3	5197.2	-395603.3	33.	-1.3	274.2	-7.9	184.0	-329.5	-25708.7	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	86	nodr	38	21	467	MY	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	324.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-115.3	12873.2	640.2	3087.1	5128.8	-339592.3	49.	-1.3	270.2	-7.9	184.0	-200.8	-12385.8	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
1.	-115.3	12873.2	640.2	3087.1	5128.8	-339592.3	81.	-1.3	262.2	-7.9	184.0	-56.7	-12634.0	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
3.	-115.3	12871.8	640.2	3087.1	3528.2	-307401.0	104.	-1.3	254.3	-7.9	184.0	314.2	-4240.8	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
4.	-115.3	12871.1	640.2	3087.1	2727.9	-291311.6	130.	-1.3	250.3	-7.9	184.0	442.9	-141.2	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
5.	-115.3	12870.4	640.2	3087.1	1512.9	-24929.5	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	45.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
6.	-115.3	12869.1	640.2	3087.1	1127.3	-25915.5	0.	-1.3	247.6	-7.9	184.0	-18.0	-41.0	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
9.	-115.3	12868.4	640.2	3087.1	-471.4	-26962.9	16.	-2.4	-278.6	3.7	-168.5	-32.5	-462.9	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
30.	-115.3	12812.7	640.2	3087.1	-1273.7	-120877.8	16.	-2.4	-278.6	3.7	-168.5	-32.5	-462.9	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	45	nodr	21	30	467	MY	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	180.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-25.6	2061.3	-34.8	-288.1	-1247.6	-97286.5	49.	-2.4	-286.6	3.7	-168.5	-153.6	-1306.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
16.	-25.6	2072.3	-34.8	-288.1	-708.1	-13088.7	65.	-2.4	-290.5	3.7	-168.5	-214.1	-1895.7	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
31.	-25.6	2061.3	-34.8	-288.1	-142.6	-97286.5	81.	-2.4	-286.6	3.7	-168.5	-153.6	-1306.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
49.	-25.6	2054.3	-34.8	-288.1	422.9	-63811.5	98.	-2.4	-298.5	3.7	-168.5	-331.5	-2806.6	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
65.	-25.6	2045.3	-34.8	-288.1	988.4	-8022.9	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	360.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
81.	-25.6	2086.3	-34.8	-288.1	1512.9	-24929.5	0.	-1.3	247.6	-7.9	184.0	-18.0	-41.0	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
98.	-25.6	2027.3	-34.8	-288.1	2119.5	33655.5	10.	-1.4	6.8	-0.9	-2.6	-367.4	-38301.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
114.	-25.6	2008.2	-34.8	-288.1	2685.0	-85925.2	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	135.	210.1	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
130.	-25.6	2009.2	-34.8	-288.1	3250.5	101248.5	0.	-1.4	6.2	-0.9	-2.6	-365.0	-38005.2	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	58	nodr	29	467	MY	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	225.	210.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-68.4	-2869.8	24.0	120.1	0.0	341.9	5.	-1.4	5.6	-0.9	-2.6	-362.7	-38070.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
1.	-68.4	-2878.8	24.0	120.1	-301.5	-46365.9	10.	-1.4	4.4	-0.9	-2.6	-357.9	-38045.6	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
33.	-68.4	-2887.8	24.0	120.1	-780.9	-93270.0	13.	-1.4	3.8	-0.9	-2.6	-355.6	-38035.4	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
49.	-68.4	-2896.8	24.0	120.1	-1171.4	-140220.5	15.	-1.4	3.1	-0.9	-2.6	-353.2	-38026.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
65.	-68.4	-2905.8	24.0	120.1	-1561.9	-187837.3	18.	-1.4	2.5	-0.9	-2.6	-350.8	-38019.7	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
81.	-68.4	-2914.8	24.0	120.1	-1952.3	-234604.4	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	315.	210.1	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
98.	-68.4	-2923.9	24.0	120.1	-2343.3	-293685.6	0.	-1.5	8.8	-0.9	-2.6	-347.4	-38011.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
120.	-68.4	-2941.9	24.0	120.1	-3212.8	-377441.6	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	360.	210.1	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	47	nodr	961	42	467	MY	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	45.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-63.5	-6860.5	-19.4	-96.8	-3127.8	-377441.6	49.	-3.7	294.0	-0.3	162.3	-203.1	-2324.9	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
1.	-63.5	-6861.2	-19.4	-96.8	-3099.5	-363168.2	65.	-3.7	290.0	-0.3	162.3	-188.3	-1869.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
4.	-63.5	-6861.9	-19.4	-96.8	-3048.2	-154895.2	81.	-3.7	286.0	-0.3	162.3	-139.3	-13789.4	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
6.	-63.5	-6862.6	-19.4	-96.8	-3051.1	-403623.0	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	180.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
9.	-63.5	-6863.0	-19.4	-96.8	-3056.9	-412336.6	0.	-3.7	282.1	-0.3	162.3	-138.3	-1869.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
16.	-63.5	-6864.0	-19.4	-96.8	-3007.7	-42108.2	114.	-3.7	278.1	-0.3	162.3	-138.3	-1869.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
30.	-63.5	-6864.7	-19.4	-96.8	-2978.5	-422811.6	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	1.	-912.1	20.1	2651.0	0.0	9941.3	-75.4	0.0	1.	-912.1	20.1	2651.0	0.0	9941.3	-75.4	0.0
Asta	60	nodr	962	963	467	MY	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	4.	-911.6	20.1	2651.0	0.0	9941.3	-75.4	0.0	1.	-911.6	20.1	2651.0	0.0	9941.3	-75.4	0.0
0.	-192.1	6977.7	-3.8	-19.0	-2940.0	-463106.1	5.	-37.0	2.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-911.6	20.1	2651.0	0.0	9941.3	-75.4	0.0
1.	-192.1	6977.0	-3.8	-19.0	-2915.2	-45484.4	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	4.	-911.6	20.1	2651.0	0.0	9941.3	-75.4	0.0	1.	-911.6	20.1	2651.0	0.0	9941.3	-75.4	0.0
4.	-192.1	6976.4	-3.8	-19.0	-2930.5	-445635.3	99.	-37.0	2.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-911.6	20.1	2651.0	0.0	9941.3	-75.4	0.0
5.	-192.1	6975.7	-3.8	-19.0	-2921.0	-428244.4	124.	-37.0	2.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-911.6	20.1	2651.0	0.0	9941.3	-75.4	0.0
6.	-192.1	6974.3	-3.8	-19.0	-2916.3	-419595.1	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	1.	-2363.7	-148.5	5953.6	0.0	11861.2	-25.1	0.0	1.	-2363.7	-148.5	5953.6	0.0	11861.2	-25.1	0.0
9.	-192.1	6973.9	-3.8	-19.0	-29																								

49.	-169.1	-1708.8	-23.8	-237.7	875.0	-47188.3	230.	-15.8	-1258.5	-5.9	-15.5	677.8	-43550.5	33.	32.5	1386.8	-2.8	10.4	-94.3	-71105.1	4.	-1703.3	33.9	3701.3	0.0	2313.3	-21.2
65.	-169.1	1099.0	-23.8	237.7	1261.1	-29256.1	Asta	138	nodi	975	953			49.	32.5	1377.8	-2.8	10.4	-48.3	-48643.3	5.	-1703.1	33.9	3701.3	0.0	0.0	0.0
81.	-169.1	1090.0	-23.8	237.7	1641.2	-11470.7	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ
98.	-169.1	1081.0	-23.8	237.7	2033.2	6169.4	0.	0.	-54.4	1188.6	0.0	0.0	0.0	81.	32.5	1359.8	-2.8	10.4	-43.8	-4158.6	1.	-1189.0	-54.4	0.0	0.0	0.0	
114.	-169.1	1072.0	-23.8	237.7	2419.3	2386.6	29.	-54.4	891.4	0.0	0.0	-0.1	2900.7	98.	32.5	1350.8	-2.8	10.4	89.9	-4982.0	0.	-1189.0	-54.4	0.0	0.0	272.1	
130.	-169.1	1063.0	-23.8	237.7	2810.4	1063.0	86.	-54.4	1364.7	0.0	0.0	0.0	6407.6	130.	32.5	1337.2	-2.8	10.4	182.0	-6744.1	1.	-1189.0	-54.4	0.0	0.0	0.0	
PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ
0.	-8.3	297.3	24.9	5.7	2805.3	40205.3	115.	-54.4	297.2	0.0	0.0	-0.6	64071.9	0.	-20.9	-782.9	8.5	42.5	0.0	104.5	3.	-1189.1	-54.4	0.0	0.0	136.0	
18.	-8.3	343.3	24.9	5.7	2368.9	44800.5	173.	-54.4	-594.3	0.0	0.0	-0.7	51256.9	0.	-20.9	-771.9	8.5	42.5	-130.0	-1235.6	3.	-1189.1	-54.4	0.0	0.0	102.0	
35.	-8.3	391.3	24.9	5.7	1915.5	48013.5	140.	-54.4	-801.3	0.0	0.0	-0.8	27867.7	0.	-20.9	-780.9	8.5	42.5	-118.0	-1774.8	4.	-1189.0	-54.4	0.0	0.0	68.0	
53.	-8.3	464.9	24.9	5.7	1496.1	43682.2	230.	-54.4	-1188.6	0.0	0.0	-0.9	-2.6	35.	-20.9	-789.9	8.5	42.5	-276.0	-4982.0	4.	-1188.8	-54.4	0.0	0.0	34.0	
70.	-8.3	510.2	24.9	5.7	1040.0	441	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ
88.	-8.3	473.0	24.9	5.7	631.3	32518.7	0.	0.	-1189.0	0.0	0.0	-0.9	-2.6	65.	-20.9	-788.9	8.5	42.5	-552.0	-10653.9	5.	-1189.0	-54.4	0.0	0.0	170.1	
105.	-8.3	527.1	24.9	5.7	184.9	37985.1	18.	-768.9	612.9	1.6	-5.8	207.0	3011.1	0.	-768.9	8.5	20.9	0.0	25.1	-690.0	60.	-2962.9	-2219.4	-229.7	0.0	42408.3	
123.	-8.3	578.2	24.9	5.7	249.5	10570.3	35.	-768.9	241.7	1.6	-5.8	179.1	12117.7	0.	-768.9	8.5	20.9	0.0	78.4	-43.8	15.	-2929.5	-2219.4	-229.7	0.0	39052.2	
140.	-8.3	635.2	24.9	5.7	68.9	44484.8	70.	-768.9	56.2	1.6	-5.8	123.3	20573.5	0.	-768.9	8.5	20.9	0.0	25.1	-690.0	30.	-2929.7	-2219.4	-229.7	0.0	33606.1	
PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ
0.	-70.2	-1907.7	-15.8	2303.9	-215.0	-11749.7	105.	-768.9	129.4	1.6	-5.8	95.4	19922.6	0.	-762.9	8.5	20.9	0.0	104.5	-42.5	75.	-2884.0	-2219.4	-229.7	0.0	32159.8	
1.	-70.2	-1908.4	-15.8	2303.9	-295.2	-118832.7	123.	-768.9	-500.6	1.6	-5.8	39.6	8908.3	0.	-762.9	8.5	20.9	0.0	91.4	-37.2	105.	-2870.2	-2219.4	-229.7	0.0	19318.0	
3.	-70.2	-1909.1	-15.8	2303.9	-275.5	-122238.6	Asta	142	nodi	970	738			1.	-762.7	8.5	20.9	0.0	65.3	-26.5	120.	-2847.4	-2219.4	-229.7	0.0	1875.2	
5.	-70.2	-1909.8	-15.8	2303.9	-253.8	-124662.4	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ
7.	-70.2	-1910.5	-15.8	2303.9	-236.1	-126939.0	0.	0.	-1189.0	0.0	0.0	-0.9	-2.6	1.	-762.7	8.5	20.9	0.0	65.3	-26.5	120.	-2847.4	-2219.4	-229.7	0.0	1875.2	
9.	-70.2	-1911.2	-15.8	2303.9	-216.4	-129381.5	10.	-70.2	-1913.2	-15.8	2303.9	-157.2	-136532.3	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
18.	-70.2	-1911.8	-15.8	2303.9	-196.6	-131770.9	35.	-76.8	-167.5	1.2	30.6	182.0	61305.3	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
35.	-70.2	-1912.5	-15.8	2303.9	-176.9	-134162.1	53.	-25.6	-319.5	1.2	30.6	118.6	56863.4	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
53.	-70.2	-1913.2	-15.8	2303.9	-157.2	-136532.3	88.	-25.6	-627.7	1.2	30.6	76.3	40375.2	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
Asta	124	nodi	735	747			105.	-768.9	56.2	1.6	-5.8	95.4	19922.6	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ
0.	69.2	2109.1	12.5	1500.4	-158.2	-122928.8	123.	-76.8	-167.5	1.2	30.6	118.6	56863.4	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
1.	69.2	2108.4	12.5	1500.4	-215.8	-120029.9	140.	-25.6	-1089.9	1.2	30.6	12.9	-4798.3	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
3.	69.2	2107.7	12.5	1500.4	-189.5	-117657.8	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ
5.	69.2	2107.0	12.5	1500.4	-205.1	-115057.3	0.	0.	-1189.0	0.0	0.0	-0.9	-2.6	1.	-762.7	8.5	20.9	0.0	65.3	-26.5	120.	-2847.4	-2219.4	-229.7	0.0	1875.2	
7.	69.2	2106.3	12.5	1500.4	-236.3	-109757.9	10.	-70.2	-1913.2	-15.8	2303.9	-157.2	-136532.3	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
9.	69.2	2105.6	12.5	1500.4	-267.6	-104495.6	35.	-76.8	-167.5	1.2	30.6	118.6	56863.4	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
18.	69.2	2104.2	12.5	1500.4	-287.6	-104495.6	53.	-25.6	-319.5	1.2	30.6	76.3	40375.2	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
35.	69.2	2103.5	12.5	1500.4	-283.2	-101865.7	88.	-25.6	-627.7	1.2	30.6	12.9	-4798.3	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
Asta	125	nodi	748	751			105.	-768.9	56.2	1.6	-5.8	95.4	19922.6	0.	-762.9	8.5	20.9	0.0	39.2	-15.9	15.	-25074.7	-238.5	-253.7	0.0	75949.0	
PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ
0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
1.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
2.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
3.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
4.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
5.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
6.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
7.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
8.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
9.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
10.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
11.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
12.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-0.9	0.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	0.0
13.	-765.7	48.7	-160.9	0.0	0.0	-703.7	-213.0	0.	0.	-1189.0	0.0	0.0	-														

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3.	-33.2	-856.5	-917.0	-4199.2	6679.4	7097.3	0.0	15.8	-26.3	-91.6	-505.6	81.9	-42.0	4.	34.8	627.7	-566.6	2365.4	-3713.9	-3865.2	16.1	-320.7	57.9	23	1677.8	1111.1	-952.0
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.2	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32</						

[illegible]

PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																														
																										ASTA	PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
																																																					ASTA	PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																								
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45.	0.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

3.	50.3	-60.4	-8.6	0.0	-26.7	188.7	0.	PROGR.	NORM	TYV	TYZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5	
3.	-62.7	60.5	-12.0	0.0	-37.4	-189.1	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	244.9	189.0		
3.	-50.3	60.4	8.6	0.0	21.4	-150.9	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	5.1	-1.9	-26.7	1.6	-323.5	3.9	20.0	-14.5	176.7	-443.9	1200.6		
3.	50.3	-60.5	-8.6	0.0	-21.4	150.9	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0		
3.	-62.7	60.5	-12.0	0.0	22.5	113.4	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0		
3.	-50.3	60.4	8.6	0.0	16.0	113.3	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	-1.9	-26.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9		
4.	-62.7	60.5	-12.0	0.0	-22.5	-113.4	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0		
4.	-62.7	60.5	-12.0	0.0	10.7	-75.5	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0		
4.	-50.3	60.4	8.6	0.0	-10.8	75.5	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	-1.9	-26.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9		
4.	-62.7	60.5	-12.0	0.0	-13.0	-75.5	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0		
5.	-50.3	60.4	8.6	0.0	0.0	0.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	-1.9	-26.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9		
5.	-62.7	60.5	-12.0	0.0	0.0	0.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0		
Asta	PROGR.	0.	109	nord	TYV	TYZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5						
Asta	PROGR.	0.	-861.3	900.3	-22.5	0.0	112.3	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	906.8	-974.4	-24.7	0.0	-123.6	487.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		
1.	861.3	-900.3	-22.5	0.0	112.6	450.7	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5		

5.	Asta PROGR. 0.	8.1	41.9	0.0	0.0	0.0	-26.2	76.5	8.0	0.0	0.0	3.0	686.5	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	41.5	-19.0	0.0	-35.6	-77.7	
		-6.6	-6.3	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-4.0	-915.4	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	19.0	0.0	23.7	-91.8	
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.1	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	19.0	0.0	-7.6	-44.3	
		-8.1	-41.9	0.0	0.0	0.0	0.0	-35.1	-9.1	0.1	0.0	-7.7	-1044.7	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-35.4	6.1	0.0	7.6	-44.3
		-8.0	-41.9	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-8.1	-41.9	0.0	0.0	0.0	0.0	-35.1	-9.1	0.1	0.0	-7.7	-1044.7	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-35.4	6.1	0.0	7.6	-44.3
		-8.0	-41.9	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
1.	Asta PROGR. 0.	127	746	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
2.	Asta PROGR. 0.	127	746	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm

	317.9	12.7	-23.4	81.6	7868.8	-1623.3		3.9	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5415.8	70.1		-3.9	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5415.7	70.1		0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.	-317.9	-12.7	-23.4	-81.6	-7868.8	1623.3		-4.8	0.0	0.0	0.0	0.0	0.0	0.0
	-317.9	-12.7	-23.4	-81.6	-7883.4	-1615.4		3.9	0.0	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5426.3	712.2		0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	5426.7	-712.2								
3.	-317.9	-12.7	-23.4	-81.6	-7898.1	-1607.4		3.9	0.0	0.0	0.0	0.0	0.0	0.0
	-317.9	-12.7	-23.4	-81.6	-7898.4	-1607.4		0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5437.6	72.2		245.6	8.1	-7.7	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5437.6	72.2		-245.6	-8.1	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5437.6	72.2		245.6	8.1	0.0	0.0	0.0	0.0	0.0
3.	-317.9	-12.7	-23.4	-81.6	-7898.1	-1607.4		-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	-317.9	-12.7	-23.4	-81.6	-7902.4	-1599.5		245.6	8.1	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5448.6	73.2		-245.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	-234.3	1.6	-17.5	-61.4	-5448.6	73.2		253.5	6.7	0.0	0.0	0.0	0.0	0.0
4.	-317.9	-12.7	-23.4	-81.6	-7902.4	-1599.5		-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	-317.9	-12.7	-23.4	-81.6	-7927.3	-1591.5		245.6	8.1	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5469.6	-74.3		-253.5	-6.7	0.0	0.0	1.2	385.7	0.0
	-234.3	1.6	-17.5	-61.4	-5469.6	-74.3		245.6	8.1	0.0	0.0	2.2	-465.0	0.0
4.	-317.9	-12.7	-23.4	-81.6	-7927.3	-1591.5		-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	-317.9	-12.7	-23.4	-81.6	-7942.0	-1583.5		245.6	8.1	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5470.4	-75.3		-253.5	-6.7	0.0	0.0	1.8	578.5	0.0
	-234.3	1.6	-17.5	-61.4	-5470.4	-75.3		245.6	8.1	0.0	0.0	3.3	-697.5	0.0
5.	-317.9	-12.7	-23.4	-81.6	-7942.0	-1583.5		-253.5	-6.7	0.0	0.0	-2.4	-771.4	0.0
	-317.9	-12.7	-23.4	-81.6	-7956.6	-1575.6		245.6	8.1	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5481.4	-76.3		-245.6	-8.1	0.0	0.0	-4.4	-930.1	0.0
	-234.3	1.6	-17.5	-61.4	-5481.4	-76.3		253.5	6.7	0.0	0.0	7.1	-771.4	0.0
	-317.9	-12.7	-23.4	-81.6	-7956.6	1575.6		-253.5	-6.7	0.0	0.0	-3.0	-964.2	0.0
ASTA	149	notH						245.6	8.1	0.0	0.0	3.5	-92.5	0.0
PROD.	NORM	TYV	TZZ	TORS	MY	MZ		-245.6	-8.1	0.0	0.0	-5.5	-116.6	0.0
	-21.4	13.4	-3.7	4.4	-885.7	-1576.0		253.5	6.7	0.0	0.0	3.0	964.2	0.0
	-2.6	1.0	-2.5	-9.8	-588.5	-74.8		-						
	-2.6	1.0	-2.5	-9.8	-588.4	-74.8		245.6	8.1	0.0	0.0	6.6	1395.1	0.0
42.	-21.4	13.4	-3.7	4.4	-885.7	-1576.0		-4.4	-245.6	-8.1	0.0	-6.6	-1395.1	0.0
	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		253.5	6.7	0.0	0.0	3.6	1157.0	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.4	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	7.7	1627.6	0.0
84.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
126.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
168.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
209.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
251.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
293.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
335.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
ASTA	150	notH						245.6	8.1	0.0	0.0	3.5	-92.5	0.0
PROD.	NORM	TYV	TZZ	TORS	MY	MZ		-245.6	-8.1	0.0	0.0	-5.5	-116.6	0.0
	-21.4	13.4	-3.7	4.4	-885.7	-1576.0		253.5	6.7	0.0	0.0	3.0	964.2	0.0
	-2.6	1.0	-2.5	-9.8	-588.5	-74.8		-						
	-2.6	1.0	-2.5	-9.8	-588.4	-74.8		245.6	8.1	0.0	0.0	6.6	1395.1	0.0
10.	-21.4	13.4	-3.7	4.4	-885.7	-1576.0		-4.4	-245.6	-8.1	0.0	-6.6	-1395.1	0.0
	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		253.5	6.7	0.0	0.0	3.6	1157.0	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.4	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	7.7	1627.6	0.0
34.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
67.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
101.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	-4.7	-1349.9	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		245.6	8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		-253.5	-6.7	0.0	0.0	4.7	1349.9	0.0
135.	-21.4	13.4	-3.7	4.4	-730.8	1013.0		-245.6	-8.1	0.0	0.0	-7.7	-1627.6	0.0
	-2.6	1.0	-2.5	9.8	-484.0	116.5		253.5	6.7	0.0	0.0	4.7	134	

[illegible]

[illegible]

131.	-8.6	-4.4	3.0	23.8	-302.3	176.2	38.	210.7	-0.9	0.2	20.6	-32.0	111.5	336.	-377.9	7.5	0.0	3.2	14.3	872.7	168.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	8.9	3.1	-3.1	-27.9	306.0	-127.2		-220.2	-0.1	-0.4	-24.8	43.1	5.4		377.9	-7.5	0.0	-3.2	-15.6	-1188.5		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-8.9	-3.1	-3.1	-27.9	306.0	-127.2		-220.2	0.1	0.4	-24.8	43.1	5.4		-377.9	7.5	0.0	-3.2	-15.6	-1188.5		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	8.6	4.4	-3.0	-23.8	-302.3	-176.2		-210.7	-0.9	0.2	-20.6	-32.0	111.5		274.4	-6.2	0.0	-1.3	-5.4	-938.7		-869.6	-2.9	0.0	3.8	-13.3	1143.6
150.	-8.6	-4.4	3.0	23.8	-357.9	193.7	56.	210.7	-0.9	0.2	-20.6	-36.5	94.7	Asta PROGR. 0.	377.9	-7.5	0.0	-3.2	15.6	1188.5	210.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	8.9	3.1	-3.1	-27.9	361.4	-109.7		-220.2	0.1	0.4	-24.8	-49.8	-2.7		377.9	-7.5	0.0	-3.2	15.6	1188.5		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-8.9	-3.1	-3.1	-27.9	361.4	-109.7		-220.2	0.1	0.4	-24.8	-49.8	-2.7		377.9	-7.5	0.0	-3.2	15.6	1188.5		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	8.6	4.4	-3.0	-23.8	-357.9	-193.7		-210.7	-0.9	0.2	-20.6	-36.5	94.7		377.9	-7.5	0.0	-3.2	15.6	1188.5		812.5	-4.0	0.0	1.4	-5.1	1125.7
Asta PROGR. 0.	-8.6	-4.4	3.0	23.8	-413.5	111.2	75.	210.7	-0.9	0.2	-20.6	-41.0	78.0	19.	304.2	8.0	-2.5	5.1	126.6	-727.8	252.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	8.9	3.1	-3.1	-27.9	420.7	-112.2		-220.2	0.1	0.4	-24.8	56.5	0.1		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-8.9	-3.1	-3.1	-27.9	420.7	-112.2		-220.2	0.1	0.4	-24.8	56.5	0.1		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	8.6	4.4	-3.0	-23.8	-413.5	-112.2		-210.7	-0.9	0.2	-20.6	-41.0	78.0		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
19.	-3.0	-1.8	-0.1	-7.6	928.9	-0.6	94.	210.7	-0.9	0.2	-20.6	-45.5	61.2	38.	304.2	8.0	-2.5	5.1	126.6	-727.8	336.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	63.3	-2.6		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	63.3	-2.6		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-45.5	61.2		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
38.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	113.	210.7	-0.9	0.2	-20.6	-50.0	-44.4	56.	304.2	8.0	-2.5	5.1	126.6	-727.8	75.	304.2	8.0	-2.5	5.1	126.6	-727.8
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	70.0	-5.2		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	70.0	-5.2		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-50.0	-44.4		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
75.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	131.	210.7	-0.9	0.2	-20.6	-54.5	27.7	94.	304.2	8.0	-2.5	5.1	126.6	-727.8	Asta PROGR. 0.	31	noft	342	727	727	
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	76.7	-7.9		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	76.7	-7.9		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-54.5	27.7		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
94.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	150.	210.7	-0.9	0.2	-20.6	-59.0	10.9	38.	304.2	8.0	-2.5	5.1	126.6	-727.8	56.	304.2	8.0	-2.5	5.1	126.6	-727.8
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	83.5	-10.5		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	83.5	-10.5		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-59.0	10.9		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
113.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	Asta PROGR. 0.	210.7	-0.9	0.2	-20.6	-63.0	-10.9	94.	304.2	8.0	-2.5	5.1	126.6	-727.8	113.	304.2	8.0	-2.5	5.1	126.6	-727.8
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	87.0	-13.0		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	87.0	-13.0		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-63.0	-10.9		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
131.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	56.	210.7	-0.9	0.2	-20.6	-67.5	27.7	75.	304.2	8.0	-2.5	5.1	126.6	-727.8	94.	304.2	8.0	-2.5	5.1	126.6	-727.8
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	91.0	-16.0		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	91.0	-16.0		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-67.5	27.7		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
150.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	Asta PROGR. 0.	210.7	-0.9	0.2	-20.6	-72.0	10.9	94.	304.2	8.0	-2.5	5.1	126.6	-727.8	113.	304.2	8.0	-2.5	5.1	126.6	-727.8
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	95.0	-19.0		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	95.0	-19.0		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-72.0	10.9		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
Asta PROGR. 0.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	38.	210.7	-0.9	0.2	-20.6	-76.5	27.7	75.	304.2	8.0	-2.5	5.1	126.6	-727.8	94.	304.2	8.0	-2.5	5.1	126.6	-727.8
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	100.0	-22.0		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	100.0	-22.0		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-76.5	27.7		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
94.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	113.	210.7	-0.9	0.2	-20.6	-81.0	10.9	131.	304.2	8.0	-2.5	5.1	126.6	-727.8	150.	304.2	8.0	-2.5	5.1	126.6	-727.8
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	105.0	-25.0		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	105.0	-25.0		304.2	8.0	-2.5	5.1	126.6	-727.8		-869.6	-2.9	0.0	3.8	-13.3	1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-210.7	-0.9	0.2	-20.6	-81.0	10.9		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.0	0.0	1.4	-5.1	1125.7
113.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	56.	210.7	-0.9	0.2	-20.6	-85.5	27.7	75.	304.2	8.0	-2.5	5.1	126.6	-727.8	94.	304.2	8.0	-2.5	5.1	126.6	-727.8
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	-24.8	110.0	-30.0		304.2	8.0	-2.5	5.1	126.6	-727.8		812.5	-4.				

43.	426.6	-205.3	-4.4	-15.8	728.0	20973.9	98.	53.2	-83.0	16.5	82.3	-1604.7	-6861.7	-7.1	-107.0	19.8	98.9	-643.0	-2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	20973.9	98.	53.2	-83.0	16.5	82.3	-1604.7	-6861.7	-7.1	-107.0	19.8	98.9	-643.0	-2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	20973.9	98.	53.2	-83.0	16.5	82.3	-1604.7	-6861.7	-7.1	-107.0	19.8	98.9	-643.0	-2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
85.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
128.	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
170.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
213.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
255.	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
298.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
340.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
382.	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
424.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
466.	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
508.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
550.	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
592.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
634.	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
676.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	7.1	107.0	-19.8	-98.9	643.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
718.	426.6	-205.3	-4.4	-15.																						

61.	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	177.2	-52.2	126.0	-1638.5	-10821.0	-30.5	-151.7	2.3	15.4	-35.7	-1943.0	-6.3	6.7	-9.1	-5.6	-142.4	-218.7	259.3	0.0	0.0	0.0	0.0	0.0	
	180.6	-208.4	-29.9	149.4	-1456.7	9367.7	-30.5	151.4	4.4	-29.0	101.3	-16775.9	-10.6	6.4	-11.4	-5.8	355.0	-101.8	-259.3	0.0	0.0	0.0	0.0	
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
98.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	127.5	14314.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
114.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
130.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
144.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
149.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
154.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
159.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
164.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
169.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
174.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
179.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
184.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
189.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2																					

[illegible]

2.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	41.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
3.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	83.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
4.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	124.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
5.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	165.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
6.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	206.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
7.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	248.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
8.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	289.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
9.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	330.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
10.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	371.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
11.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	412.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
12.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	453.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
13.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	494.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
14.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	535.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
15.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	576.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
16.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	617.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
17.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	658.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
18.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	699.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
19.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	740.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
20.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	781.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
21.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	822.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
22.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	863.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
23.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	904.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
24.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	945.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
25.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	986.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
26.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1027.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
27.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1068.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
28.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1109.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
29.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1150.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
30.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1191.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
31.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1232.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
32.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1273.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
33.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1314.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
34.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1355.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
35.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1396.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
36.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1437.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
37.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1478.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
38.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	1519.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
39.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-4																		

[illegible]

126.	-283.6	195.9	-6.7	-3.1	-1449.6	-1244.5
	-297.0	-203.6	7.2	-2.6	1353.3	1002.9
	-297.0	203.6	-7.2	2.6	1353.3	1002.9
	283.6	-195.9	6.7	3.1	1449.6	1244.5
168.	-283.6	195.9	-6.7	-3.1	-1449.6	-1244.5
	-297.0	-203.6	7.2	-2.6	1353.3	1002.9
	-297.0	203.6	-7.2	2.6	1353.3	1002.9
	283.6	-195.9	6.7	3.1	1449.6	1244.5
209.	-283.6	195.9	-6.7	-3.1	-884.6	-15163.9
	-297.0	-203.6	7.2	-2.6	884.6	15163.9
	-297.0	203.6	-7.2	2.6	884.6	15163.9
	283.6	-195.9	6.7	3.1	884.6	15163.9
251.	-283.6	195.9	-6.7	-3.1	-602.1	-23368.1
	-297.0	-203.6	7.2	-2.6	602.1	23368.1
	-297.0	203.6	-7.2	2.6	602.1	23368.1
	283.6	-195.9	6.7	3.1	602.1	23368.1
293.	-283.6	195.9	-6.7	-3.1	-315.3	-315.3
	-297.0	-203.6	7.2	-2.6	315.3	315.3
	-297.0	203.6	-7.2	2.6	315.3	315.3
	283.6	-195.9	6.7	3.1	315.3	315.3
335.	-283.6	195.9	-6.7	-3.1	-37.0	39776.6
	-297.0	-203.6	7.2	-2.6	37.0	-39776.6
	-297.0	203.6	-7.2	2.6	37.0	-39776.6
	283.6	-195.9	6.7	3.1	37.0	-39776.6
Asta	154	noth	760	963	37.0	
PROG.	NORM	TTY	TZZ	TORS	MYV	MZZ
0.	-40.8	0.0	0.0	0.0	0.7	0.0
	73.2	0.0	0.0	0.0	-1.0	0.0
	-73.2	0.0	0.0	0.0	1.0	0.0
	-40.8	0.0	0.0	0.0	-0.7	0.0
34.	-40.8	0.0	0.0	0.0	0.5	0.0
	73.2	0.0	0.0	0.0	-0.7	0.0
	-73.2	0.0	0.0	0.0	0.7	0.0
	-40.8	0.0	0.0	0.0	-0.5	0.0
67.	-40.8	0.0	0.0	0.0	0.2	0.0
	73.2	0.0	0.0	0.0	-0.4	0.0
	-73.2	0.0	0.0	0.0	0.4	0.0
	-40.8	0.0	0.0	0.0	-0.2	0.0
101.	-40.8	0.0	0.0	0.0	-0.1	0.0
	73.2	0.0	0.0	0.0	0.1	0.0
	-73.2	0.0	0.0	0.0	0.1	0.0
	-40.8	0.0	0.0	0.0	0.0	0.0
135.	-40.8	0.0	0.0	0.0	-0.2	0.0
	73.2	0.0	0.0	0.0	0.2	0.0
	-73.2	0.0	0.0	0.0	-0.2	0.0
	-40.8	0.0	0.0	0.0	0.2	0.0
168.	-40.8	0.0	0.0	0.0	-0.4	0.0
	73.2	0.0	0.0	0.0	0.5	0.0
	-73.2	0.0	0.0	0.0	-0.5	0.0
	-40.8	0.0	0.0	0.0	0.4	0.0
202.	-40.8	0.0	0.0	0.0	-0.6	0.0
	73.2	0.0	0.0	0.0	0.8	0.0
	-73.2	0.0	0.0	0.0	-0.8	0.0
	-40.8	0.0	0.0	0.0	0.6	0.0
236.	-40.8	0.0	0.0	0.0	-0.8	0.0
	73.2	0.0	0.0	0.0	1.0	0.0
	-73.2	0.0	0.0	0.0	-1.1	0.0
	-40.8	0.0	0.0	0.0	0.8	0.0
269.	-40.8	0.0	0.0	0.0	-1.0	0.0
	73.2	0.0	0.0	0.0	1.4	0.0
	-73.2	0.0	0.0	0.0	-1.4	0.0
	-40.8	0.0	0.0	0.0	1.0	0.0
Asta	154	noth	973	1013	37.0	
PROG.	NORM	TTY	TZZ	TORS	MYV	MZZ
0.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
29.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
58.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
86.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
115.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
144.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
173.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
201.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
230.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
Asta	156	noth	972	1011	37.0	
PROG.	NORM	TTY	TZZ	TORS	MYV	MZZ
0.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
29.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
58.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
86.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
115.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
144.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
173.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
201.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
280.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	-101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0

0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2	359	46.7	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
4.0	4.0	51.9	0.0	100.0	-7.4		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-13.9	-21.9	0.0	0.0	-1.2	-630.2	410.	-46.7	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9																	

Asta	PROGR.	176	NORM	TYV	959	742	TORS	MYV	MZZ	-133.7	-462.6	-0.1	-8.9	15.6	23240.1	-56.4	-43.8	9.2	59.8	-874.2	-592.0	-535.1	444.6	-24.3	71.7	735.5	-29279.9
15.	0.	-1089.3	129.6	247.5	0.0	-66396.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
30.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
45.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
60.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
75.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
90.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
105.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
120.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
135.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
150.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
165.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
180.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
195.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
210.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
225.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
240.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
255.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
270.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
285.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
300.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
315.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
330.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
345.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
360.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
375.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
390.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
405.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
420.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
435.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
450.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
465.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
480.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
495.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3</															

[illegible]

58/136

0.7	9.4	1.5	-70.4	137.6	2214.3
-13.2	28.2	-0.1	115.2	-13.5	2033.2
-13.2	-27.5	-1.1	-93.2	137.5	2033.2
-1.3	-56.7	-0.5	92.2	-45.1	2148.7
-1.3	-51.4	-1.5	-94.4	151.2	2174.9
-13.2	-27.7	-0.1	115.2	-13.5	2033.2
-1.3	-116.3	1.1	-93.3	99.5	1908.3
-13.2	-91.5	-0.5	92.2	-45.1	2148.7
-13.2	-132.2	-1.1	-94.4	151.2	2174.9
-13.7	-49.1	-0.1	118.3	33.0	2119.4
-13.7	-49.1	-0.1	118.3	33.0	2119.4
-1.3	-178.4	-0.5	92.2	-45.0	2173.2
-1.3	-177.1	-1.5	-94.4	151.2	2174.9
-13.2	-154.0	-0.1	115.2	-8.6	1902.7
-13.2	-154.0	-0.1	115.2	-8.6	1902.7
-1.3	-239.2	-0.5	92.2	-46.4	13719.2
-1.3	-238.9	-1.5	-70.4	137.6	14257.8
-13.7	-310.2	-0.1	118.3	-6.9	913.9
-13.7	-310.2	-0.1	118.3	-6.9	913.9
-1.3	-379.6	-0.1	118.3	25.4	1025.6
-1.3	-360.9	-0.5	92.2	-45.7	2117.5
-13.2	-379.6	-0.1	118.3	25.4	1025.6
-13.2	-360.9	-0.5	92.2	-45.7	2117.5
-13.2	-440.5	-0.1	115.2	-3.6	612.8
-13.2	-440.5	-0.1	115.2	-3.6	612.8
-1.3	-421.7	-0.5	92.2	12.2	-363.2
-13.2	-440.5	-0.1	115.2	-3.6	612.8
-13.2	-397.7	-0.1	115.2	-1.9	-294.0
145	nodt	760	760	MY	MZZ
-377.1	-40.0	19.2	0.0	96.2	199.9
-377.1	-40.0	19.2	0.0	96.2	199.9
-377.1	-33.9	6.3	0.0	31.5	169.7
-377.1	-42.9	-18.7	0.0	-93.7	-74.4
-377.1	-40.0	19.2	0.0	96.2	199.9
-377.0	36.9	-5.8	0.0	-25.4	-161.5
-377.0	36.9	-5.8	0.0	27.2	148.3
-377.0	-42.9	-18.7	0.0	-82.0	-187.9
-376.9	36.9	19.2	0.0	96.2	199.9
-376.9	36.9	5.8	0.0	21.8	118.1
-376.9	-33.9	6.3	0.0	23.6	127.3
-376.9	-42.9	-18.7	0.0	-93.7	-74.4
-376.7	-40.0	19.2	0.0	60.1	124.9
-376.7	-40.0	19.2	0.0	60.1	124.9
-376.7	-33.9	6.3	0.0	19.8	114.5
-376.7	-33.9	6.3	0.0	19.8	114.5
-376.7	42.9	-18.7	0.0	-58.6	-146.2
-376.7	42.9	-18.7	0.0	-58.6	-146.2
-376.6	36.9	-5.8	0.0	-45.5	-92.3
-376.6	36.9	-5.8	0.0	45.5	92.3
-376.6	-42.9	-18.7	0.0	-46.9	-107.4
-376.6	-42.9	-18.7	0.0	46.9	107.4
-376.4	36.9	5.8	0.0	-10.9	-69.2
-376.4	36.9	5.8	0.0	11.0	69.6
-376.4	-33.9	6.3	0.0	-33.5	-144.0
-376.3	-40.0	19.2	0.0	24.0	50.0
-376.3	-40.0	19.2	0.0	24.0	50.0
-376.3	-33.9	6.3	0.0	7.9	42.4
-376.3	-33.9	6.3	0.0	7.9	42.4
-376.2	-40.0	19.2	0.0	12.0	-53.7
-376.2	36.9	-5.8	0.0	-3.6	-23.1
-376.2	36.9	-5.8	0.0	-3.6	-23.1
-376.2	-33.9	-18.7	0.0	-11.7	-26.8
-376.2	-33.9	-18.7	0.0	11.7	26.8
-376.0	36.9	5.8	0.0	0.0	0.0
-376.0	36.9	5.8	0.0	0.0	0.0
-376.0	-33.9	-18.7	0.0	0.0	0.0
-376.0	-33.9	-18.7	0.0	0.0	0.0
145	nodt	760	213	MY	MZZ
125.2	-376.0	0.0	0.0	-0.4	0.8
125.2	-376.0	0.0	0.0	-0.4	0.8
-99.1	-376.0	0.0	0.0	-0.2	0.8
-146.1	-376.0	0.0	0.0	0.5	0.8
-146.1	-376.0	0.0	0.0	-0.5	-0.8
-119.9	-282.0	0.0	0.0	0.2	-948.7
-119.9	-282.0	0.0	0.0	-0.2	-948.7
-146.1	-282.0	0.0	0.0	0.4	-948.7
-146.1	-282.0	0.0	0.0	-0.4	-948.7
125.2	-188.0	0.0	0.0	-0.3	-1621.6
125.2	-188.0	0.0	0.0	-0.3	-1621.6
-99.1	-188.0	0.0	0.0	-0.1	-1621.6
-99.1	-188.0	0.0	0.0	0.1	-1621.6
125.2	-94.0	0.0	0.0	-0.2	-2069.7
125.2	-94.0	0.0	0.0	-0.2	-2069.7
-99.1	-94.0	0.0	0.0	-0.1	-2069.7
-99.1	-94.0	0.0	0.0	0.1	-2069.7
146.1	-94.0	0.0	0.0	0.3	-2162.1
146.1	-94.0	0.0	0.0	-0.3	-2162.1
-119.9	-282.0	0.0	0.0	0.2	-948.7
-119.9	-282.0	0.0	0.0	-0.2	-948.7
-146.1	-282.0	0.0	0.0	0.2	-2162.1
-146.1	-282.0	0.0	0.0	-0.2	-2162.1
125.2	94.0	0.0	0.0	-0.1	-2069.9
125.2	94.0	0.0	0.0	-0.1	-2069.9
-99.1	94.0	0.0	0.0	-0.1	-2069.9
-99.1	94.0	0.0	0.0	0.1	-2069.9
125.2	-188.0	0.0	0.0	-0.1	-1621.6
125.2	-188.0	0.0	0.0	-0.1	-1621.6
-99.1	-188.0	0.0	0.0	-0.0	-1621.6
-99.1	-188.0	0.0	0.0	0.0	-1621.6
-146.1	-188.0	0.0	0.0	0.1	-1621.6
-146.1	-188.0	0.0	0.0	-0.1	-1621.6
119.9	-282.0	0.0	0.0	0.0	-949.3
119.9	-282.0	0.0	0.0	0.0	-949.3
-146.1	-282.0	0.0	0.0	0.1	-949.3
-146.1	-282.0	0.0	0.0	-0.1	-949.3
125.2	376.0	0.0	0.0	0.0	0.0
125.2	376.0	0.0	0.0	0.0	0.0
-99.1	376.0	0.0	0.0	0.0	0.0
-99.1	376.0	0.0	0.0	0.0	0.0
146	nodt	773	754	MY	MZZ
-1768.5	88.6	-66.9	317.6	17700.4	-8530.4
-613.3	56.4	-27.2	155.2	4670.6	-8767.5
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-413.5	62.1	-22.6	131.5	12578.3	-8762.2
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-612.9	56.4	-27.2	155.2	4687.6	-8767.5
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-413.1	62.1	-22.6	131.5	12772.4	-8728.4
-1767.7	88.6	-66.9	317.6	17784.1	-8416.6
-612.5	56.4	-27.2	155.2	4683.3	-8762.2
-1587.9	88.6	-66.9	317.6	17784.1	-8416.6
-1767.3	88.6	-66.9	317.6	17825.9	-8364.7
-612.5	56.4	-27.2	155.2	4721.1	-8767.5
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-412.4	62.1	-22.6	131.5	12800.7	-8650.7
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-611.8	56.4	-27.2	155.2	4738.5	-8722.4
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-412.0	62.1	-22.6	131.5	12914.8	-8611.9
-1766.5	88.6	-66.9	317.6	17909.5	-8253.5
-611.4	56.4	-27.2	155.2	4738.5	-8722.4
-1586.8	88.6	-66.9	317.6	17948.0	-8039.5
-1766.5	88.6	-66.9	317.6	17948.0	-8039.5
-1766.2	88.6	-66.9	317.6	17961.3	-8128.1
-1586.2	88.6	-66.9	317.6	17961.3	-8128.1
-1586.4	94.3	-62.2	293.9	15522.0	-8795.2
-411.2	62.1	-22.6	131.5	12943.1	-8534.3
-1586.2	88.6	-66.9	317.6	17961.3	-8128.1

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18.2	0.0	0.0	0.4	0.1	0.7																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																														
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[illegible]

292.	97.9	-331.4	0.3	-1.9	-89.5	-10765.4	1.	486.1	38.7	-2.3	45.0	-262.7	-16055.1	0.	-284.9	-108.4	-3.2	-37.5	554.6	-79.2	94.	-13.9	103.6	4.0	-43.8	-453.9	-709.3
	16.9	-437.3	0.4	-1.8	-161.8	-23945.6	1.	411.7	34.7	1.1	6.0	315.5	-16658.0	0.	25	75	-3.8	473			94.	6.7	103.6	-2.5	-46.4	156.2	-1460.3
	29.4	-409.4	0.4	-1.7	-160.4	-23945.6	1.	411.7	34.7	1.1	6.0	315.5	-16658.0	0.	25	75	-3.8	473			94.	6.7	103.6	-2.5	-46.4	156.2	-1460.3
	64.1	-457.9	0.4	-1.7	-161.3	-23941.7	1.	411.7	34.7	1.1	6.0	315.5	-16658.0	0.	25	75	-3.8	473			94.	6.7	103.6	-2.5	-46.4	156.2	-1460.3
	30.5	-449.9	0.3	-1.9	-103.9	-27059.0	1.	535.6	157.2	-2.3	45.0	-367.8	-12936.6	0.	-1087.5	400.4	0.3	0.0	0.0	0.0	113.	-13.9	42.0	-3.2	-48.8	-529.7	658.8
334.	-50.6	-570.6	0.4	-1.8	-140.2	-3082.5	1.	342.2	289.3	-2.3	45.0	-1017.3	-5082.5	0.	0.	0.0	0.0	0.0	0.0	0.0	113.	6.7	103.6	-2.5	-46.4	156.2	-1460.3
	-84.2	-568.0	0.3	-1.7	-118.8	-48279.2	1.	443.5	157.5	-2.2	45.4	-132.1	-11305.4	0.	0.	0.0	0.0	0.0	0.0	0.0	113.	-11.5	42.0	3.3	-46.1	-453.2	670.6
	-1.3	-3.3	0.4	-1.0	-45.4	-1053.5	1.	41.0	45.4	-1.3	45.0	-1018.0	-453.5	0.	0.	0.0	0.0	0.0	0.0	0.0	131.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	-37.0	-568.0	0.3	-1.9	-118.8	-48294.2	1.	41.0	45.4	-1.3	45.0	-1018.0	-453.5	0.	0.	0.0	0.0	0.0	0.0	0.0	131.	-13.9	42.0	3.3	-46.1	-453.2	670.6
ASTA																											
PROGR.																											
	475.3	364.8	0.5	-15.8	-23.6	-16262.4	1.	515.0	272.1	-2.2	45.4	-60.4	-7299.7	0.	375.4	276.1	0.3	0.0	-11.5	1438.9	0.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	136.5	364.4	0.5	-15.8	-23.6	-16262.4	1.	515.0	272.1	-2.2	45.4	-60.4	-7299.7	0.	375.4	276.1	0.3	0.0	-11.5	1438.9	0.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	508.6	363.8	0.5	-13.6	-23.2	-16096.7	1.	209.3	390.3	1.1	6.0	176.8	10127.2	0.	-878.3	163.4	0.3	0.0	-22.8	2867.2	0.	6.7	-67.2	-2.5	-46.4	297.4	-65.2
	101.2	363.4	0.5	-13.6	-23.2	-16096.7	1.	209.3	390.3	1.1	6.0	176.8	10127.2	0.	-878.3	163.4	0.3	0.0	-22.8	2867.2	0.	6.7	-67.2	-2.5	-46.4	297.4	-65.2
42.	405.9	246.2	0.5	-13.8	-44.8	-3406.1	1.	21.2	390.5	1.2	6.3	-315.4	-10379.8	0.	-879.1	44.8	0.3	0.0	-45.8	6456.3	0.	9.0	-67.2	-2.5	-46.4	297.4	-65.2
	-206.0	245.9	0.2	-26.1	-55.6	-3462.0	1.	764.1	512.2	-2.3	45.4	-116.3	-3002.8	0.	-879.1	44.8	0.3	0.0	-45.8	6456.3	0.	9.0	-67.2	-2.5	-46.4	297.4	-65.2
	172.7	244.9	0.3	-26.1	-55.6	-3462.0	1.	764.1	512.2	-2.3	45.4	-116.3	-3002.8	0.	-879.1	44.8	0.3	0.0	-45.8	6456.3	0.	9.0	-67.2	-2.5	-46.4	297.4	-65.2
	336.4	217.7	0.5	-13.8	-44.8	-3406.1	1.	21.2	390.5	1.2	6.3	-315.4	-10379.8	0.	-879.1	44.8	0.3	0.0	-45.8	6456.3	0.	9.0	-67.2	-2.5	-46.4	297.4	-65.2
	-245.5	127.3	0.2	-26.1	-55.6	-3462.0	1.	764.1	512.2	-2.3	45.4	-116.3	-3002.8	0.	-879.1	44.8	0.3	0.0	-45.8	6456.3	0.	9.0	-67.2	-2.5	-46.4	297.4	-65.2
	275.2	125.7	0.2	-26.1	-55.6	-3462.0	1.	764.1	512.2	-2.3	45.4	-116.3	-3002.8	0.	-879.1	44.8	0.3	0.0	-45.8	6456.3	0.	9.0	-67.2	-2.5	-46.4	297.4	-65.2
126.	266.9	9.2	0.5	-13.8	-44.8	-3406.1	1.	21.2	390.5	1.2	6.3	-315.4	-10379.8	0.	-879.1	44.8	0.3	0.0	-45.8	6456.3	0.	9.0	-67.2	-2.5	-46.4	297.4	-65.2
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25.	122.8	0.0	0.0	0.0	0.0	4.	-869.9	3.5	-4148.2	0.0	-5185.2	-4.4	0.	-6083.5	20.1	14.9	0.0	3316.4	13564.5	3.	-595.5	-272.0	290.5	0.0	469.6	510.0
50.	122.8	0.0	0.0	0.0	0.0	4.	-869.7	3.5	-4148.2	0.0	-2592.6	-2.2	41.	-6082.2	20.1	14.9	0.0	2700.3	14391.8	4.	-595.3	-272.0	290.5	0.0	313.1	340.0
74.	122.8	0.0	0.0	0.0	0.0	5.	-869.6	3.5	-4148.2	0.0	-6032.9	0.0	85.	-6032.9	20.1	14.9	0.0	2064.2	15202.0	5.	-595.2	-272.0	290.5	0.0	156.5	170.0
99.	122.8	0.0	0.0	0.0	0.0	Asta	99	ndi	964	339	MY	MZZ	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	5.	-595.1	-272.0	290.5	0.0	0.0	0.0
124.	122.8	0.0	0.0	0.0	0.0	PROGR.	124	ndi	964	339	MY	MZZ	165.	-5982.3	20.1	14.9	0.0	852.1	16871.8	Asta	130	ndi	752	468	MY	MZZ
149.	122.8	0.0	0.0	0.0	0.0	0.	-1923.2	16.2	45.7	0.0	-1923.2	-81.0	206.	-5957.0	20.1	14.9	0.0	2700.1	15202.0	PROGR.	130	ndi	752	468	MY	MZZ
174.	122.8	0.0	0.0	0.0	0.0	1.	-1923.1	16.2	45.7	0.0	200.1	-70.9	248.	-5931.7	20.1	14.9	0.0	-380.1	18528.4	0.	-714.5	-595.1	-0.3	0.0	0.0	
198.	122.8	0.0	0.0	0.0	0.0	2.	-1923.0	16.2	45.7	0.0	171.5	-60.7	289.	-5906.4	20.1	14.9	0.0	-586.0	19131.3	0.	-714.5	-595.1	-0.3	0.0	0.0	
Asta	75	ndi	760	212	MY	2.	-1922.8	16.2	45.7	0.0	140.9	-50.6	330.	-5881.2	20.1	14.9	0.0	-1612.2	20183.1	0.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	75	ndi	760	212	MY	3.	-1922.7	16.2	45.7	0.0	118.4	-40.5	Asta	116	ndi	741	737	86.	-714.5	1.8	-0.3	0.0	28.5	-25586.4		
33.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.6	16.2	45.7	0.0	85.7	-30.4	PROGR.	116	ndi	741	737	116.	-714.5	1.8	-0.3	0.0	28.5	-25586.4		
66.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.4	16.2	45.7	0.0	57.2	-20.2	0.	-3793.3	-15.6	11.9	0.0	-2215.2	17264.7	0.	-714.5	-595.1	-0.3	0.0	0.0	
99.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.3	16.2	45.7	0.0	27.6	-10.1	4.	-3793.3	-15.6	11.9	0.0	-2215.2	17264.7	0.	-714.5	-595.1	-0.3	0.0	0.0	
133.	-13.8	0.0	0.0	0.0	0.0	5.	-1922.1	16.2	45.7	0.0	0.0	0.0	83.	-3242.7	-15.6	11.9	0.0	-3193.0	19889.8	0.	-714.5	-595.1	-0.3	0.0	0.0	
165.	-13.8	0.0	0.0	0.0	0.0	Asta	100	ndi	760	212	MY	MZZ	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	0.	-714.5	-595.1	-0.3	0.0	0.0	
198.	-13.8	0.0	0.0	0.0	0.0	PROGR.	100	ndi	760	212	MY	MZZ	165.	-5982.3	20.1	14.9	0.0	852.1	16871.8	0.	-714.5	-595.1	-0.3	0.0	0.0	
264.	-13.8	0.0	0.0	0.0	0.0	0.	-2707.3	-29.4	-3.3	0.0	-16.4	146.8	206.	-3166.8	-15.6	11.9	0.0	-4659.7	14055.1	0.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	78	ndi	976	211	MY	1.	-2707.2	-29.4	-3.3	0.0	134.4	128.5	289.	-3166.8	-15.6	11.9	0.0	-4659.7	14055.1	0.	-714.5	-595.1	-0.3	0.0	0.0	
0.	28.3	0.0	0.0	0.0	0.0	2.	-2706.9	-29.4	-3.3	0.0	-12.3	110.1	289.	-3166.8	-15.6	11.9	0.0	-4659.7	14055.1	0.	-714.5	-595.1	-0.3	0.0	0.0	
33.	28.3	0.0	0.0	0.0	0.0	3.	-2706.7	-29.4	-3.3	0.0	-8.0	31.0	330.	-3091.6	-15.6	11.9	0.0	-5637.5	12771.2	0.	-714.5	-595.1	-0.3	0.0	0.0	
66.	28.3	0.0	0.0	0.0	0.0	4.	-2706.7	-29.4	-3.3	0.0	-8.2	73.4	Asta	117	ndi	742	739	86.	-714.5	1.8	-0.3	0.0	28.5	-25586.4		
99.	28.3	0.0	0.0	0.0	0.0	4.	-2706.6	-29.4	-3.3	0.0	-6.2	55.1	PROGR.	117	ndi	742	739	117.	-714.5	1.8	-0.3	0.0	28.5	-25586.4		
132.	28.3	0.0	0.0	0.0	0.0	4.	-2706.5	-29.4	-3.3	0.0	-4.1	38.7	0.	-3516.2	-45.9	11.4	0.0	-1613.7	21067.7	0.	-714.5	-595.1	-0.3	0.0	0.0	
165.	28.3	0.0	0.0	0.0	0.0	4.	-2706.3	-29.4	-3.3	0.0	-2.1	18.4	41.	-3491.0	-45.9	11.4	0.0	-11547.2	34344.7	0.	-714.5	-595.1	-0.3	0.0	0.0	
198.	28.3	0.0	0.0	0.0	0.0	5.	-2706.2	-29.4	-3.3	0.0	0.0	0.0	83.	-3465.7	-45.9	11.4	0.0	-6945.3	31628.8	0.	-714.5	-595.1	-0.3	0.0	0.0	
231.	28.3	0.0	0.0	0.0	0.0	Asta	101	ndi	962	341	MY	MZZ	124.	-3440.4	-45.9	-111.4	0.0	-2353.9	28988.8	0.	-714.5	-595.1	-0.3	0.0	0.0	
264.	28.3	0.0	0.0	0.0	0.0	PROGR.	101	ndi	962	341	MY	MZZ	165.	-3415.1	-45.9	-111.4	0.0	-2353.9	28988.8	0.	-714.5	-595.1	-0.3	0.0	0.0	
Asta	79	ndi	749	468	MY	0.	-2617.0	-12.4	-3.2	0.0	-15.9	61.9	206.	-3389.8	-45.9	-111.4	0.0	-6834.9	29472.9	0.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	79	ndi	749	468	MY	1.	-2616.8	-12.4	-3.2	0.0	-13.9	54.2	248.	-3364.5	-45.9	-111.4	0.0	-11429.3	20755.0	0.	-714.5	-595.1	-0.3	0.0	0.0	
33.	-50.7	0.0	0.0	0.0	0.0	2.	-2616.6	-12.4	-3.2	0.0	-9.9	38.7	289.	-3339.2	-45.9	-111.4	0.0	-16023.7	18377.1	0.	-714.5	-595.1	-0.3	0.0	0.0	
66.	-50.7	0.0	0.0	0.0	0.0	3.	-2616.3	-12.4	-3.2	0.0	-6.0	23.2	330.	-3314.5	-45.9	-111.4	0.0	-20618.1	15131.9	0.	-714.5	-595.1	-0.3	0.0	0.0	
99.	-50.7	0.0	0.0	0.0	0.0	4.	-2616.1	-12.4	-3.2	0.0	-4.0	15.5	PROGR.	102	ndi	962	341	165.	-5982.3	20.1	14.9	0.0	852.1	16871.8		
133.	-50.7	0.0	0.0	0.0	0.0	4.	-2616.1	-12.4	-3.2	0.0	-4.0	15.5	0.	-221.3	-790.0	18.9	56.0	2181.5	76931.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
165.	-50.7	0.0	0.0	0.0	0.0	5.	-2615.9	-12.4	-3.2	0.0	-2.0	7.7	16.	-221.3	-790.0	18.9	56.0	2181.5	76931.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
198.	-50.7	0.0	0.0	0.0	0.0	PROGR.	102	ndi	962	341	MY	MZZ	35.	-221.3	-790.0	18.9	56.0	2181.5	76931.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
264.	-50.7	0.0	0.0	0.0	0.0	0.	-2008.2	15.0	-125.1	0.0	-425.4	-75.2	70.	-221.3	-790.0	18.9	56.0	2181.5	76931.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	79	ndi	749	468	MY	1.	-2008.0	15.0	-125.1	0.0	-347.3	-65.8	88.	-221.3	-790.0	18.9	56.0	2181.5	76931.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
33.	508.4	0.0	0.0	0.0	0.0	1.	-2007.9	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-790.0	18.9	56.0	2181.5	76931.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
66.	508.4	0.0	0.0	0.0	0.0	2.	-2007.7	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-790.0	18.9	56.0	2181.5	76931.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
99.	508.4	0.0	0.0	0.0	0.0	3.	-2007.6	15.0	-125.1	0.0	-312.7	-37.6	130.	-221.3	-790.0	18.9	56.0	2181.5	76931.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
132.	508.4	0.0	0.0	0.0	0.0	4.	-2007.3	15.0	-125.1	0.0	-156.3	-18.8	Asta	120	ndi	745	746	165.	-5982.3	20.1	14.9	0.0	852.1	16871.8		
165.	508.4	0.0	0.0	0.0	0.0	5.	-2007.1	15.0	-125.1	0.0	-78.2	-9.4	16.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
198.	508.4	0.0	0.0	0.0	0.0	Asta	104	ndi	962	341	MY	MZZ	49.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
231.	508.4	0.0	0.0	0.0	0.0	0.	-1683.4	-61.8	3997.8	0.0	17988.8	319.1	16.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
264.	508.4	0.0	0.0	0.0	0.0	1.	-1683.2	-61.8	3997.8	0.0	15740.2	279.2	81.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
Asta	83	ndi	467	470	MY	2.	-1683.1	-61.8	3997.8	0.0	13401.6	239.3	98.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
PROGR.	83	ndi	467	470	MY	3.	-1682.9	-61.8	3997.8	0.0	11243.0	199.4	130.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
0.	632.7	0.0	0.0	0.0	0.0	4.	-1682.7	-61.8	3997.8	0.0	6745.8	119.7	Asta	130	ndi	745	746	165.	-5982.3	20.1	14.9	0.0	852.1	16871.8		
45.	632.7	0.0	0.0	0.0	0.0	5.	-1682.5	-61.8	3997.8	0.0	4497.2	79.8	0.	-113.6	767.7	-15.9	-159.2	-187.6	-68801.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
134.	632.7	0.0	0.0	0.0	0.0	PROGR.	105	ndi	962	341	MY	MZZ	16.	-113.6	767.7	-15.9	-159.2	-187.6	-68801.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
179.	632.7	0.0	0.0	0.0	0.0	0.	-6531.1	-455.0	6202.0	0.0	31009.8	2275.0	16.	-113.6	767.7	-15.9	-159.2	-187.6	-68801.6	0.	-714.5	-595.1	-0.3	0.0	0.0	
224.	632.7	0.0	0.0	0.0	0.0	1.	-6530.9	-455.0	6202.0	0.0	27133.6	1990.6	49.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
269.	632.7	0.0	0.0	0.0	0.0	2.	-6530.7	-455.0	6202.0	0.0	24246.2	179.8	81.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
313.	632.7	0.0	0.0	0.0	0.0	3.	-6530.5	-455.0	6202.0	0.0	21361.4	142.9	130.	-475.2	-590.2	1.7	-1359.9	-0.0	125.2	4.4	0.0	-36.1	18384.2			
358.	632.7	0.0	0.0	0.0	0.0	4.	-6530.3	-455.0	6202.0																	

PROGR.	ASTA	181	modi	957	28
1	NORM	tyz	tyz	TZZ	TORS
15	-1140.8	66.1	52.0	0.0	0.0
30	-1140.8	66.1	52.0	0.0	0.0
45	-1140.8	66.1	52.0	0.0	0.0
60	-1140.8	66.1	52.0	0.0	0.0
75	-1140.8	66.1	52.0	0.0	0.0
90	-1140.8	66.1	52.0	0.0	0.0
105	-1140.8	66.1	52.0	0.0	0.0
120	-1140.8	66.1	52.0	0.0	0.0

4 COLEZIONI ASTE		9 Rara Vertotti			
PROGR.	NORM	tyz	tyz	TZZ	TORS
1	Peso_proprio_____	+1.00			
2	Permanente_____	+1.00			
3	Permanente_____	+1.00			
4	Neve,<3000m,1_m_____	+1.00			

1	+1.00+001	+1.00+002	+1.00+003	+1.00+004
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collezioni di misura: pro e freeze [cm]:NORM,tyz,TZZ				
PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52.0	0.0
90	-114.0	66.1	52.0	0.0
105	-114.0	66.1	52.0	0.0
120	-114.0	66.1	52.0	0.0

PROGR.	NORM	tyz	TZZ	TORS
1	-118.4	66.1	52.0	0.0
15	-114.0	66.1	52.0	0.0
30	-114.0	66.1	52.0	0.0
45	-114.0	66.1	52.0	0.0
60	-114.0	66.1	52.0	0.0
75	-114.0	66.1	52	

-118.0	MMY	MZZ
-118.0	286.1	10806.0
-118.0	239.5	8652.8
-118.0	192.8	6683.0
-118.0	146.2	4993.1
-118.0	99.5	34796.8
-118.0	52.2	24413.6
-118.0	6.2	12472.6
-118.0	-40.4	4964.6
-118.0	-67.1	-131.7
731		
-109.7	MMY	MZZ
-109.7	292.5	110748.9
-109.7	333.3	88572.9
-109.7	374.8	67017.9
-109.7	414.8	50919.1
-109.7	455.6	35841.3
-109.7	496.4	23136.3
-109.7	537.1	12383.9
-109.7	577.2	6094.1
-109.7	618.7	-142.5
473		
TORS	MMY	MZZ
0.0	0.0	0.0
0.0	-23.5	30264.5
0.0	-46.9	49988.8
0.0	-70.4	59172.9
0.0	-93.8	57816.7
0.0	-117.3	45503.2
0.0	-140.7	23483.5
0.0	-164.2	-9893.4
0.0	-187.7	-53010.6
342		
TORS	MMY	MZZ
48.7	-83.0	45568.3
48.7	-105.6	28631.5
48.7	-128.2	15638.1
48.7	-150.8	19271.4
48.7	-173.4	29211.9
48.7	-196.0	22913.3
48.7	-218.6	8948.9
48.7	-241.2	-15555.8
48.7	-263.8	-50060.7
727		
TORS	MMY	MZZ
-91.4	-252.2	-50067.7
-91.4	-205.7	-33774.6
-91.4	-159.3	-23142.4
-91.4	-112.8	-13420.8
-91.4	-66.4	-5802.9
-91.4	-19.9	-97.0
-91.4	26.5	1864.5
-91.4	73.0	2094.1
-91.4	119.4	-109.0
730		
TORS	MMY	MZZ
-94.9	-161.9	-53010.6
-94.9	-128.7	-37087.1
-94.9	-195.5	-25192.4
-94.9	-112.4	-14692.4
-94.9	-229.2	-7305.1
-94.9	-246.0	-1710.6
-94.9	-262.8	-178.5
-94.9	-279.7	1780.2
-94.9	-296.5	1381.5
38		
TORS	MMY	MZZ
43.6	2464.8	38665.6
43.6	2029.6	35132.8
43.6	1594.1	31584.0
43.6	1159.1	28607.3
43.6	723.8	2354.5
43.6	288.5	2190.8
43.6	-146.5	18549.0
43.6	-582.0	15196.2
43.6	-1017.3	11843.5
39		
TORS	MMY	MZZ
-2.4	-1016.9	-25583.2
-2.4	-842.6	-21070.7
-2.4	-668.3	-16558.2
-2.4	-494.1	-12045.8
-2.4	-319.8	-7533.3
-2.4	-145.6	-3020.9
-2.4	28.7	1491.6
-2.4	202.9	604.1
-2.4	377.4	10016.5
41		
TORS	MMY	MZZ
0.0	-5064.5	19900.6
0.0	-4822.6	13297.9
0.0	-2960.6	5050.8
0.0	-1958.7	17607.9
0.0	-896.8	2047.1
0.0	145.2	22686.2
0.0	167.1	2523.3
0.0	2229.1	27764.4
0.0	-1324.2	48596.9
0.0	303.3	50303.5
42		
TORS	MMY	MZZ
6.3	3576.2	55582.8
6.3	3135.7	14594.2
6.3	2695.3	11001.3
6.3	2254.8	7408.4
6.3	1814.4	3815.5
6.3	1373.9	222.6
6.3	93.5	-3370.3
6.3	693.0	-6963.2
6.3	52.6	-10556.1
314.5		
TORS	MMY	MZZ
314.5	0.0	314.7
314.5	-102.2	35627.8
314.5	-204.4	71882.8
314.5	-306.6	107050.4
314.5	-408.8	144130.6
314.5	-510.4	189257.3
314.5	-613.2	217038.8
314.5	-715.6	253646.4
314.5	-817.6	290508.8
29		
TORS	MMY	MZZ
-203.7	-5296.2	-274910.1
-203.7	-4634.6	-240343.2
-203.7	-3972.2	-206017.7
-203.7	-3310.4	-171247.0

73/136

67.	-4.7	0.0	0.0	0.9	0.1	1.5	
68.	-4.7	0.0	0.0	0.9	0.2	1.5	
101.	-4.7	0.0	0.0	0.9	0.3	1.5	
125.	-4.7	0.0	0.0	0.9	0.4	1.5	
168.	-4.7	0.0	0.0	0.9	0.5	1.5	
202.	-4.7	0.0	0.0	0.9	0.5	1.5	
236.	-4.7	0.0	0.0	0.9	0.6	1.5	
269.	-4.7	0.0	0.0	0.9	0.6	1.5	
Asta	154	nodi	973	712			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	6.2	-795.8	0.0	0.0	0.0	0.0	
29.	6.2	-596.8	0.0	0.0	0.0	-2010.8	
38.	6.2	-397.9	0.0	0.0	0.0	-3437.9	
62.	6.2	-198.9	0.0	0.0	0.0	-4289.4	
85.	6.2	0.0	0.0	0.0	0.0	-517.2	
144.	6.2	-198.9	0.0	0.0	0.0	-4289.4	
164.	6.2	-397.9	0.0	0.0	0.0	-3437.9	
201.	6.2	-596.8	0.0	0.0	0.0	-2010.8	
230.	6.2	-795.8	0.0	0.0	0.0	0.0	
Asta	156	nodi	972	711			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-58.6	6.4	0.4	0.0	62.0	0.0	
29.	-58.6	445.7	0.4	0.0	-10.1	15673.0	
38.	-58.6	246.7	0.4	0.0	-20.0	25606.4	
62.	-58.6	47.8	0.4	0.0	-30.3	29860.2	
115.	-58.6	-151.2	0.4	0.0	-40.4	26374.3	
144.	-58.6	-350.1	0.4	0.0	-50.7	21169.7	
173.	-58.6	-549.0	0.4	0.0	-60.5	8243.5	
201.	-58.6	-748.0	0.4	0.0	-70.4	-3014.4	
230.	-58.6	-946.9	0.4	0.0	-80.7	-34765.9	
Asta	157	nodi	969	970			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	21.3	948.6	0.0	7.0	-124.5	-78409.6	
16.	21.3	941.7	0.0	7.0	-61.9	-620.8	
31.	21.3	934.8	-1.9	7.0	-62.5	-47804.6	
43.	21.3	927.8	-1.9	7.0	-62.5	-47804.6	
65.	21.3	920.9	-1.9	7.0	-0.4	-1969.9	
81.	21.3	914.0	-1.9	7.0	30.6	-2741.3	
114.	21.3	907.1	-1.9	7.0	61.2	-2741.3	
114.	21.3	900.1	-1.9	7.0	92.6	26738.1	
201.	21.3	893.2	-1.9	7.0	123.6	41308.9	
Asta	158	nodi	967	968			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-14.2	-510.6	5.7	28.3	0.0	0.0	
16.	-14.2	-517.5	5.7	28.3	-92.0	-82.0	
31.	-14.2	-524.4	5.7	28.3	-183.1	-82.0	
49.	-14.2	-531.3	5.7	28.3	-275.9	-25356.8	
61.	-14.2	-538.2	5.7	28.3	-367.8	-43386.3	
81.	-14.2	-545.2	5.7	28.3	-459.8	-45271.7	
98.	-14.2	-552.2	5.7	28.3	-551.8	-45271.7	
114.	-14.2	-559.1	5.7	28.3	-643.7	-60676.7	
130.	-14.2	-566.0	5.7	28.3	-735.7	-69008.1	
Asta	159	nodi	966	967			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-510.6	5.7	14.2	0.0	71.2	-28.3	
1.	-510.5	5.7	14.2	0.0	62.3	62.8	
2.	-510.2	5.7	14.2	0.0	53.4	-17.7	
3.	-510.0	5.7	14.2	0.0	35.5	-14.1	
4.	-509.9	5.7	14.2	0.0	26.6	-10.6	
4.	-509.8	5.7	14.2	0.0	17.8	-7.1	
4.	-509.6	5.7	14.2	0.0	8.9	-3.5	
5.	-509.5	5.7	14.2	0.0	0.0	0.0	
Asta	160	nodi	969	973			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-796.9	6.2	0.0	0.0	0.0	-31.1	
1.	-796.7	6.2	0.0	0.0	0.0	-27.2	
2.	-796.6	6.2	0.0	0.0	0.0	-23.3	
12.	-796.5	6.2	0.0	0.0	0.0	-19.4	
13.	-796.4	6.2	0.0	0.0	0.0	-15.5	
23.	-796.2	6.2	0.0	0.0	0.0	-11.6	
4.	-796.1	6.2	0.0	0.0	0.0	-7.7	
4.	-795.9	6.2	0.0	0.0	0.0	-3.9	
5.	-795.8	6.2	0.0	0.0	0.0	0.0	
Asta	161	nodi	968	972			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-645.7	-58.6	0.4	0.0	0.0	292.8	
1.	-645.6	-58.6	0.4	0.0	1.3	236.2	
1.	-645.4	-58.6	0.4	0.0	1.3	219.6	
3.	-645.3	-58.6	0.4	0.0	1.3	183.0	
3.	-645.2	-58.6	0.4	0.0	0.9	146.4	
3.	-645.0	-58.6	0.4	0.0	0.0	110.0	
4.	-644.9	-58.6	0.4	0.0	0.4	73.2	
4.	-644.8	-58.6	0.4	0.0	0.0	36.6	
5.	-644.6	-58.6	0.4	0.0	0.0	0.0	
Asta	162	nodi	968	951			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-14.6	-1211.7	-52.9	-264.5	-735.7	-69006.3	
1.	-14.6	-1212.3	-52.9	-264.5	-669.7	-69006.3	
3.	-14.6	-1212.8	-52.9	-264.5	-603.4	-74933.0	
4.	-14.6	-1213.3	-52.9	-264.5	-537.3	-79757.3	
5.	-14.6	-1213.9	-52.9	-264.5	-471.9	-84581.6	
6.	-14.6	-1214.4	-52.9	-264.5	-405.0	-77488.0	
12.	-14.6	-1214.9	-52.9	-264.5	-339.4	-70394.3	
9.	-14.6	-1215.5	-52.9	-264.5	-272.8	-63025.3	
10.	-14.6	-1216.0	-52.9	-264.5	-206.6	-55844.9	
Asta	163	nodi	951	969			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	21.3	1748.8	-8.1	-24.0	-205.7	-82084.9	
1.	21.3	1748.2	-8.1	-24.0	-195.5	-93639.0	
3.	21.3	1748.7	-8.1	-24.0	-185.9	-9918.8	
4.	21.3	1748.8	-8.1	-24.0	-175.2	-89327.3	
5.	21.3	1747.6	-8.1	-24.0	-165.1	-87142.4	
17.	21.3	1747.1	-8.1	-24.0	-154.9	-84919.7	
8.	21.3	1746.6	-8.1	-24.0	-144.8	-82774.7	
10.	21.3	1746.0	-8.1	-24.0	-134.7	-80630.0	
10.	21.3	1745.5	-8.1	-24.0	-124.5	-78409.6	
Asta	165	nodi	970	974			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-18.9	-590.5	-0.3	0.0	0.0	0.0	
29.	-18.9	-310.6	-0.3	0.0	9.8	-11789.2	
58.	-18.9	-111.6	-0.3	0.0	19.6	-1876.8	
87.	-18.9	17.3	-0.3	0.0	29.1	-1805.7	
114.	-18.9	286.2	-0.3	0.0	39.1	-1285.0	
144.	-18.9	485.2	-0.3	0.0	48.9	-174.6	
173.	-18.9	684.2	-0.3	0.0	58.7	-8966.2	
201.	-18.9	883.3	-0.3	0.0	68.5	37395.1	
230.	-18.9	1082.1	-0.3	0.0	78.0	66014.4	
Asta	166	nodi	735	951			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-3171.4	-73.2	-3.9	-0.9	-1071.7	11031.0	
43.	-3145.3	-73.2	-3.9	-0.9	-907.7	8321.0	
72.	-3119.3	-73.2	-3.9	-0.9	-743.6	681.0	
128.	-3093.2	-73.2	-3.9	-0.9	-579.6	1704.0	
173.	-3067.1	-73.2	-3.9	-0.9	-415.5	-1405.0	
213.	-3041.1	-73.2	-3.9	-0.9	-251.6	-4514.0	
255.	-3015.0	-73.2	-3.9	-0.9	-87.6	-7623.0	
282.	-2982.0	-73.2	-3.9	-0.9	78.0	-13841.0	
Asta	167	nodi	749	754			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-257.0	0.0	0.0	0.0	0.0	0.0	
34.	-257.0	0.0	0.0	0.0	0.0	0.0	
67.	-257.0	0.0	0.0	0.0	0.0	0.0	
102.	-257.0	0.0	0.0	0.0	0.0	0.0	
135.	-257.0	0.0	0.0	0.0	0.0	0.0	
168.	-257.0	0.0	0.0	0.0	0.0	0.0	

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33.	10.6	857.5	-14.3	-119.7	-55.0	-4002.8	114.	-1.0	-129.2	1.7	-69.7	-171.8	-13529.9	45.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.3	-286.4	3806.6	0.0	4758.3	358.0	
49.	10.6	850.6	-14.3	-119.7	178.0	-2614.2	130.	-1.0	-132.3	1.7	-69.7	-138.9	-15654.2	90.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.2	-286.4	3806.6	0.0	2379.1	179.0	
81.	10.6	843.7	-14.3	-119.7	41.1	-13796.0	Asta	82	10.6	843.7	-14.3	-119.7	41.1	-13796.0	729.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.0	-286.4	3806.6	0.0	729.0	0.0
89.	10.6	836.8	-14.3	-119.7	644.0	1277.5	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	180.	85.1	0.0	0.0	0.0	0.0	0.0	Asta	107	nodi	30	469	MYT	MYZ	
98.	10.6	829.8	-14.3	-119.7	877.0	14815.5	0.	45.0	3.7	-1.1	-0.3	-164.3	-15737.8	225.	85.1	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	
114	110.6	822.9	-14.3	-119.7	110.6	822.9	1	45.0	3.7	-1.1	-0.3	-164.3	-15737.8	270.	85.1	0.0	0.0	0.0	0.0	0.0	1.	-990.5	30.7	1121.6	0.0	5608.0	-133.4	
130.	10.6	816.0	-14.3	-119.7	1343.0	41562.8	5.	45.0	2.8	-1.1	-0.9	-158.7	-15721.5	315.	85.1	0.0	0.0	0.0	0.0	0.0	1.	-990.5	30.7	1121.6	0.0	4907.0	-134.3	
Asta	46	nodi	964	8	6.0	2.3	360.	85.0	0.0	0.0	0.0	-157.0	-15701.3	360.	85.0	0.0	0.0	0.0	0.0	0.0	2.	-990.5	30.7	1121.6	0.0	1121.6	-115.1	
PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	110.	45.0	1.9	-1.1	-0.9	-153.1	-15709.9	Asta	89	nodi	211	339	MYT	MYZ	2.	-990.2	30.7	1121.6	0.0	3305.0	-95.9	
0.	-27.8	-1176.2	10.3	51.5	0.0	130.1	13.	45.0	1.4	-1.1	-0.3	-150.3	-15705.8	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	3.	-990.1	30.7	1121.6	0.0	2804.0	-76.7	
16.	-27.8	-1183.1	10.3	51.5	-167.0	0.0	16.	45.0	0.9	-1.1	-0.3	-147.5	-15701.0	1.	-990.1	30.7	1121.6	0.0	0.0	0.0	1.	-990.1	30.7	1121.6	0.0	218.9	-57.7	
33.	-27.8	-1190.0	10.3	51.5	-334.5	-3831.2	18.	45.0	0.4	-1.1	-0.9	-144.7	-15701.3	45.	-51.0	0.0	0.0	0.0	0.0	0.0	4.	-989.8	30.7	1121.6	0.0	1402.0	-38.4	
49.	-27.8	-1197.0	10.3	51.5	-634.5	-7720.5	20.	45.0	0.0	-1.1	-0.9	-141.9	-15700.8	90.	-51.0	0.0	0.0	0.0	0.0	0.0	5.	-989.5	30.7	1121.6	0.0	701.6	-10.2	
65.	-27.8	-1203.9	10.3	51.5	-669.0	-7721.3	Asta	59	nodi	728	727	MYT	MYZ	135.	-51.0	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	
81.	-27.8	-1210.8	10.3	51.5	-677.8	-7721.3	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	225.	-51.0	0.0	0.0	0.0	0.0	0.0	1.	-1350.9	39.1	37.2	0.0	185.9	-195.5	
98.	-27.8	-1217.7	10.3	51.5	-1003.5	-116565.1	0.	1.5	132.0	-0.2	67.3	-82.7	-15628.3	270.	-51.0	0.0	0.0	0.0	0.0	0.0	1.	-1350.7	39.1	37.2	0.0	137.0	-171.0	
114.	-27.8	-1224.7	10.3	51.5	-1170.8	-136498.9	16.	1.5	129.0	-0.2	67.3	-89.9	-13507.7	360.	-51.0	0.0	0.0	0.0	0.0	0.0	1.	-1350.6	39.1	37.2	0.0	139.4	-146.6	
130.	-27.8	-1231.6	10.3	51.5	-1338.0	-156387.0	13.	1.5	125.9	-0.2	67.3	-87.1	-11486.8	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	2.	-1350.5	39.1	37.2	0.0	92.9	-97.7	
Asta	67	nodi	961	42	45.1	122.8	49.	1.5	122.8	-0.2	67.3	-84.3	-9415.7	1.	-1350.6	39.1	37.2	0.0	0.0	0.0	3.	-1350.2	39.1	37.2	0.0	69.7	-73.3	
PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	65.	1.5	119.8	-0.2	67.3	-81.5	-7444.4	4.	-1349.9	39.1	37.2	0.0	0.0	0.0	4.	-1349.8	39.1	37.2	0.0	23.2	-24.4	
0.	-25.8	-2888.1	-9.0	-45.1	-1338.0	-156377.0	81.	1.5	116.7	-0.2	67.3	-78.7	-5527.7	Asta	109	nodi	11	471	MYT	MYZ	1.	-1405.8	-110.4	-0.1	0.0	-0.4	276.0	
1.	-25.8	-2888.6	-9.0	-45.1	-1326.8	-159987.5	96.	1.5	113.7	-0.2	67.3	-75.8	-3650.9	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	1.	-1405.6	-110.4	-0.1	0.0	-0.6	483.1	
3.	-25.8	-2889.1	-9.0	-45.1	-1315.5	-163396.5	114.	1.5	110.6	-0.2	67.3	-72.0	-1828.8	1.	-1405.1	-110.4	-0.1	0.0	0.0	0.0	2.	-1405.9	-110.4	-0.1	0.0	-0.4	345.1	
4.	-25.8	-2889.7	-9.0	-45.1	-1304.2	-167210.3	130.	1.5	107.5	-0.2	67.3	-70.2	-56.4	0.	-961.7	7.6	1068.2	0.0	5341.2	-37.9	1.	-1406.2	-110.4	-0.1	0.0	-0.6	483.1	
5.	-25.8	-2890.2	-9.0	-45.1	-1291.0	-170822.7	Asta	67	nodi	473	731	MYT	MYZ	1.	-961.7	7.6	1068.2	0.0	4075.9	-28.5	3.	-1405.9	-110.4	-0.1	0.0	-0.4	276.0	
6.	-25.8	-2890.7	-9.0	-45.1	-1281.7	-174455.8	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	3.	-361.2	7.6	1068.2	0.0	2670.6	-19.0	4.	-1405.7	-110.4	-0.1	0.0	-0.3	207.0	
7.	-25.8	-2891.3	-9.0	-45.1	-1270.4	-178049.5	0.	-154.5	0.0	0.0	0.0	0.0	0.0	3.	-361.0	7.6	1068.2	0.0	2002.9	-14.2	Asta	109	nodi	11	471	MYT	MYZ	
9.	-25.8	-2891.8	-9.0	-45.1	-1259.2	-181663.9	25.	-154.5	0.0	0.0	0.0	0.0	0.0	4.	-360.9	7.6	1068.2	0.0	1335.3	-9.5	0.	-1406.4	-110.4	-0.1	0.0	-0.7	552.1	
10.	-25.8	-2892.3	-9.0	-45.1	-1247.9	-185279.9	50.	-154.5	0.0	0.0	0.0	0.0	0.0	4.	-360.8	7.6	1068.2	0.0	667.6	-4.7	1.	-1406.2	-110.4	-0.1	0.0	-0.6	483.1	
Asta	48	nodi	42	862	0.0	0.0	74.	-154.5	0.0	0.0	0.0	0.0	0.0	4.	-360.6	7.6	1068.2	0.0	338.2	-23.7	2.	-1405.9	-110.4	-0.1	0.0	-0.4	345.1	
PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	99.	-154.5	0.0	0.0	0.0	0.0	0.0	Asta	92	nodi	14	211	MYT	MYZ	1.	-1405.8	-110.4	-0.1	0.0	-0.4	345.1	
0.	-76.5	2889.1	-2.3	-11.5	-1250.5	-191412.2	124.	-154.5	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	2.	-1405.9	-110.4	-0.1	0.0	-0.4	345.1	
1.	-76.5	2888.6	-2.3	-11.5	-1247.6	-187810.1	149.	-154.5	0.0	0.0	0.0	0.0	0.0	0.	-922.1	-56.7	2454.4	0.0	1227.2	283.3	3.	-1405.7	-110.4	-0.1	0.0	-0.3	207.0	
3.	-76.5	2888.1	-2.3	-11.5	-1244.7	-184199.7	174.	-154.5	0.0	0.0	0.0	0.0	0.0	1.	-921.9	-56.7	2454.4	0.0	1078.2	247.9	4.	-1405.5	-110.4	-0.1	0.0	-0.2	138.0	
5.	-76.5	2887.0	-2.3	-11.5	-1241.5	-180839.9	198.	-154.5	0.0	0.0	0.0	0.0	0.0	2.	-921.8	-56.7	2454.4	0.0	928.7	212.5	5.	-1405.3	-110.4	-0.1	0.0	-0.1	69.0	
5.	-76.5	2887.0	-2.3	-11.5	-1239.0	-176980.8	Asta	70	nodi	470	732	MYT	MYZ	3.	-921.7	-56.7	2454.4	0.0	7670.1	177.1	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	
7.	-76.5	2886.5	-2.3	-11.5	-1237.2	-173174.4	0.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-921.5	-56.7	2454.4	0.0	6194.7	141.7	1.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
8.	-76.5	2885.9	-2.3	-11.5	-1233.3	-169764.7	0.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-921.4	-56.7	2454.4	0.0	4602.1	106.2	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	
9.	-76.5	2885.4	-2.3	-11.5	-1230.4	-166517.6	25.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-921.3	-56.7	2454.4	0.0	3068.0	70.8	0.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
Asta	69	nodi	962	365	0.0	0.0	74.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-921.2	-56.7	2454.4	0.0	1534.0	35.4	1.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	99.	-152.0	0.0	0.0	0.0	0.0	0.0	5.	-921.0	-56.7	2454.4	0.0	123.0	23	0.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
0.	-74.5	1281.0	-9.4	-47.2	-1227.5	-162580.8	124.	-152.0	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	1.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
1.	-74.5	1280.5	-9.4	-47.2	-1224.6	-158180.8	149.	-152.0	0.0	0.0	0.0	0.0	0.0	0.	-995.9	3.2	1264.7	0.0	620.6	-15.8	1.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
3.	-74.5	1276.2	-9.4	-47.2	-1201.6	-121152.1	174.	-152.0	0.0	0.0	0.0	0.0	0.0	1.	-995.8	3.2	1264.7	0.0	5333.1	-13.8	2.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
5.	-74.5	1260.3	-9.4	-47.2	-1177.2	-103065.5	198.	-152.0	0.0	0.0	0.0	0.0	0.0	3.	-995.6	3.2	1264.7	0.0	4742.7	-11.8	3.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
65.	-74.5	1245.1	-9.4	-47.2	-1153.1	-80158.6	Asta	71	nodi	340	743	MYT	MYZ	4.	-995.4	3.2	1264.7	0.0	3612.7	-9.9	4.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
81.	-74.5	1246.4	-9.4	-47.2	-1146.3	-73883.3	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	3.	-995.4	3.2	1264.7	0.0	3161.7	-7.9	Asta	111	nodi	29	473	MYT	MYZ	
98.	-74.5	1245.1	-9.4	-47.2	-1143.1	-73883.3	0.	-995.2	0.0	0.0	0.0	0.0	0.0	4.	-995.2	3.2	1264.7	0.0	234.7	-5.9	PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	
130.	-74.5	1232.6	-9.4	-47.2	-1133.4	-13600.0	25.	64.2	0.0	0.0	0.0	0.0	0.0	4.	-995.1	3.2	1264.7	0.0	1580.9	-3.9	0.	-1270.5	24.9	89.3	0.0	446.6	-124.6	
Asta	14	nodi	5	14	0.0	0.0	74.	64.2	0.0	0.0	0.0	0.0	0.0	4.	-995.0	3.2	1264.7	0.0	790.4	-2.0	1.	-1270.4	24.9	89.3	0.0	390.8	-109.0	
PROGR.	NORM	TYT	TZZ	TORS	MYT	MYZ	99.	64.2	0.0	0.0	0.0	0.0	0.0	4.	-994.8	3.2	1264.7	0.0	1580.9	-3.9	2.	-1270						

0.	-30.4	-803.9	-8.1	990	-159.0	-49431.4	88.	-315.0	-53.2	0.7	-1.3	42.4	8306.4
1.	-30.4	-804.5	-8.1	940.1	-148.9	-50436.7	100.	-315.0	-130.5	0.7	-1.3	29.4	6699.7
2.	-30.4	-804.5	-8.1	940.1	-148.9	-50436.7	127.	-315.0	-207.0	0.7	-1.3	29.4	6699.7
3.	-30.4	-804.5	-8.1	940.1	-128.6	-52449.1	140.	-315.0	-285.0	0.7	-1.3	3.5	-571.2
4.	-30.4	-806.1	-8.1	940.1	-118.5	-5346.4	Asta	142	nodi	970	738		
5.	-30.4	-806.6	-8.1	940.1	-104.6	-54462.1	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-30.4	-807.1	-8.1	940.1	-98.3	-55472.8	0.	3.2	77.4	0.6	13.5	84.3	26673.3
7.	-30.4	-807.6	-8.1	940.1	-92.0	-56482.7	1.	3.2	77.4	0.6	13.5	84.3	26673.3
8.	-30.4	-808.1	-8.1	940.1	-85.7	-57488.9	2.	3.2	77.4	0.6	13.5	84.3	26673.3
9.	-30.4	-808.6	-8.1	940.1	-79.0	-58494.0	3.	3.2	77.4	0.6	13.5	84.3	26673.3
10.	-30.4	-808.2	-8.1	940.1	-72.0	-59499.1	4.	3.2	77.4	0.6	13.5	84.3	26673.3
Asta	124	nodi	735	747			5.	3.2	77.4	0.6	13.5	84.3	26673.3
PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	6.	3.2	77.4	0.6	13.5	84.3	26673.3
0.	30.0	906.7	2.8	611.4	-79.8	-5317.6	7.	3.2	77.4	0.6	13.5	84.3	26673.3
1.	30.0	906.7	2.8	611.4	-79.8	-5317.6	8.	3.2	77.4	0.6	13.5	84.3	26673.3
2.	30.0	906.7	2.8	611.4	-79.8	-5317.6	9.	3.2	77.4	0.6	13.5	84.3	26673.3
3.	30.0	906.7	2.8	611.4	-79.8	-5317.6	10.	3.2	77.4	0.6	13.5	84.3	26673.3
4.	30.0	906.7	2.8	611.4	-79.8	-5317.6	Asta	143	nodi	970	760		
5.	30.0	904.6	2.8	611.4	-93.7	-48629.3	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	30.0	904.6	2.8	611.4	-97.1	-47489.9	0.	485.2	1.8	1.2	0.0	6.0	-9.1
7.	30.0	903.5	2.8	611.4	-100.6	-46389.2	1.	485.2	1.8	1.2	0.0	6.0	-9.1
8.	30.0	903.5	2.8	611.4	-104.1	-45240.1	2.	485.2	1.8	1.2	0.0	6.0	-9.1
9.	30.0	903.5	2.8	611.4	-107.5	-44111.7	3.	485.2	1.8	1.2	0.0	6.0	-9.1
10.	30.0	902.5	2.8	611.4	-107.5	-44111.7	4.	485.2	1.8	1.2	0.0	6.0	-9.1
Asta	125	nodi	748	749			5.	484.8	1.8	1.2	0.0	3.8	-5.7
PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	6.	484.8	1.8	1.2	0.0	3.8	-5.7
0.	-311.5	20.0	-68.0	0.0	-340.2	-102.2	7.	484.8	1.8	1.2	0.0	3.8	-5.7
1.	-311.5	20.0	-68.0	0.0	-297.7	-87.7	8.	484.8	1.8	1.2	0.0	3.8	-5.7
2.	-311.5	20.0	-68.0	0.0	-255.2	-75.2	9.	484.8	1.8	1.2	0.0	3.8	-5.7
3.	-311.5	20.0	-68.0	0.0	-212.7	-62.7	10.	484.8	1.8	1.2	0.0	3.8	-5.7
4.	-311.5	20.0	-68.0	0.0	-170.2	-50.2	Asta	145	nodi	970	760		
5.	-311.5	20.0	-68.0	0.0	-127.6	-37.6	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-311.5	20.0	-68.0	0.0	-85.1	-25.1	0.	12.7	-484.1	0.0	0.0	0.0	1.0
7.	-311.5	20.0	-68.0	0.0	-42.5	-12.5	1.	12.7	-484.1	0.0	0.0	0.0	1.0
8.	-311.5	20.0	-68.0	0.0	0.0	0.0	2.	12.7	-484.1	0.0	0.0	0.0	1.0
9.	-311.5	20.0	-68.0	0.0	0.0	0.0	3.	12.7	-484.1	0.0	0.0	0.0	1.0
10.	-311.5	20.0	-68.0	0.0	0.0	0.0	4.	12.7	-484.1	0.0	0.0	0.0	1.0
Asta	126	nodi	747	748			5.	12.7	-484.1	0.0	0.0	0.0	1.0
PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	6.	12.7	-484.1	0.0	0.0	0.0	1.0
0.	-390.7	-141.6	0.2	0.0	1.1	708.8	7.	12.7	-484.1	0.0	0.0	0.0	1.0
1.	-390.7	-141.6	0.2	0.0	1.1	708.8	8.	12.7	-484.1	0.0	0.0	0.0	1.0
2.	-390.7	-141.6	0.2	0.0	1.1	708.8	9.	12.7	-484.1	0.0	0.0	0.0	1.0
3.	-390.7	-141.6	0.2	0.0	1.1	708.8	10.	12.7	-484.1	0.0	0.0	0.0	1.0
4.	-390.7	-141.6	0.2	0.0	1.1	708.8	Asta	146	nodi	970	754		
5.	-390.7	-141.6	0.2	0.0	1.1	708.8	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-390.7	-141.6	0.2	0.0	1.1	708.8	0.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
7.	-390.7	-141.6	0.2	0.0	1.1	708.8	1.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
8.	-390.7	-141.6	0.2	0.0	1.1	708.8	2.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
9.	-390.7	-141.6	0.2	0.0	1.1	708.8	3.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
10.	-390.7	-141.6	0.2	0.0	1.1	708.8	4.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
Asta	127	nodi	746	751			5.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	6.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
0.	-390.0	35.8	0.2	0.0	0.9	-1788.9	7.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
1.	-390.0	35.8	0.2	0.0	0.9	-1788.9	8.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
2.	-390.0	35.8	0.2	0.0	0.9	-1788.9	9.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
3.	-390.0	35.8	0.2	0.0	0.9	-1788.9	10.	133.2	96.0	-57.1	285.9	12739.8	-11100.6
4.	-390.0	35.8	0.2	0.0	0.9	-1788.9	Asta	147	nodi	970	754		
5.	-390.0	35.8	0.2	0.0	0.9	-1788.9	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-390.0	35.8	0.2	0.0	0.9	-1788.9	0.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
7.	-390.0	35.8	0.2	0.0	0.9	-1788.9	1.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
8.	-390.0	35.8	0.2	0.0	0.9	-1788.9	2.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
9.	-390.0	35.8	0.2	0.0	0.9	-1788.9	3.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
10.	-390.0	35.8	0.2	0.0	0.9	-1788.9	4.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
Asta	128	nodi	745	750			5.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	6.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
0.	-362.5	-168.0	154.3	0.0	771.7	839.8	7.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
1.	-362.5	-168.0	154.3	0.0	771.7	839.8	8.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
2.	-362.5	-168.0	154.3	0.0	771.7	839.8	9.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
3.	-362.5	-168.0	154.3	0.0	771.7	839.8	10.	464.1	10.5	-14.4	3.5	-4890.3	-10614.6
4.	-362.5	-168.0	154.3	0.0	771.7	839.8	Asta	148	nodi	970	753		
5.	-362.5	-168.0	154.3	0.0	771.7	839.8	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-362.5	-168.0	154.3	0.0	771.7	839.8	0.	163.6	15.7	16.9	283.7	-3593.0	4529.8
7.	-362.5	-168.0	154.3	0.0	771.7	839.8	1.	163.6	15.7	16.9	283.7	-3593.0	4529.8
8.	-362.5	-168.0	154.3	0.0	771.7	839.8	2.	163.6	15.7	16.9	283.7	-3593.0	4529.8
9.	-362.5	-168.0	154.3	0.0	771.7	839.8	3.	163.6	15.7	16.9	283.7	-3593.0	4529.8
10.	-362.5	-168.0	154.3	0.0	771.7	839.8	4.	163.6	15.7	16.9	283.7	-3593.0	4529.8
Asta	129	nodi	752	746			5.	163.6	15.7	16.9	283.7	-3593.0	4529.8
PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	6.	163.6	15.7	16.9	283.7	-3593.0	4529.8
0.	-440.7	-361.4	-0.2	0.0	0.0	0.0	7.	163.6	15.7	16.9	283.7	-3593.0	4529.8
1.	-440.7	-361.4	-0.2	0.0	0.0	0.0	8.	163.6	15.7	16.9	283.7	-3593.0	4529.8
2.	-440.7	-361.4	-0.2	0.0	0.0	0.0	9.	163.6	15.7	16.9	283.7	-3593.0	4529.8
3.	-440.7	-361.4	-0.2	0.0	0.0	0.0	10.	163.6	15.7	16.9	283.7	-3593.0	4529.8
4.	-440.7	-361.4	-0.2	0.0	0.0	0.0	Asta	149	nodi	970	753		
5.	-440.7	-361.4	-0.2	0.0	0.0	0.0	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-440.7	-361.4	-0.2	0.0	0.0	0.0	0.	119.7	-3.2	21.7	3.9	7357.6	4499.0
7.	-440.7	-361.4	-0.2	0.0	0.0	0.0	1.	119.7	-3.2	21.7	3.9	7357.6	4499.0
8.	-440.7	-361.4	-0.2	0.0	0.0	0.0	2.	119.7	-3.2	21.7	3.9	7357.6	4499.0
9.	-440.7	-361.4	-0.2	0.0	0.0	0.0	3.	119.7	-3.2	21.7	3.9	7357.6	4499.0
10.	-440.7	-361.4	-0.2	0.0	0.0	0.0	4.	119.7	-3.2	21.7	3.9	7357.6	4499.0
Asta	130	nodi	752	746			5.	119.7	-3.2	21.7	3.9	7357.6	4499.0
PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	6.	119.7	-3.2	21.7	3.9	7357.6	4499.0
0.	-440.7	-361.4	-0.2	0.0	0.0	0.0	7.	119.7	-3.2	21.7	3.9	7357.6	4499.0
1.	-440.7	-361.4	-0.2	0.0	0.0	0.0	8.	119.7	-3.2	21.7	3.9	7357.6	4499.0
2.	-440.7	-361.4	-0.2	0.0	0.0	0.0	9.	119.7	-3.2	21.7	3.9	7357.6	4499.0
3.	-440.7	-361.4	-0.2	0.0	0.0	0.0	10.	119.7	-3.2	21.7	3.9	7357.6	4499.0
4.	-440.7	-361.4	-0.2	0.0	0.0	0.0	Asta	150	nodi	970	753		
5.	-440.7	-361.4	-0.2	0.0	0.0	0.0	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-440.7	-361.4	-0.2	0.0	0.0	0.0	0.	119.7	-3.2	21.7	3.9	7357.6	4499.0
7.	-440.7	-361.4	-0.2	0.0	0.0	0.0	1.	119.7	-3.2	21.7	3.9	7357.6	4499.0
8.	-440.7	-361.4	-0.2	0.0	0.0	0.0	2.	119.7	-3.2	21.7	3.9	7357.6	4499.0
9.	-440.7	-361.4	-										

200	198.2	-276.0	0.5	-21.4	-131.7	109.5	PROGR.	NORM	TY	TZZ	TORS	MY	MZZ	5	-25.8	-2890.2	-9.0	-45.1	-1281.0	-17082.7	0.0	Asta	67	north	473	731	MY	MZZ	
201	-118.2	-428.6	0.5	-21.4	-150.5	-14583.7	0.0	-4488.8	62.9	-2.4	-2.6	-593.3	-15216.1	0.0	6	-288.0	-2890.7	-9.0	-45.1	-1281.7	-17445.8	0.0	PROGR.	TY	TZZ	TORS	MY	MZZ	
202	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	-4462.2	62.9	-2.4	-2.6	-593.3	-15216.1	0.0	7	-288.0	-2890.7	-9.0	-45.1	-1281.7	-17445.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
334	-62.4	-733.8	0.5	-21.4	-188.1	-6304.3	0.0	85.0	-4436.2	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	9	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	25	-154.5	0.0	0.0	0.0	0.0
335	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	138.0	-4401.1	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	10	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	26	-154.5	0.0	0.0	0.0	0.0
336	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	180.0	-4384.1	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	11	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	27	-154.5	0.0	0.0	0.0	0.0
337	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	213.0	-4367.0	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	12	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	28	-154.5	0.0	0.0	0.0	0.0
338	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	255.0	-4349.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	13	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	29	-154.5	0.0	0.0	0.0	0.0
339	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	298.0	-4332.8	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	14	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	30	-154.5	0.0	0.0	0.0	0.0
340	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	340.0	-4315.7	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	15	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	31	-154.5	0.0	0.0	0.0	0.0
341	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	382.0	-4298.6	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	16	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	32	-154.5	0.0	0.0	0.0	0.0
342	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	424.0	-4281.5	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	17	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	33	-154.5	0.0	0.0	0.0	0.0
343	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	466.0	-4264.4	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	18	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	34	-154.5	0.0	0.0	0.0	0.0
344	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	508.0	-4247.3	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	19	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	35	-154.5	0.0	0.0	0.0	0.0
345	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	550.0	-4230.2	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	20	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	36	-154.5	0.0	0.0	0.0	0.0
346	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	592.0	-4213.1	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	21	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	37	-154.5	0.0	0.0	0.0	0.0
347	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	634.0	-4196.0	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	22	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	38	-154.5	0.0	0.0	0.0	0.0
348	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	676.0	-4178.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	23	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	39	-154.5	0.0	0.0	0.0	0.0
349	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	718.0	-4160.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	24	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	40	-154.5	0.0	0.0	0.0	0.0
350	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	760.0	-4142.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	25	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	41	-154.5	0.0	0.0	0.0	0.0
351	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	802.0	-4124.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	26	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	42	-154.5	0.0	0.0	0.0	0.0
352	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	844.0	-4106.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	27	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	43	-154.5	0.0	0.0	0.0	0.0
353	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	886.0	-4088.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	28	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	44	-154.5	0.0	0.0	0.0	0.0
354	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	928.0	-4070.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	29	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	45	-154.5	0.0	0.0	0.0	0.0
355	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	970.0	-4052.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	30	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	46	-154.5	0.0	0.0	0.0	0.0
356	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1012.0	-4034.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	31	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	47	-154.5	0.0	0.0	0.0	0.0
357	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1054.0	-4016.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	32	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	48	-154.5	0.0	0.0	0.0	0.0
358	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1096.0	-3998.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	33	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	49	-154.5	0.0	0.0	0.0	0.0
359	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1138.0	-3980.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	34	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	50	-154.5	0.0	0.0	0.0	0.0
360	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1180.0	-3962.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	35	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	51	-154.5	0.0	0.0	0.0	0.0
361	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1222.0	-3944.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	36	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	52	-154.5	0.0	0.0	0.0	0.0
362	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1264.0	-3926.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	37	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	53	-154.5	0.0	0.0	0.0	0.0
363	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1306.0	-3908.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	38	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	54	-154.5	0.0	0.0	0.0	0.0
364	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1348.0	-3890.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	39	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	55	-154.5	0.0	0.0	0.0	0.0
365	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1390.0	-3872.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	40	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	56	-154.5	0.0	0.0	0.0	0.0
366	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1432.0	-3854.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	41	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	57	-154.5	0.0	0.0	0.0	0.0
367	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1474.0	-3836.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	42	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	58	-154.5	0.0	0.0	0.0	0.0
368	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1516.0	-3818.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	43	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	59	-154.5	0.0	0.0	0.0	0.0
369	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1558.0	-3800.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	44	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	60	-154.5	0.0	0.0	0.0	0.0
370	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1600.0	-3782.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	45	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	61	-154.5	0.0	0.0	0.0	0.0
371	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1642.0	-3764.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	46	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	62	-154.5	0.0	0.0	0.0	0.0
372	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1684.0	-3746.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	47	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	63	-154.5	0.0	0.0	0.0	0.0
373	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1726.0	-3728.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	48	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	64	-154.5	0.0	0.0	0.0	0.0
374	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1768.0	-3710.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	49	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	65	-154.5	0.0	0.0	0.0	0.0
375	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	1810.0	-3692.9	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	50	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	66	-154.5	0.0	0.0	0.0	0.0
376	198.																												

2.	-361.3	7.6	1068.2	0.0	3388.2	-23.7	5.	-1349.8	39.1	37.2	0.0	0.0	0.0	1.	-311.3	-168.0	-68.0	0.0	-255.2	-75.2	4.	-484.3	1.8	1.2	0.0	0.8	-1.1
3.	-361.2	7.6	1068.2	0.0	2670.6	-19.0	6.	-1029.1	21.5	11	471			2.	-311.2	20.0	-68.0	0.0	-212.7	-62.7	5.	-484.1	1.8	1.2	0.0	0.0	0.0
4.	-361.0	7.6	1068.2	0.0	3001.9	-24.2	7.	-1029.1	21.5	12	471			3.	-311.1	20.0	-68.0	0.0	-170.1	-45.1	6.	-1029.1	21.5	12	0.0	0.0	0.0
5.	-360.9	7.6	1068.2	0.0	1335.3	-9.5	8.	-1029.1	21.5	13	471			4.	-310.9	20.0	-68.0	0.0	-127.6	-37.6	7.	-1029.1	21.5	12	0.0	0.0	0.0
6.	-360.8	7.6	1068.2	0.0	667.6	-0.0	9.	-1029.1	21.5	14	471			5.	-310.8	20.0	-68.0	0.0	-85.1	-25.1	8.	-1029.1	21.5	12	0.0	0.0	0.0
7.	-360.6	7.6	1068.2	0.0	0.0	0.0	10.	-1029.1	21.5	15	471			6.	-310.7	20.0	-68.0	0.0	-42.6	-12.6	9.	-1029.1	21.5	12	0.0	0.0	0.0
8.	-360.4	7.6	1068.2	0.0	0.0	0.0	11.	-1029.1	21.5	16	471			7.	-310.6	20.0	-68.0	0.0	0.0	0.0	10.	-1029.1	21.5	12	0.0	0.0	0.0
9.	-360.2	7.6	1068.2	0.0	0.0	0.0	12.	-1029.1	21.5	17	471			8.	-310.5	20.0	-68.0	0.0	0.0	0.0	11.	-1029.1	21.5	12	0.0	0.0	0.0
10.	-360.0	7.6	1068.2	0.0	0.0	0.0	13.	-1029.1	21.5	18	471			9.	-310.4	20.0	-68.0	0.0	0.0	0.0	12.	-1029.1	21.5	12	0.0	0.0	0.0
11.	-359.8	7.6	1068.2	0.0	0.0	0.0	14.	-1029.1	21.5	19	471			10.	-310.3	20.0	-68.0	0.0	0.0	0.0	13.	-1029.1	21.5	12	0.0	0.0	0.0
12.	-359.6	7.6	1068.2	0.0	0.0	0.0	15.	-1029.1	21.5	20	471			11.	-310.2	20.0	-68.0	0.0	0.0	0.0	14.	-1029.1	21.5	12	0.0	0.0	0.0
13.	-359.4	7.6	1068.2	0.0	0.0	0.0	16.	-1029.1	21.5	21	471			12.	-310.1	20.0	-68.0	0.0	0.0	0.0	15.	-1029.1	21.5	12	0.0	0.0	0.0
14.	-359.2	7.6	1068.2	0.0	0.0	0.0	17.	-1029.1	21.5	22	471			13.	-310.0	20.0	-68.0	0.0	0.0	0.0	16.	-1029.1	21.5	12	0.0	0.0	0.0
15.	-359.0	7.6	1068.2	0.0	0.0	0.0	18.	-1029.1	21.5	23	471			14.	-309.9	20.0	-68.0	0.0	0.0	0.0	17.	-1029.1	21.5	12	0.0	0.0	0.0
16.	-358.8	7.6	1068.2	0.0	0.0	0.0	19.	-1029.1	21.5	24	471			15.	-309.8	20.0	-68.0	0.0	0.0	0.0	18.	-1029.1	21.5	12	0.0	0.0	0.0
17.	-358.6	7.6	1068.2	0.0	0.0	0.0	20.	-1029.1	21.5	25	471			16.	-309.7	20.0	-68.0	0.0	0.0	0.0	19.	-1029.1	21.5	12	0.0	0.0	0.0
18.	-358.4	7.6	1068.2	0.0	0.0	0.0	21.	-1029.1	21.5	26	471			17.	-309.6	20.0	-68.0	0.0	0.0	0.0	20.	-1029.1	21.5	12	0.0	0.0	0.0
19.	-358.2	7.6	1068.2	0.0	0.0	0.0	22.	-1029.1	21.5	27	471			18.	-309.5	20.0	-68.0	0.0	0.0	0.0	21.	-1029.1	21.5	12	0.0	0.0	0.0
20.	-358.0	7.6	1068.2	0.0	0.0	0.0	23.	-1029.1	21.5	28	471			19.	-309.4	20.0	-68.0	0.0	0.0	0.0	22.	-1029.1	21.5	12	0.0	0.0	0.0
21.	-357.8	7.6	1068.2	0.0	0.0	0.0	24.	-1029.1	21.5	29	471			20.	-309.3	20.0	-68.0	0.0	0.0	0.0	23.	-1029.1	21.5	12	0.0	0.0	0.0
22.	-357.6	7.6	1068.2	0.0	0.0	0.0	25.	-1029.1	21.5	30	471			21.	-309.2	20.0	-68.0	0.0	0.0	0.0	24.	-1029.1	21.5	12	0.0	0.0	0.0
23.	-357.4	7.6	1068.2	0.0	0.0	0.0	26.	-1029.1	21.5	31	471			22.	-309.1	20.0	-68.0	0.0	0.0	0.0	25.	-1029.1	21.5	12	0.0	0.0	0.0
24.	-357.2	7.6	1068.2	0.0	0.0	0.0	27.	-1029.1	21.5	32	471			23.	-309.0	20.0	-68.0	0.0	0.0	0.0	26.	-1029.1	21.5	12	0.0	0.0	0.0
25.	-357.0	7.6	1068.2	0.0	0.0	0.0	28.	-1029.1	21.5	33	471			24.	-308.9	20.0	-68.0	0.0	0.0	0.0	27.	-1029.1	21.5	12	0.0	0.0	0.0
26.	-356.8	7.6	1068.2	0.0	0.0	0.0	29.	-1029.1	21.5	34	471			25.	-308.8	20.0	-68.0	0.0	0.0	0.0	28.	-1029.1	21.5	12	0.0	0.0	0.0
27.	-356.6	7.6	1068.2	0.0	0.0	0.0	30.	-1029.1	21.5	35	471			26.	-308.7	20.0	-68.0	0.0	0.0	0.0	29.	-1029.1	21.5	12	0.0	0.0	0.0
28.	-356.4	7.6	1068.2	0.0	0.0	0.0	31.	-1029.1	21.5	36	471			27.	-308.6	20.0	-68.0	0.0	0.0	0.0	30.	-1029.1	21.5	12	0.0	0.0	0.0
29.	-356.2	7.6	1068.2	0.0	0.0	0.0	32.	-1029.1	21.5	37	471			28.	-308.5	20.0	-68.0	0.0	0.0	0.0	31.	-1029.1	21.5	12	0.0	0.0	0.0
30.	-356.0	7.6	1068.2	0.0	0.0	0.0	33.	-1029.1	21.5	38	471			29.	-308.4	20.0	-68.0	0.0	0.0	0.0	32.	-1029.1	21.5	12	0.0	0.0	0.0
31.	-355.8	7.6	1068.2	0.0	0.0	0.0	34.	-1029.1	21.5	39	471			30.	-308.3	20.0	-68.0	0.0	0.0	0.0	33.	-1029.1	21.5	12	0.0	0.0	0.0
32.	-355.6	7.6	1068.2	0.0	0.0	0.0	35.	-1029.1	21.5	40	471			31.	-308.2	20.0	-68.0	0.0	0.0	0.0	34.	-1029.1	21.5	12	0.0	0.0	0.0
33.	-355.4	7.6	1068.2	0.0	0.0	0.0	36.	-1029.1	21.5	41	471			32.	-308.1	20.0	-68.0	0.0	0.0	0.0	35.	-1029.1	21.5	12	0.0	0.0	0.0
34.	-355.2	7.6	1068.2	0.0	0.0	0.0	37.	-1029.1	21.5	42	471			33.	-308.0	20.0	-68.0	0.0	0.0	0.0	36.	-1029.1	21.5	12	0.0	0.0	0.0
35.	-355.0	7.6	1068.2	0.0	0.0	0.0	38.	-1029.1	21.5	43	471			34.	-307.9	20.0	-68.0	0.0	0.0	0.0	37.	-1029.1	21.5	12	0.0	0.0	0.0
36.	-354.8	7.6	1068.2	0.0	0.0	0.0	39.	-1029.1	21.5	44	471			35.	-307.8	20.0	-68.0	0.0	0.0	0.0	38.	-1029.1	21.5	12	0.0	0.0	0.0
37.	-354.6	7.6	1068.2	0.0	0.0	0.0	40.	-1029.1	21.5	45	471			36.	-307.7	20.0	-68.0	0.0	0.0	0.0	39.	-1029.1	21.5	12	0.0	0.0	0.0
38.	-354.4	7.6	1068.2	0.0	0.0	0.0	41.	-1029.1	21.5	46	471			37.	-307.6	20.0	-68.0	0.0	0.0	0.0	40.	-1029.1	21.5	12	0.0	0.0	0.0
39.	-354.2	7.6	1068.2	0.0	0.0	0.0	42.	-1029.1	21.5	47	471			38.	-307.5	20.0	-68.0	0.0	0.0	0.0	41.	-1029.1	21.5	12	0.0	0.0	0.0
40.	-354.0	7.6	1068.2	0.0	0.0	0.0	43.	-1029.1	21.5	48	471			39.	-307.4	20.0	-68.0	0.0	0.0	0.0	42.	-1029.1	21.5	12	0.0	0.0	0.0
41.	-353.8	7.6	1068.2	0.0	0.0	0.0	44.	-1029.1	21.5	49	471			40.	-307.3	20.0	-68.0	0.0	0.0	0.0	43.	-1029.1	21.5	12	0.0	0.0	0.0
42.	-353.6	7.6	1068.2	0.0	0.0	0.0	45.	-1029.1	21.5	50	471			41.	-307.2	20.0	-68.0	0.0	0.0	0.0	44.	-1029.1	21.5	12	0.0	0.0	0.0
43.	-353.4	7.6	1068.2	0.0	0.0	0.0	46.	-1029.1	21.5	51	471			42.	-307.1	20.0	-68.0	0.0	0.0	0.0	45.	-1029.1	21.5	12	0.0	0.0	0.0
44.	-353.2	7.6	1068.2	0.0	0.0	0.0	47.	-1029.1	21.5	52	471			43.	-307.0	20.0	-68.0	0.0	0.0	0.0	46.	-1029.1	21.5	12	0.0	0.0	0.0
45.	-353.0	7.6	1068.2	0.0	0.0	0.0	48.	-1029.1	21.5	53	471			44.	-306.9	20.0	-68.0	0.0	0.0	0.0	47.	-1029.1	21.5	12	0.0	0.0	0.0
46.	-352.8	7.6	1068.2	0.0	0.0	0.0	49.	-1029.1	21.5	54	471			45.	-306.8	20.0	-68.0	0.0	0.0	0.0	48.	-1029.1	21.5	12	0.0	0.0	0.0
47.	-352.6	7.6	1068.2	0.0	0.0	0.0	50.	-1029.1	21.5	55	471			46.	-306.7	20.0	-68.0	0.0	0.0	0.0	49.	-1029.1	21.5	12	0.0	0.0	0.0
48.	-352.4	7.6	1068.2	0.0	0.0	0.0	51.	-1029.1	21.5	56	471			47.	-306.6	20.0	-68.0	0.0	0.0	0.0	50.	-1029.1	21.5	12	0.0	0.0	0.0
49.	-352.2	7.6	1068.2	0.0	0.0	0.0	52.	-1029.1	21.5	57	471			48.	-306.5	20.0	-68.0	0.0	0.0	0.0	51.	-1029.1	21.5	12	0.0	0.0	0.0
50.	-352.0	7.6	1068.2	0.0	0.0	0.0	53.	-1029.1	21.5	58	471			49.	-306.4	20.0	-68.0	0.0	0.0	0.0	52.	-1029.1	21.5	12	0.0	0.0	0.0
51.	-351.8	7.6	1068.2	0.0	0.0	0.0	54.	-1029.1	21.5	59	471			50.	-306.3	20.0	-68.0	0.0	0.0	0.0	53.	-1029.1	21.5	12	0.0	0.0	0.0
52.	-351.6	7.6	1068.2	0.0	0.0	0.0	55.	-1029.1	21.5	60	471			51.	-306.2	20.0	-68.0	0.0	0.0	0.0	54.	-1029.1	21.5	12	0.0	0.0	0.0
53.	-351.4	7.6	1068.2	0.0	0.0	0.0	56.	-1029.1	21.5	61	471			52.	-306.1	20.0	-68.0	0.0	0.0	0.0	55.	-1029.1	21.5	12	0.0	0.0	0.0
54.	-351.2	7.6	1068.2	0.0	0.0	0.0	57.	-1029.1	21.5	62	471			53.	-306.0	20.0	-68.0	0.0	0.0	0.0	56.	-1029.1	21.5	12	0.0	0.0	0.0
55.	-351.0	7.6	1068.2	0.0																							

34/136

128.	-4385.2	86.5	-1.8	-0.3	-347.3	-10222.8	16.	-61.2	-843.1	-36.9	-184.7	600.4	-2540.6	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		20.	-89.9	-18.6	-73.9	-11.6	239.0	-14348.6
	-4461.1	39.3	-3.0	-4.8	-306.9	-8042.6		-59.3	-817.4	-41.6	-208.1	676.5	-2483.3		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2		-116.4	-18.1	-69.7	-11.0	95.1	-14495.2
	-4559.1	86.5	-1.8	-0.0	-259.2	-8501.8	33.	-59.3	-850.8	-36.9	-184.7	600.4	-2540.6		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2	ASTA	-116.4	-18.1	-69.7	-11.0	95.1	-14495.2
170.	-4335.0	39.3	-3.0	-4.8	-179.6	-6371.7		-59.3	-824.3	-41.6	-208.1	1353.0	-15797.4	16.	NORM	TYT	TZZ	TORS	MYT	MZZ		PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
	-4333.1	86.5	-1.8	-0.0	-196.9	-2863.8		-61.2	-857.0	-36.9	-184.7	1801.2	-30367.6		0.	-65.2	121.3	-3.1	-76.7	-183.1	-15996.3		-6.2	121.3	-3.1	-76.7	-183.1	-15996.3
213.	-4009.0	39.3	-3.0	-4.8	-811.3	-808.3		-61.2	-851.3	-36.9	-184.7	1801.2	-30367.6	33.	NORM	TYT	TZZ	TORS	MYT	MZZ		16.	-6.2	121.3	-3.1	-76.7	-183.1	-15996.3
	-4307.0	86.5	-1.8	-0.3	-121.7	808.3	65.	-61.2	-863.9	-36.9	-184.7	2041.2	-44150.0		0.	-65.2	121.3	-3.1	-76.7	-183.1	-15996.3	ASTA	-6.2	121.3	-3.1	-76.7	-183.1	-15996.3
255.	-4382.9	39.3	-3.0	-4.8	-918.3	-808.3		-61.2	-851.3	-36.9	-184.7	1801.2	-30367.6	49.	NORM	TYT	TZZ	TORS	MYT	MZZ		16.	-6.2	121.3	-3.1	-76.7	-183.1	-15996.3
	-4281.0	86.5	-1.8	-0.0	-46.5	-870.8	81.	-61.2	-870.8	-36.9	-184.7	300.2	-58245.0		0.	-65.2	121.3	-3.1	-76.7	-183.1	-15996.3	PROGR.	-6.2	121.3	-3.1	-76.7	-183.1	-15996.3
298.	-4356.9	39.3	-3.0	-4.8	202.3	-1358.9		-59.3	-845.1	-41.6	-208.1	338.2	-56990.2	65.	NORM	TYT	TZZ	TORS	MYT	MZZ		33.	-6.2	115.1	-3.1	-76.7	-183.1	-15996.3
	-4254.9	86.5	-1.8	-0.0	-46.5	-870.8	98.	-59.3	-871.8	-36.9	-184.7	338.2	-56990.2		0.	-65.2	121.3	-3.1	-76.7	-183.1	-15996.3	ASTA	-6.2	117.0	-3.2	-75.4	-171.4	-10322.6
340.	-4330.8	39.3	-3.0	-4.8	329.6	312.7		-59.3	-852.0	-41.6	-208.1	405.9	-70279.6	81.	NORM	TYT	TZZ	TORS	MYT	MZZ		49.	-6.2	114.0	-3.2	-75.4	-171.4	-10322.6
	-4028.9	86.5	-1.8	-0.0	-46.5	-870.8	114.	-59.3	-884.7	-36.9	-184.7	405.9	-70279.6		0.	-65.2	121.3	-3.1	-76.7	-183.1	-15996.3	PROGR.	-6.2	114.0	-3.2	-75.4	-171.4	-10322.6
ASTA	-4330.8	39.3	-3.0	-4.8	329.6	312.7		-59.3	-852.0	-41.6	-208.1	405.9	-70279.6	98.	NORM	TYT	TZZ	TORS	MYT	MZZ		65.	-6.2	114.0	-3.2	-75.4	-171.4	-10322.6
PROGR.	-4330.8	39.3	-3.0	-4.8	329.6	312.7		-59.3	-852.0	-41.6	-208.1	405.9	-70279.6	114.	NORM	TYT	TZZ	TORS	MYT	MZZ		81.	-6.2	114.0	-3.2	-75.4	-171.4	-10322.6
0.	-11921.1	22.8	-32.2	0.0	-3314.7	16129.2	130.	-59.3	-865.9	-41.6	-208.1	5411.8	-98396.0	ASTA	-100.0	1219.2	-6.7	-33.7	-109.6	-1079.1		114.	-5.2	101.7	-3.2	-75.4	-171.4	-10322.6
21.	-11082.8	130.1	-36.9	0.0	-3996.5	4029.3	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		98.	-6.2	102.9	-3.1	-75.4	-171.4	-10322.6
21.	-11082.8	130.1	-36.9	0.0	-3996.5	4029.3	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
41.	-11895.9	130.1	-36.9	0.0	-3175.4	1410.6	0.	1.1	-2569.0	247.8	1258.1	4803.1	-138932.2	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
	-11895.9	130.1	-36.9	0.0	-3175.4	1410.6	0.	1.1	-2569.0	247.8	1258.1	4803.1	-138932.2	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
62.	-11882.2	22.8	-32.2	0.0	-120.1	17542.3	0.	1.1	-2569.0	247.8	1258.1	4803.1	-138932.2	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
63.	-11884.8	130.1	-36.9	0.0	-1653.3	3954.9	3.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
82.	-11870.6	22.8	-32.2	0.0	-655.2	18013.3	3.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
	-11870.6	22.8	-32.2	0.0	-655.2	18013.3	3.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
103.	-11857.9	22.8	-32.2	0.0	9.6	8484.4	3.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
	-11857.9	22.8	-32.2	0.0	9.6	8484.4	3.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
124.	-11845.3	22.8	-32.2	0.0	674.5	18955.4	5.	0.6	-2562.0	328.0	1210.7	3772.0	-147995.4	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
	-11846.9	130.1	-36.9	0.0	629.9	12003.2	6.	1.1	-2571.6	247.8	1258.1	3254.3	-154996.6	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
144.	-11832.6	22.8	-32.2	0.0	1339.4	19405.4	6.	1.1	-2571.6	247.8	1258.1	3254.3	-154996.6	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
	-11834.2	130.1	-36.9	0.0	1391.0	14685.9	6.	1.1	-2572.2	247.8	1258.1	2944.6	-158211.5	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
165.	-11820.0	22.8	-32.2	0.0	2004.2	19897.4	9.	1.1	-2572.2	247.8	1258.1	2944.6	-158211.5	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
	-11821.6	130.1	-36.9	0.0	2152.0	17368.7	9.	1.1	-2572.2	247.8	1258.1	2634.8	-161427.0	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
ASTA	-11821.6	130.1	-36.9	0.0	2152.0	17368.7	9.	1.1	-2572.2	247.8	1258.1	2634.8	-161427.0	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
PROGR.	-11821.6	130.1	-36.9	0.0	2152.0	17368.7	9.	1.1	-2572.2	247.8	1258.1	2634.8	-161427.0	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	99.8	-3.1	-75.4	-171.4	-10322.6
0.	-5996.5	-76.3	6.5	6.0	2197.7	15102.9	0.	0.6	-2562.0	328.0	1210.7	2542.1	-157025.9	81.	NORM	TYT	TZZ	TORS	MYT	MZZ		81.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
	-5977.2	-25.0	7.0	0.0	2197.7	15102.9	0.	0.6	-2562.0	328.0	1210.7	2542.1	-157025.9	114.	NORM	TYT	TZZ	TORS	MYT	MZZ		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
42.	-5970.8	-76.3	6.5	6.0	1927.0	11097.3	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
	-5951.6	-25.0	7.0	0.0	1807.3	5505.4	0.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
84.	-5949.1	-76.3	6.5	6.0	1694.4	1276.3	1.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
	-5925.9	-25.0	7.0	0.0	1787.3	4458.6	1.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
126.	-5916.1	-76.3	6.5	6.0	1480.6	1480.6	3.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
	-5900.2	-25.0	7.0	0.0	1495.2	3411.8	3.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
209.	-5884.9	-76.3	6.5	6.0	844.3	-875.4	3.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
	-5848.9	-25.0	7.0	0.0	844.3	-875.4	3.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
251.	-5842.4	-76.3	6.5	6.0	573.7	-407.0	3.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	PROGR.	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
	-5823.2	-25.0	7.0	0.0	573.7	-407.0	3.	-54.7	5807.8	289.8	1394.4	2232.8	-151817.3	ASTA	-100.0	1219.2	-6.7	-33.7	109.6	-1079.1		114.	-6.2	101.7	-3.2	-75.4	-171.4	-10322.6
293.	-5816.8	-76.3																										

[illegible]

[illegible]

[illegible]

126.	-44.5	-11.7	-0.3	20.5	77.1	-7099.9	130.	69.8	989.4	-19.4	-97.2	0.0	-349.2	3.	-180.2	1072.2	-3.5	-21.3	-101.1	-31368.5	231.	-5.6	0.0	0.0	0.0	0.0
168.	25.0	106.9	-0.3	20.5	91.1	-5100.4	131.	69.8	989.4	-19.4	-97.2	0.0	-349.2	4.	-180.2	1071.7	-3.5	-21.3	-96.7	-3003.6	264.	-5.6	0.0	0.0	0.0	0.0
210.	94.4	137.1	-0.3	20.5	101.1	-5100.4	132.	69.8	989.4	-19.4	-97.2	0.0	-349.2	5.	-180.2	1071.2	-3.5	-21.3	-91.2	-2683.3	297.	-5.6	0.0	0.0	0.0	0.0
252.	163.9	343.9	-0.3	20.5	119.2	-13840.3	133.	69.8	989.4	-19.4	-97.2	0.0	-349.2	6.	-180.2	1070.6	-3.5	-21.3	-87.9	-2730.7	330.	-5.6	0.0	0.0	0.0	0.0
294.	233.4	462.4	-0.3	20.5	133.2	-20781.5	134.	69.8	989.4	-19.4	-97.2	0.0	-349.2	7.	-180.2	1070.1	-3.5	-21.3	-83.5	-2402.7	363.	-5.6	0.0	0.0	0.0	0.0
336.	301.9	581.0	-0.3	20.5	147.2	-27617.7	135.	69.8	989.4	-19.4	-97.2	0.0	-349.2	8.	-180.2	1069.6	-3.5	-21.3	-79.0	-2067.5	396.	-5.6	0.0	0.0	0.0	0.0
378.	370.4	699.5	-0.3	20.5	161.3	-34543.9	136.	69.8	989.4	-19.4	-97.2	0.0	-349.2	9.	-180.2	1069.1	-3.5	-21.3	-74.5	-1732.3	429.	-5.6	0.0	0.0	0.0	0.0
420.	439.9	818.0	-0.3	20.5	175.4	-41470.1	137.	69.8	989.4	-19.4	-97.2	0.0	-349.2	10.	-180.2	1068.6	-3.5	-21.3	-69.5	-1397.1	462.	-5.6	0.0	0.0	0.0	0.0
462.	509.4	936.5	-0.3	20.5	189.5	-48396.3	138.	69.8	989.4	-19.4	-97.2	0.0	-349.2	11.	-180.2	1068.1	-3.5	-21.3	-64.5	-1061.9	495.	-5.6	0.0	0.0	0.0	0.0
504.	579.9	1055.0	-0.3	20.5	203.6	-55322.5	139.	69.8	989.4	-19.4	-97.2	0.0	-349.2	12.	-180.2	1067.6	-3.5	-21.3	-59.5	-726.7	528.	-5.6	0.0	0.0	0.0	0.0
546.	649.4	1170.5	-0.3	20.5	217.7	-62248.7	140.	69.8	989.4	-19.4	-97.2	0.0	-349.2	13.	-180.2	1067.1	-3.5	-21.3	-54.5	-391.5	561.	-5.6	0.0	0.0	0.0	0.0
588.	719.9	1286.0	-0.3	20.5	231.8	-69174.9	141.	69.8	989.4	-19.4	-97.2	0.0	-349.2	14.	-180.2	1066.6	-3.5	-21.3	-49.5	-50.3	594.	-5.6	0.0	0.0	0.0	0.0
630.	789.4	1401.5	-0.3	20.5	245.9	-76101.1	142.	69.8	989.4	-19.4	-97.2	0.0	-349.2	15.	-180.2	1066.1	-3.5	-21.3	-44.5	40.9	627.	-5.6	0.0	0.0	0.0	0.0
672.	859.9	1517.0	-0.3	20.5	260.0	-83027.3	143.	69.8	989.4	-19.4	-97.2	0.0	-349.2	16.	-180.2	1065.6	-3.5	-21.3	-39.5	151.3	660.	-5.6	0.0	0.0	0.0	0.0
714.	929.4	1632.5	-0.3	20.5	274.1	-89953.5	144.	69.8	989.4	-19.4	-97.2	0.0	-349.2	17.	-180.2	1065.1	-3.5	-21.3	-34.5	262.7	693.	-5.6	0.0	0.0	0.0	0.0
756.	999.9	1748.0	-0.3	20.5	288.2	-96879.7	145.	69.8	989.4	-19.4	-97.2	0.0	-349.2	18.	-180.2	1064.6	-3.5	-21.3	-29.5	374.1	726.	-5.6	0.0	0.0	0.0	0.0
798.	1069.4	1863.5	-0.3	20.5	302.3	-103805.9	146.	69.8	989.4	-19.4	-97.2	0.0	-349.2	19.	-180.2	1064.1	-3.5	-21.3	-24.5	485.5	759.	-5.6	0.0	0.0	0.0	0.0
840.	1139.9	1979.0	-0.3	20.5	316.4	-110732.1	147.	69.8	989.4	-19.4	-97.2	0.0	-349.2	20.	-180.2	1063.6	-3.5	-21.3	-19.5	596.9	792.	-5.6	0.0	0.0	0.0	0.0
882.	1209.4	2094.5	-0.3	20.5	330.5	-117658.3	148.	69.8	989.4	-19.4	-97.2	0.0	-349.2	21.	-180.2	1063.1	-3.5	-21.3	-14.5	708.3	825.	-5.6	0.0	0.0	0.0	0.0
924.	1279.9	2210.0	-0.3	20.5	344.6	-124584.5	149.	69.8	989.4	-19.4	-97.2	0.0	-349.2	22.	-180.2	1062.6	-3.5	-21.3	-9.5	819.7	858.	-5.6	0.0	0.0	0.0	0.0
966.	1349.4	2325.5	-0.3	20.5	358.7	-131510.7	150.	69.8	989.4	-19.4	-97.2	0.0	-349.2	23.	-180.2	1062.1	-3.5	-21.3	-4.5	931.1	891.	-5.6	0.0	0.0	0.0	0.0
1008.	1419.9	2441.0	-0.3	20.5	372.8	-138436.9	151.	69.8	989.4	-19.4	-97.2	0.0	-349.2	24.	-180.2	1061.6	-3.5	-21.3	0.5	1042.5	924.	-5.6	0.0	0.0	0.0	0.0
1050.	1489.4	2556.5	-0.3	20.5	386.9	-145363.1	152.	69.8	989.4	-19.4	-97.2	0.0	-349.2	25.	-180.2	1061.1	-3.5	-21.3	5.5	1153.9	957.	-5.6	0.0	0.0	0.0	0.0
1092.	1559.9	2672.0	-0.3	20.5	401.0	-152289.3	153.	69.8	989.4	-19.4	-97.2	0.0	-349.2	26.	-180.2	1060.6	-3.5	-21.3	10.5	1265.3	990.	-5.6	0.0	0.0	0.0	0.0
1134.	1629.4	2787.5	-0.3	20.5	415.1	-159215.5	154.	69.8	989.4	-19.4	-97.2	0.0	-349.2	27.	-180.2	1060.1	-3.5	-21.3	15.5	1376.7	1023.	-5.6	0.0	0.0	0.0	0.0
1176.	1699.9	2903.0	-0.3	20.5	429.2	-166141.7	155.	69.8	989.4	-19.4	-97.2	0.0	-349.2	28.	-180.2	1059.6	-3.5	-21.3	20.5	1488.1	1056.	-5.6	0.0	0.0	0.0	0.0
1218.	1769.4	3018.5	-0.3	20.5	443.3	-173067.9	156.	69.8	989.4	-19.4	-97.2	0.0	-349.2	29.	-180.2	1059.1	-3.5	-21.3	25.5	1599.5	1089.	-5.6	0.0	0.0	0.0	0.0
1260.	1839.9	3134.0	-0.3	20.5	457.4	-179994.1	157.	69.8	989.4	-19.4	-97.2	0.0	-349.2	30.	-180.2	1058.6	-3.5	-21.3	30.5	1710.9	1122.	-5.6	0.0	0.0	0.0	0.0
1302.	1909.4	3249.5	-0.3	20.5	471.5	-186920.3	158.	69.8	989.4	-19.4	-97.2	0.0	-349.2	31.	-180.2	1058.1	-3.5	-21.3	35.5	1822.3	1155.	-5.6	0.0	0.0	0.0	0.0
1344.	1979.9	3365.0	-0.3	20.5	485.6	-193846.5	159.	69.8	989.4	-19.4	-97.2	0.0	-349.2	32.	-180.2	1057.6	-3.5	-21.3	40.5	1933.7	1188.	-5.6	0.0	0.0	0.0	0.0
1386.	2049.4	3480.5	-0.3	20.5	499.7	-200772.7	160.	69.8	989.4	-19.4	-97.2	0.0	-349.2	33.	-180.2	1057.1	-3.5	-21.3	45.5	2045.1	1221.	-5.6	0.0	0.0	0.0	0.0
1428.	2119.9	3596.0	-0.3	20.5	513.8	-207698.9	161.	69.8	989.4	-19.4	-97.2	0.0	-349.2	34.	-180.2	1056.6	-3.5	-21.3	50.5	2156.5	1254.	-5.6	0.0	0.0	0.0	0.0
1470.	2189.4	3711.5	-0.3	20.5	527.9	-214625.1	162.	69.8	989.4	-19.4	-97.2	0.0	-349.2	35.	-180.2	1056.1	-3.5	-21.3	55.5	2267.9	1287.	-5.6	0.0	0.0	0.0	0.0
1512.	2259.9	3827.0	-0.3	20.5	542.0	-221551.3	163.	69.8	989.4	-19.4	-97.2	0.0	-349.2	36.	-180.2	1055.6	-3.5	-21.3	60.5	2379.3	1320.	-5.6	0.0	0.0	0.0	0.0
1554.	2329.4	3942.5	-0.3	20.5	556.1	-228477.5	164.	69.8	989.4	-19.4	-97.2	0.0	-349.2	37.	-180.2	1055.1	-3.5	-21.3	65.5	2490.7	1353.	-5.6	0.0	0.0	0.0	0.0
1596.	2399.9	4058.0	-0.3	20.5	570.2	-235403.7	165.	69.8	989.4	-19.4	-97.2	0.0	-349.2	38.	-180.2	1054.6	-3.5	-21.3	70.5	2602.1	1386.	-5.6	0.0	0.0	0.0	0.0
1638.	2469.4	4173.5	-0.3	20.5	584.3	-242329.9	166.	69.8	989.4	-19.4	-97.2	0.0	-349.2	39.	-180.2	1054.1	-3.5	-21.3	75.5	2713.5	1419.	-5.6	0.0	0.0	0.0	0.0
1680.	2539.9	4289.0	-0.3	20.5	598.4	-249256.1	167.	69.8	989.4	-19.4	-97.2	0.0	-349.2	40.	-180.2	1053.6	-3.5	-21.3	80.5	2824.9	1452.	-5.6	0.0	0.0	0.0	0.0
1722.	2609.4	4404.5	-0.3	20.5	612.5	-256182.3	168.	69.8	989.4	-19.4	-97.2	0.0	-349.2	41.	-180.2	1053.1	-3.5	-21.3	85.5	2936.3	1485.	-5.6	0.0	0.0	0.0	0.0
1764.	2679.9	4520.0	-0.3	20.5	626.6	-263108.5	169.	69.8	989.4	-19.4	-97.2	0.0	-349.2	42.	-180.2	1052.6	-3.5	-21.3	90.5	3047.7	1518.	-5.6	0.0	0.0	0.0	0.0
1806.	2749.4	4635.5	-0.3	20.5	640.7	-270034.7	170.	69.8	989.4	-19.4	-97.2	0.0	-349.2	43.	-180.2	1052.1	-3.5	-21.3	95.5	3159.1	1551.	-5.6	0.0	0.0	0.0	0.0
1848.	2819.9	4751.0	-0.3	20.5	654.8	-276960.9	171.	69.8	989.4	-19.4	-97.2	0.0	-349.2	44.	-180.2	1051.6	-3.5	-21.3	100.5	3270.5	1584.	-5.6	0.0	0.0	0.0	0.0
1890.	2889.4	4866.5	-0.3	20.5	668.9	-283887.1	172.	69.8	989.4	-19.4	-97.2	0.0	-349.2	45.	-180.2	1051.1	-3.5	-21.3	105.5	3381.9	1617.	-5.6	0.0	0.0	0.0	0.0
1932.	2959.9	4982.0	-0.3	20.5	683.0	-290813.3	173.	69.8	989.4	-19.4	-97.2	0.0	-349.2	46.	-180.2	1050.6	-3.5	-21.3	110.5	3493.3	1650.	-5.6	0.0	0.0	0.0	0.0
1974.	3029.4	5097.5	-0.3	20.5	697.1	-297739.5	174.	69.8	989.4	-19.4	-97.2	0.0	-349.2	47.	-180.2	1050.1	-3.5	-21.3	115.5	3604.7	1683.	-5.6	0.0	0.0	0.0	0.0
2016.	3099.9	5213.0	-0.3	20.5	711.2	-304665.7	175.	69.8	989.4	-19.4	-97.2	0.0	-349.2	48.	-180.2	1049.6	-3.5	-21.3	120.5	3716.1	1716.	-5.6	0.0	0.0	0.0	0.0
2058.	3169.4	5328.5	-0.3	20.5	725.3	-311591.9	176.	69.8	989.4	-19.4	-97.2	0.0	-349.2	49.	-180.2	1049.1	-3.5	-21.3	125.5	3827.5	1749.	-5.6	0.0	0.0	0.0	0.0
2100.	3239.9	5444.0	-0.3	20.5	739.4	-318518.1	177.	69.8	989.4	-19.4	-97.2	0.0	-349.2	50.	-180.2	1048.6	-3.5	-21.3	130.5	3938.9	1782.	-5.6	0.0	0.0	0.0	0.0
2142.	3309.4	5559.5	-0.3	20.5	753.5	-325444.3	178.	69.8	989.4	-19.4	-97.2	0.0	-349.2	51.	-180.2	1048.1	-3.5	-21.3	135.5	4050.3	1815.	-5.6	0.0	0.0	0.0	0.0
2184.	3379.9	5675.0	-0.3	20.5	767.6	-332370.																				

1.	-1292.0	-15.7	-1.6	0.0	-6.9	68.8	248.	-1762.5	-5.1	4.7	0.0	-2322.4	7084.3	0.	280.2	302.6	0.1	0.0	0.0	209.	-873.2	0.3	16.8	2.5	2390.2	3189.1								
1.	-1291.9	-15.7	-1.6	0.0	-5.9	58.9	289.	-1737.3	-5.1	4.7	0.0	-2317.5	6875.1	29.	280.2	208.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1							
2.	-1291.7	-15.7	-1.6	0.0	-5.9	58.9	330.	-1721.0	-5.1	4.7	0.0	-2317.0	6875.0	58.	280.2	208.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1							
3.	-1291.6	-15.7	-1.6	0.0	-3.9	39.3	Asta	117	742	739	MY	NZZ	739	86.	280.2	20.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1							
3.	-1291.5	-15.7	-1.6	0.0	-2.9	29.5	PROGR.	117	742	739	MY	NZZ	739	115.	280.2	-73.5	0.1	0.0	-17.0	13147.7	Asta	150	780	953	MY	NZZ	780							
3.	-1291.4	-15.7	-1.6	0.0	-1.9	19.5	0.	-1304.6	-31.4	-53.9	0.0	-7828.6	17780.5	144.	280.2	-107.5	0.1	0.0	-21.3	9717.7	PROGR.	150	780	953	MY	NZZ	780							
4.	-1291.2	-15.7	-1.6	0.0	-1.0	9.8	41.	-1889.3	-31.4	-53.9	0.0	-9605.9	16485.6	173.	280.2	-261.5	0.1	0.0	-25.6	3546.0	0.	-4.8	0.0	0.0	0.4	0.0	0.4							
5.	-1291.0	-15.7	-1.6	0.0	-0.9	3.4	13.	-1864.0	-31.4	-53.9	0.0	-7702.7	15393.2	201.	280.2	-355.5	0.1	0.0	-29.8	1327.5	135.	-4.8	0.0	0.0	0.4	0.0	0.4							
Asta	101	742	739	MY	NZZ	739	124.	-1838.7	-31.4	-53.9	0.0	-1160.4	13895.8	230.	280.2	-449.5	0.1	0.0	-34.1	-16893.6	307.	-4.8	0.0	0.0	0.4	0.1	0.7							
PROGR.	101	742	739	MY	NZZ	739	365.	-1813.4	-31.4	-53.9	0.0	-1062.4	12600.9	Asta	134	750	468	MY	NZZ	468	601.	-4.8	0.0	0.0	0.4	0.1	0.7							
1.	-1252.4	-5.4	-1.5	0.0	-7.5	27.0	178.	-1781.1	-31.4	-53.9	0.0	-303.5	2878.6	PROGR.	134	750	468	MY	NZZ	468	135.	-4.8	0.0	0.0	0.4	0.1	0.7							
1.	-1252.3	-5.4	-1.5	0.0	-6.5	23.6	248.	-1762.5	-31.4	-53.9	0.0	-9507.9	10011.1	0.	-110.0	-305.0	-0.2	0.0	0.0	0.0	368.	-4.8	0.0	0.0	0.4	0.2	0.7							
1.	-1252.2	-5.4	-1.5	0.0	-5.5	20.2	289.	-1737.3	-31.4	-53.9	0.0	-7702.7	15393.2	0.	-110.0	-305.0	-0.2	0.0	0.0	0.0	202.	-4.8	0.0	0.0	0.4	0.2	0.7							
2.	-1252.0	-5.4	-1.5	0.0	-4.7	16.9	330.	-1762.5	-31.4	-53.9	0.0	-9953.4	7421.3	58.	-110.0	-313.0	-0.2	0.0	10.2	-12039.9	368.	-4.8	0.0	0.0	0.4	0.3	0.7							
2.	-1251.9	-5.4	-1.5	0.0	-3.7	12.5	Asta	119	742	739	MY	NZZ	739	Asta	119	742	739	MY	NZZ	739	289.	-4.8	0.0	0.0	0.4	0.3	0.7							
3.	-1251.7	-5.4	-1.5	0.0	-2.8	10.1	PROGR.	119	742	739	MY	NZZ	739	115.	-110.0	73.0	-0.2	0.0	20.3	-13229.0	Asta	154	780	973	212	MY	NZZ	780						
4.	-1251.6	-5.4	-1.5	0.0	-1.9	6.7	0.	106.7	-134.6	9.1	26.0	1052.1	36841.0	144.	-110.0	367.0	-0.2	0.0	25.4	-9779.5	PROGR.	154	780	973	212	MY	NZZ	780						
4.	-1251.5	-5.4	-1.5	0.0	-0.9	3.4	18.	106.7	-134.6	9.1	26.0	1052.1	36841.0	201.	-110.0	367.0	-0.2	0.0	30.5	-3827.4	58.	2.6	-188.0	0.0	0.0	0.4	0.0							
5.	-1251.3	-5.4	-1.5	0.0	0.0	0.0	35.	106.7	-256.3	9.1	26.0	733.0	30000.8	230.	-110.0	355.0	-0.2	0.0	35.6	5277.5	29.	2.6	-282.0	0.0	0.0	0.0	-949.4	0.0						
Asta	102	742	739	MY	NZZ	739	52.	106.7	-317.1	9.1	26.0	574.4	24893.9	0.	-110.0	449.0	-0.2	0.0	40.0	16785.0	58.	2.6	-188.0	0.0	0.0	0.0	0.0	-16216.2	0.0					
PROGR.	102	742	739	MY	NZZ	739	70.	106.7	-387.9	9.1	26.0	413.8	18802.3	Asta	136	749	469	469	469	469	86.	2.6	-94.0	0.0	0.0	0.0	0.0	-20270.2	0.0					
0.	-954.3	7.5	-57.1	0.0	-283.6	-37.5	88.	106.7	-438.8	9.1	26.0	254.2	11736.1	PROGR.	136	749	469	469	469	469	115.	2.6	0.0	0.0	0.0	0.0	0.0	-2162.6	0.0					
1.	-954.2	7.5	-57.1	0.0	-249.9	-32.8	105.	106.7	-499.6	9.1	26.0	34.6	3545.3	0.	142.9	240.9	0.0	0.0	0.0	0.0	144.	2.6	94.0	0.0	0.0	0.0	0.0	-20270.2	0.0					
1.	-954.1	7.5	-57.1	0.0	-214.2	-28.1	123.	106.7	-560.4	9.1	26.0	-65.0	-5730.1	29.	142.9	146.9	0.0	0.0	-5.8	5573.8	173.	2.6	188.0	0.0	0.0	0.0	0.0	-16216.2	0.0					
2.	-953.9	7.5	-57.1	0.0	-178.5	-23.4	140.	106.7	-631.3	9.1	26.0	-224.6	-16007.1	0.	142.9	146.9	0.0	0.0	-11.5	8444.8	201.	2.6	282.0	0.0	0.0	0.0	0.0	0.0	-949.4	0.0				
3.	-953.8	7.5	-57.1	0.0	-142.8	-18.7	Asta	120	745	746	MY	NZZ	746	86.	142.9	-41.1	0.2	0.0	-17.3	8613.2	230.	2.6	376.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
4.	-953.5	7.5	-57.1	0.0	-71.4	-9.4	PROGR.	120	745	746	MY	NZZ	746	115.	142.9	-135.2	0.2	0.0	-23.0	1616.8	PROGR.	120	745	746	MY	NZZ	746	211	MY	NZZ	746			
4.	-953.4	7.5	-57.1	0.0	-35.7	-4.7	0.	-229.4	-278.1	1.1	-659.0	0.0	604.7	144.	142.9	-229.2	0.2	0.0	-28.8	841.8	PROGR.	120	745	746	MY	NZZ	746	211	MY	NZZ	746			
Asta	104	746	747	MY	NZZ	747	16.	-229.4	-285.0	1.1	-659.0	-17.2	-3971.0	173.	142.9	-323.2	0.2	0.0	-34.6	-7029.9	0.	-25.2	305.7	0.2	0.0	0.0	0.0	0.0	0.0					
PROGR.	104	746	747	MY	NZZ	747	33.	-229.4	-292.0	1.1	-659.0	-34.5	-8659.3	201.	142.9	-417.2	0.2	0.0	-40.3	-17493.3	58.	-25.2	117.6	0.2	0.0	0.0	0.0	0.0	-14.8	14200.9				
0.	-790.0	-30.8	1698.2	0.0	8490.9	153.8	49.	-229.4	-298.9	1.1	-659.0	-51.7	-13460.2	230.	142.9	-511.2	0.2	0.0	-46.1	-13085.4	58.	-25.2	117.6	0.2	0.0	0.0	0.0	0.0	-9.9	12170.0				
1.	-790.0	-30.8	1698.2	0.0	8490.9	153.8	81.	-229.4	-312.8	1.1	-659.0	-86.2	-23399.5	PROGR.	137	753	754	MY	NZZ	754	86.	-25.2	23.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
1.	-790.0	-30.8	1698.2	0.0	8490.9	153.8	98.	-229.4	-319.7	1.1	-659.0	-103.4	-28338.1	0.	-6.8	352.1	-1.9	-4.6	-220.0	-8487.8	115.	-25.2	-70.4	0.2	0.0	0.0	0.0	0.0	-19.7	13529.2				
2.	-789.9	-30.8	1698.2	0.0	8490.9	153.8	115.	-229.4	-318.6	1.1	-659.0	-124.4	-33361.1	PROGR.	137	753	754	MY	NZZ	754	144.	-25.2	-164.4	0.2	0.0	0.0	0.0	0.0	0.0	-24.7	10354.7			
2.	-789.8	-30.8	1698.2	0.0	8490.9	153.8	130.	-229.4	-333.5	1.1	-659.0	-137.9	-39152.8	0.	-6.8	352.1	-1.9	-4.6	-220.0	-8487.8	173.	-25.2	-164.4	0.2	0.0	0.0	0.0	0.0	0.0	-24.7	10354.7			
3.	-789.6	-30.8	1698.2	0.0	8490.9	153.8	Asta	121	747	747	MY	NZZ	747	58.	-6.8	164.1	-1.9	-4.6	-100.4	6315.6	201.	-25.2	-352.4	0.2	0.0	0.0	0.0	0.0	0.0	-34.6	-4702.2			
3.	-789.5	-30.8	1698.2	0.0	8490.9	153.8	PROGR.	121	747	747	MY	NZZ	747	115.	-6.8	-23.9	-1.9	-4.6	-1.2	10380.2	230.	-25.2	-352.4	0.2	0.0	0.0	0.0	0.0	0.0	0.0	-34.6	-4702.2		
4.	-789.3	-30.8	1698.2	0.0	8490.9	153.8	0.	-90.6	412.8	-7.6	-75.0	-97.9	-3539.9	PROGR.	138	750	995	993	993	993	65.	-7.8	-268.4	2.5	12.5	-162.7	-16504.3	11.	-7.8	-273.5	2.5	12.5	-162.7	-16504.3
4.	-789.2	-30.8	1698.2	0.0	8490.9	153.8	61.	-90.6	385.0	-7.6	-75.0	-97.9	-3539.9	0.	-90.6	-118.0	-1.9	-4.6	85.5	6340.5	81.	-7.8	-268.4	2.5	12.5	-162.7	-16504.3	11.	-7.8	-273.5	2.5	12.5	-162.7	-16504.3
5.	-789.1	-30.8	1698.2	0.0	8490.9	153.8	81.	-90.6	378.1	-7.6	-75.0	-97.9	-3539.9	Asta	138	750	995	993	993	993	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8
Asta	106	746	747	MY	NZZ	747	88.	-90.6	371.2	-7.6	-75.0	-97.9	-3539.9	PROGR.	138	750	995	993	993	993	81.	0.0	465.5	-1.0	3.5	-20.9	-908.7	81.	0.0	465.5	-1.0	3.5	-20.9	-908.7
PROGR.	106	746	747	MY	NZZ	747	114.	-90.6	364.3	-7.6	-75.0	-97.9	-3539.9	0.	-90.6	-118.0	-1.9	-4.6	85.5	6340.5	49.	0.0	479.4	-1.0	3.5	-11.8	-16163.1	49.	0.0	479.4	-1.0	3.5	-11.8	-16163.1
0.	-1311.1	218.9	-5793.2	0.0	-2896.8	-109.7	130.	-90.6	357.3	-7.6	-75.0	-97.9	-3539.9	PROGR.	138	750	995	993	993	993	65.	-7.8	-268.4	2.5	12.5	-162.7	-16504.3	65.	-7.8	-268.4	2.5	12.5	-162.7	-16504.3
1.	-1311.0	218.9	-5793.2	0.0	-2896.8	-109.7	Asta	122	748	748	MY	NZZ	748	115.	-90.6	-118.0	-1.9	-4.6	85.5	6340.5	81.	-7.8	-268.4	2.5	12.5	-162.7	-16504.3	81.	-7.8	-268.4	2.5	12.5	-162.7	-16504.3
2.	-1310.8	218.9	-5793.2	0.0	-2896.8	-109.7	PROGR.	122	748	748	MY	NZZ	748	130.	-90.6	-118.0	-1.9	-4.6	85.5	6340.5	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8
3.	-1310.5	218.9	-5793.2	0.0	-2896.8	-109.7	0.	-90.6	357.3	-7.6	-75.0	-97.9	-3539.9	Asta	138	750	995	993	993	993	65.	-7.8	-268.4	2.5	12.5	-162.7	-16504.3	65.	-7.8	-268.4	2.5	12.5	-162.7	-16504.3
4.	-1310.4	218.9	-5793.2																															

PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-125.8	0.0	0.0	0.0	0.0	0.0
34.	-125.8	0.0	0.0	0.0	0.0	0.0
67.	-125.8	0.0	0.0	0.0	0.0	0.0
101.	-125.8	0.0	0.0	0.0	0.0	0.0
135.	-125.8	0.0	0.0	0.0	0.0	0.0
168.	-125.8	0.0	0.0	0.0	0.0	0.0
202.	-125.8	0.0	0.0	0.0	0.0	0.0
236.	-125.8	0.0	0.0	0.0	0.0	0.0
269.	-125.8	0.0	0.0	0.0	0.0	0.0
Asta	168	noth	753	953		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	19.4	0.0	0.0	0.0	0.0	0.0
51.	19.4	0.0	0.0	0.0	0.0	0.0
103.	19.4	0.0	0.0	0.0	0.0	0.0
154.	19.4	0.0	0.0	0.0	0.0	0.0
205.	19.4	0.0	0.0	0.0	0.0	0.0
257.	19.4	0.0	0.0	0.0	0.0	0.0
308.	19.4	0.0	0.0	0.0	0.0	0.0
359.	19.4	0.0	0.0	0.0	0.0	0.0
410.	19.4	0.0	0.0	0.0	0.0	0.0
Asta	169	noth	741	754		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	142.5	0.0	0.0	0.0	0.0	0.0
51.	142.5	0.0	0.0	0.0	0.0	0.0
102.	142.5	0.0	0.0	0.0	0.0	0.0
152.	142.5	0.0	0.0	0.0	0.0	0.0
203.	142.5	0.0	0.0	0.0	0.0	0.0
254.	142.5	0.0	0.0	0.0	0.0	0.0
305.	142.5	0.0	0.0	0.0	0.0	0.0
356.	142.5	0.0	0.0	0.0	0.0	0.0
406.	142.5	0.0	0.0	0.0	0.0	0.0
Asta	170	noth	740	953		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-553.3	10.5	1202.5	0.0	6012.6	-52.7
1.	-553.2	10.5	1202.5	0.0	5261.0	-46.1
2.	-553.1	10.5	1202.5	0.0	4509.4	-39.6
3.	-552.9	10.5	1202.5	0.0	3757.9	-33.0
4.	-552.8	10.5	1202.5	0.0	3006.3	-26.4
5.	-552.7	10.5	1202.5	0.0	2254.7	-19.8
6.	-552.5	10.5	1202.5	0.0	1503.1	-13.2
7.	-552.4	10.5	1202.5	0.0	751.6	-6.6
8.	-552.2	10.5	1202.5	0.0	0.0	0.0
Asta	171	noth	738	975		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-377.1	-17.3	0.0	0.0	0.0	86.6
1.	-377.0	-17.3	0.0	0.0	0.0	75.7
2.	-376.8	-17.3	0.0	0.0	0.0	64.9
3.	-376.7	-17.3	0.0	0.0	0.0	54.1
4.	-376.6	-17.3	0.0	0.0	0.0	43.3
5.	-376.4	-17.3	0.0	0.0	0.0	32.5
6.	-376.3	-17.3	0.0	0.0	0.0	21.6
7.	-376.2	-17.3	0.0	0.0	0.0	10.8
8.	-376.0	-17.3	0.0	0.0	0.0	0.0
Asta	172	noth	40	978		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-10163.7	-888.8	-17.5	0.0	-6752.6	103550.9
15.	-10070.0	-888.8	-17.5	0.0	-6489.1	90218.3
30.	-9976.2	-888.8	-17.5	0.0	-6226.3	76885.8
45.	-9882.5	-888.8	-17.5	0.0	-5963.4	63553.2
60.	-9788.7	-888.8	-17.5	0.0	-5700.6	50220.7
75.	-9695.0	-888.8	-17.5	0.0	-5437.7	36888.1
90.	-9601.2	-888.8	-17.5	0.0	-5174.9	23555.6
105.	-9507.5	-888.8	-17.5	0.0	-4912.0	10223.0
120.	-9413.7	-888.8	-17.5	0.0	-4649.1	-3109.5
Asta	173	noth	954	37		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-8791.4	26.8	-41.2	0.0	-19951.1	-375.7
15.	-8697.6	26.8	-41.2	0.0	-19332.9	-339.8
30.	-8603.9	26.8	-41.2	0.0	-18714.6	-299.9
45.	-8510.1	26.8	-41.2	0.0	-18096.3	-260.0
60.	-8416.4	26.8	-41.2	0.0	-17478.0	-218.0
75.	-8322.6	26.8	-41.2	0.0	-16859.8	-176.1
90.	-8228.9	26.8	-41.2	0.0	-16241.5	-134.2
105.	-8135.1	26.8	-41.2	0.0	-15623.2	-92.3
120.	-8041.4	26.8	-41.2	0.0	-15004.9	-50.4
Asta	174	noth	958	734		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-4015.0	703.6	-67.5	0.0	-15330.2	-8302.4
15.	-3921.2	703.6	-67.5	0.0	-14317.6	-7247.9
30.	-3827.5	703.6	-67.5	0.0	-13305.1	-6193.4
45.	-3733.7	703.6	-67.5	0.0	-12292.5	-5137.9
60.	-3640.0	703.6	-67.5	0.0	-11279.9	-4083.4
75.	-3546.2	703.6	-67.5	0.0	-10267.4	-3028.9
90.	-3452.5	703.6	-67.5	0.0	-9254.8	-1971.4
105.	-3358.7	703.6	-67.5	0.0	-8242.2	-917.9
120.	-3265.0	703.6	-67.5	0.0	-7229.7	1395.5
Asta	175	noth	960	741		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-2546.8	460.8	-138.5	0.0	-24959.2	-5642.5
15.	-2453.0	460.8	-138.5	0.0	-22881.7	-4953.1
30.	-2359.3	460.8	-138.5	0.0	-20804.2	-4263.7
45.	-2265.5	460.8	-138.5	0.0	-18726.7	-3573.3
60.	-2171.8	460.8	-138.5	0.0	-16649.2	-2876.9
75.	-2078.0	460.8	-138.5	0.0	-14571.7	-2180.5
90.	-1984.3	460.8	-138.5	0.0	-12494.3	-1494.1
105.	-1890.5	460.8	-138.5	0.0	-10416.8	-802.7
120.	-1796.8	460.8	-138.5	0.0	-8339.3	-111.3
Asta	176	noth	959	742		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-2664.6	-317.1	6.9	0.0	-16951.0	3023.6
15.	-2570.8	-317.1	6.9	0.0	-17054.7	2546.0
30.	-2477.1	-317.1	6.9	0.0	-17158.4	2070.5
45.	-2383.3	-317.1	6.9	0.0	-17262.1	1594.0
60.	-2289.6	-317.1	6.9	0.0	-17365.8	1117.5
75.	-2195.8	-317.1	6.9	0.0	-17469.4	641.0
90.	-2102.1	-317.1	6.9	0.0	-17573.1	168.4
105.	-2008.3	-317.1	6.9	0.0	-17676.8	-307.1
120.	-1914.6	-317.1	6.9	0.0	-17780.5	-782.6
Asta	178	noth	37	19		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	0.0	380.1	0.6	-1421.6	20.0	-3827.8
1.	0.0	380.6	0.6	-1421.6	19.2	-3351.7
3.	0.0	380.1	0.6	-1421.6	18.5	-2876.6
4.	0.0	379.5	0.6	-1421.6	17.7	-2401.6
5.	0.0	379.0	0.6	-1421.6	16.9	-1927.5
6.	0.0	378.5	0.6	-1421.6	16.2	-1454.4
8.	0.0	377.9	0.6	-1421.6	15.4	-981.4
9.	0.0	377.4	0.6	-1421.6	14.6	-509.3
10.	0.0	376.9	0.6	-1421.6	13.8	-37.9
Asta	181	noth	957	28		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-540.5	14.8	257.8	0.0	30940.0	-1778.1
15.	-540.5	14.8	257.8	0.0	2707.5	-155.8
30.	-540.5	14.8	257.8	0.0	2320.0	-133.5
45.	-540.5	14.8	257.8	0.0	1933.5	-111.1
60.	-540.5	14.8	257.8	0.0	1547.0	-89.0
75.	-540.5	14.8	257.8	0.0	1160.5	-66.8
90.	-540.5	14.8	257.8	0.0	773.0	-44.5
105.	-540.5	14.8	257.8	0.0	387.5	-22.3
120.	-540.5	14.8	257.8	0.0	0.0	0.0

[illegible]

COLLETTAZIONE		COSTI RETTANGOLARI		CONFEZIONE			
misura		9 Torcette_add_Y		9 Torcette_add_Y			
misura		9 Torcette_add_Y		9 Torcette_add_Y			
GC810	415	55	=	0.	51	=	0.
GC811	416	55	=	0.	51	=	0.
GC812	417	55	=	0.	51	=	0.
GC813	418	55	=	0.	51	=	0.
GC814	419	55	=	0.	51	=	0.
GC815	420	55	=	0.	51	=	0.
GC816	421	55	=	0.	51	=	0.
GC817	422	55	=	0.	51	=	0.
GC818	423	55	=	0.	51	=	0.
GC819	424	55	=	0.	51	=	0.
GC820	425	55	=	0.	51	=	0.
GC821	426	55	=	0.	51	=	0.
GC822	427	55	=	0.	51	=	0.
GC823	428	55	=	0.	51	=	0.
GC824	429	55	=	0.	51	=	0.
GC825	430	55	=	0.	51	=	0.
GC826	431	55	=	0.	51	=	0.
GC827	432	55	=	0.	51	=	0.
GC828	433	55	=	0.	51	=	0.
GC829	434	55	=	0.	51	=	0.
GC830	435	55	=	0.	51	=	0.
GC831	436	55	=	0.	51	=	0.
GC832	437	55	=	0.	51	=	0.
GC833	438	55	=	0.	51	=	0.
GC834	439	55	=	0.	51	=	0.
GC835	440	55	=	0.	51	=	0.
GC836	441	55	=	0.	51	=	0.
GC837	442	55	=	0.	51	=	0.
GC838	443	55	=	0.	51	=	0.
GC839	444	55	=	0.	51	=	0.
GC840	445	55	=	0.	51	=	0.
GC841	446	55	=	0.	51	=	0.
GC842	447	55	=	0.	51	=	0.
GC843	448	55	=	0.	51	=	0.
GC844	449	55	=	0.	51	=	0.
GC845	450	55	=	0.	51	=	0.
GC846	451	55	=	0.	51	=	0.
GC847	452	55	=	0.	51	=	0.
GC848	453	55	=	0.	51	=	0.
GC849	454	55	=	0.	51	=	0.
GC850	455	55	=	0.	51	=	0.

COMBINAZIONE

GUICIO	454	SS =	11.1	SI =	11.1
GUICIO	455	SS =	10.9	SI =	10.9
GUICIO	456	SS =	12.8	SI =	12.8
GUICIO	457	SS =	4.6	SI =	4.6
GUICIO	458	SS =	5.8	SI =	5.8
GUICIO	459	SS =	5.4	SI =	5.4
GUICIO	460	SS =	4.1	SI =	4.1
GUICIO	461	SS =	3.1	SI =	3.1
GUICIO	462	SS =	6.5	SI =	6.5
GUICIO	463	SS =	5.1	SI =	5.1
GUICIO	464	SS =	3.8	SI =	3.8
GUICIO	465	SS =	4.2	SI =	4.2
GUICIO	466	SS =	3.7	SI =	3.7
GUICIO	467	SS =	3.5	SI =	3.5
GUICIO	468	SS =	4.5	SI =	4.5
GUICIO	469	SS =	4.0	SI =	4.0
GUICIO	470	SS =	4.1	SI =	4.1
GUICIO	471	SS =	3.5	SI =	3.5
GUICIO	472	SS =	4.4	SI =	4.4
GUICIO	473	SS =	4.3	SI =	4.3
GUICIO	474	SS =	4.2	SI =	4.2
GUICIO	475	SS =	2.8	SI =	2.8
GUICIO	476	SS =	4.1	SI =	4.1
GUICIO	477	SS =	3.1	SI =	3.1
GUICIO	478	SS =	2.9	SI =	2.9
GUICIO	479	SS =	1.2	SI =	1.2
GUICIO	480	SS =	2.9	SI =	2.9
GUICIO	481	SS =	1.2	SI =	1.2
GUICIO	482	SS =	5.7	SI =	5.7
GUICIO	483	SS =	4.7	SI =	4.7
GUICIO	484	SS =	3.7	SI =	3.7
GUICIO	485	SS =	4.9	SI =	4.9
GUICIO	486	SS =	4.3	SI =	4.3
GUICIO	487	SS =	6.2	SI =	6.2
GUICIO	488	SS =	2.2	SI =	2.2
GUICIO	489	SS =	6.8	SI =	6.8
GUICIO	490	SS =	21.7	SI =	21.7
GUICIO	491	SS =	19.4	SI =	19.4
GUICIO	492	SS =	6.0	SI =	6.0
GUICIO	493	SS =	7.3	SI =	7.3
GUICIO	494	SS =	1.4	SI =	1.4
GUICIO	495	SS =	6.0	SI =	6.0
GUICIO	496	SS =	17.3	SI =	17.3
GUICIO	497	SS =	11.3	SI =	11.3
GUICIO	498	SS =	2.5	SI =	2.5
GUICIO	499	SS =	4.8	SI =	4.8
tensione max =		21.7	guscio =	490	

SOLLECITAZIONE GUICIO RETTANGOLARE
CASO DI CARICO : 3 SLU VENTOF

N. 5 CONDIZIONI ANALISI STATICA
1 peso proprio + 1.30
2 permanenti + 1.50
3 A'var. abitazione + 1.50
4 neve (-1000h/m) + 1.50
5 vento + 1.50

1) +1.30*c001 +1.50*c002 +1.50*c003 +1.50*c004 +1.50*c005
2) +1.30*c001 +1.50*c002 +1.50*c003 +1.50*c004 -1.50*c005
Unità di misura: SI,SS [daN/cm2]

GUICIO	415	SS =	3.5	SI =	3.5
		SS =	2.9	SI =	2.9
GUICIO	416	SS =	2.6	SI =	2.6
		SS =	1.9	SI =	1.9
GUICIO	417	SS =	9.5	SI =	9.5
		SS =	7.6	SI =	7.6
GUICIO	418	SS =	9.6	SI =	9.6
		SS =	8.0	SI =	8.0
GUICIO	419	SS =	24.2	SI =	24.2
		SS =	19.0	SI =	19.0
GUICIO	420	SS =	17.6	SI =	17.6
		SS =	16.6	SI =	16.6
GUICIO	421	SS =	18.2	SI =	18.2
		SS =	22.2	SI =	22.2
GUICIO	422	SS =	16.6	SI =	16.6

COMBINAZIONE

		SS =	17.1	SI =	17.1
GUICIO	423	SS =	6.9	SI =	6.9
		SS =	8.4	SI =	8.4
GUICIO	424	SS =	7.5	SI =	7.5
		SS =	8.7	SI =	8.7
GUICIO	425	SS =	2.4	SI =	2.4
		SS =	3.1	SI =	3.1
GUICIO	426	SS =	1.6	SI =	1.6
		SS =	2.0	SI =	2.0
GUICIO	427	SS =	6.6	SI =	6.6
		SS =	5.7	SI =	5.7
GUICIO	428	SS =	8.1	SI =	8.1
		SS =	7.1	SI =	7.1
GUICIO	429	SS =	4.7	SI =	4.7
		SS =	4.4	SI =	4.4
GUICIO	430	SS =	10.9	SI =	10.9
		SS =	9.3	SI =	9.3
GUICIO	431	SS =	11.8	SI =	11.8
		SS =	10.2	SI =	10.2
GUICIO	432	SS =	9.9	SI =	9.9
		SS =	9.0	SI =	9.0
GUICIO	433	SS =	15.5	SI =	15.5
		SS =	13.5	SI =	13.5
GUICIO	434	SS =	15.1	SI =	15.1
		SS =	13.7	SI =	13.7
GUICIO	435	SS =	22.4	SI =	22.4
		SS =	17.6	SI =	17.6
GUICIO	436	SS =	14.3	SI =	14.3
		SS =	13.2	SI =	13.2
GUICIO	437	SS =	14.6	SI =	14.6
		SS =	13.6	SI =	13.6
GUICIO	438	SS =	17.6	SI =	17.6
		SS =	20.6	SI =	20.6
GUICIO	439	SS =	8.8	SI =	8.8
		SS =	8.2	SI =	8.2
GUICIO	440	SS =	10.4	SI =	10.4
		SS =	10.5	SI =	10.5
GUICIO	441	SS =	9.2	SI =	9.2
		SS =	9.8	SI =	9.8
GUICIO	442	SS =	5.4	SI =	5.4
		SS =	6.8	SI =	6.8
GUICIO	443	SS =	7.3	SI =	7.3
		SS =	7.9	SI =	7.9
GUICIO	444	SS =	4.6	SI =	4.6
		SS =	5.3	SI =	5.3
GUICIO	445	SS =	3.7	SI =	3.7
		SS =	2.2	SI =	2.2
GUICIO	446	SS =	5.3	SI =	5.3
		SS =	3.4	SI =	3.4
GUICIO	447	SS =	4.0	SI =	4.0
		SS =	3.0	SI =	3.0
GUICIO	448	SS =	7.9	SI =	7.9
		SS =	5.1	SI =	5.1
GUICIO	449	SS =	9.3	SI =	9.3
		SS =	6.4	SI =	6.4
GUICIO	450	SS =	9.0	SI =	9.0
		SS =	6.6	SI =	6.6
GUICIO	451	SS =	17.1	SI =	17.1
		SS =	10.5	SI =	10.5
GUICIO	452	SS =	12.8	SI =	12.8
		SS =	10.3	SI =	10.3
GUICIO	453	SS =	19.6	SI =	19.6
		SS =	11.9	SI =	11.9
GUICIO	454	SS =	11.4	SI =	11.4
		SS =	12.1	SI =	12.1
GUICIO	455	SS =	11.8	SI =	11.8
		SS =	10.0	SI =	10.0
GUICIO	456	SS =	12.2	SI =	12.2

		SS =	13.9	SI =	13.9
GUICIO	457	SS =	4.2	SI =	4.2
		SS =	5.0	SI =	5.0
GUICIO	458	SS =	5.7	SI =	5.7
		SS =	5.9	SI =	5.9
GUICIO	459	SS =	5.4	SI =	5.4
		SS =	5.4	SI =	5.4
GUICIO	460	SS =	3.7	SI =	3.7
		SS =	4.5	SI =	4.5
GUICIO	461	SS =	3.0	SI =	3.0
		SS =	3.5	SI =	3.5
GUICIO	462	SS =	3.8	SI =	3.8
		SS =	9.5	SI =	9.5
GUICIO	463	SS =	4.1	SI =	4.1
		SS =	6.2	SI =	6.2
GUICIO	464	SS =	3.3	SI =	3.3
		SS =	4.5	SI =	4.5
GUICIO	465	SS =	5.4	SI =	5.4
		SS =	3.9	SI =	3.9
GUICIO	466	SS =	2.7	SI =	2.7
		SS =	5.6	SI =	5.6
GUICIO	467	SS =	3.1	SI =	3.1
		SS =	4.3	SI =	4.3
GUICIO	468	SS =	3.3	SI =	3.3
		SS =	5.7	SI =	5.7
GUICIO	469	SS =	6.3	SI =	6.3
		SS =	4.2	SI =	4.2
GUICIO	470	SS =	3.5	SI =	3.5
		SS =	4.8	SI =	4.8
GUICIO	471	SS =	4.1	SI =	4.1
		SS =	3.8	SI =	3.8
GUICIO	472	SS =	3.6	SI =	3.6
		SS =	5.5	SI =	5.5
GUICIO	473	SS =	3.6	SI =	3.6
		SS =	5.2	SI =	5.2
GUICIO	474	SS =	3.4	SI =	3.4
		SS =	5.1	SI =	5.1
GUICIO	475	SS =	1.9	SI =	1.9
		SS =	3.9	SI =	3.9
GUICIO	476	SS =	2.9	SI =	2.9
		SS =	5.4	SI =	5.4
GUICIO	477	SS =	2.1	SI =	2.1
		SS =	4.1	SI =	4.1
GUICIO	478	SS =	1.9	SI =	1.9
		SS =	4.8	SI =	4.8
GUICIO	479	SS =	0.4	SI =	0.4
		SS =	2.1	SI =	2.1
GUICIO	480	SS =	2.1	SI =	2.1
		SS =	5.8	SI =	5.8
GUICIO	481	SS =	1.2	SI =	1.2
		SS =	1.9	SI =	1.9
GUICIO	482	SS =	6.4	SI =	6.4
		SS =	6.9	SI =	6.9
GUICIO	483	SS =	4.0	SI =	4.0
		SS =	5.4	SI =	5.4
GUICIO	484	SS =	5.7	SI =	5.7
		SS =	3.0	SI =	3.0
GUICIO	485	SS =	4.2	SI =	4.2
		SS =	6.2	SI =	6.2
GUICIO	486	SS =	2.9	SI =	2.9
		SS =	5.8	SI =	5.8
GUICIO	487	SS =	10.3	SI =	10.3
		SS =	2.7	SI =	2.7
GUICIO	488	SS =	2.9	SI =	2.9
		SS =	1.4	SI =	1.4
GUICIO	489	SS =	8.2	SI =	8.2
		SS =	5.4	SI =	5.4
GUICIO	490	SS =	26.0	SI =	26.0
		SS =	17.8	SI =	17.8

GUICIO	491	SS =	19.3	SI =	19.3
		SS =	20.3	SI =	20.3
GUICIO	492	SS =	6.1	SI =	6.1
		SS =	5.8	SI =	5.8
GUICIO	493	SS =	3.8	SI =	3.8
		SS =	11.6	SI =	11.6
GUICIO	494	SS =	1.9	SI =	1.9
		SS =	1.0	SI =	1.0
GUICIO	495	SS =	8.3	SI =	8.3
		SS =	3.6	SI =	3.6
GUICIO	496	SS =	24.7	SI =	24.7
		SS =	9.9	SI =	9.9
GUICIO	497	SS =	6.1	SI =	6.1
		SS =	16.7	SI =	16.7
GUICIO	498	SS =	2.6	SI =	2.6
		SS =	4.2	SI =	4.2
GUICIO	499	SS =	4.2	SI =	4.2
		SS =	5.5	SI =	5.5
tensione max =		26.0	guscio =	490	

SOLLECITAZIONE GUICIO RETTANGOLARE
CASO DI CARICO : 4 SISMAX SLU

N. 2 CONDIZIONI ANALISI STATICA
6 SISMAX + 1.00
8 Torcente_add_X + 1.00
1) +1.00*c006 +1.00*c008
2) -1.00*c006 +1.00*c008
3) +1.00*c006 -1.00*c008
4) -1.00*c006 -1.00*c008
Unità di misura: SI,SS [daN/cm2]

GUSC10	415	SS =	0.4	SI =	0.4
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.4	SI =	0.4
GUSC10	416	SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
GUSC10	417	SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
GUSC10	418	SS =	0.6	SI =	0.6
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.6	SI =	0.6
GUSC10	419	SS =	2.5	SI =	2.5
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.5	SI =	2.5
GUSC10	420	SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
GUSC10	421	SS =	2.7	SI =	2.7
		SS =	3.1	SI =	3.1
		SS =	3.1	SI =	3.1
		SS =	2.7	SI =	2.7
GUSC10	422	SS =	1.9	SI =	1.9
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	1.9	SI =	1.9
GUSC10	423	SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
GUSC10	424	SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.6	SI =	0.6
GUSC10	425	SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6

QJSCIO 426 SS = 0.6 SI = 0.6
SS = 0.3 SI = 0.3
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.3 SI = 0.3
QJSCIO 427 SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
QJSCIO 428 SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
QJSCIO 429 SS = 0.7 SI = 0.7
SS = 0.8 SI = 0.8
SS = 0.8 SI = 0.8
SS = 0.7 SI = 0.7
QJSCIO 430 SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
QJSCIO 431 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 432 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 433 SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.1 SI = 1.1
QJSCIO 434 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 435 SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
QJSCIO 436 SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
QJSCIO 437 SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
QJSCIO 438 SS = 2.0 SI = 2.0
SS = 2.3 SI = 2.3
SS = 2.3 SI = 2.3
SS = 2.0 SI = 2.0
QJSCIO 439 SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.2 SI = 1.2
QJSCIO 440 SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
QJSCIO 441 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
QJSCIO 442 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2

QJSCIO 443 SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
QJSCIO 444 SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
QJSCIO 445 SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
QJSCIO 446 SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
QJSCIO 447 SS = 1.4 SI = 1.4
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.4 SI = 1.4
QJSCIO 448 SS = 1.4 SI = 1.4
SS = 1.5 SI = 1.5
SS = 1.5 SI = 1.5
SS = 1.4 SI = 1.4
QJSCIO 449 SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
QJSCIO 450 SS = 1.7 SI = 1.7
SS = 2.0 SI = 2.0
SS = 2.0 SI = 2.0
SS = 1.7 SI = 1.7
QJSCIO 451 SS = 3.4 SI = 3.4
SS = 3.7 SI = 3.7
SS = 3.7 SI = 3.7
SS = 3.4 SI = 3.4
QJSCIO 452 SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
QJSCIO 453 SS = 3.5 SI = 3.5
SS = 3.8 SI = 3.8
SS = 3.8 SI = 3.8
SS = 3.5 SI = 3.5
QJSCIO 454 SS = 2.7 SI = 2.7
SS = 3.2 SI = 3.2
SS = 3.2 SI = 3.2
SS = 2.7 SI = 2.7
QJSCIO 455 SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.2 SI = 1.2
QJSCIO 456 SS = 3.1 SI = 3.1
SS = 3.5 SI = 3.5
SS = 3.5 SI = 3.5
SS = 3.1 SI = 3.1
QJSCIO 457 SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.1 SI = 1.1
QJSCIO 458 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
QJSCIO 459 SS = 1.7 SI = 1.7
SS = 1.9 SI = 1.9
SS = 1.9 SI = 1.9
SS = 1.7 SI = 1.7

QJSCIO 460 SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
QJSCIO 461 SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
QJSCIO 462 SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
QJSCIO 463 SS = 1.3 SI = 1.3
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.3 SI = 1.3
QJSCIO 464 SS = 1.4 SI = 1.4
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.4 SI = 1.4
QJSCIO 465 SS = 1.7 SI = 1.7
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.7 SI = 1.7
QJSCIO 466 SS = 1.5 SI = 1.5
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.5 SI = 1.5
QJSCIO 467 SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
QJSCIO 468 SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
QJSCIO 469 SS = 2.1 SI = 2.1
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 2.1 SI = 2.1
QJSCIO 470 SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
QJSCIO 471 SS = 1.9 SI = 1.9
SS = 1.5 SI = 1.5
SS = 1.5 SI = 1.5
SS = 1.9 SI = 1.9
QJSCIO 472 SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
QJSCIO 473 SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
QJSCIO 474 SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
QJSCIO 475 SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
QJSCIO 476 SS = 0.4 SI = 0.4
SS = 0.5 SI = 0.5
SS = 0.5 SI = 0.5
SS = 0.4 SI = 0.4

QJSCIO 477 SS = 0.6 SI = 0.6
SS = 0.5 SI = 0.5
SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
QJSCIO 478 SS = 1.3 SI = 1.3
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.3 SI = 1.3
QJSCIO 479 SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
QJSCIO 480 SS = 1.4 SI = 1.4
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.4 SI = 1.4
QJSCIO 481 SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
QJSCIO 482 SS = 2.8 SI = 2.8
SS = 2.0 SI = 2.0
SS = 2.0 SI = 2.0
SS = 2.8 SI = 2.8
QJSCIO 483 SS = 1.0 SI = 1.0
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 1.0 SI = 1.0
QJSCIO 484 SS = 2.0 SI = 2.0
SS = 1.4 SI = 1.4
SS = 1.4 SI = 1.4
SS = 2.0 SI = 2.0
QJSCIO 485 SS = 1.3 SI = 1.3
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.3 SI = 1.3
QJSCIO 486 SS = 1.7 SI = 1.7
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.7 SI = 1.7
QJSCIO 487 SS = 2.5 SI = 2.5
SS = 1.7 SI = 1.7
SS = 1.7 SI = 1.7
SS = 2.5 SI = 2.5
QJSCIO 488 SS = 1.5 SI = 1.5
SS = 1.8 SI = 1.8
SS = 1.8 SI = 1.8
SS = 1.5 SI = 1.5
QJSCIO 489 SS = 1.9 SI = 1.9
SS = 2.1 SI = 2.1
SS = 2.1 SI = 2.1
SS = 1.9 SI = 1.9
QJSCIO 490 SS = 2.5 SI = 2.5
SS = 2.6 SI = 2.6
SS = 2.6 SI = 2.6
SS = 2.5 SI = 2.5
QJSCIO 491 SS = 1.8 SI = 1.8
SS = 1.9 SI = 1.9
SS = 1.9 SI = 1.9
SS = 1.8 SI = 1.8
QJSCIO 492 SS = 0.9 SI = 0.9
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 0.9 SI = 0.9
QJSCIO 493 SS = 2.4 SI = 2.4
SS = 1.8 SI = 1.8
SS = 1.8 SI = 1.8
SS = 2.4 SI = 2.4
QJSCIO 494 SS = 0.9 SI = 0.9

		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
QUSC10	495	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.2	SI =	2.2
QUSC10	496	SS =	3.5	SI =	3.5
		SS =	4.0	SI =	4.0
		SS =	4.0	SI =	4.0
		SS =	3.5	SI =	3.5
QUSC10	497	SS =	2.8	SI =	2.8
		SS =	3.2	SI =	3.2
		SS =	3.2	SI =	3.2
		SS =	2.8	SI =	2.8
QUSC10	498	SS =	1.4	SI =	1.4
		SS =	1.9	SI =	1.9
		SS =	1.9	SI =	1.9
		SS =	1.4	SI =	1.4
QUSC10	499	SS =	0.9	SI =	0.9
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
tensione max =		SS =	0.9	SI =	0.9
		4.0	guscio =	496	

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 5 S15WY SLU
N. 2 CONDIZIONI ANALISI STATICA
7 S15WY SLU +- 1.00
9 Torcente_add_Y +- 1.00
1) +1.00e+007 +1.00e+009
2) -1.00e+007 +1.00e+009
3) +1.00e+007 -1.00e+009
4) -1.00e+007 -1.00e+009
Unità di misura: SI, SS [daN/cm2]

COMBINAZIONE

		SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
QUSC10	425	SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
QUSC10	426	SS =	0.3	SI =	0.3
		SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
		SS =	0.3	SI =	0.3
QUSC10	427	SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
QUSC10	428	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	429	SS =	0.5	SI =	0.5
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.5	SI =	0.5
QUSC10	430	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	431	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	432	SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
QUSC10	433	SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
QUSC10	434	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	435	SS =	3.1	SI =	3.1
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	3.1	SI =	3.1
QUSC10	436	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSC10	437	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	438	SS =	3.0	SI =	3.0
		SS =	2.7	SI =	2.7
		SS =	2.7	SI =	2.7
		SS =	3.0	SI =	3.0
QUSC10	439	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	440	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
QUSC10	441	SS =	0.8	SI =	0.8
		SS =	0.7	SI =	0.7

		SS =	0.7	SI =	0.7
		SS =	0.8	SI =	0.8
QUSC10	442	SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
		SS =	2.2	SI =	2.2
		SS =	2.0	SI =	2.0
QUSC10	443	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
QUSC10	444	SS =	0.6	SI =	0.6
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.6	SI =	0.6
QUSC10	445	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
QUSC10	446	SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
QUSC10	447	SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
QUSC10	448	SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.5	SI =	1.5
QUSC10	449	SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
QUSC10	450	SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.4	SI =	1.4
QUSC10	451	SS =	4.5	SI =	4.5
		SS =	4.8	SI =	4.8
		SS =	4.8	SI =	4.8
		SS =	4.5	SI =	4.5
QUSC10	452	SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
QUSC10	453	SS =	4.2	SI =	4.2
		SS =	4.1	SI =	4.1
		SS =	4.1	SI =	4.1
		SS =	4.2	SI =	4.2
QUSC10	454	SS =	3.1	SI =	3.1
		SS =	3.4	SI =	3.4
		SS =	3.4	SI =	3.4
		SS =	3.1	SI =	3.1
QUSC10	455	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSC10	456	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
QUSC10	457	SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.6	SI =	0.6
QUSC10	458	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5

		SS =	0.5	SI =	0.5
QUSC10	459	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
QUSC10	460	SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
QUSC10	461	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSC10	462	SS =	3.1	SI =	3.1
		SS =	3.2	SI =	3.2
		SS =	3.2	SI =	3.2
		SS =	3.1	SI =	3.1
QUSC10	463	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSC10	464	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSC10	465	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
QUSC10	466	SS =	1.7	SI =	1.7
		SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
		SS =	1.7	SI =	1.7
QUSC10	467	SS =	1.0	SI =	1.0
		SS =	1.1	SI =	1.1
		SS =	1.1	SI =	1.1
		SS =	1.0	SI =	1.0
QUSC10	468	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSC10	469	SS =	2.6	SI =	2.6
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	2.6	SI =	2.6
QUSC10	470	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
QUSC10	471	SS =	2.4	SI =	2.4
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.4	SI =	2.4
QUSC10	472	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.1	SI =	2.1
QUSC10	473	SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
QUSC10	474	SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
QUSC10	475	SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2

		SS =	1.2	SI =	1.2
GUSCIO	476	SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
GUSCIO	477	SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
		SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
GUSCIO	478	SS =	2.2	SI =	2.2
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	479	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
GUSCIO	480	SS =	2.9	SI =	2.9
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	2.9	SI =	2.9
GUSCIO	481	SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
GUSCIO	482	SS =	2.4	SI =	2.4
		SS =	2.5	SI =	2.5
		SS =	2.5	SI =	2.5
		SS =	2.4	SI =	2.4
GUSCIO	483	SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
GUSCIO	484	SS =	2.2	SI =	2.2
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
GUSCIO	485	SS =	1.3	SI =	1.3
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
GUSCIO	486	SS =	1.9	SI =	1.9
		SS =	2.2	SI =	2.2
		SS =	2.2	SI =	2.2
		SS =	1.9	SI =	1.9
GUSCIO	487	SS =	2.9	SI =	2.9
		SS =	3.6	SI =	3.6
		SS =	3.6	SI =	3.6
		SS =	2.9	SI =	2.9
GUSCIO	488	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
GUSCIO	489	SS =	1.6	SI =	1.6
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
GUSCIO	490	SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
GUSCIO	491	SS =	3.8	SI =	3.8
		SS =	3.7	SI =	3.7
		SS =	3.7	SI =	3.7
		SS =	3.8	SI =	3.8
GUSCIO	492	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1

GUSCIO	493	SS =	4.2	SI =	4.2
		SS =	4.3	SI =	4.3
		SS =	4.3	SI =	4.3
		SS =	4.2	SI =	4.2
GUSCIO	494	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
GUSCIO	496	SS =	6.9	SI =	6.9
		SS =	7.3	SI =	7.3
		SS =	7.3	SI =	7.3
		SS =	6.9	SI =	6.9
GUSCIO	497	SS =	4.3	SI =	4.3
		SS =	5.0	SI =	5.0
		SS =	5.0	SI =	5.0
		SS =	4.3	SI =	4.3
GUSCIO	498	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.3	SI =	1.3
GUSCIO	499	SS =	0.7	SI =	0.7
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.7	SI =	0.7
tensione max = 7,3 guscio = 496					
SOLLECITAZIONE GUSCI RETTANGOLARI					
CASO DI CARICO : 6 SLU con SISMAS					
N. 3 CONDIZIONI ANALISI STATICA					
1 Presollecitazione + 1.00					
2 Permanente + 1.00					
3 Azione_distribuzione + 0.30					
N. 1 CASI DI CARICO					
4 SISMAS SLU 1.00					
1) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.001					
2) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.002					
3) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.003					
4) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.004					
Unità di misura: SI,SS (kN/cm2)					
GUSCIO	415	SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.1	SI =	1.1
GUSCIO	416	SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
GUSCIO	417	SS =	3.5	SI =	3.5
		SS =	2.6	SI =	2.6
		SS =	3.4	SI =	3.4
		SS =	2.5	SI =	2.5
GUSCIO	418	SS =	3.6	SI =	3.6
		SS =	2.5	SI =	2.5
		SS =	3.5	SI =	3.5
		SS =	2.4	SI =	2.4
GUSCIO	419	SS =	9.2	SI =	9.2
		SS =	5.8	SI =	5.8
		SS =	9.0	SI =	9.0
		SS =	5.5	SI =	5.5
GUSCIO	420	SS =	7.5	SI =	7.5
		SS =	4.1	SI =	4.1
		SS =	7.6	SI =	7.6
		SS =	4.0	SI =	4.0
GUSCIO	421	SS =	9.5	SI =	9.5
		SS =	4.2	SI =	4.2
		SS =	9.9	SI =	9.9
		SS =	4.8	SI =	4.8
GUSCIO	422	SS =	7.6	SI =	7.6
		SS =	3.7	SI =	3.7
		SS =	7.7	SI =	7.7

GUSCIO	423	SS =	3.9	SI =	3.9
		SS =	3.3	SI =	3.3
		SS =	2.1	SI =	2.1
		SS =	3.5	SI =	3.5
GUSCIO	424	SS =	2.3	SI =	2.3
		SS =	3.4	SI =	3.4
		SS =	2.0	SI =	2.0
		SS =	3.6	SI =	3.6
GUSCIO	425	SS =	2.2	SI =	2.2
		SS =	1.4	SI =	1.4
		SS =	0.9	SI =	0.9
		SS =	1.4	SI =	1.4
GUSCIO	426	SS =	1.0	SI =	1.0
		SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
GUSCIO	427	SS =	2.8	SI =	2.8
		SS =	1.9	SI =	1.9
		SS =	2.9	SI =	2.9
		SS =	1.9	SI =	1.9
GUSCIO	428	SS =	3.3	SI =	3.3
		SS =	2.1	SI =	2.1
		SS =	3.4	SI =	3.4
		SS =	2.1	SI =	2.1
GUSCIO	429	SS =	2.1	SI =	2.1
		SS =	1.4	SI =	1.4
		SS =	2.2	SI =	2.2
		SS =	1.4	SI =	1.4
GUSCIO	430	SS =	3.8	SI =	3.8
		SS =	3.4	SI =	3.4
		SS =	3.9	SI =	3.9
		SS =	3.4	SI =	3.4
GUSCIO	431	SS =	4.3	SI =	4.3
		SS =	3.4	SI =	3.4
		SS =	4.4	SI =	4.4
		SS =	3.4	SI =	3.4
GUSCIO	432	SS =	3.9	SI =	3.9
		SS =	2.5	SI =	2.5
		SS =	4.0	SI =	4.0
		SS =	2.6	SI =	2.6
GUSCIO	433	SS =	5.2	SI =	5.2
		SS =	5.5	SI =	5.5
		SS =	5.3	SI =	5.3
		SS =	5.5	SI =	5.5
GUSCIO	434	SS =	5.6	SI =	5.6
		SS =	4.7	SI =	4.7
		SS =	5.7	SI =	5.7
		SS =	4.8	SI =	4.8
GUSCIO	435	SS =	7.8	SI =	7.8
		SS =	6.3	SI =	6.3
		SS =	7.6	SI =	7.6
		SS =	6.2	SI =	6.2
GUSCIO	436	SS =	4.8	SI =	4.8
		SS =	5.0	SI =	5.0
		SS =	5.0	SI =	5.0
		SS =	5.1	SI =	5.1
GUSCIO	437	SS =	5.6	SI =	5.6
		SS =	4.5	SI =	4.5
		SS =	5.7	SI =	5.7
		SS =	4.7	SI =	4.7
GUSCIO	438	SS =	7.9	SI =	7.9
		SS =	5.2	SI =	5.2
		SS =	8.4	SI =	8.4
		SS =	5.7	SI =	5.7
GUSCIO	439	SS =	3.3	SI =	3.3
		SS =	2.8	SI =	2.8
		SS =	3.5	SI =	3.5
		SS =	3.1	SI =	3.1

GUSCIO	457	SS = 1.9	SI = 1.9
		SS = 2.4	SI = 2.4
		SS = 1.7	SI = 1.7
		SS = 2.2	SI = 2.2
GUSCIO	458	SS = 2.2	SI = 2.2
		SS = 2.9	SI = 2.9
		SS = 2.2	SI = 2.2
		SS = 2.8	SI = 2.8
GUSCIO	459	SS = 1.8	SI = 1.8
		SS = 3.4	SI = 3.4
		SS = 1.9	SI = 1.9
		SS = 3.3	SI = 3.3
GUSCIO	460	SS = 1.8	SI = 1.8
		SS = 2.1	SI = 2.1
		SS = 1.8	SI = 1.8
		SS = 2.2	SI = 2.2
GUSCIO	461	SS = 1.8	SI = 1.8
		SS = 1.8	SI = 1.8
		SS = 1.7	SI = 1.7
		SS = 1.9	SI = 1.9
GUSCIO	462	SS = 2.2	SI = 2.2
		SS = 4.4	SI = 4.4
		SS = 2.0	SI = 2.0
		SS = 4.3	SI = 4.3
GUSCIO	463	SS = 2.2	SI = 2.2
		SS = 2.7	SI = 2.7
		SS = 2.1	SI = 2.1
		SS = 2.8	SI = 2.8
GUSCIO	464	SS = 2.1	SI = 2.1
		SS = 2.2	SI = 2.2
		SS = 2.0	SI = 2.0
		SS = 2.3	SI = 2.3
GUSCIO	465	SS = 2.5	SI = 2.5
		SS = 2.8	SI = 2.8
		SS = 2.2	SI = 2.2
		SS = 2.6	SI = 2.6
GUSCIO	466	SS = 2.0	SI = 2.0
		SS = 2.4	SI = 2.4
		SS = 1.6	SI = 1.6
		SS = 2.4	SI = 2.4
GUSCIO	467	SS = 2.0	SI = 2.0
		SS = 2.2	SI = 2.2
		SS = 1.9	SI = 1.9
		SS = 2.4	SI = 2.4
GUSCIO	468	SS = 2.2	SI = 2.2
		SS = 2.2	SI = 2.2
		SS = 1.9	SI = 1.9
		SS = 2.2	SI = 2.2
GUSCIO	469	SS = 2.6	SI = 2.6
		SS = 2.6	SI = 2.6
		SS = 2.5	SI = 2.5
		SS = 2.9	SI = 2.9
GUSCIO	470	SS = 2.1	SI = 2.1
		SS = 2.2	SI = 2.2
		SS = 2.1	SI = 2.1
		SS = 2.3	SI = 2.3
GUSCIO	471	SS = 2.6	SI = 2.6
		SS = 1.9	SI = 1.9
		SS = 2.5	SI = 2.5
		SS = 2.2	SI = 2.2
GUSCIO	472	SS = 2.5	SI = 2.5
		SS = 2.6	SI = 2.6
		SS = 2.4	SI = 2.4
		SS = 2.6	SI = 2.6
GUSCIO	473	SS = 2.2	SI = 2.2
		SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.4	SI = 2.4
GUSCIO	474	SS = 2.4	SI = 2.4

GUSCIO	475	SS = 1.7	SI = 1.7
		SS = 2.4	SI = 2.4
		SS = 1.9	SI = 1.9
		SS = 1.5	SI = 1.5
GUSCIO	476	SS = 1.6	SI = 1.6
		SS = 1.4	SI = 1.4
		SS = 1.7	SI = 1.7
		SS = 1.9	SI = 1.9
GUSCIO	477	SS = 2.0	SI = 2.0
		SS = 1.9	SI = 1.9
		SS = 2.0	SI = 2.0
		SS = 1.8	SI = 1.8
GUSCIO	478	SS = 1.2	SI = 1.2
		SS = 1.7	SI = 1.7
		SS = 1.3	SI = 1.3
		SS = 2.5	SI = 2.5
GUSCIO	479	SS = 0.9	SI = 0.9
		SS = 2.2	SI = 2.2
		SS = 1.0	SI = 1.0
		SS = 0.6	SI = 0.6
GUSCIO	480	SS = 0.4	SI = 0.4
		SS = 0.6	SI = 0.6
		SS = 0.5	SI = 0.5
		SS = 1.7	SI = 1.7
GUSCIO	481	SS = 2.2	SI = 2.2
		SS = 1.2	SI = 1.2
		SS = 2.0	SI = 2.0
		SS = 1.0	SI = 1.0
GUSCIO	482	SS = 0.7	SI = 0.7
		SS = 0.9	SI = 0.9
		SS = 0.6	SI = 0.6
		SS = 4.5	SI = 4.5
GUSCIO	483	SS = 2.1	SI = 2.1
		SS = 3.6	SI = 3.6
		SS = 2.3	SI = 2.3
		SS = 2.3	SI = 2.3
GUSCIO	484	SS = 2.0	SI = 2.0
		SS = 2.0	SI = 2.0
		SS = 1.8	SI = 1.8
		SS = 3.8	SI = 3.8
GUSCIO	485	SS = 0.8	SI = 0.8
		SS = 3.3	SI = 3.3
		SS = 1.2	SI = 1.2
		SS = 2.2	SI = 2.2
GUSCIO	486	SS = 2.8	SI = 2.8
		SS = 1.9	SI = 1.9
		SS = 2.8	SI = 2.8
		SS = 2.0	SI = 2.0
GUSCIO	487	SS = 2.6	SI = 2.6
		SS = 1.7	SI = 1.7
		SS = 2.6	SI = 2.6
		SS = 2.9	SI = 2.9
GUSCIO	488	SS = 4.1	SI = 4.1
		SS = 3.0	SI = 3.0
		SS = 5.3	SI = 5.3
		SS = 1.2	SI = 1.2
GUSCIO	489	SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
		SS = 2.1	SI = 2.1
		SS = 1.6	SI = 1.6
GUSCIO	490	SS = 4.0	SI = 4.0
		SS = 1.7	SI = 1.7
		SS = 3.8	SI = 3.8
		SS = 6.4	SI = 6.4
GUSCIO	491	SS = 8.4	SI = 8.4
		SS = 6.3	SI = 6.3
		SS = 8.3	SI = 8.3
		SS = 6.1	SI = 6.1

GUSCIO	492	SS = 7.5	SI = 7.5
		SS = 5.9	SI = 5.9
		SS = 7.3	SI = 7.3
		SS = 1.8	SI = 1.8
GUSCIO	493	SS = 3.1	SI = 3.1
		SS = 1.4	SI = 1.4
		SS = 2.8	SI = 2.8
		SS = 3.8	SI = 3.8
GUSCIO	494	SS = 3.4	SI = 3.4
		SS = 3.2	SI = 3.2
		SS = 3.4	SI = 3.4
		SS = 0.8	SI = 0.8
GUSCIO	495	SS = 1.3	SI = 1.3
		SS = 0.9	SI = 0.9
		SS = 1.2	SI = 1.2
		SS = 2.3	SI = 2.3
GUSCIO	496	SS = 3.7	SI = 3.7
		SS = 2.6	SI = 2.6
		SS = 3.7	SI = 3.7
		SS = 6.2	SI = 6.2
GUSCIO	497	SS = 8.6	SI = 8.6
		SS = 7.0	SI = 7.0
		SS = 9.1	SI = 9.1
		SS = 5.2	SI = 5.2
GUSCIO	498	SS = 6.8	SI = 6.8
		SS = 4.9	SI = 4.9
		SS = 5.5	SI = 5.5
		SS = 1.1	SI = 1.1
GUSCIO	499	SS = 2.6	SI = 2.6
		SS = 1.3	SI = 1.3
		SS = 2.0	SI = 2.0
		SS = 1.9	SI = 1.9
GUSCIO	421	SS = 2.7	SI = 2.7
		SS = 1.7	SI = 1.7
		SS = 2.7	SI = 2.7
		tensione max = 9.9	guscio = 421

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 7 SLU con SISNAV
N. 3 CONDIZIONE ANALIST. STATICA
1 Peso proprio + 1.00
2 Permanente + 1.00
3 Accarichi + 0.30
N. 1 CASO DI CARICO
5 SISNAV SLU 1.00
1) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c005.001
2) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c005.002
3) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c005.003
4) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c005.004
Unità di misura: SI,SS [daN/cm2]

COMBINAZIONE

GUSCIO	422	SS = 5.3	SI = 5.3
		SS = 9.3	SI = 9.3
		SS = 5.1	SI = 5.1
		SS = 6.2	SI = 6.2
GUSCIO	423	SS = 5.5	SI = 5.5
		SS = 6.1	SI = 6.1
		SS = 5.4	SI = 5.4
		SS = 3.7	SI = 3.7
GUSCIO	424	SS = 1.9	SI = 1.9
		SS = 3.5	SI = 3.5
		SS = 1.8	SI = 1.8
		SS = 3.6	SI = 3.6
GUSCIO	425	SS = 2.2	SI = 2.2
		SS = 3.4	SI = 3.4
		SS = 2.1	SI = 2.1
		SS = 1.4	SI = 1.4
GUSCIO	426	SS = 0.7	SI = 0.7
		SS = 1.4	SI = 1.4
		SS = 0.6	SI = 0.6
		SS = 0.9	SI = 0.9
GUSCIO	427	SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
		SS = 2.7	SI = 2.7
		SS = 1.8	SI = 1.8
GUSCIO	428	SS = 2.7	SI = 2.7
		SS = 2.2	SI = 2.2
		SS = 3.2	SI = 3.2
		SS = 2.2	SI = 2.2
GUSCIO	429	SS = 3.1	SI = 3.1
		SS = 1.6	SI = 1.6
		SS = 1.8	SI = 1.8
		SS = 1.5	SI = 1.5
GUSCIO	430	SS = 1.8	SI = 1.8
		SS = 2.8	SI = 2.8
		SS = 4.4	SI = 4.4
		SS = 2.8	SI = 2.8
GUSCIO	431	SS = 4.4	SI = 4.4
		SS = 3.1	SI = 3.1
		SS = 4.6	SI = 4.6
		SS = 3.0	SI = 3.0
GUSCIO	432	SS = 4.6	SI = 4.6
		SS = 2.9	SI = 2.9
		SS = 3.7	SI = 3.7
		SS = 2.9	SI = 2.9
GUSCIO	433	SS = 3.7	SI = 3.7
		SS = 4.2	SI = 4.2
		SS = 6.5	SI = 6.5
		SS = 4.1	SI = 4.1
GUSCIO	434	SS = 6.5	SI = 6.5
		SS = 4.4	SI = 4.4
		SS = 5.8	SI = 5.8
		SS = 4.4	SI = 4.4
GUSCIO	435	SS = 5.7	SI = 5.7
		SS = 5.4	SI = 5.4
		SS = 9.4	SI = 9.4
		SS = 5.3	SI = 5.3
GUSCIO	436	SS = 9.5	SI = 9.5
		SS = 4.4	SI = 4.4
		SS = 5.4	SI = 5.4
		SS = 4.3	SI = 4.3
GUSCIO	437	SS = 5.3	SI = 5.3
		SS = 5.3	SI = 5.3
		SS = 4.4	SI = 4.4
		SS = 5.4	SI = 5.4
GUSCIO	438	SS = 5.4	SI = 5.4
		SS = 9.3	SI = 9.3

		SS = 6.1	SI = 6.1
		SS = 9.0	SI = 9.0
		SS = 6.0	SI = 6.0
QUSCIO	439	SS = 3.0	SI = 3.0
		SS = 3.3	SI = 3.3
		SS = 2.9	SI = 2.9
		SS = 3.2	SI = 3.2
QUSCIO	440	SS = 3.8	SI = 3.8
		SS = 3.6	SI = 3.6
		SS = 3.7	SI = 3.7
		SS = 3.6	SI = 3.6
QUSCIO	441	SS = 3.7	SI = 3.7
		SS = 3.0	SI = 3.0
		SS = 3.7	SI = 3.7
		SS = 3.0	SI = 3.0
QUSCIO	442	SS = 3.7	SI = 3.7
		SS = 1.9	SI = 1.9
		SS = 3.9	SI = 3.9
		SS = 1.8	SI = 1.8
QUSCIO	443	SS = 3.3	SI = 3.3
		SS = 2.4	SI = 2.4
		SS = 3.2	SI = 3.2
		SS = 2.4	SI = 2.4
QUSCIO	444	SS = 2.2	SI = 2.2
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.4	SI = 1.4
QUSCIO	445	SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
		SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
QUSCIO	446	SS = 0.8	SI = 0.8
		SS = 2.6	SI = 2.6
		SS = 0.8	SI = 0.8
		SS = 2.6	SI = 2.6
QUSCIO	447	SS = 0.8	SI = 0.8
		SS = 1.5	SI = 1.5
		SS = 0.7	SI = 0.7
		SS = 1.7	SI = 1.7
QUSCIO	448	SS = 1.2	SI = 1.2
		SS = 3.9	SI = 3.9
		SS = 1.2	SI = 1.2
		SS = 3.9	SI = 3.9
QUSCIO	449	SS = 1.5	SI = 1.5
		SS = 4.4	SI = 4.4
		SS = 1.5	SI = 1.5
		SS = 4.3	SI = 4.3
QUSCIO	450	SS = 1.5	SI = 1.5
		SS = 3.9	SI = 3.9
		SS = 1.5	SI = 1.5
		SS = 3.9	SI = 3.9
QUSCIO	451	SS = 3.3	SI = 3.3
		SS = 9.2	SI = 9.2
		SS = 3.4	SI = 3.4
		SS = 8.9	SI = 8.9
QUSCIO	452	SS = 3.2	SI = 3.2
		SS = 5.7	SI = 5.7
		SS = 3.2	SI = 3.2
		SS = 5.7	SI = 5.7
QUSCIO	453	SS = 3.3	SI = 3.3
		SS = 9.3	SI = 9.3
		SS = 3.3	SI = 3.3
		SS = 9.4	SI = 9.4
QUSCIO	454	SS = 6.1	SI = 6.1
		SS = 4.7	SI = 4.7
		SS = 6.4	SI = 6.4
		SS = 4.8	SI = 4.8
QUSCIO	455	SS = 3.2	SI = 3.2
		SS = 5.1	SI = 5.1

		SS = 3.2	SI = 3.2
		SS = 5.1	SI = 5.1
QUSCIO	456	SS = 5.8	SI = 5.8
		SS = 4.7	SI = 4.7
		SS = 5.9	SI = 5.9
		SS = 4.8	SI = 4.8
QUSCIO	457	SS = 1.9	SI = 1.9
		SS = 1.6	SI = 1.6
		SS = 2.1	SI = 2.1
		SS = 1.7	SI = 1.7
QUSCIO	458	SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.3	SI = 2.3
		SS = 2.3	SI = 2.3
QUSCIO	459	SS = 1.9	SI = 1.9
		SS = 1.9	SI = 1.9
		SS = 2.0	SI = 2.0
		SS = 1.9	SI = 1.9
QUSCIO	460	SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
		SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
QUSCIO	461	SS = 1.9	SI = 1.9
		SS = 1.4	SI = 1.4
		SS = 1.9	SI = 1.9
		SS = 1.3	SI = 1.3
QUSCIO	462	SS = 5.4	SI = 5.4
		SS = 1.9	SI = 1.9
		SS = 5.5	SI = 5.5
		SS = 1.9	SI = 1.9
QUSCIO	463	SS = 3.3	SI = 3.3
		SS = 1.3	SI = 1.3
		SS = 3.4	SI = 3.4
		SS = 1.3	SI = 1.3
QUSCIO	464	SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
		SS = 2.5	SI = 2.5
		SS = 1.2	SI = 1.2
QUSCIO	465	SS = 2.3	SI = 2.3
		SS = 3.2	SI = 3.2
		SS = 2.4	SI = 2.4
		SS = 3.4	SI = 3.4
QUSCIO	466	SS = 3.2	SI = 3.2
		SS = 1.3	SI = 1.3
		SS = 3.4	SI = 3.4
		SS = 1.0	SI = 1.0
QUSCIO	467	SS = 2.3	SI = 2.3
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.2	SI = 1.2
QUSCIO	468	SS = 2.8	SI = 2.8
		SS = 0.9	SI = 0.9
		SS = 2.9	SI = 2.9
		SS = 1.0	SI = 1.0
QUSCIO	469	SS = 2.4	SI = 2.4
		SS = 4.2	SI = 4.2
		SS = 2.7	SI = 2.7
		SS = 3.8	SI = 3.8
QUSCIO	470	SS = 2.7	SI = 2.7
		SS = 1.5	SI = 1.5
		SS = 2.6	SI = 2.6
		SS = 1.3	SI = 1.3
QUSCIO	471	SS = 2.6	SI = 2.6
		SS = 2.9	SI = 2.9
		SS = 2.5	SI = 2.5
		SS = 3.0	SI = 3.0
QUSCIO	472	SS = 3.2	SI = 3.2
		SS = 2.6	SI = 2.6

		SS = 3.4	SI = 3.4
		SS = 2.4	SI = 2.4
QUSCIO	473	SS = 3.0	SI = 3.0
		SS = 1.5	SI = 1.5
		SS = 3.0	SI = 3.0
		SS = 1.4	SI = 1.4
QUSCIO	474	SS = 3.0	SI = 3.0
		SS = 1.7	SI = 1.7
		SS = 2.9	SI = 2.9
		SS = 1.7	SI = 1.7
QUSCIO	475	SS = 2.4	SI = 2.4
		SS = 1.1	SI = 1.1
		SS = 2.4	SI = 2.4
		SS = 1.0	SI = 1.0
QUSCIO	476	SS = 3.2	SI = 3.2
		SS = 0.6	SI = 0.6
		SS = 3.2	SI = 3.2
		SS = 0.7	SI = 0.7
QUSCIO	477	SS = 2.4	SI = 2.4
		SS = 0.8	SI = 0.8
		SS = 2.4	SI = 2.4
		SS = 0.9	SI = 0.9
QUSCIO	478	SS = 3.2	SI = 3.2
		SS = 1.1	SI = 1.1
		SS = 3.2	SI = 3.2
		SS = 1.1	SI = 1.1
QUSCIO	479	SS = 1.3	SI = 1.3
		SS = 0.5	SI = 0.5
		SS = 1.3	SI = 1.3
		SS = 0.5	SI = 0.5
QUSCIO	480	SS = 3.8	SI = 3.8
		SS = 2.5	SI = 2.5
		SS = 4.1	SI = 4.1
		SS = 2.4	SI = 2.4
QUSCIO	481	SS = 1.3	SI = 1.3
		SS = 0.9	SI = 0.9
		SS = 1.4	SI = 1.4
		SS = 0.9	SI = 0.9
QUSCIO	482	SS = 3.3	SI = 3.3
		SS = 3.7	SI = 3.7
		SS = 3.6	SI = 3.6
		SS = 4.1	SI = 4.1
QUSCIO	483	SS = 2.5	SI = 2.5
		SS = 1.3	SI = 1.3
		SS = 2.7	SI = 2.7
		SS = 1.5	SI = 1.5
QUSCIO	484	SS = 1.8	SI = 1.8
		SS = 3.8	SI = 3.8
		SS = 1.9	SI = 1.9
		SS = 4.1	SI = 4.1
QUSCIO	485	SS = 3.4	SI = 3.4
		SS = 1.5	SI = 1.5
		SS = 3.5	SI = 3.5
		SS = 1.4	SI = 1.4
QUSCIO	486	SS = 3.3	SI = 3.3
		SS = 1.6	SI = 1.6
		SS = 3.4	SI = 3.4
		SS = 1.3	SI = 1.3
QUSCIO	487	SS = 1.7	SI = 1.7
		SS = 6.5	SI = 6.5
		SS = 1.9	SI = 1.9
		SS = 5.7	SI = 5.7
QUSCIO	488	SS = 0.7	SI = 0.7
		SS = 1.4	SI = 1.4
		SS = 0.5	SI = 0.5
		SS = 1.6	SI = 1.6
QUSCIO	489	SS = 0.7	SI = 0.7
		SS = 3.7	SI = 3.7
		SS = 0.8	SI = 0.8

		SS = 3.8	SI = 3.8
GUSCIO	490	SS = 4.1	SI = 4.1
		SS = 11.9	SI = 11.9
		SS = 4.2	SI = 4.2
		SS = 11.9	SI = 11.9
GUSCIO	491	SS = 8.0	SI = 8.0
		SS = 7.1	SI = 7.1
		SS = 8.1	SI = 8.1
		SS = 7.1	SI = 7.1
GUSCIO	492	SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.5	SI = 2.5
		SS = 2.3	SI = 2.3
GUSCIO	493	SS = 6.8	SI = 6.8
		SS = 1.8	SI = 1.8
		SS = 6.9	SI = 6.9
		SS = 1.9	SI = 1.9
GUSCIO	494	SS = 0.1	SI = 0.1
		SS = 0.9	SI = 0.9
		SS = 0.1	SI = 0.1
		SS = 0.9	SI = 0.9
GUSCIO	495	SS = 0.4	SI = 0.4
		SS = 4.4	SI = 4.4
		SS = 0.4	SI = 0.4
		SS = 4.3	SI = 4.3
GUSCIO	496	SS = 1.0	SI = 1.0
		SS = 13.6	SI = 13.6
		SS = 1.0	SI = 1.0
		SS = 13.3	SI = 13.3
GUSCIO	497	SS = 8.9	SI = 8.9
		SS = 1.4	SI = 1.4
		SS = 9.6	SI = 9.6
		SS = 1.4	SI = 1.4
GUSCIO	498	SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
GUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
tensione max =		13.6	guscio = 496
SOLLECITAZIONI GUSCI RETTANGOLARI			
CASO DI CARICO : 8 Rara			
COMBINAZIONE			
N. 4 CONDIZIONI ANALISI STATICA			
1		Reso_proprio	+ 1.00
2		Permanente	+ 1.00
3		Accvar_abitazione	+ 1.00
4		Newe_(<3000.s10)	+ 1.00
1) +1.00*c001 -+1.00*c002 +1.00*c003 +1.00*c004			
unità di misura: SI,SS [daN/cm2]			
GUSCIO	415	SS = 2.2	SI = 2.2
GUSCIO	416	SS = 1.5	SI = 1.5
GUSCIO	417	SS = 5.8	SI = 5.8
GUSCIO	418	SS = 5.9	SI = 5.9
GUSCIO	419	SS = 14.5	SI = 14.5
GUSCIO	420	SS = 11.5	SI = 11.5
GUSCIO	421	SS = 13.6	SI = 13.6
GUSCIO	422	SS = 11.3	SI = 11.3
GUSCIO	423	SS = 5.2	SI = 5.2
GUSCIO	424	SS = 5.5	SI = 5.5
GUSCIO	425	SS = 1.9	SI = 1.9
GUSCIO	426	SS = 1.2	SI = 1.2
GUSCIO	427	SS = 4.2	SI = 4.2
GUSCIO	428	SS = 5.1	SI = 5.1
GUSCIO	429	SS = 3.0	SI = 3.0
GUSCIO	430	SS = 6.8	SI = 6.8
GUSCIO	431	SS = 7.4	SI = 7.4
GUSCIO	432	SS = 6.3	SI = 6.3
GUSCIO	433	SS = 9.8	SI = 9.8
GUSCIO	434	SS = 9.8	SI = 9.8

GUSCIO 435 SS = 13.5 SI = 13.5
GUSCIO 436 SS = 9.3 SI = 9.3
GUSCIO 437 SS = 9.5 SI = 9.5
GUSCIO 438 SS = 12.5 SI = 12.5
GUSCIO 439 SS = 5.8 SI = 5.8
GUSCIO 440 SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.4 SI = 6.4
GUSCIO 442 SS = 3.9 SI = 3.9
GUSCIO 443 SS = 5.2 SI = 5.2
GUSCIO 444 SS = 3.3 SI = 3.3
GUSCIO 445 SS = 2.0 SI = 2.0
GUSCIO 446 SS = 3.0 SI = 3.0
GUSCIO 447 SS = 2.3 SI = 2.3
GUSCIO 448 SS = 4.4 SI = 4.4
GUSCIO 449 SS = 5.3 SI = 5.3
GUSCIO 450 SS = 5.2 SI = 5.2
GUSCIO 451 SS = 8.8 SI = 8.8
GUSCIO 452 SS = 7.8 SI = 7.8
GUSCIO 453 SS = 10.6 SI = 10.6
GUSCIO 454 SS = 7.6 SI = 7.6
GUSCIO 455 SS = 7.4 SI = 7.4
GUSCIO 456 SS = 8.7 SI = 8.7
GUSCIO 457 SS = 3.1 SI = 3.1
GUSCIO 458 SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.8 SI = 2.8
GUSCIO 461 SS = 2.2 SI = 2.2
GUSCIO 462 SS = 4.4 SI = 4.4
GUSCIO 463 SS = 3.5 SI = 3.5
GUSCIO 464 SS = 2.6 SI = 2.6
GUSCIO 465 SS = 2.9 SI = 2.9
GUSCIO 466 SS = 2.6 SI = 2.6
GUSCIO 467 SS = 2.4 SI = 2.4
GUSCIO 468 SS = 3.1 SI = 3.1
GUSCIO 469 SS = 2.8 SI = 2.8
GUSCIO 470 SS = 2.9 SI = 2.9
GUSCIO 471 SS = 2.4 SI = 2.4
GUSCIO 472 SS = 3.1 SI = 3.1
GUSCIO 473 SS = 3.0 SI = 3.0
GUSCIO 474 SS = 2.9 SI = 2.9
GUSCIO 475 SS = 2.0 SI = 2.0
GUSCIO 476 SS = 2.9 SI = 2.9
GUSCIO 477 SS = 2.1 SI = 2.1
GUSCIO 478 SS = 2.0 SI = 2.0
GUSCIO 479 SS = 0.8 SI = 0.8
GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 9 Rara VentoX
N. 4 CONDIZIONI ANALISI STATICA
1 Pieno proprio + 1.00

COMBINAZIONE

2 Permanente + 1.00
3 Avar. abitazione + 1.00
4 Neve (<1000h, 1m) + 1.00
1) +1.00*c001 -1.00*c002 +1.00*c003 +1.00*c004
Unità di misura: SI, SS [daN/cm2]
GUSCIO 415 SS = 2.2 SI = 2.2
GUSCIO 416 SS = 1.5 SI = 1.5
GUSCIO 417 SS = 5.8 SI = 5.8
GUSCIO 418 SS = 5.9 SI = 5.9
GUSCIO 419 SS = 14.5 SI = 14.5
GUSCIO 420 SS = 11.5 SI = 11.5
GUSCIO 421 SS = 13.6 SI = 13.6
GUSCIO 422 SS = 11.3 SI = 11.3
GUSCIO 423 SS = 5.2 SI = 5.2
GUSCIO 424 SS = 5.5 SI = 5.5
GUSCIO 425 SS = 1.9 SI = 1.9
GUSCIO 426 SS = 1.2 SI = 1.2
GUSCIO 427 SS = 4.2 SI = 4.2
GUSCIO 428 SS = 5.1 SI = 5.1
GUSCIO 429 SS = 3.0 SI = 3.0
GUSCIO 430 SS = 6.8 SI = 6.8
GUSCIO 431 SS = 7.4 SI = 7.4
GUSCIO 432 SS = 6.3 SI = 6.3
GUSCIO 433 SS = 9.8 SI = 9.8
GUSCIO 434 SS = 9.8 SI = 9.8
GUSCIO 435 SS = 13.5 SI = 13.5
GUSCIO 436 SS = 9.3 SI = 9.3
GUSCIO 437 SS = 9.5 SI = 9.5
GUSCIO 438 SS = 12.5 SI = 12.5
GUSCIO 439 SS = 5.8 SI = 5.8
GUSCIO 440 SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.4 SI = 6.4
GUSCIO 442 SS = 3.9 SI = 3.9
GUSCIO 443 SS = 5.2 SI = 5.2
GUSCIO 444 SS = 3.3 SI = 3.3
GUSCIO 445 SS = 2.0 SI = 2.0
GUSCIO 446 SS = 3.0 SI = 3.0
GUSCIO 447 SS = 2.3 SI = 2.3
GUSCIO 448 SS = 4.4 SI = 4.4
GUSCIO 449 SS = 5.3 SI = 5.3
GUSCIO 450 SS = 5.2 SI = 5.2
GUSCIO 451 SS = 8.8 SI = 8.8
GUSCIO 452 SS = 7.8 SI = 7.8
GUSCIO 453 SS = 10.6 SI = 10.6
GUSCIO 454 SS = 7.6 SI = 7.6
GUSCIO 455 SS = 7.4 SI = 7.4
GUSCIO 456 SS = 8.7 SI = 8.7
GUSCIO 457 SS = 3.1 SI = 3.1
GUSCIO 458 SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.8 SI = 2.8
GUSCIO 461 SS = 2.2 SI = 2.2
GUSCIO 462 SS = 4.4 SI = 4.4
GUSCIO 463 SS = 3.5 SI = 3.5
GUSCIO 464 SS = 2.6 SI = 2.6
GUSCIO 465 SS = 2.9 SI = 2.9
GUSCIO 466 SS = 2.6 SI = 2.6
GUSCIO 467 SS = 2.4 SI = 2.4
GUSCIO 468 SS = 3.1 SI = 3.1
GUSCIO 469 SS = 2.8 SI = 2.8
GUSCIO 470 SS = 2.9 SI = 2.9
GUSCIO 471 SS = 2.4 SI = 2.4
GUSCIO 472 SS = 3.1 SI = 3.1
GUSCIO 473 SS = 3.0 SI = 3.0
GUSCIO 474 SS = 2.9 SI = 2.9
GUSCIO 475 SS = 2.0 SI = 2.0
GUSCIO 476 SS = 2.9 SI = 2.9
GUSCIO 477 SS = 2.1 SI = 2.1
GUSCIO 478 SS = 2.0 SI = 2.0
GUSCIO 479 SS = 0.8 SI = 0.8
GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 10 Rara VentoY

COMBINAZIONE

N. 5 CONDIZIONE ANALISI STATICA
1 Pieno proprio + 1.00
2 Permanente + 1.00
3 Avar. abitazione + 1.00
4 Neve (<1000h, 1m) + 1.00
5 Vento, Y +- 1.00
1) +1.00*c001 +1.00*c002 +1.00*c003 +1.00*c004 +1.00*c005
2) +1.00*c001 +1.00*c002 +1.00*c003 +1.00*c004 -1.00*c005
Unità di misura: SI, SS [daN/cm2]
GUSCIO 415 SS = 2.4 SI = 2.4
SS = 2.0 SI = 2.0
GUSCIO 416 SS = 1.8 SI = 1.8
SS = 1.3 SI = 1.3
GUSCIO 417 SS = 6.4 SI = 6.4
SS = 5.2 SI = 5.2
GUSCIO 418 SS = 6.5 SI = 6.5
SS = 5.4 SI = 5.4
GUSCIO 419 SS = 16.3 SI = 16.3
SS = 12.8 SI = 12.8
GUSCIO 420 SS = 11.8 SI = 11.8
SS = 11.2 SI = 11.2
GUSCIO 421 SS = 12.3 SI = 12.3
SS = 15.0 SI = 15.0
GUSCIO 422 SS = 11.2 SI = 11.2
SS = 11.5 SI = 11.5
GUSCIO 423 SS = 4.7 SI = 4.7
SS = 5.7 SI = 5.7
GUSCIO 424 SS = 5.1 SI = 5.1
SS = 5.8 SI = 5.8
GUSCIO 425 SS = 1.6 SI = 1.6
SS = 2.1 SI = 2.1
GUSCIO 426 SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
GUSCIO 427 SS = 4.5 SI = 4.5
SS = 3.9 SI = 3.9
GUSCIO 428 SS = 5.5 SI = 5.5
SS = 4.8 SI = 4.8
GUSCIO 429 SS = 3.2 SI = 3.2
SS = 3.0 SI = 3.0
GUSCIO 430 SS = 7.4 SI = 7.4
SS = 6.3 SI = 6.3
GUSCIO 431 SS = 7.9 SI = 7.9
SS = 6.9 SI = 6.9
GUSCIO 432 SS = 6.7 SI = 6.7
SS = 6.1 SI = 6.1
GUSCIO 433 SS = 10.5 SI = 10.5
SS = 9.2 SI = 9.2
GUSCIO 434 SS = 10.2 SI = 10.2
SS = 9.3 SI = 9.3
GUSCIO 435 SS = 15.1 SI = 15.1

SS = 11.9 SI = 11.9
GUSCIO 436 SS = 9.7 SI = 9.7
SS = 8.9 SI = 8.9
GUSCIO 437 SS = 9.8 SI = 9.8
SS = 9.2 SI = 9.2
GUSCIO 438 SS = 11.9 SI = 11.9
SS = 14.0 SI = 14.0
GUSCIO 439 SS = 6.0 SI = 6.0
SS = 5.6 SI = 5.6
GUSCIO 440 SS = 7.1 SI = 7.1
SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.3 SI = 6.3
SS = 6.6 SI = 6.6
GUSCIO 442 SS = 3.7 SI = 3.7
SS = 4.6 SI = 4.6
GUSCIO 443 SS = 5.0 SI = 5.0
SS = 5.4 SI = 5.4
GUSCIO 444 SS = 3.1 SI = 3.1
SS = 3.6 SI = 3.6
GUSCIO 445 SS = 2.5 SI = 2.5
SS = 1.5 SI = 1.5
GUSCIO 446 SS = 3.6 SI = 3.6
SS = 2.3 SI = 2.3
GUSCIO 447 SS = 2.6 SI = 2.6
SS = 2.0 SI = 2.0
GUSCIO 448 SS = 5.4 SI = 5.4
SS = 3.5 SI = 3.5
GUSCIO 449 SS = 6.3 SI = 6.3
SS = 4.4 SI = 4.4
GUSCIO 450 SS = 6.0 SI = 6.0
SS = 4.5 SI = 4.5
GUSCIO 451 SS = 11.5 SI = 11.5
SS = 7.2 SI = 7.2
GUSCIO 452 SS = 8.7 SI = 8.7
SS = 7.0 SI = 7.0
GUSCIO 453 SS = 13.2 SI = 13.2
SS = 8.1 SI = 8.1
GUSCIO 454 SS = 7.8 SI = 7.8
SS = 8.3 SI = 8.3
GUSCIO 455 SS = 8.0 SI = 8.0
SS = 6.8 SI = 6.8
GUSCIO 456 SS = 8.3 SI = 8.3
SS = 9.4 SI = 9.4
GUSCIO 457 SS = 2.9 SI = 2.9
SS = 3.4 SI = 3.4
GUSCIO 458 SS = 3.9 SI = 3.9
SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.6 SI = 2.6
SS = 3.1 SI = 3.1
GUSCIO 461 SS = 2.1 SI = 2.1
SS = 2.4 SI = 2.4
GUSCIO 462 SS = 2.6 SI = 2.6
SS = 6.5 SI = 6.5
GUSCIO 463 SS = 2.9 SI = 2.9
SS = 4.3 SI = 4.3
GUSCIO 464 SS = 2.3 SI = 2.3
SS = 3.1 SI = 3.1
GUSCIO 465 SS = 3.7 SI = 3.7
SS = 2.7 SI = 2.7
GUSCIO 466 SS = 1.9 SI = 1.9
SS = 3.8 SI = 3.8
GUSCIO 467 SS = 2.2 SI = 2.2
SS = 2.9 SI = 2.9
GUSCIO 468 SS = 2.3 SI = 2.3
SS = 3.9 SI = 3.9
GUSCIO 469 SS = 4.3 SI = 4.3

		SS =	2.9	SI =	2.9
GUSCIO	470	SS =	2.5	SI =	2.5
		SS =	3.3	SI =	3.3
GUSCIO	471	SS =	2.9	SI =	2.9
		SS =	2.6	SI =	2.6
GUSCIO	472	SS =	2.5	SI =	2.5
		SS =	3.8	SI =	3.8
GUSCIO	473	SS =	2.6	SI =	2.6
		SS =	3.6	SI =	3.6
GUSCIO	474	SS =	2.4	SI =	2.4
		SS =	3.5	SI =	3.5
GUSCIO	475	SS =	1.4	SI =	1.4
		SS =	2.7	SI =	2.7
GUSCIO	476	SS =	2.1	SI =	2.1
		SS =	3.7	SI =	3.7
GUSCIO	477	SS =	1.5	SI =	1.5
		SS =	2.8	SI =	2.8
GUSCIO	478	SS =	1.4	SI =	1.4
		SS =	3.3	SI =	3.3
GUSCIO	479	SS =	0.3	SI =	0.3
		SS =	1.4	SI =	1.4
GUSCIO	480	SS =	1.4	SI =	1.4
		SS =	4.0	SI =	4.0
GUSCIO	481	SS =	0.8	SI =	0.8
		SS =	1.3	SI =	1.3
GUSCIO	482	SS =	4.4	SI =	4.4
		SS =	4.7	SI =	4.7
GUSCIO	483	SS =	2.8	SI =	2.8
		SS =	3.7	SI =	3.7
GUSCIO	484	SS =	4.0	SI =	4.0
		SS =	2.0	SI =	2.0
GUSCIO	485	SS =	2.9	SI =	2.9
		SS =	4.3	SI =	4.3
GUSCIO	486	SS =	2.1	SI =	2.1
		SS =	4.0	SI =	4.0
GUSCIO	487	SS =	7.0	SI =	7.0
		SS =	2.0	SI =	2.0
GUSCIO	488	SS =	1.9	SI =	1.9
		SS =	0.9	SI =	0.9
GUSCIO	489	SS =	5.5	SI =	5.5
		SS =	3.6	SI =	3.6
GUSCIO	490	SS =	17.5	SI =	17.5
		SS =	12.0	SI =	12.0
GUSCIO	491	SS =	13.0	SI =	13.0
		SS =	13.7	SI =	13.7
GUSCIO	492	SS =	4.1	SI =	4.1
		SS =	3.9	SI =	3.9
GUSCIO	493	SS =	2.6	SI =	2.6
		SS =	7.8	SI =	7.8
GUSCIO	494	SS =	1.3	SI =	1.3
		SS =	0.7	SI =	0.7
GUSCIO	495	SS =	5.6	SI =	5.6
		SS =	2.5	SI =	2.5
GUSCIO	496	SS =	16.7	SI =	16.7
		SS =	6.8	SI =	6.8
GUSCIO	497	SS =	4.4	SI =	4.4
		SS =	11.4	SI =	11.4
GUSCIO	498	SS =	1.8	SI =	1.8
		SS =	2.8	SI =	2.8
GUSCIO	499	SS =	2.9	SI =	2.9
		SS =	3.8	SI =	3.8
		tensione max =	17.5	guscio =	490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 11 Frequente Ventax

N. 4 CONDIZIONI ANALISI STATICA

1	Peso_proprio	_____	+	1.00
2	Permanente	_____	+	1.00
3	A'Var_abbattazione	_____	+	0.50
4	Neve_(c<300m_s1m)	_____	+	0.20

1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004
Unità di misura: SI,SS [daN/cm2]

GUSCIO 415 SS = 1.4 SI = 1.4

COMBINAZIONE

GUSCIO	416	SS =	1.0	SI =	1.0
GUSCIO	417	SS =	3.7	SI =	3.7
GUSCIO	418	SS =	3.8	SI =	3.8
GUSCIO	419	SS =	9.0	SI =	9.0
GUSCIO	420	SS =	7.2	SI =	7.2
GUSCIO	421	SS =	8.6	SI =	8.6
GUSCIO	422	SS =	7.2	SI =	7.2
GUSCIO	423	SS =	3.4	SI =	3.4
GUSCIO	424	SS =	3.5	SI =	3.5
GUSCIO	425	SS =	1.2	SI =	1.2
GUSCIO	426	SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
GUSCIO	429	SS =	2.0	SI =	2.0
GUSCIO	430	SS =	4.4	SI =	4.4
GUSCIO	431	SS =	4.7	SI =	4.7
GUSCIO	432	SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.3	SI =	6.3
GUSCIO	434	SS =	6.3	SI =	6.3
GUSCIO	435	SS =	8.6	SI =	8.6
GUSCIO	436	SS =	6.0	SI =	6.0
GUSCIO	437	SS =	6.1	SI =	6.1
GUSCIO	438	SS =	8.1	SI =	8.1
GUSCIO	439	SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
GUSCIO	442	SS =	2.6	SI =	2.6
GUSCIO	443	SS =	3.3	SI =	3.3
GUSCIO	444	SS =	2.1	SI =	2.1
GUSCIO	445	SS =	1.4	SI =	1.4
GUSCIO	446	SS =	2.0	SI =	2.0
GUSCIO	447	SS =	1.4	SI =	1.4
GUSCIO	448	SS =	3.0	SI =	3.0
GUSCIO	449	SS =	3.6	SI =	3.6
GUSCIO	450	SS =	3.3	SI =	3.3
GUSCIO	451	SS =	5.8	SI =	5.8
GUSCIO	452	SS =	5.2	SI =	5.2
GUSCIO	453	SS =	6.6	SI =	6.6
GUSCIO	454	SS =	5.1	SI =	5.1
GUSCIO	455	SS =	4.9	SI =	4.9
GUSCIO	456	SS =	5.7	SI =	5.7
GUSCIO	457	SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
GUSCIO	460	SS =	2.1	SI =	2.1
GUSCIO	461	SS =	1.6	SI =	1.6
GUSCIO	462	SS =	3.0	SI =	3.0
GUSCIO	463	SS =	2.6	SI =	2.6
GUSCIO	464	SS =	1.9	SI =	1.9
GUSCIO	465	SS =	2.1	SI =	2.1
GUSCIO	466	SS =	1.9	SI =	1.9
GUSCIO	467	SS =	1.8	SI =	1.8
GUSCIO	468	SS =	2.1	SI =	2.1
GUSCIO	469	SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.1	SI =	2.1
GUSCIO	471	SS =	1.8	SI =	1.8
GUSCIO	472	SS =	2.3	SI =	2.3
GUSCIO	473	SS =	2.2	SI =	2.2
GUSCIO	474	SS =	2.2	SI =	2.2
GUSCIO	475	SS =	1.4	SI =	1.4
GUSCIO	476	SS =	2.1	SI =	2.1
GUSCIO	477	SS =	1.6	SI =	1.6
GUSCIO	478	SS =	1.5	SI =	1.5
GUSCIO	479	SS =	0.6	SI =	0.6
GUSCIO	480	SS =	1.6	SI =	1.6
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.3	SI =	2.3

GUSCIO	484	SS =	2.1	SI =	2.1
GUSCIO	485	SS =	2.5	SI =	2.5
GUSCIO	486	SS =	2.2	SI =	2.2
GUSCIO	487	SS =	3.3	SI =	3.3
GUSCIO	488	SS =	0.8	SI =	0.8
GUSCIO	489	SS =	2.8	SI =	2.8
GUSCIO	490	SS =	9.1	SI =	9.1
GUSCIO	491	SS =	8.3	SI =	8.3
GUSCIO	492	SS =	2.4	SI =	2.4
GUSCIO	493	SS =	3.3	SI =	3.3
GUSCIO	494	SS =	0.6	SI =	0.6
GUSCIO	495	SS =	2.6	SI =	2.6
GUSCIO	496	SS =	7.7	SI =	7.7
GUSCIO	497	SS =	5.5	SI =	5.5
GUSCIO	498	SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.5	SI =	2.5
		tensione max =	9.1	guscio =	490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 12 Frequente Ventax

N. 4 CONDIZIONI ANALISI STATICA

1	Peso_proprio	_____	+	1.00
2	Permanente	_____	+	1.00
3	A'Var_abbattazione	_____	+	0.50
4	Neve_(c<300m_s1m)	_____	+	0.20

1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004
Unità di misura: SI,SS [daN/cm2]

GUSCIO	415	SS =	1.4	SI =	1.4
GUSCIO	416	SS =	1.0	SI =	1.0
GUSCIO	417	SS =	3.7	SI =	3.7
GUSCIO	418	SS =	3.8	SI =	3.8
GUSCIO	419	SS =	9.0	SI =	9.0
GUSCIO	420	SS =	7.2	SI =	7.2
GUSCIO	421	SS =	8.6	SI =	8.6
GUSCIO	422	SS =	7.2	SI =	7.2
GUSCIO	423	SS =	3.4	SI =	3.4
GUSCIO	424	SS =	3.5	SI =	3.5
GUSCIO	425	SS =	1.2	SI =	1.2
GUSCIO	426	SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
GUSCIO	429	SS =	2.0	SI =	2.0
GUSCIO	430	SS =	4.4	SI =	4.4
GUSCIO	431	SS =	4.7	SI =	4.7
GUSCIO	432	SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.3	SI =	6.3
GUSCIO	434	SS =	6.3	SI =	6.3
GUSCIO	435	SS =	8.6	SI =	8.6
GUSCIO	436	SS =	6.0	SI =	6.0
GUSCIO	437	SS =	6.1	SI =	6.1
GUSCIO	438	SS =	8.1	SI =	8.1
GUSCIO	439	SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
GUSCIO	442	SS =	2.6	SI =	2.6
GUSCIO	443	SS =	3.3	SI =	3.3
GUSCIO	444	SS =	2.1	SI =	2.1
GUSCIO	445	SS =	1.4	SI =	1.4
GUSCIO	446	SS =	2.0	SI =	2.0
GUSCIO	447	SS =	1.4	SI =	1.4
GUSCIO	448	SS =	3.0	SI =	3.0
GUSCIO	449	SS =	3.6	SI =	3.6
GUSCIO	450	SS =	3.3	SI =	3.3
GUSCIO	451	SS =	5.8	SI =	5.8
GUSCIO	452	SS =	5.2	SI =	5.2
GUSCIO	453	SS =	6.6	SI =	6.6
GUSCIO	454	SS =	5.1	SI =	5.1
GUSCIO	455	SS =	4.9	SI =	4.9
GUSCIO	456	SS =	5.7	SI =	5.7
GUSCIO	457	SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
GUSCIO	460	SS =	2.1	SI =	2.1

COMBINAZIONE

GUSCIO	461	SS =	1.6	SI =	1.6
GUSCIO	462	SS =	3.0	SI =	3.0
GUSCIO	463	SS =	2.6	SI =	2.6
GUSCIO	464	SS =	1.9	SI =	1.9
GUSCIO	465	SS =	2.1	SI =	2.1
GUSCIO	466	SS =	1.9	SI =	1.9
GUSCIO	467	SS =	1.8	SI =	1.8
GUSCIO	468	SS =	2.1	SI =	2.1
GUSCIO	469	SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.1	SI =	2.1
GUSCIO	471	SS =	1.8	SI =	1.8
GUSCIO	472	SS =	2.3	SI =	2.3
GUSCIO	473	SS =	2.2	SI =	2.2
GUSCIO	474	SS =	2.2	SI =	2.2
GUSCIO	475	SS =	1.4	SI =	1.4
GUSCIO	476	SS =	2.1	SI =	2.1
GUSCIO	477	SS =	1.6	SI =	1.6
GUSCIO	478	SS =	1.5	SI =	1.5
GUSCIO	479	SS =	0.6	SI =	0.6
GUSCIO	480	SS =	1.6	SI =	1.6
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.3	SI =	2.3
GUSCIO	484	SS =	2.1	SI =	2.1
GUSCIO	485	SS =	2.5	SI =	2.5
GUSCIO	486	SS =	2.2	SI =	2.2
GUSCIO	487	SS =	3.3	SI =	3.3
GUSCIO	488	SS =	0.8	SI =	0.8
GUSCIO	489	SS =	2.8	SI =	2.8
GUSCIO	490	SS =	9.1	SI =	9.1
GUSCIO	491	SS =	8.3	SI =	8.3
GUSCIO	492	SS =	2.4	SI =	2.4
GUSCIO	493	SS =	3.3	SI =	3.3
GUSCIO	494	SS =	0.6	SI =	0.6
GUSCIO	495	SS =	2.6	SI =	2.6
GUSCIO	496	SS =	7.7	SI =	7.7
GUSCIO	497	SS =	5.5	SI =	5.5
GUSCIO	498	SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.5	SI =	2.5
		tensione max =	9.1	guscio =	490

		SS =	1.3	SI =	1.3
GUSCIO	426	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.8	SI =	2.8
		SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
		SS =	3.2	SI =	3.2
GUSCIO	429	SS =	2.0	SI =	2.0
		SS =	1.9	SI =	1.9
GUSCIO	430	SS =	4.5	SI =	4.5
		SS =	4.3	SI =	4.3
GUSCIO	431	SS =	4.8	SI =	4.8
		SS =	4.6	SI =	4.6
GUSCIO	432	SS =	4.1	SI =	4.1
		SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.4	SI =	6.4
		SS =	6.2	SI =	6.2
GUSCIO	434	SS =	6.4	SI =	6.4
		SS =	6.2	SI =	6.2
GUSCIO	435	SS =	8.9	SI =	8.9
		SS =	8.3	SI =	8.3
GUSCIO	436	SS =	6.1	SI =	6.1
		SS =	5.9	SI =	5.9
GUSCIO	437	SS =	6.1	SI =	6.1
		SS =	6.0	SI =	6.0
GUSCIO	438	SS =	7.9	SI =	7.9
		SS =	8.4	SI =	8.4
GUSCIO	439	SS =	3.8	SI =	3.8
		SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.5	SI =	4.5
		SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
		SS =	4.2	SI =	4.2
GUSCIO	442	SS =	2.6	SI =	2.6
		SS =	2.7	SI =	2.7
GUSCIO	443	SS =	3.3	SI =	3.3
		SS =	3.4	SI =	3.4
GUSCIO	444	SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	445	SS =	1.5	SI =	1.5
		SS =	1.3	SI =	1.3
GUSCIO	446	SS =	2.1	SI =	2.1
		SS =	1.9	SI =	1.9
GUSCIO	447	SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
GUSCIO	448	SS =	3.1	SI =	3.1
		SS =	2.8	SI =	2.8
GUSCIO	449	SS =	3.8	SI =	3.8
		SS =	3.4	SI =	3.4
GUSCIO	450	SS =	3.5	SI =	3.5
		SS =	3.1	SI =	3.1
GUSCIO	451	SS =	6.3	SI =	6.3
		SS =	5.4	SI =	5.4
GUSCIO	452	SS =	5.3	SI =	5.3
		SS =	5.0	SI =	5.0
GUSCIO	453	SS =	7.1	SI =	7.1
		SS =	6.1	SI =	6.1
GUSCIO	454	SS =	5.1	SI =	5.1
		SS =	5.1	SI =	5.1
GUSCIO	455	SS =	5.1	SI =	5.1
		SS =	4.8	SI =	4.8
GUSCIO	456	SS =	5.5	SI =	5.5
		SS =	5.8	SI =	5.8
GUSCIO	457	SS =	2.0	SI =	2.0
		SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
		SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3

GUSCIO	460	SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	461	SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
GUSCIO	462	SS =	2.6	SI =	2.6
		SS =	3.4	SI =	3.4
GUSCIO	463	SS =	2.4	SI =	2.4
		SS =	2.7	SI =	2.7
GUSCIO	464	SS =	1.8	SI =	1.8
		SS =	2.0	SI =	2.0
GUSCIO	465	SS =	2.3	SI =	2.3
		SS =	2.0	SI =	2.0
GUSCIO	466	SS =	1.7	SI =	1.7
		SS =	2.1	SI =	2.1
GUSCIO	467	SS =	1.7	SI =	1.7
		SS =	1.9	SI =	1.9
GUSCIO	468	SS =	1.9	SI =	1.9
		SS =	2.3	SI =	2.3
GUSCIO	469	SS =	2.4	SI =	2.4
		SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
GUSCIO	471	SS =	1.8	SI =	1.8
		SS =	1.9	SI =	1.9
GUSCIO	472	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
GUSCIO	473	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
GUSCIO	474	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
GUSCIO	475	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
GUSCIO	476	SS =	2.0	SI =	2.0
		SS =	2.3	SI =	2.3
GUSCIO	477	SS =	1.5	SI =	1.5
		SS =	1.7	SI =	1.7
GUSCIO	478	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
GUSCIO	479	SS =	0.4	SI =	0.4
		SS =	0.7	SI =	0.7
GUSCIO	480	SS =	1.2	SI =	1.2
		SS =	1.9	SI =	1.9
GUSCIO	481	SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
GUSCIO	482	SS =	2.7	SI =	2.7
		SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
GUSCIO	484	SS =	2.3	SI =	2.3
		SS =	1.8	SI =	1.8
GUSCIO	485	SS =	2.4	SI =	2.4
		SS =	2.7	SI =	2.7
GUSCIO	486	SS =	2.0	SI =	2.0
		SS =	2.4	SI =	2.4
GUSCIO	487	SS =	3.9	SI =	3.9
		SS =	2.8	SI =	2.8
GUSCIO	488	SS =	0.9	SI =	0.9
		SS =	0.7	SI =	0.7
GUSCIO	489	SS =	3.0	SI =	3.0
		SS =	2.6	SI =	2.6
GUSCIO	490	SS =	9.7	SI =	9.7
		SS =	8.6	SI =	8.6
GUSCIO	491	SS =	8.2	SI =	8.2
		SS =	8.4	SI =	8.4
GUSCIO	492	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
GUSCIO	493	SS =	2.7	SI =	2.7
		SS =	3.9	SI =	3.9

GUSCIO	494	SS =	0.7	SI =	0.7
		SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.9	SI =	2.9
		SS =	2.3	SI =	2.3
GUSCIO	496	SS =	8.7	SI =	8.7
		SS =	6.7	SI =	6.7
GUSCIO	497	SS =	4.8	SI =	4.8
		SS =	6.2	SI =	6.2
GUSCIO	498	SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.4	SI =	2.4
		SS =	2.6	SI =	2.6
tensione max =		9.7	guscio =	490	

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 14 Quasi Perm
N. 3 CONDIZIONE ANALISI STATICA
1 Peso proprio + 1.00
2 Permanente + 1.00
3 Azioni abilitazione + 0.30
1) +1.00*0.01 +1.00*0.02 +0.30*0.03
Unità di misura: SI,SS [daN/cm2]

GUSCIO	415	SS =	1.1	SI =	1.1
GUSCIO	416	SS =	0.8	SI =	0.8
GUSCIO	417	SS =	3.0	SI =	3.0
GUSCIO	418	SS =	3.0	SI =	3.0
GUSCIO	419	SS =	7.1	SI =	7.1
GUSCIO	420	SS =	5.8	SI =	5.8
GUSCIO	421	SS =	6.9	SI =	6.9
GUSCIO	422	SS =	5.7	SI =	5.7
GUSCIO	423	SS =	2.7	SI =	2.7
GUSCIO	424	SS =	2.8	SI =	2.8
GUSCIO	425	SS =	1.0	SI =	1.0
GUSCIO	426	SS =	0.6	SI =	0.6
GUSCIO	427	SS =	2.2	SI =	2.2
GUSCIO	428	SS =	2.6	SI =	2.6
GUSCIO	429	SS =	1.6	SI =	1.6
GUSCIO	430	SS =	3.6	SI =	3.6
GUSCIO	431	SS =	3.8	SI =	3.8
GUSCIO	432	SS =	3.2	SI =	3.2
GUSCIO	433	SS =	5.1	SI =	5.1
GUSCIO	434	SS =	5.1	SI =	5.1
GUSCIO	435	SS =	6.9	SI =	6.9
GUSCIO	436	SS =	4.8	SI =	4.8
GUSCIO	437	SS =	4.9	SI =	4.9
GUSCIO	438	SS =	6.6	SI =	6.6
GUSCIO	439	SS =	3.0	SI =	3.0
GUSCIO	440	SS =	3.7	SI =	3.7
GUSCIO	441	SS =	3.3	SI =	3.3
GUSCIO	442	SS =	2.2	SI =	2.2
GUSCIO	443	SS =	2.7	SI =	2.7
GUSCIO	444	SS =	1.7	SI =	1.7
GUSCIO	445	SS =	1.2	SI =	1.2
GUSCIO	446	SS =	1.7	SI =	1.7
GUSCIO	447	SS =	1.0	SI =	1.0
GUSCIO	448	SS =	2.4	SI =	2.4
GUSCIO	449	SS =	2.9	SI =	2.9
GUSCIO	450	SS =	2.6	SI =	2.6
GUSCIO	451	SS =	4.8	SI =	4.8
GUSCIO	452	SS =	4.3	SI =	4.3
GUSCIO	453	SS =	5.2	SI =	5.2
GUSCIO	454	SS =	4.2	SI =	4.2
GUSCIO	455	SS =	4.1	SI =	4.1
GUSCIO	456	SS =	4.6	SI =	4.6
GUSCIO	457	SS =	1.7	SI =	1.7
GUSCIO	458	SS =	2.2	SI =	2.2
GUSCIO	459	SS =	1.8	SI =	1.8
GUSCIO	460	SS =	1.9	SI =	1.9
GUSCIO	461	SS =	1.4	SI =	1.4
GUSCIO	462	SS =	2.5	SI =	2.5
GUSCIO	463	SS =	2.3	SI =	2.3
GUSCIO	464	SS =	1.7	SI =	1.7

COMBINAZIONE

GUSCIO	465	SS =	1.9	SI =	1.9
GUSCIO	466	SS =	1.6	SI =	1.6
GUSCIO	467	SS =	1.6	SI =	1.6
GUSCIO	468	SS =	1.8	SI =	1.8
GUSCIO	469	SS =	1.9	SI =	1.9
GUSCIO	470	SS =	1.9	SI =	1.9
GUSCIO	471	SS =	1.6	SI =	1.6
GUSCIO	472	SS =	2.0	SI =	2.0
GUSCIO	473	SS =	1.9	SI =	1.9
GUSCIO	474	SS =	1.9	SI =	1.9
GUSCIO	475	SS =	1.2	SI =	1.2
GUSCIO	476	SS =	1.9	SI =	1.9
GUSCIO	477	SS =	1.4	SI =	1.4
GUSCIO	478	SS =	1.3	SI =	1.3
GUSCIO	479	SS =	0.5	SI =	0.5
GUSCIO	480	SS =	1.4	SI =	1.4
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.4	SI =	2.4
GUSCIO	483	SS =	1.9	SI =	1.9
GUSCIO	484	SS =	1.9	SI =	1.9
GUSCIO	485	SS =	2.2	SI =	2.2
GUSCIO	486	SS =	1.9	SI =	1.9
GUSCIO	487	SS =	2.9	SI =	2.9
GUSCIO	488	SS =	0.6	SI =	0.6
GUSCIO	489	SS =	2.2	SI =	2.2
GUSCIO	490	SS =	7.3	SI =	7.3
GUSCIO	491	SS =	6.6	SI =	6.6
GUSCIO	492	SS =	1.9	SI =	1.9
GUSCIO	493	SS =	2.7	SI =	2.7
GUSCIO	494	SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.1	SI =	2.1
GUSCIO	496	SS =	6.3	SI =	6.3
GUSCIO	497	SS =	4.7	SI =	4.7
GUSCIO	498	SS =	1.2	SI =	1.2
GUSCIO	499	SS =	2.2	SI =	2.2
tensione max =		7.3	guscio =	490	

VERIFICA GUSCI IN C.A.:

MACROSCOPICO FONDAZ

VERIFICA ARMATURE EFFETTIVE (EFFETTO MEMBRANA + PIASTRA)

CASI DI CARICO:

Nome Descrizione
1 su VENT0
2 su VENT0
3 su VENT0
4 su su SIEWM
5 su su SIEWM
6 su su SIEWM
7 su su SIEWM

DATA:
tensione di snervamento acciaio (fyk): 4500 daN/cm2
coefficiente sicurezza acciaio: 1.15
deformazione ultima ultls: 1.97 per mille
deformazione ultima cls: 3.5 per mille
rapporto rottura/snervamento (k): 1.5
resistenza cilindrica cls (fcd): 249 daN/cm2
coefficiente di sicurezza (gamma): 1.5
coefficiente riduttivo (alpha): 0.85
copriferro inferiore (asse amatura): 3 cm
copriferro superiore (asse amatura): 3 cm
moltiplicatore sollecitazioni: 1

LEGENDA:
spess = spessore guscio, verfica effettuata su sezione Bm, con B-I cm e H="spess" cm
AF = area disposta al lembo teso, in cm2 al metro
Afc = area disposta al lembo compresso, in cm2 al metro
Mem = momento flettente (daN/cm)
Nor = sforzo normale [daN]
ecc = deformazione cls [per mille]
wfk = deformazione acciaio [per mille]

L'armatura è sufficiente se le deformazioni dei materiali sono ovunque minori delle corrispondenti deformazioni ultime.

INFERIORE ORIZZONTALE									
GUSCI	spess	AF	Afc	Mem	Nor	ecc	off	wfk	spess
415	35	4.21	4.21	1344	0.0	0.10	0.51	4.16	4.36
416	35	4.21	4.21	497	0.0	0.04	0.19	4.16	4.36
417	35	4.21	4.21	1815	0.0	0.14	0.68	4.16	4.36
418	35	4.21	4.21	511	0.0	0.04	0.19	4.16	4.36
419	35	4.21	4.21	1217	0.0	0.17	0.83	4.16	4.36
420	35	4.21	4.21	431	0.0	0.03	0.16	4.16	4.36
421	35	4.21	4.21	2247	0.0	0.17	0.85	4.16	4.36
422	35	4.21	4.21	347	0.0	0.03	0.13	4.16	4.36
423	35	4.21	4.21	1876	0.0	0.15	0.71	4.16	4.36
424	35	4.21	4.21	1242	0.0	0.17	0.83	4.16	4.36
425	35	4.21	4.21	1239	0.0	0.10	0.47	4.16	4.36
426	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
427	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36
428	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
429	35	4.21	4.21	1246	0.0	0.12	0.56	4.16	4.36
430	35	4.21	4.21	93	0.0	0.01	0.03	4.16	4.36
431	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
432	35	4.21	4.21	1530	0.0	0.12	0.56	4.16	4.36
433	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
434	35	4.21	4.21	303	0.0	0.02	0.11	4.16	4.36
435	35	4.21	4.21	1527	0.0	0.12	0.57	4.16	4.36
436	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
437	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36
438	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
439	35	4.21	4.21	1246	0.0	0.12	0.56	4.16	4.36
440	35	4.21	4.21	93	0.0	0.01	0.03	4.16	4.36
441	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
442	35	4.21	4.21	1530	0.0	0.12	0.56	4.16	4.36
443	35	4.21	4.21	303	0.0	0.02	0.11	4.16	4.36
444	35	4.21	4.21	1527	0.0	0.12	0.57	4.16	4.36
445	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
446	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36
447	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
448	35	4.21	4.21	1246	0.0	0.12	0.56	4.16	4.36
449	35	4.21	4.21	93	0.0	0.01	0.03	4.16	4.36
450	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
451	35	4.21	4.21	1530	0.0	0.12	0.56	4.16	4.36
452	35	4.21	4.21	303	0.0	0.02	0.11	4.16	4.36
453	35	4.21	4.21	1527	0.0	0.12	0.57	4.16	4.36
454	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
455	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36
456	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
457	35	4.21	4.21	1246	0.0	0.12	0.56	4.16	4.36
458	35	4.21	4.21	93	0.0	0.01	0.03	4.16	4.36
459	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
460	35	4.21	4.21	1530	0.0	0.12	0.56	4.16	4.36
461	35	4.21	4.21	303	0.0	0.02	0.11	4.16	4.36
462	35	4.21	4.21	1527	0.0	0.12	0.57	4.16	4.36
463	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
464	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36
465	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
466	35	4.21	4.21	1246	0.0	0.12	0.56	4.16	4.36
467	35	4.21	4.21	93	0.0	0.01	0.03	4.16	4.36
468	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
469	35	4.21	4.21	1530	0.0	0.12	0.56	4.16	4.36
470	35	4.21	4.21	303	0.0	0.02	0.11	4.16	4.36
471	35	4.21	4.21	1527	0.0	0.12	0.57	4.16	4.36
472	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
473	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36
474	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
475	35	4.21	4.21	1246	0.0	0.12	0.56	4.16	4.36
476	35	4.21	4.21	93	0.0	0.01	0.03	4.16	4.36
477	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
478	35	4.21	4.21	1530	0.0	0.12	0.56	4.16	4.36
479	35	4.21	4.21	303	0.0	0.02	0.11	4.16	4.36
480	35	4.21	4.21	1527	0.0	0.12	0.57	4.16	4.36
481	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
482	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36
483	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
484	35	4.21	4.21	1246	0.0	0.12	0.56	4.16	4.36
485	35	4.21	4.21	93	0.0	0.01	0.03	4.16	4.36
486	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
487	35	4.21	4.21	1530	0.0	0.12	0.56	4.16	4.36
488	35	4.21	4.21	303	0.0	0.02	0.11	4.16	4.36
489	35	4.21	4.21	1527	0.0	0.12	0.57	4.16	4.36
490	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
491	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36
492	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
493	35	4.21	4.21	1246	0.0	0.12	0.56	4.16	4.36
494	35	4.21	4.21	93	0.0	0.01	0.03	4.16	4.36
495	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
496	35	4.21	4.21	1530	0.0	0.12	0.56	4.16	4.36
497	35	4.21	4.21	303	0.0	0.02	0.11	4.16	4.36
498	35	4.21	4.21	1527	0.0	0.12	0.57	4.16	4.36
499	35	4.21	4.21	451	0.0	0.04	0.17	4.16	4.36
500	35	4.21	4.21	138	0.0	0.03	0.05	4.16	4.36

SUPERIORE ORIZZONTALE									
GUSCI	spess	AF	Afc	Mem	Nor	ecc	off	wfk	spess
415	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
416	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
417	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
418	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
419	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
420	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36
421	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36

422	35	4.21	4.21	51	0.0	0.00	0.02	4.16	4.36	0.	0.00	0.00
423	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36	157.	0.	0.01
424	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36	0.	0.00	0.06
425	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36	308.	0.	0.02
426	35	4.21	4.21	0	0.0	0.00	0.00	4.16	4.36	0.	0.00	0.12
427	35	4.21	4.21	1337	0.0	0.10	0.50	4.16	4.36	0.	0.00	0.24
428	35	4.21	4.21	1849	0.0	0.14	0.70	4.16	4.36	0.	0.00	0.00
429	35	4.21	4.21	1057	0.0	0.08	0.40	4.16	4.36	298.	0.	0.02
430	35	4.21	4.21	1413	0.0	0.11	0.53	4.16	4.36	0.	0.00	0.11
431	35	4.21	4.21	1915	0.0	0.15	0.75	4.16	4.36	0.	0.00	0.00
432	35	4.21	4.21	957	0.0	0.07	0.36	4.16	4.36	0.	0.00	0.00
433	35	4.21	4.21	1429	0.0	0.11	0.54	4.16	4.36	0.	0.00	0.00
434	35	4.21	4.21	134	0.0	0.01	0.03	4.16	4.36	0.	0.00	0.00
435	35	4.21	4.21	859	0.0	0.07	0.32	4.16	4.36	0.	0.00	0.00
436	35	4.21	4.21	1377	0.0	0.10	0.50	4.16	4.36	0.	0.00	0.00
437	35	4.21	4.21	1938	0.0	0.15	0.73	4.16	4.36	0.	0.00	0.00
438	35	4.21	4.21	966	0.0	0.09	0.46	4.16	4.36	0.	0.00	0.00
439	35	4.21	4.21	1252	0.0	0.10	0.47	4.16	4.36	101.	0.	0.01
440	35	4.21	4.21	1867	0.0	0.15	0.70	4.16	4.36	90.	0.	0.01
441	35	4.21	4.21	986	0.0	0.08	0.37	4.16	4.36	171.	0.	0.01
442	35	4.21	4.21	1112	0.0	0.09	0.42	4.16	4.36	703.	0.	0.06
443	35	4.21	4.21	1886	0.0	0.15	0.71	4.16	4.36	434.	0.	0.03
444	35	4.21	4.21	1142	0.0	0.09	0.43	4.16	4.36	363.	0.	0.03
445	35	4.21	4.21	1071	0.0	0.08	0.41	4.07	4.07	0.	0.00	0.00
446	35	4.09	4.09	1384	0.0	0.11	0.53	4.07	4.07	407.	0.	0.00
447	35	4.09	4.09	618	0.0	0.05	0.24	4.07	4.07	150.	0.	0.01
448	35	4.09	4.09	1181	0.0	0.09	0.46	4.07	4.07	0.	0.00	0.06
449	35	4.09	4.09	1254	0.0	0.10	0.49	4.07	4.07	0.	0.00	0.00
450	35	4.09	4.09	675	0.0	0.05	0.26	4.07	4.07	0.	0.00	0.00
451	35	4.09	4.09	681	0.0	0.05	0.26	4.07	4.07	0.	0.00	0.00
452	35	4.09	4.09	1490	0.0	0.12	0.58	4.07	4.07	0.	0.00	0.00
453	35	4.09	4.09	61	0.0	0.00	0.00	4.07	4.07	0.	0.00	0.00
454	35	4.09	4.09	1347	0.0	0.11	0.52	4.07	4.07	0.	0.00	0.00
455	35	4.09	4.09	1872	0.0	0.15	0.72	4.07	4.07	0.	0.00	0.00
456	35	4.09	4.09	664	0.0	0.05	0.26	4.07	4.07	0.	0.00	0.00
457	35	4.09	4.09	1343	0.0	0.11	0.52	4.07	4.07	570.	0.	0.01
458	35	4.09	4.09	1449	0.0	0.11	0.56	4.07	4.07	394.	0.	0.03
459	35	4.09	4.09	560	0.0	0.04	0.22	4.07	4.07	1185.	0.	0.03
460	35	4.09	4.09	1002	0.0	0.07	0.34	4.07	4.07	318.	0.	0.02
461	35	4.09	4.09	1356	0.0	0.11	0.52	4.07	4.07	944.	0.	0.07
462	35	4.09	4.09	1882	0.0	0.15	0.71	4.07	4.07	588.	0.	0.04
463	35	4.09	4.09	885	0.0	0.08	0.38	4.07	4.07	1547.	0.	0.12
464	35	4.09	4.09	1255	0.0	0.10	0.49	4.07	4.07	407.	0.	0.06
465	35	4.09	4.09	1686	0.0	0.15	0.73	4.07	4.07	1671.	0.	0.12
466	35	4.09	4.09	864	0.0	0.07	0.33	4.07	4.07	1367.	0.	0.11
467	35	4.09	4.09	1323	0.0	0.11	0.53	4.07	4.07	1738.	0.	0.07
468	35	4.09	4.09	1059	0.0	0.08	0.41	4.07	4.07	1864.	0.	0.15
469	35	4.09	4.09	656	0.0	0.05	0.26	4.07	4.07	969.	0.	0.03
470	35	4.09	4.09	1408	0.0	0.12	0.58	4.07	4.07	881.	0.	0.09
471	35	4.09	4.09	1231	0.0	0.10	0.48	4.07	4.07	1141.	0.	0.08
472	35	4.09	4.09	1695	0.0	0.15	0.72	4.07	4.07	1324.	0.	0.09
473	35	4.09	4.09	1582	0.0	0.12	0.61	4.07	4.07	414.	0.	0.13
474	35	4.09	4.09	1031	0.0	0.08	0.38	4.07	4.07	1243.	0.	0.07
475	35	4.09	4.09	945	0.0	0.07	0.37	4.07	4.07	312.	0.	0.02
476	35	4.09	4.09	1648	0.0	0.12	0.64	4.07	4.07	238.	0.	0.02
477	35	4.09	4.09	1091	0.0	0.08	0.40	4.07	4.07	1011.	0.	0.09
478	35	4.09	4.09	393	0.0	0.03	0.15	4.07	4.07	326.	0.	0.03
479	35	4.09	4.09	1391	0.0	0.11	0.53	4.07	4.07	125.	0.	0.03
480	35	4.09	4.09	436	0.0	0.03	0.13	4.07	4.07	704.	0.	0.06
481	35	4.09	4.09	313	0.0	0.03	0.16	4.07	4.07	368.	0.	0.03
482	35	4.09	4.09	413	0.0	0.03	0.16	4.07	4.07	172.	0.	0.03
483	35	4.09	4.09	638	0.0	0.05	0.24	4.07	4.07	2018.	0.	0.16
484	35	4.09	4.09	1096	0.0	0.08	0.40	4.07	4.07	1339.	0.	0.07
485	35	4.09	4.09	639	0.0	0.05	0.25	4.07	4.07	1596.	0.	0.13
486	35	4.09	4.09	1030	0.0	0.08	0.40	4.07	4.07	1363.	0.	0.07
487	35	4.09	4.09	383	0.0	0.03	0.15	4.07	4.07	1081.	0.	0.09
488	35	4.09	4.09	48	0.0	0.00	0.02	4.07	4.07	87.	0.	0.01
489	35	4.09	4.09	0	0.0	0.00	0.00	4.07	4.07	0.	0.00	0.03
490	35	4.09	4.09	0	0.0	0.00	0.00	4.07	4.07	0.	0.00	0.00
491	35	4.09	4.09	0	0.0	0.00	0.00	4.07	4.07	0.	0.00	0.00
492	35	4.09	4.09	104	0.0	0.01	0.04	4.07	4.07	730.	0.	0.02
493	35	4.09	4.09	369	0.0	0.03	0.14	4.07	4.07	796.	0.	0.06
494	35	4.09	4.09	683	0.0	0.05	0.24	4.07	4.07	161.	0.	0.03
495	35	4.09	4.09	286	0.0	0.02	0.11	4.07	4.07	0.	0.00	0.00
496	35	4.09	4.09	0	0.0	0.00	0.00	4.07	4.07	0.	0.00	0.00
497	35	4.09	4.09	571	0.0	0.05	0.22	4.07	4.07	132.	0.	0.01
498	35	4.09	4.09	835	0.0	0.07	0.31	4.07	4.07	674.	0.	0.05
499	35	4.09	4.09	0	0.0	0.00	0.00	4.07	4.07	126.	0.	0.05

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107/136

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VERIFICA PILASTRI:

VERIFICA PILASTRO IN CEMENTO ARMATO

Nome pilastro : P003a (ID=5)
Aste : 176
Metodo di verifica : stati limite - NTC08 (q=3.2)
Dettlilità : basca con gerarchia.
Unità di misura : cm; day; dan/cm; dan/cm; deform; %; 1/r Æ (permille)
Unità particolari : fessure {w}mm - ferrim e cm2 - sezioni:cm e derivate.
Copri-ferr (assi) : longitudoinal= 3.5 ; staffe= 2.5
Imperfetioni : M minimo = N * Æ0 ; M aggiunto = N * ei
Instabilità'ta' : rigidezza nominale {Ec2 5.8.7}; fief=3

MATERIALI

CLS : C25/30; Rck=300; fcd=249; fctd=17.91; fctm=25.58; Ecm=314472;
gc=1.5; fcd=141.1; fbd=26.86; fctd=11.94; Ecu=0.35%
ACCIAIO: B450C; ftk=5175; fyk=4500; Es=210000;
gc=1.5; fyk=3913; ftd=4500; ftd=4439.8; Eud=6.73%

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; fbd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.omegin=-15

SEZIONI UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acl=2500; i=y=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleç {e}y {e}z {e}iy {Lassi Lnet Lcr.L Cr.S} Af % am
1) 112.5 {2.5 | .4 | .4 } 120. {120. | 0. | 0. } 26.521.061120144616

CASI DI CARICO

Nome\Descrizione	Tipo	Sei
1)SU (statico)	SU (statico)	1
2)SU VENTOK	SU (statico)	1
3)SU con SIZMAX	SU (statico)	4
4)SU con SIZWAY	SU (statico)	4
5)Rara Ventok	RARA	1
6)Rara Ventok	RARA	1
7)Frequent	FREQUENTE	1
8)Frequent	FREQUENTE	1
9)Frequent	FREQUENTE	1
10)Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI SINGOLI):
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1 C 10 -1 -204890. -12752.11 -1008.6 -1.006 -8.7 -106.120.31SI
1 S 6 -1 -243580. -12752.11 -1008.6 -1.006 -8.7 -106.120.31SI

TAGLI GERARCHIA:
Asi Lp C caso Veyd- caso Veyd- caso Veyd-
1120. 6 -1 -3662.3 6 -1 0. 0 -3662.3 7 -1 107.74

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfetioni e second'ordine):
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
> 1) 3 -1 -18016.1107.27667.1105. -101. -28.61.00510.91SI
1 C 10 -1 -28958. -12752.11 -12992.11 -1008.6 -1.006 -8.7 -106.120.31SI
1 S 6 -1 -29401. -12752.11 -12992.11 -1008.6 -1.006 -8.7 -106.120.31SI

INSTABILITA' - RIGIDEZZA NOMINALE V {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -12543989.120. | 58199.2 | 8.962 | -17380.1 | -18550. | -186016. | .083

INSTABILITA' - RIGIDEZZA NOMINALE Z {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -12543989.120. | 58199.2 | 8.962 | 264220. | 279998. | 276647. | .083

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -1082. -3462.3 | 53520. | 53879. | 53520. | 1.51111. | 2.4 | .51SI
1 C 6 -1 -1082. -3462.3 | 53464.3 | 53879. | 53464.3 | 1.51111. | 2.4 | .51SI
1 S 6 -1 -1082. -3462.3 | 53408.6 | 53879. | 53408.6 | 1.51111. | 2.4 | .51SI

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -559.21 -1789.5 | 53879. | 53879. | 53879. | 1.51111. | 2.4 | .51SI
1 C 13 -1 -559.21 -1789.5 | 53842.1 | 53879. | 53842.1 | 1.51111. | 2.4 | .51SI
1 S 7 -1 -559.21 -1789.5 | 53786.7 | 53879. | 53786.7 | 1.51111. | 2.4 | .51SI

NEI LIMITE (Ned < Nmx, Nmx=63% di Ncls; Ncls=fcfdAc) {7.4.4.2.2.1};
Asta Caso Ned Nmx Ncls % NclsVEI
1) 3 -1 -1350. -229287.5 | -352750. | 1.3 | .51SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -19901.1 | -114806.4 | 181115.9 | -19. | 55.71SI
1 C 10 -1 -19901.1 | -114806.4 | 181115.9 | -19. | 55.71SI
1 S 10 -1 -19151.1 | -106746.9 | -3510.2 | -4.7 | -67.91SI

FREQUENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -1261.1 | -28975.7 | 12362.4 | -10. | 12.21SI
1 C 13 -1 -1261.1 | -28975.7 | 12362.4 | -10. | 12.21SI
1 S 13 -1 -11921.1 | -16129.2 | -3314.7 | -4.9 | -52.51SI

QUASI PERMANENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -141.1 | -8791.4 | -19951.1 | -3795.7 | -4. | -34. | .51SI
1 C 14 -1 -8791.4 | -19951.1 | -3795.7 | -4. | -34. | .51SI
1 S 14 -1 -8041.4 | -15004.9 | -580.4 | -3.4 | -34.21SI

VERIFICA PILASTRO IN CEMENTO ARMATO

Nome pilastro : P003b (ID=5)
Aste : 176
Metodo di verifica : stati limite - NTC08 (q=3.2)
Dettlilità : basca con gerarchia.
Unità di misura : cm; day; dan/cm; dan/cm; deform; %; 1/r Æ (permille)
Unità particolari : fessure {w}mm - ferrim e cm2 - sezioni:cm e derivate.
Copri-ferr (assi) : longitudoinal= 3.5 ; staffe= 2.5
Imperfetioni : M minimo = N * Æ0 ; M aggiunto = N * ei
Instabilità'ta' : rigidezza nominale {Ec2 5.8.7}; fief=3

MATERIALI

CLS : C25/30; Rck=300; fcd=249; fctd=17.91; fctm=25.58; Ecm=314472;
gc=1.5; fcd=141.1; fbd=26.86; fctd=11.94; Ecu=0.35%
ACCIAIO: B450C; ftk=5175; fyk=4500; Es=210000;
gc=1.5; fyk=3913; ftd=4500; ftd=4439.8; Eud=6.73%

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; fbd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.omegin=-15

SEZIONI UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acl=2500; i=y=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleç {e}y {e}z {e}iy {Lassi Lnet Lcr.L Cr.S} Af % am
1) 112.5 {2.5 | .4 | .4 } 120. {120. | 0. | 0. } 26.521.061120144616

CASI DI CARICO

Nome\Descrizione	Tipo	Sei
1)SU (statico)	SU (statico)	1
2)SU VENTOK	SU (statico)	1

3)SU con SIZMAX	SU (statico)	4
4)SU con SIZWAY	SU (statico)	4
5)Rara Ventok	RARA	1
6)Rara Ventok	RARA	1
7)Frequent	FREQUENTE	1
8)Frequent	FREQUENTE	1
9)Frequent	FREQUENTE	1
10)Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI SINGOLI):
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -2360580. -217537.11 -1008.6 -1.006 -8.7 -106.120.31SI
1 S 7 -1 -2371950. -217537.11 -1008.6 -1.006 -8.7 -106.120.31SI

TAGLI GERARCHIA:
Asi Lp C caso Veyd- caso Veyd- caso Veyd-
1120. 6 -1 -0. 6 -3 | 4173.1 | 7 -2 | -1459.2 | 7 -3 | 1027.1

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfetioni e second'ordine):
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
> 1) 3 -1 -10641.1 -187214.1102. -217537.1102. -1019. -25.51.017346.71SI
1 C 6 -1 -10153.1 -138871.1 -1019. -25.51.017346.71SI
1 S 3 -1 -9666.1 -10057.1104. | 28054.5 | 28. -1006. -8.51.00117.91SI

INSTABILITA' - RIGIDEZZA NOMINALE V {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -12528776.120. | 58128.6 | 8.96 | -219306.1 | -217532. | -217537. | .03

INSTABILITA' - RIGIDEZZA NOMINALE Z {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -12528776.120. | 58128.6 | 8.96 | -219306.1 | -217532. | -217537. | .03

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -1304.1 | 4173.1 | 53002.6 | 53879. | 53002.6 | 1.51111. | 2.4 | .51SI
1 C 6 -1 -1304.1 | 4173.1 | 53002.6 | 53879. | 53002.6 | 1.51111. | 2.4 | .51SI
1 S 6 -1 -1304.1 | 4173.1 | 52891.1 | 53879. | 52891.1 | 1.51111. | 2.4 | .51SI

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -456. -1459.2 | 53002.6 | 53879. | 53002.6 | 1.51111. | 2.4 | .51SI
1 C 7 -1 -456. -1459.2 | 53002.6 | 53879. | 53002.6 | 1.51111. | 2.4 | .51SI
1 S 7 -1 -456. -1459.2 | 53006.9 | 53879. | 53006.9 | 1.51111. | 2.4 | .51SI

NEI LIMITE (Ned < Nmx, Nmx=63% di Ncls; Ncls=fcfdAc) {7.4.4.2.2.1};
Asta Caso Ned Nmx Ncls % NclsVEI
1) 3 -1 -4756.7 | -229287.5 | -352750. | 1.3 | .51SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -7306.1 | -12261.7 | -14659.6 | -17.3 | 219.71SI
1 C 10 -1 -6931.1 -10469.7 | 71158.8 | -10.2 | 79.41SI
1 S 10 -1 -6556.1 -6463.7 | 3521.9 | -5. | -3.51SI

FREQUENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -131.1 | -4840. -3084. -90107.9 | -8.7 | 95.11SI
1 C 13 -1 -4465. -28932.2 | -48590.6 | -4.8 | 21.31SI
1 S 13 -1 -4090. -19122.5 | 1506.8 | -2.2 | -30.81SI

QUASI PERMANENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -141.1 | -4015. -15330.2 | -63032.4 | -6.3 | 64.41SI
1 C 14 -1 -3649. -11279.9 | -49038.4 | -3.4 | 3.41SI
1 S 14 -1 -3649. -7229.7 | 1395.5 | -1.5 | -12.81SI

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfetioni e second'ordine):
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
> 1) 3 -1 -1991.121366.11. -15412.1105. -101. -28.61.00510.91SI
1 C 3 -1 -1991.121366.11. -15412.1105. -101. -28.61.00510.91SI
1 S 3 -1 -1991.121366.11. -15412.1105. -101. -28.61.00510.91SI

INSTABILITA' - RIGIDEZZA NOMINALE V {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -12521779.120. | 58096.1 | 8.963 | -14614. | -15410. | -15412. | .006

INSTABILITA' - RIGIDEZZA NOMINALE Z {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -12521779.120. | 58096.1 | 8.963 | -14614. | -15410. | -15412. | .006

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -576.5 | 1844.9 | 52756.6 | 52756.6 | 52756.6 | 1.51111. | 2.3 | .51SI
1 C 6 -1 -576.5 | 1844.9 | 52756.6 | 52756.6 | 52756.6 | 1.51111. | 2.3 | .51SI
1 S 6 -1 -576.5 | 1844.9 | 52756.6 | 52756.6 | 52756.6 | 1.51111. | 2.3 | .51SI

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -1292.6 | 4136.3 | 52756.6 | 52756.6 | 52756.6 | 1.51111. | 2.3 | .51SI
1 C 7 -1 -1292.6 | 4136.3 | 52756.6 | 52756.6 | 52756.6 | 1.51111. | 2.3 | .51SI
1 S 7 -1 -1292.6 | 4136.3 | 52756.6 | 52756.6 | 52756.6 | 1.51111. | 2.3 | .51SI

NEI LIMITE (Ned < Nmx, Nmx=63% di Ncls; Ncls=fcfdAc) {7.4.4.2.2.1};
Asta Caso Ned Nmx Ncls % NclsVEI
1) 3 -1 -895.4 | -229287.5 | -352750. | 1.3 | .51SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -1332.3 | 147499.7 | -9442. -10.1 | 285.41SI
1 C 10 -1 -1332.3 | 147499.7 | -9442. -10.1 | 285.41SI
1 S 10 -1 -1332.3 | 147499.7 | -9442. -10.1 | 285.41SI

FREQUENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -723.5 | 50336.1 | -3388. -3.9 | 100.51SI
1 C 13 -1 -723.5 | 50336.1 | -3388. -3.9 | 100.51SI
1 S 13 -1 -723.5 | 50336.1 | -3388. -3.9 | 100.51SI

QUASI PERMANENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -141.1 | -540.5 | 30940. -188.1 | -2.1 | 49.91SI
1 C 14 -1 -540.5 | 30940. -188.1 | -2.1 | 49.91SI
1 S 14 -1 -540.5 | 30940. -188.1 | -2.1 | 49.91SI

VERIFICA PILASTRO IN CEMENTO ARMATO

Nome pilastro : P003b (ID=5)
Aste : 176
Metodo di verifica : stati limite - NTC08 (q=3.2)
Dettlilità : basca con gerarchia.
Unità di misura : cm; day; dan/cm; dan/cm; deform; %; 1/r Æ (permille)
Unità particolari : fessure {w}mm - ferrim e cm2 - sezioni:cm e derivate.
Copri-ferr (assi) : longitudoinal= 3.5 ; staffe= 2.5
Imperfetioni : M minimo = N * Æ0 ; M aggiunto = N * ei
Instabilità'ta' : rigidezza nominale {Ec2 5.8.7}; fief=3

CLS : C25/30; Rck=300; fcd=249; fctd=17.91; fctm=25.58; Ecm=314472;
gc=1.5; fcd=141.1; fbd=26.86; fctd=11.94; Ecu=0.35%
ACCIAIO: B450C; ftk=5175; fyk=4500; Es=210000;
gc=1.5; fyk=3913; ftd=4500; ftd=4439.8; Eud=6.73%

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; fbd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.omegin=-15

SEZIONI UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acl=2500; i=y=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleç {e}y {e}z {e}iy {Lassi Lnet Lcr.L Cr.S} Af % am
1) 112.5 {2.5 | .4 | .4 } 120. {120. | 0. | 0. } 26.521.061120144616

CASI DI CARICO

Nome\Descrizione	Tipo	Sei
1)SU (statico)	SU (statico)	1
2)SU VENTOK	SU (statico)	1
3)SU con SIZMAX	SU (statico)	4
4)SU con SIZWAY	SU (statico)	4
5)Rara Ventok	RARA	1
6)Rara Ventok	RARA	1
7)Frequent	FREQUENTE	1
8)Frequent	FREQUENTE	1
9)Frequent	FREQUENTE	1
10)Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

CLS : C25/30; Rck=300; fcd=249; fctd=17.91; fctm=25.58; Ecm=314472;
gc=1.5; fcd=141.1; fbd=26.86; fctd=11.94; Ecu=0.35%
ACCIAIO: B450C; ftk=5175; fyk=4500; Es=210000;
gc=1.5; fyk=3913; ftd=4500; ftd=4439.8; Eud=6.73%

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; fbd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.omegin=-15

SEZIONI UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acl=2500; i=y=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleç {e}y {e}z {e}iy {Lassi Lnet Lcr.L Cr.S} Af % am
1) 112.5 {2.5 | .4 | .4 } 120. {120. | 0. | 0. } 26.521.061120144616

CASI DI CARICO

Nome\Descrizione	Tipo	Sei
1)SU (statico)	SU (statico)	1
2)SU VENTOK	SU (statico)	1
3)SU con SIZMAX	SU (statico)	4
4)SU con SIZWAY	SU (statico)	4
5)Rara Ventok	RARA	1
6)Rara Ventok	RARA	1
7)Frequent	FREQUENTE	1
8)Frequent	FREQUENTE	1
9)Frequent	FREQUENTE	1
10)Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI SINGOLI):
Asta Caso Ned Meyd Mezd E cls oc E acc of VEI
1) 3 -1 -2329200. -217537.11 -1008.6 -1.006 -8.7 -106.120.31SI
1 S 7 -1 -2329200. -217537.11 -1008.6 -1.006 -8.7 -106.120.31SI

TAGLI GERARCHIA:
Asi Lp C caso Veyd- caso Veyd- caso Veyd-
1120. 6 -1 -1750.1 | 1844.9 | 7 -4 | -2486.2 | 7 -1 | 4136.3

TAGLIO Z:									
Asta	Caso	Ved	Ved ger.	Ved	Vrsd	Vrzd	Asw	s	ctgTIVE
1 I	7- 2	254.4	814.1	52756.6	52756.6	53413.1	1.51111	2.35	SI
1 C	7- 2	254.4	814.1	52756.6	52756.6	53356.5	1.51111	2.35	SI
1 S	7- 2	254.4	814.1	52756.6	52756.6	53300.1	1.51111	2.35	SI
NED LIMITE (Ned < Nmax ; Nmax=65% di Nc1s ; Nc1s=fcfd*Ac) [7.4.4.2.2.1]:									
Asta	Caso	Ned	Nmax	Nc1s	% Nc1sVE				
1 I	7- 3	-3838.5	-229287.5	-352750.	1.09	SI			

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	10- 1	-3521.5	-65522.6	39583.6	-6.5	68.2	SI
1 C	10- 1	-3146.5	-80845.6	10961.8	-5.9	79.3	SI
1 S	10- 1	-2771.5	-96168.7	-17660.	-7.6	135.8	SI

FREQUENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	13- 1	-2928.6	-26409.2	33187.6	-3.7	22.3	SI
1 C	13- 1	-2552.6	-20002.7	11456.7	-2.7	11.	SI
1 S	13- 1	-2178.6	-34976.2	-10274.2	-2.8	20.4	SI

QUASI PERMANENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	14- 1	-2664.6	-16951.	30223.6	-2.9	13.8	SI
1 C	14- 1	-2289.6	-17365.8	11157.5	-1.9	2.7	SI
1 S	14- 1	-1914.6	-17780.5	-7828.6	-1.7	3.4	SI

VERIFICA PILASTRO IN CEMENTO ARMATO

Nome pilastro : P03c (ID=6)
Asse : 175
Metodo di verifica : stati limite - NTC08 (n=3.2)
DatiVitali : bassa con gerarchia.
Unita' di misura : cm; dav; dav/cm; davcm; dav/cm2; deform. %; 1/r ðe'(permille)
Unita' particolari : fessure (m|mm - ferr|mm e cm2 - sezioni|cm e derivate.
CoeffFertt (assi) : long|tutti|s 3.5 ; staffe 2.5
Imperfezioni : M minimo = N * eð ; M aggiunto = N * ei
Inscab|Vital : rigidizza nominale [ðc2 5.8.7]; Fief=3

MATERIALI

CLS : C25/30; Rcs=300; fcd=240; fctd=17.91; fctm=25.58; fcm=314472;
gs=1.5; fcd=141.1; ftd=26.86; fctd=11.94; fctm=8.39;
ACCIAIO: B450c; fts=5175; fyk=4500; fts=2100000;
gs=1.5; fyð=3913; ftd=4500; ftd=4439.8; ftd=6.79%

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; ftd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.Omgel=n=35

SEZIONE UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acls=2500; iy=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleð | eð | leiz | eiy | Lassi Lnet | Lcr.I | Lcr.S | Af | % am |
1 I 1|2.5 | 2.5 | 4 | 4 | 120. | 120. | 0. | 0. | 26.52|1.06112n14+4n16 |

CASI DI CARICO

Nome	Descrizione	Tipo	Ses
1	SLU	SLU (statico)	1
2	SLU VENTOK	SLU (statico)	1
3	SLU VENTIOY	SLU (statico)	2
6	SLU con STEMAX	SLU (statico)	4
7	SLU con STEMAX	SLU (statico)	4
8	Rara	RARA	1
9	Rara Ventok	RARA	1
10	Rara Ventioy	RARA	2
11	Frequente	FREQUENTE	1
12	Frequente Ventok	FREQUENTE	1
13	Frequente Ventioy	FREQUENTE	2
14	Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI STATICI):

Asta	Caso	Mu+ min	Caso	Mu+ min	Caso	Mu- min	Caso	Mu- min
1 I	6- 1	-2345700.	6- 1	2345700.	7- 2	-2339910.	7- 2	2339980.
1 S	7- 4	-2341740.	7- 4	2341740.	7- 4	-2327280.	7- 4	2327280.

TAGLI GERARCHIA:

As	Lp	caso	VEyd-	caso	VEyd+	caso	VEzd-	caso	VEzd+
1	120.	6- 1	0.	7- 3	2053.5	7- 1	-889.8	7- 4	3.4

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfezioni e second'ordine):

Asta	Caso	NEd	MEyd	MEzd	E cls	oc	E acc	of	VE
> 1	3- 1	-4744.	-124117.1 02	-102697.1 02	-0.11	-14.9	0.11	233.	SI
1	3- 1	-4257.	-112810.1 1-	-53314.1.	-0.08	-10.8	0.07	156.7	SI
1	3- 1	-3769.	-104910.1 01	-10396.1 08	-0.05	-7.5	0.05	109.2	SI

INSTABILITA' - RIGIDENZA NOMINALE Y [ðc2 5.8.7]:

Asta	Caso	NEd	10	1n	1c1s2m	Mcal	NEd	Med	nu
1 I	3- 1	-12524066	120.	58106.5	8.9634	-122172.	-124070.	-124117.	.1013

INSTABILITA' - RIGIDENZA NOMINALE Z [ðc2 5.8.7]:

Asta	Caso	NEd	10	1n	1c1s2m	Mcal	NEd	Med	nu
1 I	3- 1	-12524066	120.	58106.5	8.9634	-100760.	-102658.	-102697.	.1013

TAGLIO Y:

Asta	Caso	Ved	Ved ger.	Ved	Vrsd	Vrzd	Asw	s	ctgTIVE
1 I	7- 3	641.7	2053.5	52009.9	53879.	52009.9	1.51111	2.4	SI
1 C	7- 3	641.7	2053.5	52854.2	53879.	52854.2	1.51111	2.4	SI
1 S	7- 3	641.7	2053.5	52796.5	53879.	52796.5	1.51111	2.4	SI

TAGLIO Z:

Asta	Caso	Ved	Ved ger.	Ved	Vrsd	Vrzd	Asw	s	ctgTIVE
1 I	7- 1	-278.1	-889.8	52921.8	53879.	52921.8	1.51111	2.4	SI
1 C	7- 1	-278.1	-889.8	52866.1	53879.	52866.1	1.51111	2.4	SI
1 S	7- 1	-278.1	-889.8	52810.3	53879.	52810.3	1.51111	2.4	SI

NED LIMITE (Ned < Nmax ; Nmax=65% di Nc1s ; Nc1s=fcfd*Ac) [7.4.4.2.2.1]:

Asta	Caso	NEd	Nmax	Nc1s	% Nc1s	VE
1	7- 1	-3434.	-229287.5	-352750.	.97	SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	10- 1	-3334.6	-82947.2	-71000.1	-10.2	153.2	SI
1 C	10- 1	-2959.6	-76003.6	-37460.4	-7.4	104.3	SI
1 S	10- 1	-2504.6	-69060.	-3503.7	-4.7	65.7	SI

FREQUENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
------	------	-----	------	------	----	----	----

1 I	13- 1	-2791.1	-37501.2	-61264.1	-6.4	81.1	SI
1 C	13- 1	-2416.1	-20240.2	-31515.2	-3.8	31.7	SI
1 S	13- 1	-2041.1	-20979.2	-1766.4	-1.6	1.	SI

QUASI PERMANENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	14- 1	-2546.8	-24959.2	-56442.5	-5.2	63.6	SI
1 C	14- 1	-2171.8	-16649.2	-28796.9	-2.8	18.3	SI
1 S	14- 1	-1796.8	-8339.3	-151.3	-1.	-4.6	SI

VERIFICA ASTE IN ACCIAIO:

VERIFICA ELEMENTI IN ACCIAIO

Numero = 15044.
Unità di misura:
Lunghezza: cm
Prop. sez.: cm
Rozze: daN
Momenti: daNm
Tensioni: daN/cm2
MATERIALE:
S235 (N 10025-2) Mod.EI = 210000000; $\rho_H = 1.050$;
fyk = 2350.0(2150.0 per sp=40 mm); fyd = 238.1(2047.6 per sp=40 mm).

CASI DI CARICO

N	Descrizione	Soll.
1	SU	1
2	SU VENTOS	2
3	SU VENTOS	2
4	SU con SISM	4
5	SU con SISM	4

CARATTERISTICHE GEOMETRICHE
P.LIN180.S001 (1)
A = 27.9857e+00 Ix= 1.3549e+03 Iy=113.3579e+00 Ix= 8.8711e+00
P.LIN180.S002 (2)
A = 78.2479e+00 Ix= 5.7065e+03 Iy= 2.0036e+03 Ix= 47.0030e+00
P.LIN180.S003 (3)
A = 54.3071e+00 Ix= 2.4964e+03 Iy=889.3628e+00 Ix= 24.5209e+00
P.LIN180.S001 (1) stato limite ultimo - ASTA (466- 470) 0.

PROGR.

COLLETTAZIONI							
Caso		MZ	MY	MT	N	TZ	TY
3-2		71104.7	117.6	-66.9	-777.7	-0.7	-1475
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-2	21	2	Sx	-505.4	0.0	0.0	505.4
3-2	21	9	Sx	444.5	-48.0	0.0	452.3
3-2	51		Ty	-25.8	0.0	128.1	223.3
3-2	51	8	Si	-500.1	47.9	0.0	507.0

COLLETTAZIONI										PROGR.		
Caso			MZ			MY	MT	N			TZ	TY
3-2			17376.2			147.5	-66.9	-990.9			-0.7	-1100
TENSIONI												
Caso	Ve	No	massimi			Sx	Tz	Ty			Si	
3-2	si	2	Sx			-157.4	0.0	0.0			157.4	
3-2	si	9				80.0	-38.2	0.0			103.8	
3-2	si	5	Ty			-32.9	0.0	97.1			171.3	
3-2	si	6	Si			-118.4	0.0	78.9			180.9	

SOLLECITAZIONI							PROGR.	
Caso			MZ	MY	MT	N	TZ	TY
3-2			-20726.0	177.3	-66.9	-1204.1	-0.7	-726
TENSIONI								
Caso	Ve	No	massimi	Sx	Tz	Ty	Si	
3-2	si	3	Sx	-188.6	0.0	0.0	188.6	
3-2	si	9		-180.7	-28.4	0.0	187.3	
3-2	si	5	Ty	-40.0	0.0	66.1	121.3	
							PROGR.	
								1

SELETTAZIONI							
Caso	MZ		MY	MT	N	TZ	TY
3-2	-43201.9		207.2	-66.9	-1417.2	-0.7	-351.8
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-2	si	3	Sx	-346.9	0.0	0.0	346.9
3-2	si	9	Tz	-337.6	-18.6	0.0	339.1
3-2	si	5	Ty	-47.1	0.0	35.1	76.9
-----							PROGR.
SOLLECITAZIONI							1

Gloso		MZ	MY	MT	N	TZ	TY
3-2		-50051.6	237.0	-66.9	-1630.4	-0.7	23.1
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-2	si	3	Sx	-401.3	0.0	0.0	401.3
3-2	si	8		274.2	-10.0	0.0	274.8
3-2	si	51	Ty	-54.2	0.0	-8.0	56.0
							PROGR.
2							
SELECCIONAZIONE							
Caso		MZ	MY	MT	N	TZ	TY
3-2		-50051.6	237.0	-66.9	-1630.4	-0.7	23.1

3-2		-41274.9		266.9		-66.9		-1843.6		-0.7		397.8	
TENSIONI													
Caso	Ve	No	massimi	Sx	Tz	Ty	Sx	Tz	Ty	Sx	Tz	Ty	
3-1	21	Sk		-352.0	0.0	0.0				352.0			
3-1	21	Sk		-208.3	-19.8	0.0				211.1			
3-1	51	Sk		-61.3	0.0	-38.9				91.2			

PROGR.													
2													
SOLLECITAZIONI :													
Caso	MZ	MY	MT	N	TZ	TY							
3-2	-16872.0	296.7	-66.9	-2056.8	-0.7	772							

SELEZIONE									
Caso	Ve	No	massimi	Sx	Tz	Ty	Si		
3-1	21	3	Sk	-198.8	0.0	0.0	198.8		
3-1	21	3	Sx	38.6	-29.6	0.0	64.2		
3-1	21	51	Ty	-68.5	0.0	-69.9	139.1		
-----								PROGR.	2
SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3-2	23157.3	326.5	-66.9	-2269.9	-0.7	1147			
TENSIONI :									
Caso	Ve	No	massimi	Sx	Tz	Ty	Si		

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-1	2	1	Sk	-249.6	0.0	0.0	249.6
3-2	2	1	Sx	-234.9	-39.4	0.0	244.7
3-2	2	1	Tz	-75.6	0.0	-100.9	190.4
3-2	2	1	Ty				

SOLLECITAZIONI :

Caso

MZ

MY

MT

N

TZ

TY

3-2

7882.8

356.4

-66.9

-2483.1

-0.7

1521

TENSIONI :

Caso

Ve

No

massimi

Sx

Tz

Ty

Si

3-2

2

1

Sk

-249.6

0.0

0.0

249.6

3-2

2

1

Sx

-234.9

-39.4

0.0

244.7

3-2

2

1

Tz

-75.6

0.0

-100.9

190.4

3-2

2

1

Ty

3-1	21	Sk	-450.2	Tz	0.0	450.2
3-1	21	Sk	-612.3	Tz	0.0	618.2
3-1	51	Sk	-82.7	Tz	0.0	-131.9
3-1	51	Sk	-242.9	Tz	0.0	242.9

VERIFICA STABILITA' :

LD = 334.						
LC = 334.	Ro = 6.96	Im = 48.0	Ncr= 252248.6	alfa(c) = 0.4900	ki= 0.8	
LC = 334.	Ro = 2.01	Im = 165.8	Ncr= 21104.6	alfa(c) = 0.4900	ki= 0.2	

VERIFICA STABILITA' :

Z	Lc = 334.0	Ro = 6.96	Im = 48.0	Ncr= 252248.6	alfa(c) = 0.4900	ki=0.8370
Y	Lc = 334.0	Ro = 2.01	Im = 165.8	Ncr= 21104.6	alfa(c) = 0.4900	ki=0.2422
Case 3-2 - Nod 2 - Asse Y						
Ned = -2483.1	Mseq = 59109.6	Mseq = 308.1	Ss = -178.5	(0.348)		
P.LIN180.S001 (1)	stato limite ultimo - ASTA (210- 330)			0.		
SELEZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	102333.6	105.5	-61.9	1464.6	-0.6	-1579.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
3-1	21	Sk	73.1	Tz	0.0	73.1
3-1	21	Sk	732.1	Tz	0.0	732.1
3-1	51	Sk	54.1	Tz	0.0	136.2

3-1	Si	Sk	733.9	-0.0	0.0	733.9
3-1	Si	9	732.1	-50.1	0.0	737.2
3-1	Si	5	54.1	0.0	136.2	242.0
SOLLECITAZIONE			PROGR.			
Caso	MZ	MY	MT	N	TZ	TY
3-1	43835.0	132.2	-61.9	1245.0	-0.6	-1204.8
TENSIONI						

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-1	1	51	Sk	337.9	0.0	0.0	337.9
3-1	1	51	Tz	335.7	-40.2	0.0	342.8
3-1	1	51	Ty	46.7	0.0	105.2	188.1

PROGR.

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-5007.6	168.6	-55.9	444.9	-0.9	-805.2
3-1	1079.8	158.8	-61.9	1025.3	-0.6	-830.2

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-1	21	1	Sx	52.0	0.0	0.0	52.0
3-1	21	5	Tz	43.8	-30.4	0.0	68.5
3-1	51	5	Tysi	39.3	0.0	74.2	134.5

SOLLECITAZIONI : PRGR. 1

Caso	MZ	MY	MT	N	TZ	TY
3-2	-30974.0	205.2	-55.9	225.3	-0.9	-430.5
3-1	-25932.0	185.4	-61.9	805.7	-0.6	-455.5

TENSIONI :

Caso	Ve	No	massimi	Sx	Tz	Ty	S1
3-1	1	5	Sk	217.3	0.0	0.0	217.3
3-1	1	9	Sz	-143.5	-20.6	0.0	147.8
3-1	1	5	Ty	31.9	0.0	43.3	81.4

SOLLECITAZIONE

Caso	MZ	MY	MT	N	TZ	TY
3-2	-41197.0	241.9	-55.9	5.6	-0.9	-56.0
3-1	-37200.4	212.1	-61.9	586.1	-0.6	-80.0

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty	S1
3-1	21	3	Sx	-284.3	0.0	0.0	284.3
3-1	21	5	Tz	-226.2	-10.8	0.0	226.9
3-1	21	5	Ty	24.5	0.0	12.3	32.5

SOLLECITAZIONE

:

Caso	MZ	MY	MT	N	TZ	TY
3-2	-35676.6	278.5	-55.9	-214.0	-0.9	318.8
3-1	-32725.3	238.7	-61.9	366.4	-0.6	293.8

TENSIONI

:

PROGR.

:

Caso	Ve	No	massimi	Sx	Tz	Ty	S1
3-1	21	3	Sx	-284.3	0.0	0.0	284.3
3-1	21	5	Tz	-226.2	-10.8	0.0	226.9
3-1	21	5	Ty	24.5	0.0	12.3	32.5

Caso		Ve	No	massimi	Sx	Tz	Ty	Sr
3-1	21	1	3	Sk	-257.1	0.0	0.0	257.1
3-1	21	1	5	Sk	230.5	-16.3	0.0	232.2
3-2	51	1	8	Tz	-2.9	0.0	-31.4	54.5
PROGR.								
2								
SOLLECITAZIONE								
Caso	MZ	MY	MT	N	TZ	TY		
3-2	-14412.8	315.2	-55.9	-433.6	-0.9	693.4	693.4	
3-1	-12506.9	265.3	-61.9	146.8	-0.6	668.8	668.8	
TENSIONI								
Caso	Ve	No	massimi	Sx	Tz	Ty		
3-1	21	1	3	Sk	-125.3	0.0	125.3	
3-1	21	1	5	Sk	88.3	0.0	99.3	
3-1	51	1	8	Sk	-10.1	0.0	-42.4	

Caso	ve	no	massimi	Sx	Tz	Ty	Sz
3-1	21	51	Sk	-125.3	0.0	0.0	125.3
3-1	51	81	Tz	88.3	-26.2	0.0	99.3
3-2	51	81	Ty	-10.1	0.0	-62.4	108.5

SOLLECITAZIONE

Caso	MZ	MY	MT	N	TZ	TY
3-2	22594.4	351.8	-55.9	-653.3	-0.9	1068.1
3-1	23455.0	292.0	-61.9	-72.8	-0.6	1043.1

TENSIONI

Caso	ve	no	massimi	Sx	Tz	Ty	Sz
3-1	21	51	Sk	-189.2	Tz	0.0	189.2
3-1	21	51	Sk	-158.4	Tz	0.0	170.2
3-1	51	81	Sk	-17.4	Tz	0.0	-39.4

3-1	21	Sk	-189.2	0.0	0.0	189.2
3-1	51	Tz	-158.4	-36.0	0.0	170.2
3-2	51	Ty	-17.4	0.0	-93.4	162.6

SOLLECITAZIONE

Caso	MZ	MY	MT	N	TZ	TY
3-2	75345.0	388.5	-55.9	-872.9	-0.9	1442.7
3-1	75160.2	318.6	-61.9	-292.5	-0.6	1417.7

TENSIONI

Caso	Ve	No	massimi	Sx	Tz	Ty
3-1	21	Sk	-549.1	Tz	0.0	549.1
3-1	21	Sk	-509.7	Tz	0.0	515.9
3-1	51	Sk	-34.6	Tz	0.0	-134.3

VERIFICA STABILITA' :

Z	L0 = 336.0	Ro = 6.96	Im = 48.3	Ncr= 248509.6	alfa(c) = 0.4900	ki=0.8349
	Lc = 336.0					

LC = 536.0 | 2.1011 m = 167.0 | NCR = 20931.6 | d11a (C) = 49000 | K1 = 2.2
 Caso 3-2 - Nodo 2 - ASSE Y
 Ned = -872.9 | Mreq = 70616.6 | Myeq = 314.5 | Ss = -615.8 (0.27)

P_UPN180_5001 (1) stato limite ultimo - ASTA (339 - 726)

SOLLECITAZIONE		MZ	MY	MT	N	TZ	TY
Caso	3-2	75345.0	363.4	148.3	-10.0	4.8	-1276
TENSIONI							
		</					

Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-1	2	1	Sk	-517.1	0.0	0.0	517.1
3-2	1	8	Tz	-500.8	54.5	0.0	509.6
3-2	1	5	Ty	5.8	0.0	118.9	206.1

PROGR.

SOLLECITAZIONE		MZ	MY	MT	N	TZ	TY
Caso		53231.6	273.6	148.3	-10.0	4.8	-1082

TENSIONI		Ve	No	massimi	Sx	Tz	Ty	Si
Caso								

3-2	21	8	Sx	-366.2	0.0	0.0	366.2
3-2	21	51	Sx	-354.0	49.4	0.0	364.1
3-2	21	51	Ty	4.3	0.0	102.9	178.3
							PROGR.
SOLLECITAZIONE							
Caso	MZ	MY	MT	N	TZ	TY	
3-1	34607.5	304.3	107.8	2.5	0.0	-887.6	
3-2	34751.8	183.8	148.3	-10.0	4.8	-888.6	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-1	21	2	Sk	-243.4	0.0	0.0	243.4
3-1	21	2	Sx	-231.2	0.0	0.0	243.6
3-1	51	2	Sx	2.8	0.0	0.0	88.9

3-1	21	Sk	-245.4	0.0	0.0	245.4
3-1	21	Sk	-231.2	44.3	0.0	243.6
3-1	51	Ty	2.8	0.0	86.9	150.5
-----PROGR.						
SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	19781.6	303.4	107.8	2.5	0.0	-693.9
3-2	19905.7	94.0	148.3	-10.0	4.8	-694.9
TENSIONI :						
Caso	Ve	No	massimi	Sx	Tz	Ty
3-1	21	Sk	-144.9	0.0	0.0	144.9
3-1	21	Sk	-132.6	0.0	0.0	149.0
3-1	51	Sk	1.2	0.0	0.0	70.8

3-2	si	8	Sx	-132.6	39.2	0.0	149.0
3-2	si	5	Ty	1.2	0.0	70.8	122.7
SOLLECITAZIONE				PROGR.			
Caso		MZ	MY	MT	N	TZ	TY
3-1		8589.4	302.5	107.8	2.5	0.0	-500
3-2		8693.2	4.2	148.3	-10.0	4.8	-501
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-1	21	21	Sk	-70.5	0.0	0.0	-70.5
3-1	21	21	Sk	-258.1	0.0	0.0	-258.1
3-1	51	51	Sk	-0.3	0.0	0.0	-54.8

3-2		si	8	3x																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
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VERIFICA STABILITA' :													
Z [L0 = 150, Ro = 6.96]m = 21.6]ncr= 1248070.3]a]fa(c) >=0.4900]ki=0.9850]													
Y [Lc = 150, Ro = 2.01]m = 74.5]ncr= 104421.1]a]fa(c) >=0.4900]ki=0.6662]													
Caso 3-1 - Noddo 2 - Assse Y													
Ned = -269.1]Mreq = 121618.6]Mreq = 320.4]ss = -836.8 (0.374)													
P.LPNR80_S001 (1) stato limite ultimo - ASTA (472- 731) 24													
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
3-2	165767.7	501.4	-179.4	N	303.9	TZ	-1.4	TY	-1881.7				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
3-2]1	4]Sk	SI	1120.5	0.0	0.0	1120.5							
3-2]1	9]Tz	SI	112.0	-74.4	0.0	113.9							
3-2]1	5]Ty	SI	19.4	0.0	0.0	171.8				19.			
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
3-2	132303.3	528.4	-179.4	N	303.9	TZ	-1.4	TY	-1687.9				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
3-2]1	4]Sk	SI	898.7	0.0	0.0	898.7							
3-2]1	9]Tz	SI	889.7	-89.3	0.0	897.8							
3-2]1	5]Ty	SI	19.8	0.0	0.0	155.8				38.			
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
3-2	102472.5	555.4	-179.4	N	303.9	TZ	-1.4	TY	-1494.1				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
3-2]1	4]Sk	SI	701.0	0.0	0.0	701.0							
3-2]1	9]Tz	SI	691.5	-64.2	0.0	700.4							
3-2]1	5]Ty	SI	20.3	0.0	0.0	139.7				56.			
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
3-1	75230.7	650.0	-147.5	N	-60.1	TZ	-5.0	TY	-1289.3				
3-2	76275.3	680.5	-179.4	N	303.9	TZ	-1.4	TY	-1300.3				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
3-1]1	2]Sk	SI	-531.0	0.0	0.0	531.0							
3-2]1	9]Tz	SI	517.5	-59.1	0.0	527.6							
3-2]1	5]Ty	SI	20.8	0.0	0.0	123.7				75.			
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
3-1	52873.4	743.2	-147.5	N	-60.1	TZ	-5.0	TY	-1095.5				
3-2	53711.8	699.5	-179.4	N	303.9	TZ	-1.4	TY	-1106.5				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
3-1]1	2]Sk	SI	-386.6	0.0	0.0	386.6							
3-2]1	9]Tz	SI	367.6	-54.0	0.0	379.4							
3-2]1	5]Ty	SI	187.7	0.0	0.0	107.7				94.			
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
3-1	34949.7	836.4	-147.5	N	-60.1	TZ	-5.0	TY	-980.7				
3-2	34782.0	686.5	-179.4	N	303.9	TZ	-1.4	TY	-912.7				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
3-1]1	2]Sk	SI	-266.4	0.0	0.0	266.4							
3-2]1	9]Tz	SI	252.9	-46.9	0.0	267.8							
3-2]1	5]Ty	SI	21.7	0.0	0.0	91.7				112.			
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
6-2	6524.1	2939.7	-38.3	N	-828.8	TZ	-25.2	TY	-229.8				
3-2	19485.9	663.5	-179.4	N	303.9	TZ	-1.4	TY	-718.9				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
6-2]1	3]Sk	SI	-205.2	0.0	0.0	205.2							
3-2]1	9]Tz	SI	140.3	-49.9	0.0	159.9							
3-2]1	5]Ty	SI	22.1	0.0	0.0	75.6				131.			
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
6-2	2701.9	3412.8	-38.3	N	-828.8	TZ	-25.2	TY	-128.5				
3-2	7823.4	690.6	-179.4	N	303.9	TZ	-1.4	TY	-525.1				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
6-2]1	3]Sk	SI	-200.3	0.0	0.0	200.3							
3-2]1	9]Tz	SI	62.8	-38.8	0.0	92.0							
3-2]1	5]Ty	SI	22.6	0.0	0.0	59.6				150.			
PROGR. :													
COLLETTAZIONE :													
Caso	MZ	MY	MT	N	TZ	TY							
3-1	-70.8	3885.9	-38.3	N	-828.8	TZ	-25.2	TY	-117.2				
3-2	-205.5	717.6	-179.4	N	303.9	TZ	-1.4	TY	-331.3				
TENSIONE :													
Caso	Ve]No]massimi	Sx	Tz	TY	SI								
3-1]1	3]Sk	SI	-204.0	0.0	0.0	204.0							
3-2]1	9]Tz	SI	9.5	-33.7	0.0	59.2							
3-2]1	5]Ty	SI	9.1	0.0	0.0	43.6				190.			
PROGR. :													

VERIFICA STABILITA' :														
[L0 = 150, Ro = 6.96]m = 21.6]ncr= 1248070.3]a]fa(c) >=0.4900]ki=0.9850]														
Y [Lc = 150, Ro = 2.01]m = 74.5]ncr= 104241.1]a]fa(c) >=0.4900]ki=0.6662]														
Caso 3-1 - Noddo 2 - Assse Y														
Ned = -60.1]Mreq = 123078.5]Mreq = 966.2]ss = -864.1 (0.380)														
P.LPNR80_S001 (1) stato limite ultimo - ASTA (28- 473) 25														
PROGR. :														
COLLETTAZIONE :														
Caso	MZ	MY	MT	N	TZ	TY								
3-2	0.0	0.0	0.0	N	-1775.5	TZ	99.4	TY	1267.1					
TENSIONE :														
Caso	Ve]No]massimi	Sx	Tz	TY	SI									
3-2]1	1]Sk	SI	47.4	0.0	0.0	63.4								
3-2]1	9]Tz	SI	43.1	41.8	0.0	96.3								
3-2]1	5]Ty	SI	-63.4	0.0	0.0	-104.8				42.				
PROGR. :														
COLLETTAZIONE :														
Caso	MZ	MY	MT	N	TZ	TY								
3-1	45104.1	3377.7	0.0	-430.4	-72.5	886.1								
3-2	45370.4	-3647.5	0.0	-1335.9	74.2	882.4								
TENSIONE :														
Caso	Ve]No]massimi	Sx	Tz	TY	SI									
3-1]1	2]Sk	SI	-475.1	0.0	0.0	475.1								
3-2]1	9]Tz	SI	245.8	29.8	0.0	251.1								
3-2]1	5]Ty	SI	-117.6	0.0	0.0	-73.8				84.				
PROGR. :														
COLLETTAZIONE :														
Caso	MZ	MY	MT	N	TZ	TY								
3-1	74646.9	6096.0	0.0	-2108.3	-47.3	511.7								
3-2	74999.0	-6235.7	0.0	-1336.3	49.0	512.4								
TENSIONE :														
Caso	Ve]No]massimi	Sx	Tz	TY	SI									
3-1]1	2]Sk	SI	-775.0	0.0	0.0	775.0								
3-2]1	9]Tz	SI	454.0	17.8	0.0	454.5								
3-2]1	5]Ty	SI	-117.6	0.0	0.0	-61.7								

PUNTO		Caso		Vel	Nel	messini	Sx	Tz	0,0	0,0	Ty	Sz	416,0	
3 - 1		1	1	1	1	1	416,0	0,0	0,0	0,0	0,0	0,0	416,0	
3 - 1		1	1	1	1	1	38,8	37,6	0,0	0,0	0,0	0,0	394,3	
3 - 1		1	1	1	1	1	166,0	0,0	0,0	117,9	0,0	0,0	204,8	
VERIFICA STABILITA' : asta tesa per tutti i casi di carico.														
P_LPJN30_0001 (- 1) stato l'inter ultimo - ASTA (750 - 460) 134 0.														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	-563,6	Tz	-0,5	Ty	-958,2
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	20,1	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-20,1	-25,2	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-70,1	0,0	0,0	79,2	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
SOLLECITAZIONE														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	15,4	0,0	0,0	-563,6	Tz	-0,5	Ty	-661,1
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	-175,5	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-174,8	-37,4	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-19,9	0,0	0,0	54,7	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
SOLLECITAZIONE														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	30,8	0,0	0,0	-563,6	Tz	-0,5	Ty	-363,9
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	-274,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-272,6	-9,6	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-19,6	0,0	0,0	30,1	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
SOLLECITAZIONE														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	46,2	0,0	0,0	-563,6	Tz	-0,5	Ty	-66,8
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	-313,8	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-313,8	-1,8	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-19,4	0,0	0,0	5,5	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
SOLLECITAZIONE														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	61,6	0,0	0,0	-563,6	Tz	-0,5	Ty	230,4
3 - 1		1	1	1	1	1	64,8	0,0	0,0	-131,6	0,0	0,0	0,0	0,0
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	-300,9	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-267,4	-6,3	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-26,4	0,0	0,0	-19,7	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
SOLLECITAZIONE														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	77,0	0,0	0,0	-563,6	Tz	-0,5	Ty	824,7
3 - 2		1	1	1	1	1	81,0	0,0	0,0	-131,6	0,0	-0,6	Ty	535,3
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	-229,2	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-193,6	-4,1	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-3,3	0,0	0,0	-44,3	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
SOLLECITAZIONE														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	92,4	0,0	0,0	-563,6	Tz	-0,5	Ty	832,4
3 - 2		1	1	1	1	1	97,2	0,0	0,0	-131,6	0,0	-0,6	Ty	832,4
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	-300,8	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-63,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-3,1	0,0	0,0	-68,8	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	-54,7	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
SOLLECITAZIONE														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	107,8	0,0	0,0	-563,6	Tz	-0,5	Ty	1121,8
3 - 2		1	1	1	1	1	113,4	0,0	0,0	-131,6	0,0	-0,6	Ty	1129,6
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	-134,3	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-124,4	-29,7	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-9,3	0,0	0,0	-93,4	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-29,3	0,0	0,0	-74,4	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
SOLLECITAZIONE														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	123,2	0,0	0,0	-563,6	Tz	-0,5	Ty	1419,0
3 - 2		1	1	1	1	1	129,6	0,0	0,0	-131,6	0,0	-0,6	Ty	1426,7
TENSIONI														
Caso		Vel		N		M		Tz		Ty		Sz		
3 - 1		1	1	1	1	1	-377,6	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-368,5	-37,5	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-35,5	0,0	0,0	0,0	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	-24,7	0,0	0,0	-39,3	0,0	0,0	0,0	0,0
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
VERIFICA STABILITA' :														
I = 230,0 ; Z = 6,961 m ; 33,31N/m = 53842,71n/mcf ; 40,4000N/(k · 0,024)														
LC = 230,0 ; Wb = 2,001 m ; 114,31N/m = 54043,14n/mcf ; 40,4000N/(k · 0,024)														
3 - 1 -														

3-1	11	21	Sx	Si	-27.71	0.01	0.0	271.5	
3-2	91	91	Tz		-78.7	-33.5	0.0	97.8	
3-1	91	61	Ty		16.8	0.0	58.7	103.1	
PROGR. 201.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-1133.8	2032.4	-17.2	-18.3	-237.1	-958.4	
3-1			-1394.6	3104.6	-13.8	-8.1	-309.1	-964.3	
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-166.9	9.0	0.0	0.0	166.9	0.0	
3-1			-71.9	-48.0	0.0	0.0	112.6	0.0	
3-1			-4.1	-0.0	0.0	85.4	123.5	0.0	
PROGR. 230.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 233.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 236.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 239.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 242.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 245.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 248.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 251.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 254.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 257.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 260.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 263.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 266.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 269.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 272.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 275.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 278.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 281.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 284.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 287.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5	-12.2	-18.3	-214.7	-1225.5	
3-1			-4941.7	-8608.0	-13.8	-13.4	302.9		
TENSIONE									
Caso	3-1		Sx	Sz	Tz	0.0	0.0	0.0	
3-1			-733.3	0.0	0.0	0.0	733.3	0.0	
3-1			-287.6	-62.5	0.0	0.0	100.3	0.0	
3-1			69.5	0.0	0.0	112.1	206.2	0.0	
PROGR. 290.									
COLLECTAZIONE									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
3-1			-432.2	89.5					

3-1	2,6	-155,8	0,0	-46,4	-0,7	-1188,6
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	4	Sk	Sx	Tz	0,0
3-1	1	8	Tz	6,3	31,2	0,0
3-2	1	5	Ty	4,3	0,0	96,3
3-2	1	5	Ty	6,3	0,0	96,3

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29898,7	136,5	0,0	101,7	0,7	-891,5
3-1	-29898,7	-136,3	0,0	-46,4	-0,7	-891,5
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,2	23,4	0,0
3-2	1	5	Ty	-4,0	0,0	73,7

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-51256,9	117,0	0,0	101,7	0,7	-594,3
3-1	-51256,9	-116,8	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	344,1	15,6	0,0
3-2	1	5	Ty	-3,6	0,0	49,1

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-64071,9	97,5	0,0	101,7	0,7	-297,2
3-1	-64071,9	-97,4	0,0	-46,4	-0,7	-297,2
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	429,2	7,9	0,0
3-2	1	5	Ty	-3,3	0,0	24,6

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-68343,8	78,0	0,0	101,7	0,7	0,0
3-1	-68343,8	-78,1	0,0	-46,4	-0,7	0,0
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	457,6	0,1	0,0
3-2	1	5	Ty	341,3	0,0	0,1

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-64072,6	58,5	0,0	101,7	0,7	297,1
3-1	-64072,6	-58,6	0,0	-46,4	-0,7	297,1
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	430,2	0,0	0,0
3-2	1	5	Ty	422,0	0,9	0,0

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-51258,2	39,0	0,0	101,7	0,7	0,0
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	0,0
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	336,9	15,6	0,0
3-2	1	5	Ty	4,3	0,0	-49,1

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29900,7	19,5	0,0	101,7	0,7	891,4
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	891,4
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,6	23,4	0,0
3-2	1	5	Ty	-19,0	0,0	199,2

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29900,7	19,5	0,0	101,7	0,7	891,4
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	891,4
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,6	23,4	0,0
3-2	1	5	Ty	-19,0	0,0	199,2

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29900,7	19,5	0,0	101,7	0,7	891,4
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	891,4
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,6	23,4	0,0
3-2	1	5	Ty	-19,0	0,0	199,2

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29900,7	19,5	0,0	101,7	0,7	891,4
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	891,4
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,6	23,4	0,0
3-2	1	5	Ty	-19,0	0,0	199,2

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29900,7	19,5	0,0	101,7	0,7	891,4
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	891,4
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,6	23,4	0,0
3-2	1	5	Ty	-19,0	0,0	199,2

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29900,7	19,5	0,0	101,7	0,7	891,4
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	891,4
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,6	23,4	0,0
3-2	1	5	Ty	-19,0	0,0	199,2

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29900,7	19,5	0,0	101,7	0,7	891,4
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	891,4
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,6	23,4	0,0
3-2	1	5	Ty	-19,0	0,0	199,2

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29900,7	19,5	0,0	101,7	0,7	891,4
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	891,4
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	202,6	23,4	0,0
3-2	1	5	Ty	-19,0	0,0	199,2

TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	425,8	7,8	0,0
3-2	1	5	Ty	0,3	0,0	24,6

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-68343,8	78,0	0,0	101,7	0,7	0,0
3-1	-68343,8	-78,1	0,0	-46,4	-0,7	0,0
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	143,9	0,0	0,0
3-2	1	5	Ty	0,0	0,0	0,0

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-64073,5	0,0	0,0	13,8	0,0	297,2
3-1	-64073,5	0,0	0,0	5,0	0,0	297,2
3-1	-64073,5	0,0	0,0	9,4	0,0	297,2
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	426,1	0,0	0,0
3-2	1	5	Ty	-45,4	7,8	0,0

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-51258,8	0,0	0,0	13,8	0,0	594,3
3-1	-51258,8	0,0	0,0	9,4	0,0	594,3
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	241,0	0,0	0,0
3-2	1	5	Ty	-340,2	15,6	0,0

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29901,0	0,0	0,0	13,8	0,0	891,5
3-1	-29901,0	0,0	0,0	9,4	0,0	891,5
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	199,1	0,0	0,0
3-2	1	5	Ty	-198,3	23,4	0,0

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29901,0	0,0	0,0	13,8	0,0	891,5
3-1	-29901,0	0,0	0,0	9,4	0,0	891,5
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	199,1	0,0	0,0
3-2	1	5	Ty	-198,3	23,4	0,0

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29901,0	0,0	0,0	13,8	0,0	891,5
3-1	-29901,0	0,0	0,0	9,4	0,0	891,5
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	199,1	0,0	0,0
3-2	1	5	Ty	-198,3	23,4	0,0

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29901,0	0,0	0,0	13,8	0,0	891,5
3-1	-29901,0	0,0	0,0	9,4	0,0	891,5
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	199,1	0,0	0,0
3-2	1	5	Ty	-198,3	23,4	0,0

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-2	-29901,0	0,0	0,0	13,8	0,0	891,5
3-1	-29901,0	0,0	0,0	9,4	0,0	891,5
TENSIONE						
Caso	Ve	No	massimi			
3-2	1	1	Sk	Sx	Tz	0,0
3-1	1	8	Tz	199,1	0,0	0,0
3-2	1	5	Ty	-198,3	23,4	0,0

Caso	MZ	MY	MT	N	TZ	TY	
3-1	23374,3	-79,9	0,0	-202,7	2,8	664,4	
3-2	23421,6	49,9	0,0	26,8	-1,7	666,1	
TENSIONE							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-1	1	1	Sk	-163,9	0,0	0,0	163,9
3-1	1	1	Sx	148,0	17,7	0,0	151,2
3-2	1	1	Tz	1,8	0,0	-55,1	95,4
3-1	1	1	Ty	-162,5	-17,2	0,0	165,2
3-1	1	1	Si				

SOLLECITAZIONE :							
Caso	MZ	My	MT	N	TZ	TY	
3- 1	-25130.2	41.5	-19.9	-10853.1	-10.8	17.9	
3- 2	16187.1	-478.7	13.5	-10088.7	-1.6	336.1	
TENSIONE :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3- 1	1	1	Sx	Si	0.0	182.9	
3- 1	1	6	Tz	Si	-182.9	0.0	
3- 2	1	1	Ty	Si	-129.0	0.0	
3- 2	1	6	Ty	Si	-129.0	0.0	

PROGR. 255.

SOLLECITAZIONE :							
Caso	MZ	MY	MT	N	TZ	TY	
3- 1	-25980.4	488.5	-19.9	-10619.2	-10.8	-17.9	
3- 2	30472.7	-412.4	13.5	-10054.8	-1.6	336.1	
TENSIONE :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3- 1	1	1	Sx	Si	0.0	0.0	186.1
3- 2	1	6	Tz	Si	-181.4	0.0	181.6
3- 2	1	9	Ty	Si	-128.6	-21.3	133.8

PROGR. 298.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 2	44758.3	-946.0	MT	13.5	-10020.9	-1.6			
3- 1	1	1	Sx	Si	0.0	208.2			
3- 1	1	6	Tz	Si	-208.2	0.0			
3- 2	1	1	9	Ty	-128.1	0.0			
3- 2	1	1	9	Ty	-128.1	0.0			

PROGR. 340.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 2	59043.8	-279.7	MT	13.5	-9987.1	-1.6			
3- 1	1	1	Sx	Si	0.0	208.2			
3- 1	1	6	Tz	Si	-208.2	0.0			
3- 2	1	1	9	Ty	-127.7	0.0			
3- 2	1	1	9	Ty	-127.7	0.0			

VERIFICA STABILITA' :									
[L0 = 340. ;									
Z [Lc = 340. ;Ro = 8.54]Im = 39.8]Ncr= 1023125.5]a]fa(b >=0.3400]ki=0.9165]									
Y [Lc = 340. ;Ro = 5.06]Im = 66.2]Ncr= 359233.9]a]fa(c >=0.4900]ki=0.7151]									
Caso 3- 1 - NodD 2 - Asse Y									
Ned = -11022.5]Mseq = -24978.2]Mseq = -897.3]Ss = -245.9 (0.110)									

P.HER200_5002 (2)									
stato limite ultimo - ASTA (-748 - 735)									
PROGR. 0.									

SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
3- 1	90763.4	-5006.5	0.0	-2840.4	-56.4	-218.8	
3- 2	-60905.4	-9669.8	0.0	-2848.5	-91.3	585.5	
TENSIONE :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3- 1	1	1	Sx	Si	0.0	547.9	
3- 1	1	6	Tz	Si	-547.9	0.0	
3- 2	1	1	9	Ty	-366.2	0.0	
3- 2	1	1	9	Ty	-366.2	0.0	

PROGR. 21.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	86251.5	-3844.0	0.0	-28453.9	-56.4	-218.8			
3- 2	-48829.4	-7785.8	0.0	-28466.0	-91.3	585.5			
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	Ty	Si		
3- 1	1	1	Sx	Si	0.0	0.0	534.0		
3- 1	1	6	Tz	Si	-269.5	0.0	270.0		
3- 2	1	9	Ty	Si	-365.5	0.0	371.0		
3- 2	1	9	Ty	Si	-365.5	-36.7	0.0		

PROGR. 41.

SOLLECITAZIONE :									
Caso		MZ	MY	MT	N	TZ	TY		
3- 1		81739.7	-2681.5	0.0	-2843.5	-56.4	-218.8		
3- 2		-36753.3	-5901.8	0.0	-2844.6	-91.3	585.5		
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	Ty	Si		
3- 1	1	1	Sx	Si	0.0	0.0	520.1		
3- 1	1	6	Tz	Si	-520.1	0.0	293.0		
3- 2	1	1	9	Ty	-364.9	0.0	370.4		
3- 2	1	1	9	Ty	-364.9	-36.7	0.0		

PROGR. 62.

Caso	MZ	MY	MT	N	TZ	TY
3- 1	77227.9	-1519.0	0.0	-2842.1	-56.4	-218.8
3- 2	-24677.3	-4017.8	0.0	-28433.1	-91.3	585.5
TENSIONE :						
Caso	Ve	No	massimi	Sx	Tz	TY
3- 1	1	1	Sx	Si	0.0	506.1
3- 1	1	6	Tz	Si	-506.1	0.0
3- 2	1	1	9	Ty	-364.3	0.0
3- 2	1	1	9	Ty	-364.3	0.0
-----						PROGR. 82.

PROGR. 82.

Caso	MZ	MY	MT	N	TZ	TY
3- 1	72716.0	-356.4	0.0	-28404.6	-56.4	-218.8
3- 2	-12601.2	-2133.9	0.0	-28416.7	-91.3	585.5
TENSIONE :						
Caso	Ve	No	massimi	Sx	Tz	Si
3- 1	1	1	Sx	-492.2	0.0	492.2
3- 1	1	6	Tz	-338.7	-9.5	0.0
3- 2	1	1	9	-363.6	0.0	369.2
3- 2	1	1	Ty	-363.6	0.0	-36.7
-----						PRGR. 103.

PROGR. 103.

Caso	MZ	MY	MT	N	TZ	TY
3-1	68204.2	806.1	0.0	-2838.2	-56.4	-218.8
3-2	-525.2	-249.9	0.0	-28400.3	-91.3	585.5
TENSIONE						
Caso	Ve	No	massimi	Sx	Tz	TY
3-1	1	1	Sx	Si	0.0	486.3
3-1	1	6	Tz	Si	-486.3	0.0
3-2	1	1	9	Ty	-363.0	0.0
3-2	1	1	9	Ty	-363.0	0.0
-----						PROGR. 124.

PROGR. 124.

Caso	MZ	MY	MT	N	TZ	TY
3- 1	63692.4	1968.6	0.0	-2837.7	-56.4	-218.8
3- 2	11550.9	1634.1	0.0	-2838.3	-91.3	585.5
TENSIONE :						
Caso	Vel	No	massimi	Sx	Tz	TY
3- 1	1	2	Sx	Si	0.0	484.0
3- 1	1	6	Tz	Si	-484.0	0.0
3- 2	1	9	Ty		-362.4	0.0
SOLLECITAZIONE :						
-----						PROGR. 144.

PROGR. 144.

3- 1	59180.5	3518.1	0.0	-28355.3	-56.4	-218.8	
3- 2	23626.9	3518.1	0.0	-28367.4	-91.3	585.5	
TENSIONE :							
Caso	Vel	No	massimi	Sx	Tz	Ty	Si
3- 1	1	1	Sx	Si	0.0	0.0	481.7
3- 1	1	6	Tz	Si	-481.7	0.0	408.2
3- 2	1	9	Ty	Si	-361.7	0.0	367.3
SOLLECITAZIONE :							PROGR. 165.

PROGR.

TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 2	1	4	Sx	-1343.7				313.7	
3- 2	1	6	Tz	1259.2	93.4	0.0		1269.6	
3- 2	1	9	Ty	-6.1	0.0	321.0		555.9	
PROGR.									
SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			130.
3- 2	1	-440679.6		533.2	N	-35.1	TZ	106.6	TZ
3- 2	1		-13864.4						-3427.2
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 2	1	4	Sx	-1537.6				1537.6	
3- 2	1	6	Tz	1441.2	89.5	0.0		1493.5	
3- 2	1	9	Ty	-6.9	0.0	321.8		557.3	

VERIFICA STABILITA' :
 Z Lc = 130. Ro = 6.78 lm = 19.2 Ncr= 3061590.91aIa(b >= 0.3400) ki= 0.9885
 Y Lc = 130. Ro = 4.04 lm = 32.1 Ncr= 1090715.11aIa(c >= 0.4900) ki= 0.9275
 Caso 3- 2 - Nodo 4 - Asse X
 Ned = -35.1 Mreq = -30509.7 Mreq = -10398.3 Ss = -1153.4 (0.515)

P.J.H.E.I.Q.5003 (3) stato limite ultimo - ASTA (20- 29) 39
 PROGR. 0.

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	-424559.2	-5021.1	-193.1	N	54.9		TZ	3299.7	
3- 2	-294674.7	-10765.9	-414.8		378.5		-83.0	3037.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	1406.7				1406.7	
3- 1	1	6	Tz	1294.8	-79.8	0.0		1302.1	
3- 1	1	9	Ty	-1.2	0.0	-299.3		518.1	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			16.
3- 1	-373011.4	-4993.4	-193.1	N	54.9		TZ	3300.7	
3- 2	-240064.8	-9497.7	-414.8		378.5		-83.0	3046.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	1229.5				1229.5	
3- 1	1	6	Tz	1132.9	-79.6	0.0		1143.1	
3- 1	1	9	Ty	-1.0	0.0	-296.3		517.1	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			32.
3- 1	-312510.0	-3765.8	-193.1	N	54.9		TZ	3281.7	
3- 2	-259601.2	-8089.4	-414.8		378.5		-83.0	3039.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	1052.7				1052.7	
3- 1	1	6	Tz	921.5	-79.1	0.0		964.4	
3- 1	1	9	Ty	-0.7	0.0	-297.7		515.7	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			49.
3- 1	-264555.8	-3138.2	-193.1	N	54.9		TZ	3286.6	
3- 2	-246284.0	-6741.2	-414.8		378.5		-83.0	3030.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	876.4				876.4	
3- 1	1	6	Tz	810.6	-79.1	0.0		864.4	
3- 1	1	9	Ty	-0.4	0.0	-296.9		514.3	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			65.
3- 1	-211246.3	-2310.5	-193.1	N	54.9		TZ	3286.6	
3- 2	-197113.0	-5392.9	-414.8		378.5		-83.0	3021.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	700.6				700.6	
3- 1	1	6	Tz	630.6	-79.1	0.0		684.4	
3- 1	1	9	Ty	-0.1	0.0	-296.1		512.9	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			81.
3- 1	-158283.9	-1882.9	-193.1	N	54.9		TZ	3254.7	
3- 2	-148088.4	-4044.7	-414.8		378.5		-83.0	3012.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	582.2				582.2	
3- 1	1	6	Tz	490.2	-79.0	0.0		508.9	
3- 1	1	9	Ty	0.2	0.0	-295.3		511.5	
3- 1	1	12	Ty	331.6	0.0	-277.7		588.2	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			98.
3- 1	-105467.8	-1255.3	-193.1	N	54.9		TZ	3245.7	
3- 2	-89210.1	-3696.5	-414.8		378.5		-83.0	3003.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	350.3				350.3	
3- 1	1	6	Tz	330.7	-78.8	0.0		357.7	
3- 1	1	6	Tz	310.4	-79.1	0.0		324.6	
3- 1	1	12	Ty	221.3	0.0	-276.9		528.3	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			114.
3- 2	-50478.2	-1348.2	-414.8	N	378.5		-83.0	2994.4	
3- 2	-52798.0	-627.6	-193.1	N	54.9		-83.0	3236.7	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 2	1	2	Sx	180.9				180.9	
3- 2	1	6	Tz	171.6	-78.6	0.0		219.1	
3- 2	1	6	Tz	0.7	0.0	-293.7		508.7	
3- 2	1	10	Ty	1.3	0.0	-293.7		508.7	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			130.
3- 1	-1891.5			N	54.9		TZ	3277.7	
3- 1	-224.6	0.0	-193.1	N	54.9		-83.0	3227.7	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 2	1	2	Sx	13.0				13.0	
3- 2	1	6	Tz	13.0	-78.5	0.0		136.5	
3- 2	1	9	Ty	11.0	0.0	-292.9		507.4	

VERIFICA STABILITA' :
 Z Lc = 130. Ro = 6.78 lm = 19.2 Ncr= 3061590.91aIa(b >= 0.3400) ki= 0.9885
 Y Lc = 130. Ro = 4.04 lm = 32.1 Ncr= 1090715.11aIa(c >= 0.4900) ki= 0.9275
 Caso 6- 2 - Nodo 3 - Asse X
 Ned = -17.0 Mreq = -10765.9 Mreq = 5447.4 Ss = -394.3 (0.176)

P.J.H.E.I.Q.5003 (3) stato limite ultimo - ASTA (41- 20) 40
 PROGR. 0.

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	-497281.5	-8081.2	-1530.1	N	59.8		TZ	7272.6	
3- 1	-157629.6	-1930.7	-4608.9		8.0		-919.4	1398.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	1667.4				1667.4	

6- 2	1	5	6	Tz	509.4		-301.3	0.0	729.2
3- 1	1	9	Ty	-2.5	0.0	-695.8		1205.1	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			1.
3- 1	-488191.3	-7698.7	-1530.1	N	59.8		TZ	7271.9	
3- 1	-155881.9	-781.4	-4608.9		8.0		-919.4	1397.9	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	1634.8				1634.8	
3- 1	1	6	Tz	1501.4	-301.3	0.0		1723.6	
3- 1	1	9	Ty	-2.4	0.0	-695.7		1205.0	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			2.
3- 1	-479101.8	-7316.2	-1530.1	N	59.8		TZ	7271.2	
3- 1	-154134.9	-367.8	-4608.9		8.0		-919.4	1397.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	1602.2				1602.2	
3- 1	1	6	Tz	1477.2	-301.3	0.0		1718.1	
3- 1	1	9	Ty	-2.2	0.0	-695.7		1204.9	

SOLLECITAZIONE									
Caso	MZ	MY	MT	N	TZ	TY			4.
3- 1	-470013.3	-6933.6	-1530.1	N	59.8		TZ	7270.5	
3- 1	-152388.5	-1517.0	-4608.9		8.0		-919.4	1396.8	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	0.0	0.0	Si	
3- 1	1	2	Sx	1569.7				1569.7	
3- 1	1	6	Tz	1485.3	-301.2	0.0		1712.5	
3- 1	1	9	Ty	-2.0	0.0	-695.6		1204.8	
3- 1	1	6	Tz	1522.1	-222.3	0.0		1570.1	

3-1	1st	9	Ty	-2.0	0.0	-695.6	1204.8
3-1	1st	9	Si	1522.1	-222.3	0.0	1570.1
SOLLECITAZIONE							5.
Caso	MZ	MY	MT	N	TZ	TY	
3-1	-460925.6	-6551.1	-1530.1	59.8	-306.0	7269.8	
6-2	-130642.8	2666.3	-4608.9	8.0	-919.4	1396.3	
TENSIONI							
Caso	Iv	No	massimi	Sx	Tz	Ty	Sz
3-1	1537.1	0.0	0.0	1537.1	0.0	1537.1	0.0

SOLLECITAZIONE :				PROG. :			
Caso	MZ	MY	MT	N	TZ	TY	
3-2	-419700.9	-6020.3	-199.0	-63.6	-39.8	-6962.1	
6-3	-127743.4	528.0	2475.6	52.9	501.5	-2668.4	
TENSIONE :							
Caso	Ve	No	massim	Sx	Tz	Ty	Si
3-2	Si	4	Sx	-1400.3	0.0	0.0	1400.3
6-3	Si	4	Sx	402.2	196.3	0.0	0.0
3-2	Si	9	Ty	-3.9	0.0	624.7	1082.0

```

VERIFICA STATISTICA :
Y      |L0 = 10. |
Z      |LC = 10. |Ro = 6.78 |Im = 1.5 |Ncr=517408865.8|alfa(b) =0.3400|ki=1.0000|
Y      |LC = 10. |Ro = 4.04 |Im = 2.5 |Ncr=184330846.8|alfa(c) =0.4900|ki=1.0000|
Caso 3 - 2 - Nodo 4 - Asse Y
Ned = -63.6 |Meqz = -463224.8 |Myeq = -6169.5 |ss = -1541.1 ( 0.689)

```

3-1	Si	4	Sx	-1377.1	0.0	0.0	1377.1
6-3	Si	5	Tz	395.4	211.1	0.0	538.5
3-1	Si	9	Tv	-7.2	0.0	-626.2	1084.7

VERIFICA STABILITA' :

Z	L0 = 10.1								
Y	Lc = 10.1	R0 = 6.78	Im = 1.5	Ncr = 517408865.8	a fa(b) = 0.3400	ki = 1.0000			
Z	Lc = 10.1	R0 = 4.04	Im = 2.5	Ncr = 184330846.8	a fa(c) = 0.4900	ki = 1.0000			

Caseo 3- 1 + Nod0 4 - Assie Y

Ned = -384.4 | Mreq = -479557.5 | Myeq = -256.9 | Ss = -1546.2 (0.691)

TENSIONI				Sx	Tz	Ty	Sy
Caso	Ve	No	massimi	-13.0	0.0	0.0	13.0
3-	1	1	Sx	0.1	-464.2	111.3	11.0
3-	1	1	Tz	-7.0	0.0	-278.0	481.6
3-	1	1	Ty				

VERIFICA STABILITA' :

$|L_0| = 130.$

Caso	VE	4	5	12	0	0	290.5
3-2	1	4	5	-290.5	0.0	0.0	290.5
3-1	5	1	9	175.9	-172.3	0.0	346.5
3-1	5	1	9	-12.3	0.0	509.9	883.2

PROGR. 2.

SOLLECITAZIONI

Caso	NZ	MT	N	TZ	TY
3-2	-93355.6	-374.3	-565.1	-9.1	-5637.0
3-1	-65446.1	-442.6	-1485.2	-3.2	-5195.8

TENSIONI

3-1	16690.4	4183.4	-502.7	-373.3	-32.3	1529.1
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	4	Sk	104.7	0.0	104.7
3-1	151	6	Tz	-69.3	-55.3	0.0
3-1	151	9	Ty	-5.0	0.0	183.2
3-1	151	10	Si	-8.7	0.0	263.8
PROGR.						
SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	41464.6	4709.0	-502.7	-373.3	TZ	1520.1
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	2	Sk	-182.1	0.0	182.1
3-1	151	6	Tz	-149.8	-11.1	0.0
3-1	151	9	Ty	-4.7	0.0	262.3
3-1	151	12	Si	-95.4	0.0	265.7

VERIFICA STABILITA' :

L0 = 130.0
 Z Lc = 130.0, Ro = 6.78 lm = 19.2 Ncr= 3061590.9, a(fa)(b) >= 0.3400 (k=0.9929)
 Y Lc = 130.0, Ro = 4.04 lm = 32.1 Ncr= 1090715.1, a(fa)(c) >= 0.4900 (k=0.9275)
 Caso 3-1 - Nod 3 - Asse Y
 Ned = -373.3 Mreq = -120620.0 Mreq = 3531.8 Ss = -425.8 (0.190)

P.JHERLO_5003 (3)						
stato limite ultimo - ASTA (748- 737)						
PROGR.						
SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	40256.3	4709.0	190.8	-131.6	TZ	746.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	2	Sk	-127.8	0.0	127.8
3-1	151	5	Tz	-121.4	27.1	0.0
3-1	151	9	Ty	-0.3	0.0	125.3
PROGR.						
SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	51963.6	2847.9	190.8	-131.6	TZ	592.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	2	Sk	-194.6	0.0	194.6
3-1	151	5	Tz	-162.9	24.4	0.0
3-1	151	9	Ty	-1.1	0.0	101.9

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	60974.7	986.7	190.8	-131.6	TZ	437.9
3-1	29464.3	2878.3	-179.3	115.0	TZ	-459.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	-206.7	0.0	206.7
3-1	151	5	Tz	-195.7	21.6	0.0
3-1	151	9	Ty	3.4	0.0	80.9

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	67289.5	874.4	190.8	-131.6	TZ	283.8
3-1	20074.9	3866.7	-179.3	115.0	TZ	-613.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	-225.9	0.0	225.9
3-1	151	5	Tz	-54.0	-22.5	0.0
3-1	151	9	Ty	3.9	0.0	60.3

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	70908.0	-2735.6	190.8	-131.6	TZ	129.7
3-1	7989.2	4855.0	-179.3	115.0	TZ	-767.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	-225.9	0.0	225.9
3-1	151	5	Tz	-13.1	-25.2	0.0
3-1	151	9	Ty	4.3	0.0	74.0

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	71830.3	-6596.8	190.8	-131.6	TZ	-24.2
3-1	6792.8	5843.4	-179.3	115.0	TZ	-921.7
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	-274.0	0.0	274.0
3-1	151	5	Tz	-36.4	-28.0	0.0
3-1	151	9	Ty	4.7	0.0	87.7

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	70956.3	-6457.9	190.8	-131.6	TZ	-178.8
3-1	24071.0	6831.7	-179.3	115.0	TZ	-1075.8
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	-285.0	0.0	285.0
3-1	151	5	Tz	94.5	-30.8	0.0
3-1	151	9	Ty	5.2	0.0	101.4

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	65986.0	-5319.1	190.8	-131.6	TZ	-332.5
3-1	44445.5	7820.1	-179.3	115.0	TZ	-1229.9
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	-287.4	0.0	287.4
3-1	151	5	Tz	-121.3	-12.5	0.0
3-1	151	9	Ty	5.6	0.0	115.1

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	67316.2	8808.4	-179.3	115.0	TZ	-56.5
3-1	297.1	237.1	0.0	0.0	TZ	297.1
3-1	236.7	-36.3	0.0	0.0	TZ	244.9
3-1	6.1	0.0	0.0	128.9	TZ	223.1

SOLLECITAZIONE :												
Caso		MZ		MY		MT		N		TZ		TY
3-1												
3-2												
TENSIONI												
Caso	Ve	No	massimi		Sx		Tz		Ty		Si	
3-1	151	3	Sk				0.0				297.1	
3-2	151	5	Sz		236.7		-36.3		0.0		244.9	
3-2	151	9	Ty		6.1		0.0		128.8		223.1	

VERTICALE STATISTICA :												

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3-1	180039.5	406.5	2315.3	N	-15.6	TZ	13.0	2563.4	
TENSIONI									
Caso	Ve	No	massimi	Sx	Tz	Si			
3-1	151	3	Sk	-580.9	0.0	580.9			
3-1	151	6	Tz	-175.8	-169.3	0.0			
3-1	151	9	Ty	-0.1	0.0	303.3			
3-1	151	8	Si	-578.1	168.6	0.0			
SOLLECITAZIONE :									

Caso	MZ		MY	MT	N	TZ	TY
3-1	119083.9		-60.5	2173.9	14.8	-45.2	-1916.6
3-2	115811.4		-569.4	2433.9	-155.2	13.7	-1898.8
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Si	
3-1	51	2	Sx	382.4	0.0	0.0	382.4
3-2	61	6	Tz	369.5	163.9	0.0	466.0
3-2	51	3	TY	-3.1	0.0	248.2	429.8
3-2	51	13	Si	-244.3	0.0	237.9	479.0

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	127480.1	-4.0	2173.9	14.8	-45.2	-1917.3
3-1	181818.5	-586.5	2433.9	-155.2	13.7	-1899.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	2	Sk	389.6	0.0	389.6
3-1	151	6	Tz	377.1	163.9	0.0
3-1	151	9	Ty	394.2	163.9	0.0
3-1	151	13	Si	-249.3	0.0	237.9

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	123877.1	12.5	2173.9	14.8	-45.2	-1920.0
3-1	120560.1	-603.6	2433.9	-155.2	13.7	-1900.2
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	397.7	0.0	397.7
3-1	151	6	Tz	392.4	164.0	0.0
3-1	151	9	Ty	-3.1	0.0	248.3
3-1	151	13	Si	-254.3	0.0	238.0

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	126275.0	109.0	2173.9	14.8	-45.2	-1918.7
3-1	122955.8	-620.6	2433.9	-155.2	13.7	-1900.9
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	405.9	0.0	405.9
3-1	151	6	Tz	392.4	164.0	0.0
3-1	151	9	Ty	-3.1	0.0	248.3
3-1	151	13	Si	-398.1	164.0	0.0

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	128673.7	165.5	2173.9	14.8	-45.2	-1920.3
3-1	125312.4	-637.7	2433.9	-155.2	13.7	-1901.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	414.1	0.0	414.1
3-1	151	6	Tz	400.1	164.0	0.0
3-1	151	9	Ty	-3.1	0.0	248.4
3-1	151	13	Si	-405.8	164.0	0.0

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	131073.3	222.0	2173.9	14.8	-45.2	-1920.0
3-1	127689.8	-654.8	2433.9	-155.2	13.7	-1902.3
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	1	Sk	422.3	0.0	422.3
3-1	151	6	Tz	407.7	164.0	0.0
3-1	151	9	Ty	-3.1	0.0	248.4
3-1	151	13	Si	-413.5	164.0	0.0

3-1	Si	1	Sx	422.3	0.0	0.0	422.3
3-2	Si	6	Ty	407.7	164.0	0.0	496.9
3-2	Si	9	Ty	-3.1	0.0	248.5	530.6
3-2	Si	7	Si	-413.5	164.0	0.0	401.6

8.

SOLLECITAZIONE :							PROGR.	
Caso		MZ	MY	MT	N	TZ	TY	
3-1		-133473.8	278.5	2173.9	14.8	-45.2	-1920.7	
3-1		-130068.0	-671.8	2433.9	-155.2	13.7	-1903.0	

TENSIONI							
Caso		Ve	No	massimi	Sx	Tz	Si

COLLETTA									
Caso	NZ	MV	MT	N	TZ	TY			
3-2	-5172.6	-202.4	15.6	-28.3	3.1	-816.7			
3-1	-6953.1	-901.6	69.4	-13.5	13.9	-781.1			
TENSIONI									
Caso	Vel	Mez	Sx	Tz	Ty	Sl			
3-2	1	0.0	0.0	0.0	0.0	168.3			
3-1	1	160.4	18.2	0.0	0.0	163.5			
3-2	4	0.0	0.0	0.0	0.0	204.3			
3-1	4	Tz	-166.9	15.6	0.0	169.0			
PROGR.									
3-2	1	0.0	0.0	0.0	0.0	211.5			
3-1	1	-253.0	15.6	-28.3	3.1	-816.7			
3-1	4	-1127.0	69.4	-13.5	13.9	-790.1			
COLLETTA									
Caso	NZ	MV	MT	N	TZ	TY			
3-2	-7807.6	-303.7	15.6	-28.3	3.1	-834.7			
3-1	-6512.9	-901.6	69.4	-13.5	13.9	-808.1			
3-1	62301.6	-1127.0	69.4	-13.5	13.9	-790.1			
TENSIONI									
Caso	Vel	Mez	Sx	Tz	Ty	Sl			
3-2	1	-211.3	0.0	0.0	0.0	211.5			
3-1	1	201.8	18.3	0.0	0.0	204.3			
3-2	4	-0.6	0.0	73.8	127.9	255.8			
3-1	4	Si	-209.7	15.8	0.0	221.5			
PROGR.									
3-2	1	0.0	0.0	0.0	0.0	211.5			
3-1	1	-253.0	15.6	-28.3	3.1	-816.7			
3-1	4	-1127.0	69.4	-13.5	13.9	-790.1			
COLLETTA									
Caso	NZ	MV	MT	N	TZ	TY			
3-2	-7807.6	-303.7	15.6	-28.3	3.1	-834.7			
3-1	-6512.9	-901.6	69.4	-13.5	13.9	-808.1			
3-1	62301.6	-1127.0	69.4	-13.5	13.9	-790.1			
TENSIONI									
Caso	Vel	Mez	Sx	Tz	Ty	Sl			
3-2	1	-211.3	0.0	0.0	0.0	211.5			
3-1	1	201.8	18.3	0.0	0.0	204.3			
3-2	4	-0.6	0.0	73.8	127.9	255.8			
3-1	4	Si	-209.7	15.8	0.0	221.5			
PROGR.									
3-2	1	0.0	0.0	0.0	0.0	211.5			
3-1	1	-253.0	15.6	-28.3	3.1	-816.7			
3-1	4	-1127.0	69.4	-13.5	13.9	-790.1			
COLLETTA									
Caso	NZ	MV	MT	N	TZ	TY			
3-2	-7807.6	-303.7	15.6	-28.3	3.1	-834.7			
3-1	-6512.9	-901.6	69.4	-13.5	13.9	-808.1			
3-1	62301.6	-1127.0	69.4	-13.5	13.9	-790.1			
TENSIONI									
Caso	Vel	Mez	Sx	Tz	Ty	Sl			
3-2	1	-211.3	0.0	0.0	0.0	211.5			
3-1	1	201.8	18.3	0.0	0.0	204.3			
3-2	4	-0.6	0.0	73.8	127.9	255.8			
3-1	4	Si	-209.7	15.8	0.0	221.5			
PROGR.									
3-2	1	0							

VERIFICA STABILITA' :

L0 = 130.

L1 = 130.

L2 = 130.

Ro = 6.74 m = 32.1 [Ncr]

Ro = 12.1 [Ncr]

Ro = 10.95 [Ncr]

10000.91 [a]faib

10000.91 [a]faib

10000.91 [a]faib

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SOLLECITAZIONE									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-15078.7	75.41	-4608.11	-2.31	41.61	1522.91		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	-49.0	Tz	0.0	49.0		
3-1	1	5	Sx	-48.4	Tz	0.0	476.5		
3-1	1	9	Tz	0.0	0.0	-285.9	495.2		
3-1	1	10	Si	-0.1	0.0	-285.9	495.1		1.
PROGR.									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-1374.6	23.41	-4608.11	-2.31	41.61	1522.91		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	-42.5	Tz	0.0	42.5		
3-1	1	5	Tz	42.2	273.7	0.0	475.9		
3-1	1	9	Tz	0.0	0.0	-285.8	495.1		
3-1	1	10	Si	-0.1	0.0	-285.8	495.1		2.
PROGR.									
SOLLECITAZIONE									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-9369.0	-80.5	-4608.11	-2.31	41.61	1521.6		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	-36.4	Tz	0.0	36.4		
3-1	1	5	Tz	36.0	273.7	0.0	475.3		
3-1	1	9	Tz	-0.1	0.0	-285.8	495.0		4.
PROGR.									
SOLLECITAZIONE									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-9369.0	-80.5	-4608.11	-2.31	41.61	1521.6		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	-30.8	Tz	0.0	30.8		
3-1	1	5	Sx	29.8	273.6	0.0	474.9		
3-1	1	9	Tz	-0.1	0.0	-285.7	494.9		5.
PROGR.									
SOLLECITAZIONE									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-7467.5	-132.51	-4608.11	-2.31	41.61	1520.9		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	-25.2	Tz	0.0	25.2		
3-1	1	5	Tz	23.6	273.6	0.0	474.5		
3-1	1	9	Tz	-0.1	0.0	-285.7	494.8		6.
PROGR.									
SOLLECITAZIONE									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-5566.9	-184.41	-4608.11	-2.31	41.61	1520.2		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	-19.5	Tz	0.0	19.5		
3-1	1	5	Sx	17.4	273.6	0.0	474.2		
3-1	1	9	Tz	-0.1	0.0	-285.6	494.7		8.
PROGR.									
SOLLECITAZIONE									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-3667.1	-236.41	-4608.11	-2.31	41.61	1519.5		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	-13.9	Tz	0.0	13.9		
3-1	1	5	Tz	11.2	273.6	0.0	474.0		
3-1	1	9	Tz	-0.1	0.0	-285.5	494.6		9.
PROGR.									
SOLLECITAZIONE									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-1768.2	-288.41	-4608.11	-2.31	41.61	1518.8		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	-8.3	Tz	0.0	8.3		
3-1	1	5	Sx	5.0	273.6	0.0	473.9		
3-1	1	9	Tz	-0.2	0.0	-285.5	494.5		10.
PROGR.									
SOLLECITAZIONE									
Caso	3-1	MZ	MY	MT	N	TZ	TY		
3-1	1	-315.6	449.31	-1472.8	1.1	-45.6	-68.4		
3-1	1	125.9	-340.3	-4608.11	-2.31	41.61	1518.1		
TENSIONI									
Caso	Ve	No	max						
3-1	1	1	Sx	5.1	Tz	0.0	5.1		
3-1	1	5	Sx	-1.2	273.6	0.0	473.8		
3-1	1	9	Tz	-0.2	0.0	-285.4	494.3		
VERIFICA SCELTA1A :									
I L0 = 30.1									
Z L0 = 10; (Ro = 6.78) m = 1.5 (Ncr=51470865.8) (a/b = 30.3400 / (ki=1.0000)									
Z Cso = 10; (Ro = 4.04) m = 2.5 (Ncr=158430846.8) (a/b = 30.4000 / (ki=1.0000)									
Caso 1-1 = Nodo 4 = Azze V									
NEd = -2.31 (Nzed = -13309.0) (Myeq = -255.2158 = -38.6 (C 0.017)									

S7	200.	7.	S27	144.	7.
S8	78.8	7.	S28	144.	7.
S9	124.6	7.	S29	150.	7.
S10	178.	7.	S30	150.	7.
S11	150.	7.	S31	150.	7.
S12	150.	7.	S32	150.	7.
S13	150.	7.	S33	150.	7.
S14	150.	7.	S34	150.	7.
S15	144.	7.	S35	150.	7.
S16	144.	7.	S36	150.	7.
S17	144.	7.	S37	150.	7.
S18	144.	7.	S38	150.	7.
S19	150.	7.	S39	150.	7.
S20	178.	7.	S40	150.	7.

MATERIE				
Acciaio S 235 (R 360)				
fcd 40mm<80mm				
2238.1				
Acciaio tirafond S 275 (R 430)				
fcd 2200.				

SOLLECITAZIONE AGENTI E STATO TENSIONALE

Combinazione di sollecitazioni agenti Caso 6 As. 35. Nd. 978

N: -6527.5 Ty: 23.5 Tz: 60.1

Mt: 0 My: 9575 Mz: 10090

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft,Ed / Td,Rd									
Num	Pv,Ed	Pv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Tad,Rd	Co-1	Co-2
1	16.1	3240.5	13714.3	-38.1	4860.7	19543.2	3564.	0	0
2	16.1	3240.5	13714.3	-26.7	4860.7	19543.2	3564.	0	0
3	16.1	3240.5	13714.3	-26.7	4860.7	19543.2	3564.	0	0
4	16.1	3240.5	13714.3	-34.	4860.7	19543.2	3564.	0	0

Verifica saldature									
Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome S_pmp Talpa,Talpe Seq-1 Seq-2 S_lim-1 S_lim-2Ver									
S2	31.9	7	0.	31.9	31.9	1997.5	2350.	1st	1st
S3	35.4	7	0.	35.4	35.4	1997.5	2350.	1st	1st
S4	35.9	7	0.	35.9	35.9	1997.5	2350.	1st	1st
S5	38.4	7	0.	38.4	38.4	1997.5	2350.	1st	1st
S6	42.2	7	0.	42.2	42.2	1997.5	2350.	1st	1st
S7	42.7	7	0.	42.7	42.7	1997.5	2350.	1st	1st
S8	38.1	7	0.	38.1	38.1	1997.5	2350.	1st	1st
S9	42.7	7	0.	42.7	42.7	1997.5	2350.	1st	1st
S10	42.7	7	0.	42.7	42.7	1997.5	2350.	1st	1st
S11	35.4	7	0.	35.4	35.4	1997.5	2350.	1st	1st
S12	35.8	7	0.	35.8	35.8	1997.5	2350.	1st	1st
S13	48.2	7	0.	48.2	48.2	1997.5	2350.	1st	1st
S14	48.6	7	0.	48.6	48.6	1997.5	2350.	1st	1st
S15	40.8	7	0.	40.8	40.8	1997.5	2350.	1st	1st
S16	40.4	7	0.	40.4	40.4	1997.5	2350.	1st	1st
S17	47.3	7	0.	47.3	47.3	1997.5	2350.	1st	1st
S18	47.7	7	0.	47.7	47.7	1997.5	2350.	1st	1st
S20	35.7	7	0.	35.7	35.7	1997.5	2350.	1st	1st
S21	28.9	7	0.	28.9	28.9	1997.5	2350.	1st	1st
S22	28.5	7	0.	28.5	28.5	1997.5	2350.	1st	1st
S23	41.7	7	0.	41.7	41.7	1997.5	2350.	1st	1st
S24	41.4	7	0.	41.4	41.4	1997.5	2350.	1st	1st
S25	28.9	7	0.	28.9	28.9	1997.5	2350.	1st	1st
S26	28.5	7	0.	28.5	28.5	1997.5	2350.	1st	1st
S27	35.7	7	0.	35.7	35.7	1997.5	2350.	1st	1st
S28	35.9	7	0.	35.9	35.9	1997.5	2350.	1st	1st
S29	0.	119.9	58.6	131.4	58.6	1997.5	2350.	1st	1st
S30	81.7	68.7	131.8	140.4	68.7	1997.5	2350.	1st	1st
S31	0.	185.1	58.6	194.1	58.6	1997.5	2350.	1st	1st
S32	104.5	84.6	58.6	146.7	84.6	1997.5	2350.	1st	1st
S33	104.5	84.6	134.4	104.5	134.4	1997.5	2350.	1st	1st
S34	104.5	84.6	104.5	156.5	104.5	1997.5	2350.	1st	1st
S35	104.5	84.6	134.4	104.5	134.4	1997.5	2350.	1st	1st
S36	0.	252.5	80.1	264.9	80.1	1997.5	2350.	1st	1st
S37	81.7	78.3	80.1	137.7	78.3	1997.5	2350.	1st	1st
S38	0.	187.3	80.1	203.7	80.1	1997.5	2350.	1st	1st
S39	81.7	68.7	0.	106.8	81.7	1997.5	2350.	1st	1st
S40	81.7	68.7	0.	106.8	81.7	1997.5	2350.	1st	1st

Verifica piastra				
Smax fcdVer				
72.7 2238.11St				
Verifica nervature				
Posizione Smax fcdVer				
Z 312. 2238.11St				
Y 285.5 2238.11St				

Verifica pressione sul calcestruzzo				
Smax fcdVer				
3.6 141.11St				

NDO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONE AGENTI Caso 6 As. 35. Nd. 978

Combinazione di sollecitazioni agenti Caso 3 As. 35. Nd. 978

N: -28482.5 Ty: 585.5 Tz: -91.3

Mt: 0 My: -9670 Mz: -60905

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft,Ed / Td,Rd									
Num	Pv,Ed	Pv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Tad,Rd	Co-1	Co-2
1	148.1	3240.5	13714.3	-142.8	4860.7	19543.2	3564.	0	0
2	148.1	3240.5	13714.3	-135.4	4860.7	19543.2	3564.	0	0
3	148.1	3240.5	13714.3	-95.3	4860.7	19543.2	3564.	0	0
4	148.1	3240.5	13714.3	-87.9	4860.7	19543.2	3564.	0	0

Verifica saldature									
Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome S_pmp Talpa,Talpe Seq-1 Seq-2 S_lim-1 S_lim-2Ver									
S1	171.1	6.5	1.	171.1	171.1	1997.5	2350.	1st	1st
S2	178.1	1.	0.	178.1	178.1	1997.5	2350.	1st	1st
S3	181.5	1.	0.	181.5	181.5	1997.5	2350.	1st	1st
S4	174.	1.	0.	174.	174.	1997.5	2350.	1st	1st
S5	171.	6.5	1.	171.1	171.1	1997.5	2350.	1st	1st
S6	136.4	1.	0.	136.4	136.4	1997.5	2350.	1st	1st
S7	127.	1.	0.	127.1	127.1	1997.5	2350.	1st	1st
S8	140.5	1.	0.	140.5	140.5	1997.5	2350.	1st	1st
S10	172.5	6.5	0.	172.6	172.5	1997.5	2350.	1st	1st
S11	168.4	6.5	0.	168.4	168.4	1997.5	2350.	1st	1st
S12	208.1	6.5	0.	208.2	208.1	1997.5	2350.	1st	1st
S13	131.	6.5	0.	131.1	131.	1997.5	2350.	1st	1st
S14	130.6	6.5	0.	130.8	130.6	1997.5	2350.	1st	1st
S15	172.	1.	0.	172.	172.	1997.5	2350.	1st	1st
S16	174.5	1.	0.	174.5	174.5	1997.5	2350.	1st	1st
S17	132.6	1.	0.	132.6	132.6	1997.5	2350.	1st	1st
S18	130.1	1.	0.	130.1	130.1	1997.5	2350.	1st	1st
S20	179.8	6.5	0.	179.9	179.8	1997.5	2350.	1st	1st
S21	215.	1.	0.	215.1	215.	1997.5	2350.	1st	1st
S22	215.4	6.5	0.	215.5	215.4	1997.5	2350.	1st	1st
S23	137.9	6.5	0.	137.7	137.9	1997.5	2350.	1st	1st
S24	137.9	6.5	0.	138.	137.9	1997.5	2350.	1st	1st

S25	184.	1.	0.	184.	184.	1997.5	2350.	1st	1st
S26	186.5	1.	0.	186.5	186.5	1997.5	2350.	1st	1st
S27	144.6	1.	0.	144.6	144.6	1997.5	2350.	1st	1st
S28	142.1	1.	0.	142.1	142.1	1997.5	2350.	1st	1st
S29	0.	1048.7	332.6	1100.2	332.6	1997.5	2350.	1st	1st
S30	409.8	363.9	332.6	641.1	363.9	1997.5	2350.	1st	1st
S31	0.	982.9	332.6	1037.6	332.6	1997.5	2350.	1st	1st
S32	186.8	349.5	332.6	638.4	349.5	1997.5	2350.	1st	1st
S33	386.8	347.8	0.	520.2	386.8	1997.5	2350.	1st	1st
S34	386.8	347.8	241.5	573.5	628.3	1997.5	2350.	1st	1st
S35	386.8	347.8	0.	520.2	386.8	1997.5	2350.	1st	1st
S36	0.	575.9	241.5	643.5	241.5	1997.5	2350.	1st	1st
S37	409.8	363.9	241.5	685.7	363.9	1997.5	2350.	1st	1st
S38	0.	641.8	241.5	685.7	241.5	1997.5	2350.	1st	1st
S39	409.8	363.9	0.	548.	409.8	1997.5	2350.	1st	1st
S40	409.8	363.9	0.	548.	409.8	1997.5	2350.	1st	1st

Verifica piastra				
Smax fcdVer				
419.8 2238.11St				
Verifica nervature				
Posizione Smax fcdVer				
Z 1107.1 2238.11St				
Y 1178.7 2238.11St				

Verifica pressione sul calcestruzzo				
Smax fcdVer				
14.9 141.11St				

NDO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONE AGENTI Caso 3

S2	153.8	.8	0.	153.8	153.8	1997.5	2350	.151
S3	153	.8	0.	153	153	1997.5	2350	.151
S4	150.7	.8	0.	150.7	150.7	1997.5	2350	.151
S5	159.5	2.	0.	159.5	159.5	1997.5	2350	.151
S6	159.9	.8	0.	159.9	159.9	1997.5	2350	.151
S7	163.9	.8	0.	163.9	163.9	1997.5	2350	.151
S8	163.9	.8	0.	163.9	163.9	1997.5	2350	.151
S9	158.1	2.	0.	158.1	158.1	1997.5	2350	.151
S10	148.1	2.	0.	148.1	148.1	1997.5	2350	.151
S11	147.8	2.	0.	147.8	147.8	1997.5	2350	.151
S12	167.1	.8	0.	167.1	167.1	1997.5	2350	.151
S13	166.8	2.	0.	166.8	166.8	1997.5	2350	.151
S14	148.3	2.	0.	148.3	148.3	1997.5	2350	.151
S15	147.7	.8	0.	147.7	147.7	1997.5	2350	.151
S16	158.1	2.	0.	158.1	158.1	1997.5	2350	.151
S17	158.6	.8	0.	158.6	158.6	1997.5	2350	.151
S18	163.6	2.	0.	163.6	163.6	1997.5	2350	.151
S19	153.1	2.	0.	153.1	153.1	1997.5	2350	.151
S20	153.3	2.	0.	153.3	153.3	1997.5	2350	.151
S21	172.1	2.	0.	172.1	172.1	1997.5	2350	.151
S22	172.3	2.	0.	172.3	172.3	1997.5	2350	.151
S23	157.4	.8	0.	157.4	157.4	1997.5	2350	.151
S24	156.8	2.	0.	156.8	156.8	1997.5	2350	.151
S25	167.1	.8	0.	167.1	167.1	1997.5	2350	.151
S26	167.7	.8	0.	167.7	167.7	1997.5	2350	.151
S27	0.	787.3	277.1	834.6	277.1	1997.5	2350	.151
S28	303.8	277.1	578.8	684.4	277.1	1997.5	2350	.151
S29	0.	737.3	277.1	787.7	277.1	1997.5	2350	.151
S30	389.8	291.7	771.5	560.2	667.	1997.5	2350	.151
S31	389.8	291.7	0.	486.9	389.8	1997.5	2350	.151
S32	389.8	309.1	319.4	591.2	709.3	1997.5	2350	.151
S33	389.8	291.7	0.	486.9	389.8	1997.5	2350	.151
S34	0.	837.1	319.4	895.9	319.4	1997.5	2350	.151
S35	407.3	303.8	319.4	606.9	726.7	1997.5	2350	.151
S36	0.	837.1	319.4	895.9	319.4	1997.5	2350	.151
S37	407.3	303.8	0.	508.1	407.3	1997.5	2350	.151
S38	0.	837.1	319.4	895.9	319.4	1997.5	2350	.151
S39	407.3	303.8	0.	508.1	407.3	1997.5	2350	.151
S40	407.3	303.8	0.	508.1	407.3	1997.5	2350	.151

Verifica piastra									
Smax fdlver									
Posizione Z									
147.3 2238.1151									

Verifica nervature									
Smax fdlver									
Posizione Z									
113.1 2238.1151									
Y									

Verifica pressione sul calcestruzzo									
Smax fdlver									
Posizione Z									
1071.9 2238.1151									
Y									

Verifica piastra									
Smax fdlver									
Posizione Z									
147.3 2238.1151									
Y									

Verifica nervature									
Smax fdlver									
Posizione Z									
113.1 2238.1151									
Y									

Verifica pressione sul calcestruzzo									
Smax fdlver									
Posizione Z									
1071.9 2238.1151									
Y									

Verifica piastra									
Smax fdlver									
Posizione Z									
147.3 2238.1151									
Y									

Verifica nervature									
Smax fdlver									
Posizione Z									
113.1 2238.1151									
Y									

Verifica pressione sul calcestruzzo									
Smax fdlver									
Posizione Z									
1071.9 2238.1151									
Y									

Verifica piastra									
Smax fdlver									
Posizione Z									
147.3 2238.1151									
Y									

Verifica nervature									
Smax fdlver									
Posizione Z									
113.1 2238.1151									
Y									

Verifica pressione sul calcestruzzo									
Smax fdlver									
Posizione Z									
1071.9 2238.1151									
Y									

Verifica piastra									
Smax fdlver									
Posizione Z									
147.3 2238.1151									
Y									

Verifica nervature									
Smax fdlver									
Posizione Z									
113.1 2238.1151									
Y									

Verifica pressione sul calcestruzzo									
Smax fdlver									
Posizione Z									
1071.9 2238.1151									
Y									

Verifica piastra									
Smax fdlver									
Posizione Z									
147.3 2238.1151									
Y									

Verifica nervature									
Smax fdlver									
Posizione Z									
113.1 2238.1151									
Y									

2238.1	2047.6	141.1	verifica piastra
Acciaio tirafondi S 275 (Fe 430)			Smax
fd			914.1
7000			2238.1
			fd ver
			SI

Verifica piastra			
Smax		fdlVer	
377.5	2238.1	St'	
Verifica nervature			
Smax		fdlVer	
Posizione		502	2238.1 St'
Z			
Y	437.8	2238.1	St'
Verifica pressione sul calcestruzzo			
Smax		fdlVer	
6.3	141.1	St'	

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 112 Nd. 734									
Combinazione di sollecitazioni agenti Caso 3 As. 112 Nd. 734									

N: -8956.7					Ty: 30.2		Tz: 22.5		
Mc: 0					My: 5003		Mz: 20095		

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft,Ed / T ad, Rd									
Nome S,grpi T ad,paI T ad,peI Seq-1 Seq-2 S,lim-1 S,lim-2 Ver									
1	9.4	3240.5 13714.3	-26.5	4860.7 19543.2	3564.	0.	0.	0.	0.
2	9.4	3240.5 13714.3	-30.4	4860.7 19543.2	3564.	0.	0.	0.	0.
3	9.4	3240.5 13714.3	-42.2	4860.7 19543.2	3564.	0.	0.	0.	0.
4	9.4	3240.5 13714.3	-46.	4860.7 19543.2	3564.	0.	0.	0.	0.

Verifica saldature									
Seq-1, S,lim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, S,lim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome S,grpi T ad,paI T ad,peI Seq-1 Seq-2 S,lim-1 S,lim-2 Ver									
S1	52.	5.4	0.	32.5	32.	1997.5	2350.	St'	
S2	29.3	8.	0.	29.3	29.3	1997.5	2350.	St'	
S3	40.4	-8.	0.	40.4	40.4	1997.5	2350.	St'	
S4	34.2	8.	0.	34.2	34.2	1997.5	2350.	St'	
S5	54.	5.4	0.	32.	32.	1997.5	2350.	St'	
S6	37.4	-8.	0.	37.4	37.4	1997.5	2350.	St'	
S7	42.4	-2.	0.	42.4	42.4	1997.5	2350.	St'	
S8	46.6	-8.	0.	46.6	46.6	1997.5	2350.	St'	
S9	42.3	-8.	0.	42.3	42.3	1997.5	2350.	St'	
S10	37.2	5.4	0.	37.6	37.2	1997.5	2350.	St'	
S11	57.	5.4	0.	101.5	101.4	1997.5	2350.	St'	
S12	101.8	-8.	0.	102.	101.8	1997.5	2350.	St'	
S13	101.6	5.4	0.	101.7	101.6	1997.5	2350.	St'	
S14	101.1	5.4	0.	101.3	101.1	1997.5	2350.	St'	
S15	42.9	-8.	0.	42.9	42.9	1997.5	2350.	St'	
S16	46.4	-8.	0.	46.4	46.4	1997.5	2350.	St'	
S17	35.6	-8.	0.	35.6	35.6	1997.5	2350.	St'	
S18	46.	46.	0.	46.	46.	1997.5	2350.	St'	
S19	46.9	3.9	0.	46.9	46.9	1997.5	2350.	St'	
S20	45.3	5.4	0.	45.6	45.3	1997.5	2350.	St'	
S21	95.1	5.4	0.	95.1	95.1	1997.5	2350.	St'	
S22	93.	5.4	0.	93.2	93.	1997.5	2350.	St'	
S23	109.5	5.4	0.	109.6	109.5	1997.5	2350.	St'	
S24	109.9	5.4	0.	109.9	109.9	1997.5	2350.	St'	
S25	27.5	-8.	0.	27.5	27.5	1997.5	2350.	St'	
S26	40.	40.	0.	40.	40.	1997.5	2350.	St'	
S27	50.	-8.	0.	50.	50.	1997.5	2350.	St'	
S28	54.5	-8.	0.	54.5	54.5	1997.5	2350.	St'	
S29	9.7	0.	0.	9.7	9.7	1997.5	2350.	St'	
S30	14.9	201.2	97.7	224.2	112.6	1997.5	2350.	St'	
S31	68.1	97.7	0.	68.1	68.1	1997.5	2350.	St'	
S32	43.6	175.7	97.7	205.7	141.3	1997.5	2350.	St'	
S33	43.6	175.7	0.	181.	43.6	1997.5	2350.	St'	
S34	43.6	175.7	0.	141.3	43.6	1997.5	2350.	St'	
S35	43.6	175.7	0.	181.	43.6	1997.5	2350.	St'	
S36	139.	0.	182.9	171.	40.3	1997.5	2350.	St'	
S37	14.9	201.2	174.	244.8	186.3	1997.5	2350.	St'	
S38	115.7	0.	444.	174.	175.	1997.5	2350.	St'	
S39	14.9	201.2	0.	201.8	14.9	1997.5	2350.	St'	
S40	14.9	201.2	0.	201.8	14.9	1997.5	2350.	St'	

Verifica piastra			
S _{max}		f _d /v _r	
138.3	2238.1	s _t '	
Verifica nervature			
Posizione	S _{max}	f _d /v _r	
Z	434.3	2238.1 s _t '	
Y	379.8	2238.1 s _t '	

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 7 As. 117 Nd. 742									
Combinazione di sollecitazioni agenti Caso 3 As. 117 Nd. 742									

N: -6277.6					Ty: 354.3		Tz: -152.3		
Mc: 0					My: -36373		Mz: -36373		

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft,Ed / T ad, Rd									
Nome S,grpi T ad,paI T ad,peI Seq-1 Seq-2 S,lim-1 S,lim-2 Ver									
1	96.4	3240.5 13714.3	-48.	4860.7 19543.2	3564.	0.	0.	0.	0.
2	96.4	3240.5 13714.3	-31.2	4860.7 19543.2	3564.	0.	0.	0.	0.
3	96.4	3240.5 13714.3	-19.6	4860.7 19543.2	3564.	0.	0.	0.	0.
4	96.4	3240.5 13714.3	-2.9	4860.7 19543.2	3564.	0.	0.	0.	0.

Verifica saldature									
Seq-1, S,lim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, S,lim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome S,grpi T ad,paI T ad,peI Seq-1 Seq-2 S,lim-1 S,lim-2 Ver									
S1	43.9	3.9	0.	44.1	43.9	1997.5	2350.	St'	
S2	53.1	1.6	0.	53.2	53.1	1997.5	2350.	St'	
S3	55.2	1.6	0.	55.2	55.2	1997.5	2350.	St'	
S4	44.	1.6	0.	44.	44.	1997.5	2350.	St'	
S5	43.3	3.9	0.	43.2	43.	1997.5	2350.	St'	
S6	21.5	1.6	0.	21.6	21.5	1997.5	2350.	St'	
S7	28.7	1.6	0.	28.7	28.7	1997.5	2350.	St'	
S8	16.4	1.9	0.	16.4	16.4	1997.5	2350.	St'	
S9	38.3	3.9	0.	38.5	38.3	1997.5	2350.	St'	
S10	60.	3.9	0.	60.4	60.	1997.5	2350.	St'	
S11	60.	3.9	0.	60.4	60.	1997.5	2350.	St'	
S12	59.3	3.9	0.	59.3	59.3	1997.5	2350.	St'	
S13	14.1	1.9	0.	14.6	14.1	1997.5	2350.	St'	
S14	100.1	30.	0.	100.2	100.1	1997.5	2350.	St'	
S15	38.1	3.9	0.	38.2	38.1	1997.5	2350.	St'	
S16	10.6	1.6	0.	10.6	10.6	1997.5	2350.	St'	
S17	14.6	1.6	0.	14.7	14.6	1997.5	2350.	St'	
S18	13.1	1.6	0.	13.2	13.1	1997.5	2350.	St'	
S19	54.7	3.9	0.	54.8	54.7	1997.5	2350.	St'	
S20	75.9	3.9	0.	75.2	75.1	1997.5	2350.	St'	
S21	75.9	3.9	0.	75.9	75.9	1997.5	2350.	St'	
S22	28.1	3.9	0.	29.1	28.1	1997.5	2350.	St'	
S23	28.1	3.9	0.	29.9	28.1	1997.5	2350.	St'	
S24	28.1	3.9	0.	29.9	28.1	1997.5	2350.	St'	
S25	20.7	1.6	0.	20.7	20.7	1997.5	2350.	St'	
S26	66.5	1.6	0.	66.5	66.5	1997.5	2350.	St'	
S27	150.5	1.9	0.	150.5	150.5	1997.5	2350.	St'	
S28	40.	1.6	0.	40.	40.	1997.5	2350.	St'	
S29	0.	374.6	90.1	385.3	90.1	1997.5	2350.	St'	
S30	150.6	125.5	90.1	200.7	125.5	1997.5	2350.	St'	
S31	0.	226.5	90.1	243.8	90.1	1997.5	2350.	St'	
S32	150.6	97.5	90.1	145.	97.5	1997.5	2350.	St'	
S33	58.9	89.3	0.	107.	58.9	1997.5	2350.	St'	
S34	58.9	89.							

S24	166.7	6.1	0.	166.8	166.7	1997.5	2350.	[.5T]
S25	15.7	1.9	0.	15.9	15.7	1997.5	2350.	[.5T]
S26	21.3	1.1	0.	21.4	21.3	1997.5	2350.	[.5T]
S27	92.6	1.9	0.	92.6	92.6	1997.5	2350.	[.5T]
S28	98.6	1.9	0.	98.6	98.6	1997.5	2350.	[.5T]
S29	0.	274.9	0.	66.1	281.2	1997.5	2350.	[.5T]
S30	61.2	312.7	0.	66.1	325.4	1997.5	2350.	[.5T]
S31	0.	458	0.	66.1	462.8	1997.5	2350.	[.5T]
S32	2.	175.1	0.	68.1	187.2	1997.5	2350.	[.5T]
S33	2.	175.1	0.	68.1	187.2	1997.5	2350.	[.5T]
S34	2.	185.1	0.	69.6	198.4	1997.5	2350.	[.5T]
S35	2.	175.1	0.	69.6	198.4	1997.5	2350.	[.5T]
S36	0.	784.3	0.	784.3	784.3	1997.5	2350.	[.5T]
S37	61.2	312.7	0.	784.3	784.3	1997.5	2350.	[.5T]
S38	0.	784.3	0.	784.3	784.3	1997.5	2350.	[.5T]
S39	61.2	312.7	0.	784.3	784.3	1997.5	2350.	[.5T]
S40	61.2	312.7	0.	784.3	784.3	1997.5	2350.	[.5T]

Verifica piastra	
Smx	[.5T]
Y	1373.9
Z	2238.1
Y	1373.9
Z	2238.1

Verifica nervature	
Posizione	Smx
Y	1010.6
Z	2238.1
Y	1373.9
Z	2238.1

Verifica pressione sul calcestruzzo	
Smx	[.5T]
Y	27.7
Z	141.1

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 117 Nd. 742

Combinazione di sollecitazioni agenti Caso 7 As. 176 Nd. 0

N	-3003.9	Ty	464	Tz	-224.6
Mc	0	My	-76337	Mz	-2259

Verifica tirafond										
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)										
Co-3: Ft,Ed / T.ad,Rd										
Num	Fv,Ed	Fv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Tad,Rd	Co-1	Co-2	Co-3
1	128.9	3240.5	13714.3	193.6	4860.7	19543.2	3564.	.07	.04	.05
2	128.9	3240.5	13714.3	-63.9	4860.7	19543.2	3564.	.04	.01	.02
3	128.9	3240.5	13714.3	193.6	4860.7	19543.2	3564.	.07	.04	.05
4	128.9	3240.5	13714.3	-58.2	4860.7	19543.2	3564.	.04	.01	.02

Verifica saldature									
Seq-1, Seq-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome	S.p.rp	Tau.p.a	Tau.p.e	Seq-1	Seq-2	Seq-1	Seq-2	Seq-1	Seq-2
S1	15.5	2.4	0.	11.8	11.5	1997.5	2350.	S16	83.6
S2	11.5	2.4	0.	11.8	11.5	1997.5	2350.	S17	82.1
S3	43.8	2.4	0.	43.7	43.7	1997.5	2350.	S18	82.1
S4	43.7	2.4	0.	43.7	43.7	1997.5	2350.	S19	13.1
S5	18.5	2.4	0.	18.5	18.5	1997.5	2350.	S20	8.6
S6	42.3	2.4	0.	42.4	42.3	1997.5	2350.	S21	11.5
S7	42.2	2.4	0.	42.2	42.2	1997.5	2350.	S22	11.5
S8	10.8	2.4	0.	10.8	10.8	1997.5	2350.	S23	11.5
S9	46.1	5.1	0.	46.1	46.1	1997.5	2350.	S24	14.4
S10	46.1	5.1	0.	46.1	46.1	1997.5	2350.	S25	49.2
S11	44.7	5.1	0.	44.7	44.7	1997.5	2350.	S26	49.1
S12	47.6	5.1	0.	47.6	47.6	1997.5	2350.	S27	50.6
S13	41.5	5.1	0.	41.5	41.5	1997.5	2350.	S28	50.7
S14	44.4	5.1	0.	44.7	44.4	1997.5	2350.	S29	0.
S15	83.5	2.4	0.	83.6	83.5	1997.5	2350.	S30	24.6
S16	83.6	2.4	0.	83.6	83.6	1997.5	2350.	S31	0.
S17	82.1	2.4	0.	82.1	82.1	1997.5	2350.	S32	216.1
S18	82.1	2.4	0.	82.1	82.1	1997.5	2350.	S33	216.1
S19	13.1	1.1	0.	12.6	13.1	1997.5	2350.	S34	216.1
S20	8.6	5.1	0.	8.6	8.6	1997.5	2350.	S35	216.1
S21	11.5	2.4	0.	14.1	11.5	1997.5	2350.	S36	0.
S22	11.5	2.4	0.	14.6	11.5	1997.5	2350.	S37	24.6
S23	11.5	2.4	0.	14.6	11.5	1997.5	2350.	S38	0.
S24	14.4	5.1	0.	15.3	14.4	1997.5	2350.	S39	24.6
S25	49.2	2.4	0.	49.2	49.2	1997.5	2350.	S40	24.6
S26	49.1	2.4	0.	49.1	49.1	1997.5	2350.		
S27	50.6	2.4	0.	50.7	50.6	1997.5	2350.		
S28	50.7	2.4	0.	50.8	50.7	1997.5	2350.		
S29	0.	157.5	28.2	160.	157.5	1997.5	2350.		
S30	24.6	31.1	28.2	24.6	24.6	1997.5	2350.		
S31	0.	375.2	28.2	376.3	28.2	1997.5	2350.		
S32	216.1	123.5	246.2	216.1	216.1	1997.5	2350.		
S33	216.1	123.5	0.	246.9	216.1	1997.5	2350.		
S34	216.1	123.5	0.	246.9	216.1	1997.5	2350.		
S35	216.1	123.5	0.	246.9	216.1	1997.5	2350.		
S36	0.	359.8	11.9	360.	11.9	1997.5	2350.		
S37	24.6	27.1	11.9	24.6	27.1	1997.5	2350.		
S38	0.	172.9	11.9	173.3	11.9	1997.5	2350.		
S39	24.6	13.7	0.	28.1	24.6	1997.5	2350.		
S40	24.6	13.7	0.	28.1	24.6	1997.5	2350.		

Verifica piastra	
Smx	[.5T]
Y	583.5
Z	2238.1
Y	583.5
Z	2238.1

Verifica nervature	
Posizione	Smx
Y	467.6
Z	2238.1
Y	467.6
Z	2238.1

Verifica pressione sul calcestruzzo	
Smx	[.5T]
Y	9.6
Z	141.1

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 7 As. 176 Nd. 0

Combinazione di sollecitazioni agenti Caso 7 As. 117 Nd. 742

N	-3003.9	Ty	432.9	Tz	-22.5
Mc	0	My	-7259	Mz	-76337

Verifica tirafondi										
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)										
Co-3: Ft,Ed / T.ad,Rd										
Num	Pv,Ed	Pv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	T.ad,Rd	Co-1	Co-2	Co-3
1	108.4	3240.5	13714.3	-58.6	4860.7	19543.2	3564.	.03	.01	.01
2	108.4	3240.5	13714.3	-64.8	4860.7	19543.2	3564.	.03	.01	.01
3	108.4	3240.5	13714.3	208.3	4860.7	19543.2	3564.	.06	.04	.04
4	108.4	3240.5	13714.3	214.	4860.7	19543.2	3564.	.06	.04	.04

Verifica saldature							
Seq-1, Seq-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)							
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)							
Nome	S.p.rp	Tau.p.a	Tau.p.e	Seq-1	Seq-2	Seq-1	Seq-2
S1	35.6	4.8	0.	35.9	35.6	1997.5	2350.
S2	40.8	4.8	0.	40.8	40.8	1997.5	2350.
S3	45.1	4.8	0.	45.1	45.1	1997.5	2350.
S4	39.8	4.8	0.	39.8	39.8	1997.5	2350.
S5	35.5	4.8	0.	35.9	35.5	1997.5	2350.
S6	7.9	4.8	0.	7.9	7.9	1997.5	2350.
S7	12.7	4.8	0.	12.7	12.7	1997.5	2350.
S8	41.1	4.8	0.	41.1	41.1	1997.5	2350.
S9	41.1	4.8	0.	41.1	41.1	1997.5	2350.
S10	41.1	4.8	0.	41.1	41.1	1997.5	2350.
S11	85.8	4.8	0.	85.8	85.6	1997.5	2350.
S12	85.6	4.8	0.	85.7	85.6	1997.5	2350.
S13	54.3	4.8	0.	54.5	54.3	1997.5	2350.
S14	54.4	4.8	0.	54.6	54.4	1997.5	2350.
S15	40.3	4.8	0.	40.3	40.3	1997.5	2350.

S16	43.4	4.8	0.	43.4	43.4	1997.5	2350.
S17	10.2	4.8	0.	10.2	10.2	1997.5	2350.
S18	13.4	4.8	0.	13.4	13.4	1997.5	2350.
S19	42.7	4.8	0.	43.	42.7	1997.5	2350.
S20	42.7	4.8	0.	43.	42.7	1997.5	2350.
S21	87.2	4.8	0.	87.3	87.2	1997.5	2350.
S22	134	4.8	0.	87.4	134	1997.5	2350.
S23	52.8	4.8	0.	53.	52.8	1997.5	2350.
S24	52.8	4.8	0.	53.	52.8	1997.5	2350.
S25	43.1	4.8	0.	43.1	43.1	1997.5	2350.
S26	46.2	4.8	0.	46.2	46.2	1997.5	2350.
S27	7.4	4.8	0.	7.4	7.4	1997.5	2350.
S28	10.6	4.8	0.	10.6	10.6	1997.5	2350.
S29	70.9	376.7	0.	70.9	70.9	1997.5	2350.
S30	38.3	136.4	70.9	138.5	109.2	1997.5	2350.
S31	38.3	136.4	70.9	138.5	109.2	1997.5	2350.
S32	32.8	125.1	70.9	147.5	103.8	1997.5	2350.
S33	32.8	125.1	0.	129.4	32.8	1997.5	2350.
S34	32.8	125.1	0.	130.8	32.8	1997.5	2350.
S35	32.8	125.1	0.	129.4	32.8	1997.5	2350.
S36	0.	167.7	53.1	175.9	53.1	1997.5	2350.
S37	38.3	136.4	53.1	151.3	91.4	1997.5	2350.
S38	0.	151.9	53.1	140.9	53.1	1997.5	2350.
S39	38.3	136.4	0.	141.7	38.3	1997.5	2350.
S40	38.3	136.4	0.	141.7	38.3	1997.5	2350.

Verifica piastra	
Smx	[.5T]
Y	568.1
Z	2238.1
Y	568.1
Z	2238.1

Verifica nervature	
Posizione	Smx
Y	389.2
Z	2238.1
Y	568.1
Z	2238.1

Verifica pressione sul calcestruzzo	
Smx	[.5T]
Y	10.
Z	141.1

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 7 As. 117 Nd. 742

Combinazione di sollecitazioni agenti Caso 1 As. 117 Nd. 742

N	-5160.4	Ty	-98.4	Tz	-166
Mc	0	My	-24032	Mz	55286

Verifica tirafondi										
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)										
Co-3: Ft,Ed / T.ad,Rd										
Num	Fv,Ed	Pv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Tad,Rd	Co-1	Co-2	Co-3
1	48,2	3240,5	13714,3	-6,1	4860,7	19543,2	3564,0	.01	0,0	0,0
2	48,2	3240,5	13714,3	16,4	4860,7	19543,2	3564,0	.02	0,0	0,0
3	48,2	3240,5	13714,3	-55,4	4860,7	19543,2	3564,0	.01	0,0	0,0
4	48,2	3240,5	13714,3	-32,6	4860,7	19543,2	3564,0	.01	.01	.02

Verifica saldature							
Seq-1, Seq-1:		NTC 2008, 4.2.8.2.4 formula (4.2.78)					
Seq-2, Seq-2:		NTC 2008, 4.2.8.2.4 formula (4.2.79)					
Nome	S.p.rp	Tau.p.a	Tau.p.e	Seq-1	Seq-2	Seq-1	Seq-2
S1	31.6	1.1	0.	31.6	31.6	1997.5	2350.
S2	19.5	1.8	0.	19.6	19.5	1997.5	2350.
S3	16.4	1.8	0.	16.5	16.4	1997.5	2350.
S4	9.4	1.8	0.	9.6	9.4	1997.5	2350.
S5	41.6	1.1	0.	41.6	41.6	1997.5	2350.
S6	43.5	1.8	0.	43.6	43.5	1997.5	2350.
S7	56.8	1.8	0.	56.8	56.8	1997.5	2350.
S8	37.1	1.1	0.	37.1	37.1	1997.5	2350.
S10	37.6	1.1	0.	37.6	37.6	1997.5	2350.
S11	30.4	1.1	0.	30.4	30.4	1997.5	2350.
S12	31.5	1.1	0.	31.5	31.5	1997.5	2350.
S13	70.8	1.8	0.	70.8	70.8	1997.5	2350.
S14	69.9	1.1	0.	69.9	69.9	1997.5	2350.
S15	10.7	1.8	0.	10.7	10.7	1997.5	2350.
S16	12.7	1.8	0.	12.7	12.7	1997.5	2350.
S17	37.3	1.8	0.	37.3	37.3	1997.5	2350.
S18	36.5	1.8	0.	36.5	36.5	1997.5	2350.
S20	55.7	1.1	0.	55.7	55.7	1997.5	2350.
S21	57.7	1.1	0.	57.7	57.7	1997.5	2350.
S22	17.7	1.1	0.	17.7	17.7	1997.5	2350.
S23	87.1	1.1	0.	87.1	87.1	1997.5	2350.
S24	88	1.1	0.	88	88	1997.5	2350.
S25	31.2	1.1	0.	31.2	31.2	1997.5	2350.
S26	29	1.1	0.	29	29	1997.5	2350.
S27	67	1.8	0.	67	67	1997.5	2350.
S28	69.3	1.8	0.	69.3	69.3	1997.5	2350.
S29	0.	46.4	10.3	47.6	10.3	1997.5	2350.
S30	41.8	10.3	136.8	41.8	10.3	1997.5	2350.
S31	0.	136.3	10.3	136.8	10.3	1997.5	2350.
S32	98.9	10.3	99.3	98.9	52.1	1997.5	2350.
S33	98.9	10.3	99.3	98.9	52.1	1997.5	2350.
S34	41.8	106.4	115.5	163.1	157.3	1997.5	2350.
S35	41.8	106.4	115.5	163.1	157.3	1997.5	2350.
S36	0.	231.9	115.5	277.7	115.5	1997.5	2350.
S37	0.	231.9	115.5	277.7	115.5	1997.5	2350.
S38	0.	414.7	115.5	430	115.5	1997.5	2350.
S39	99.6	115.5	0.	179	99.6	1997.5	2350.
S40	99.6	115.5	0.	179	99.6	1997.5	2350.

S51	29.61	12.51	0.	32.11	29.61	1997.51	2350.151*
S56	46.31	3.21	0.	46.41	46.31	1997.51	2350.151*
S71	46.21	3.21	0.	46.31	46.21	1997.51	2350.151*
S8	24.31	3.21	0.	24.61	24.31	1997.51	2350.151*
S10	48.31	12.51	0.	48.81	48.31	1997.51	2350.151*
S11	46.71	12.51	0.	46.81	46.71	1997.51	2350.151*
S12	48.71	12.51	0.	50.31	48.71	1997.51	2350.151*
S13	45.81	12.51	0.	45.91	45.81	1997.51	2350.151*
S14	47.81	12.51	0.	49.41	47.81	1997.51	2350.151*
S15	73.81	3.21	0.	73.91	73.81	1997.51	2350.151*
S16	73.91	3.21	0.	73.91	73.91	1997.51	2350.151*
S17	73.41	3.21	0.	73.41	73.41	1997.51	2350.151*
S18	73.41	3.21	0.	73.41	73.41	1997.51	2350.151*
S20	9.11	12.51	0.	15.41	9.11	1997.51	2350.151*
S21	11.41	12.51	0.	15.41	11.41	1997.51	2350.151*
S22	9.41	12.51	0.	15.71	9.41	1997.51	2350.151*
S23	10.51	12.51	0.	16.31	10.51	1997.51	2350.151*
S24	8.51	12.51	0.	15.11	8.51	1997.51	2350.151*
S25	16.61	3.21	0.	16.91	16.61	1997.51	2350.151*
S26	16.61	3.21	0.	16.91	16.61	1997.51	2350.151*
S27	17.11	3.21	0.	17.31	17.11	1997.51	2350.151*
S28	17.11	3.21	0.	17.41	17.11	1997.51	2350.151*
S29	0.11	26.41	53.11	59.21	0.11	1997.51	2350.151*
S30	17.51	54.61	53.11	78.11	17.51	1997.51	2350.151*
S31	0.11	307.71	53.11	332.11	0.11	1997.51	2350.151*
S32	143.71	95.51	53.11	180.51	143.71	1997.51	2350.151*
S33	143.71	95.51	54.61	181.11	143.71	1997.51	2350.151*
S34	143.71	95.51	54.61	181.11	143.71	1997.51	2350.151*
S35	143.71	95.51	54.61	181.11	143.71	1997.51	2350.151*
S36	0.11	322.81	54.61	327.51	0.11	1997.51	2350.151*
S37	17.51	53.31	54.61	78.31	17.51	1997.51	2350.151*
S38	0.11	322.81	54.61	327.51	0.11	1997.51	2350.151*
S39	17.51	8.61	0.	19.51	17.51	1997.51	2350.151*
S40	17.51	8.61	0.	19.51	17.51	1997.51	2350.151*

Verifica piastra							
Smx1 fdlVer							
361.71 2238.1151*							

Verifica nervature							
Posizione Smx fdlVer							
Z 361.71 2238.1151*							
Y 355.31 2238.1151*							

Verifica pressione sul calcestruzzo							
Smx1 fdlVer							
4.61 141.1151*							

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 175 Nd. 0

Combinazione di sollecitazioni agenti Caso 7 As. 175 Nd. 0

N: -2604 Ty: -641.7 Tz: -240.2

Mt: 0 Mx: 65881 Mz: 2735

Verifica tirafond							
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)							
Co-3: Ft,Ed / Tsd,Ed							
Num Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed							
1	171.31	3240.51	13714.31	171.11	4860.71	19543.21	3564.108 .04 .05151*
2	171.31	3240.51	13714.31	-49.31	4860.71	19543.21	3564.108 .01 .01151*
3	171.31	3240.51	13714.31	164.41	4860.71	19543.21	3564.108 .03 .05151*
4	171.31	3240.51	13714.31	-56.11	4860.71	19543.21	3564.105 .01 .02151*

Verifica saldature							
Seq-1, SLim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)							
Seq-2, SLim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)							
Nome S,prp1 Tsd,prp1 Tsd,prp1 Seq-1 Seq-2 SLim-1 SLim-2Ver							
S1	13.61	1.71	0.	15.41	13.61	1997.51	2350.151*
S2	9.51	2.61	0.	9.81	9.51	1997.51	2350.151*
S3	36.21	2.61	0.	36.31	36.21	1997.51	2350.151*
S4	36.31	2.61	0.	36.41	36.31	1997.51	2350.151*
S5	16.21	7.11	0.	17.71	16.21	1997.51	2350.151*
S6	38.11	2.61	0.	38.11	38.11	1997.51	2350.151*
S7	38.21	2.61	0.	38.21	38.21	1997.51	2350.151*
S8	10.21	6.21	0.	10.61	10.21	1997.51	2350.151*
S10	40.11	7.11	0.	40.61	40.11	1997.51	2350.151*
S11	35.61	3.51	0.	35.61	35.61	1997.51	2350.151*
S12	38.11	7.11	0.	38.81	38.11	1997.51	2350.151*
S13	39.11	7.11	0.	39.71	39.11	1997.51	2350.151*
S14	41.61	7.11	0.	41.61	41.61	1997.51	2350.151*
S15	70.61	2.61	0.	70.71	70.61	1997.51	2350.151*
S16	70.51	2.61	0.	70.61	70.51	1997.51	2350.151*
S17	72.41	2.61	0.	72.41	72.41	1997.51	2350.151*
S18	72.51	2.61	0.	72.61	72.51	1997.51	2350.151*
S20	11.51	7.11	0.	11.51	11.51	1997.51	2350.151*
S21	10.61	7.11	0.	12.81	10.61	1997.51	2350.151*
S22	13.11	7.11	0.	14.91	13.11	1997.51	2350.151*
S23	7.11	7.11	0.	10.11	7.11	1997.51	2350.151*
S24	9.61	7.11	0.	12.11	9.61	1997.51	2350.151*
S25	43.91	2.61	0.	44.11	43.91	1997.51	2350.151*
S26	44.11	2.61	0.	44.11	44.11	1997.51	2350.151*
S27	42.11	2.61	0.	42.21	42.11	1997.51	2350.151*
S28	42.11	2.61	0.	42.11	42.11	1997.51	2350.151*
S29	0.11	35.31	21.11	35.31	0.11	1997.51	2350.151*
S30	21.11	22.91	21.11	37.41	21.11	1997.51	2350.151*
S31	0.11	306.21	21.11	306.91	0.11	1997.51	2350.151*
S32	186.41	109.91	21.11	217.41	186.41	1997.51	2350.151*
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S34	186.41	109.91	16.11	217.11	186.41	1997.51	2350.151*
S35	186.41	109.91	0.	216.41	186.41	1997.51	2350.151*
S36	0.11	306.91	16.11	327.31	0.11	1997.51	2350.151*
S37	21.11	27.61	39.11	57.41	21.11	1997.51	2350.151*
S38	0.11	133.81	16.11	163.11	0.11	1997.51	2350.151*
S39	21.11	11.91	0.	24.11	21.11	1997.51	2350.151*
S40	21.11	11.91	0.	24.11	21.11	1997.51	2350.151*

Verifica piastra							
Smx1 fdlVer							
460.11 2238.1151*							

Verifica nervature							
Posizione Smx fdlVer							
Z 460.11 2238.1151*							
Y 425.91 2238.1151*							

Verifica pressione sul calcestruzzo							
Smx1 fdlVer							
8.41 141.1151*							

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 7 As. 175 Nd. 0

Combinazione di sollecitazioni agenti Caso 3 As. 175 Nd. 0

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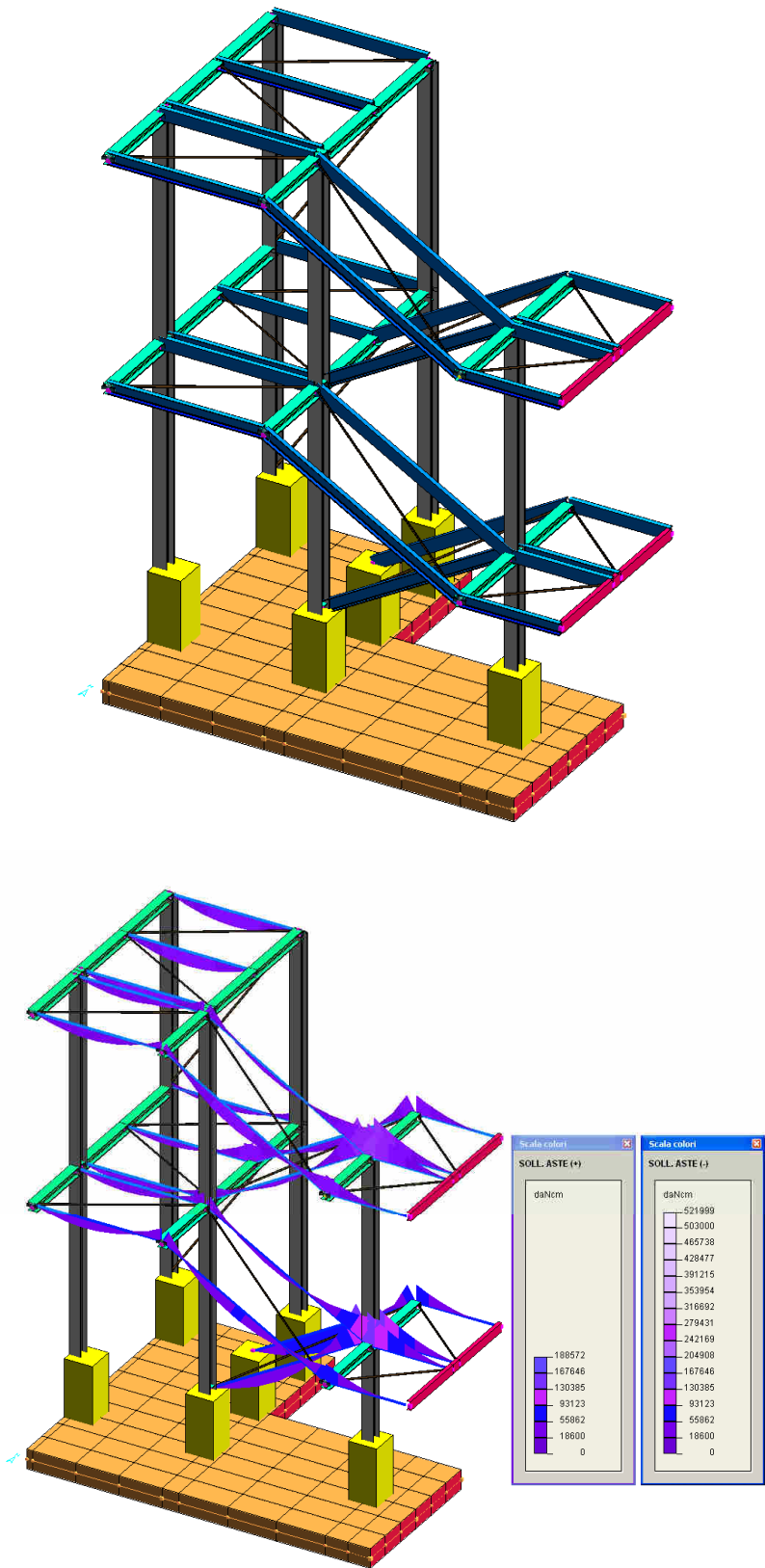
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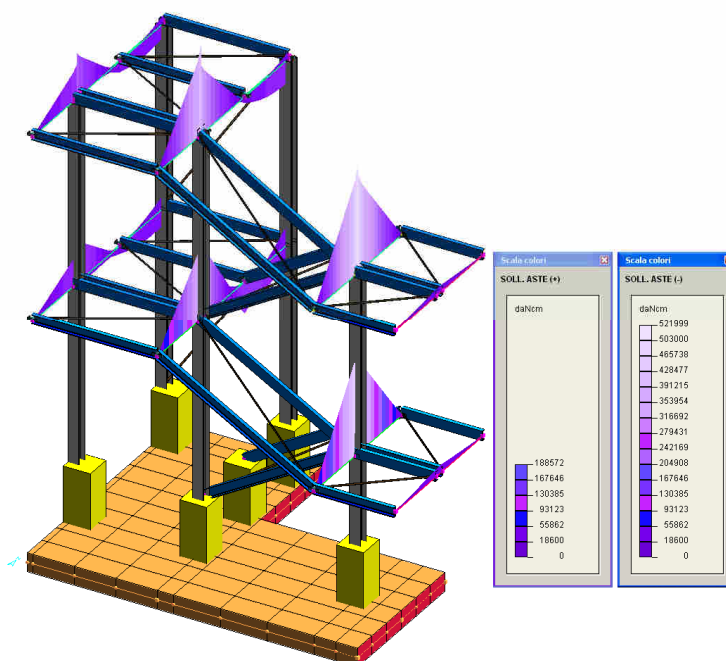
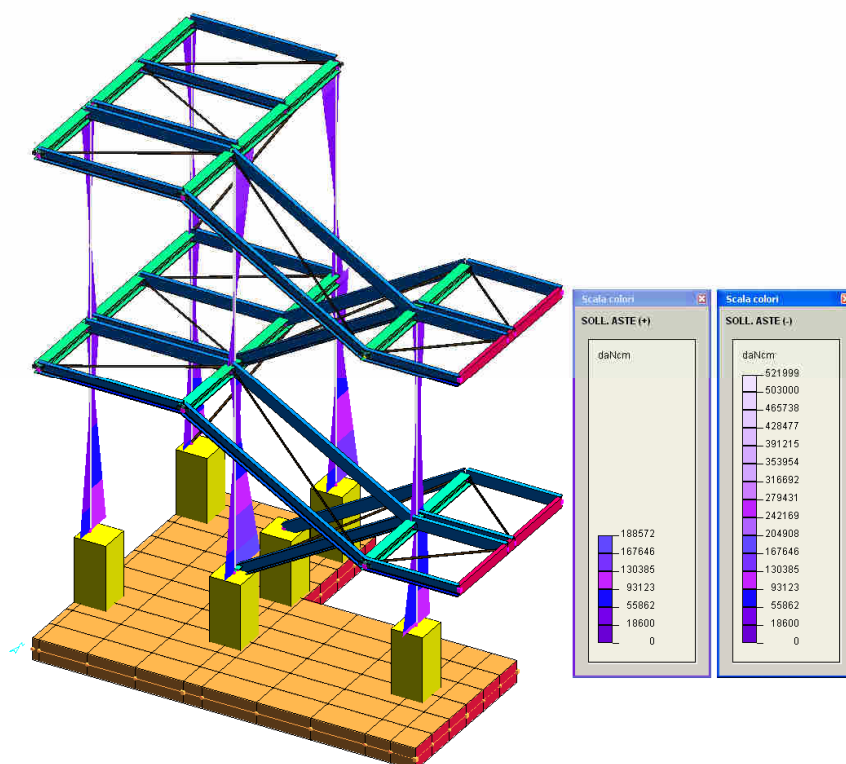
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Co-3: Ft,Ed / Tsd,Ed							
Num Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed Ft,Ed / Tsd,Ed							
1	201.61	3240.51	13714.31	201.71	4860.71	19543.21	3564.108 .01 .02151*
2	201.61	3240.51	13714.31	310.71	4860.71	19543.21	3564.111 .06 .09151*
3	201.61	3240.51	13714.31	74.91	4860.71	19543.21	3564.106 .01 .02151*
4	201.61	3240.51	13714.31	326.71	4860.71	19543.21	3564.111 .07 .09151*

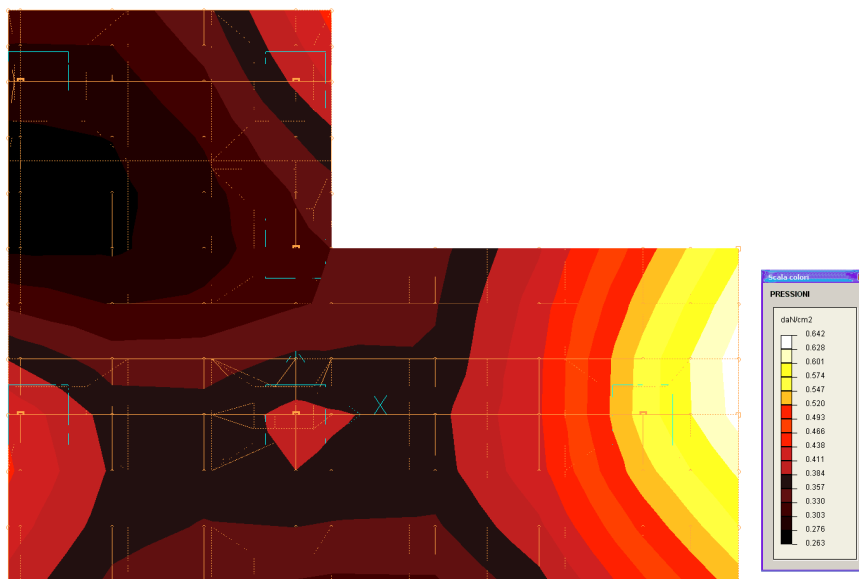
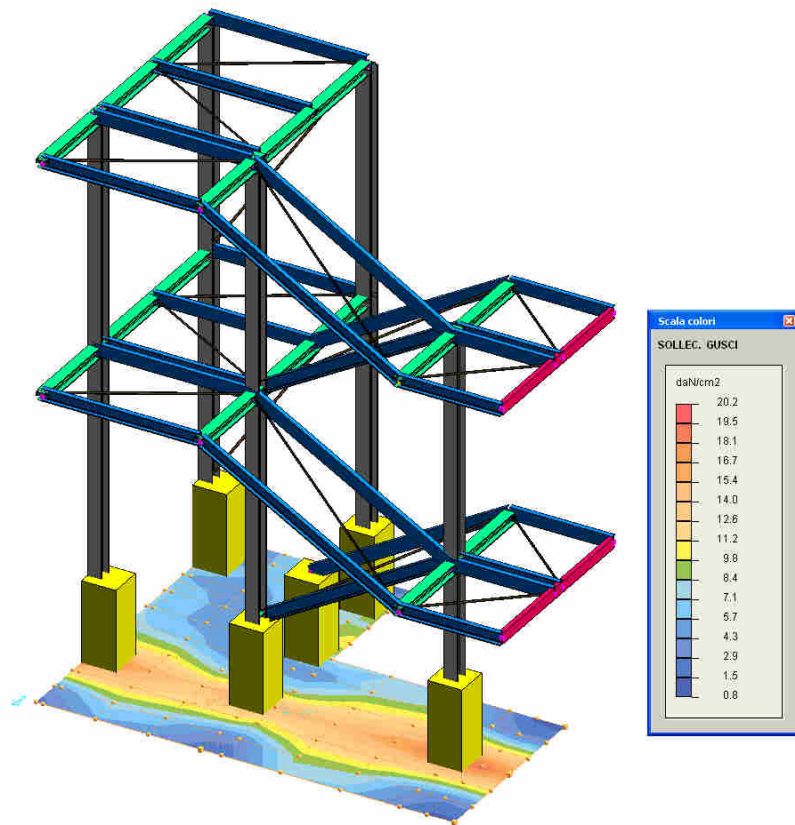
Verifica saldature

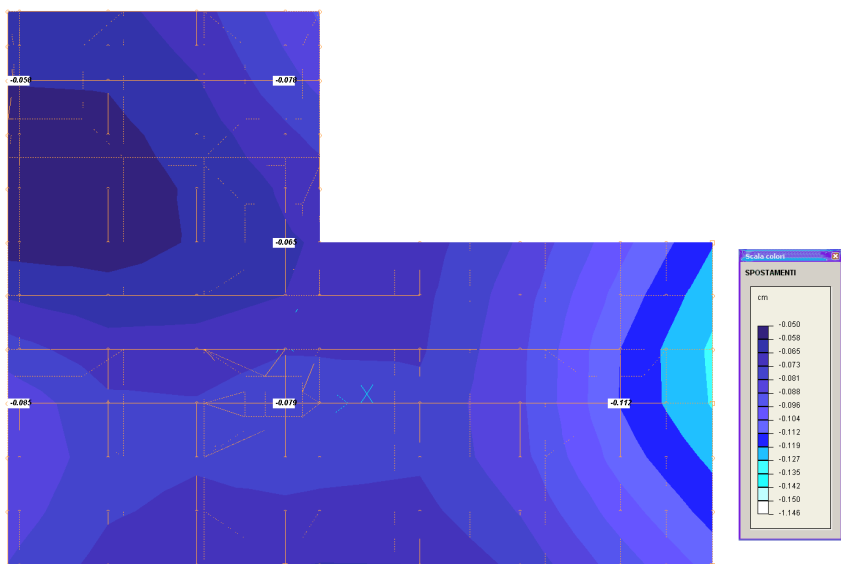
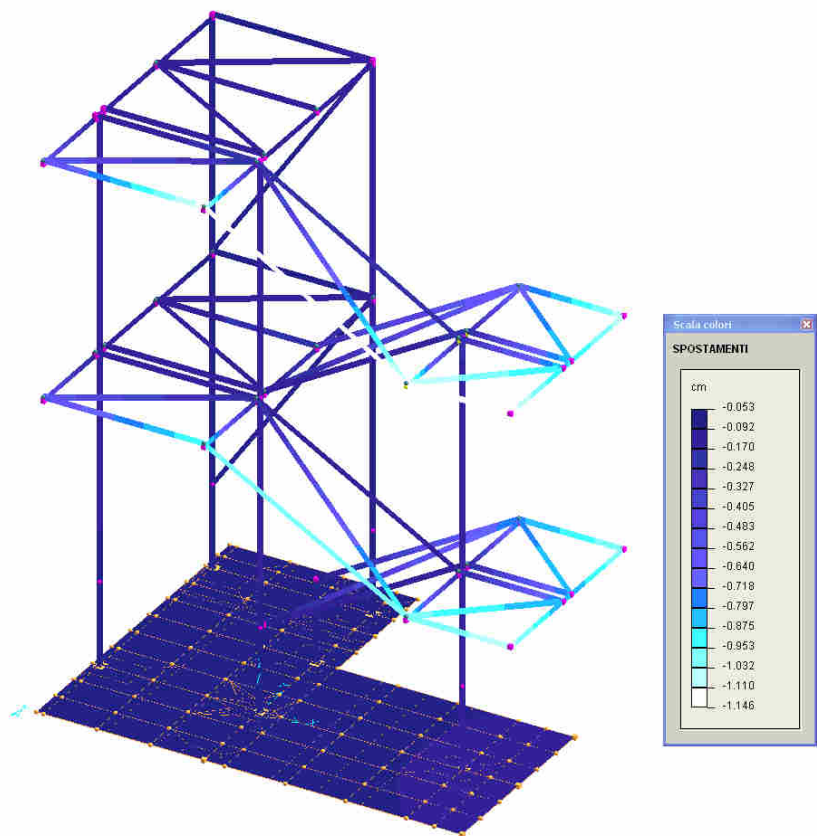
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							SLim-2Ver
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S10	20.3	8.8	0.	22.1	20.3	1997.5	2350.151*
S11	12.3	8.8	0.	15.1	12.3	1997.5	2350.151*
S12	16.3	8.8	0.	18.5	16.3	1997.5	2350.151*
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S17	71.1	1.7	0.	71.1	71.1	1997.5	2350.151*
S18	71.3	1.7	0.	71.3	71.3	1997.5	2350.151*
S20	61.6	8.8	0.	62.6	61.6	1997.5	2350.151*
S21	61.8	8.8	0.	62.8	61.8	1997.5	2350.151*
S22	65.5	8.8	0.	65.5	65.5	1997.5	2350.151*
S23	53.6	8.8	0.	53.6	53.6	1997.5	2350.151*
S24	57.5	8.8	0.	58.2	57.5	1997.5	2350.151*
S25	112.6	1.7	0.	112.6	112.6	1997.5	2350.151*
S26	112.6	1.7	0.	112.6	112.6	1997.5	2350.151*
S27	108.6	1.7	0.	108.6	108.6	1997.5	2350.151*
S28	136.2	1.7	0.	136.2	136.2	1997.5	2350.151*
S29	0.	507.5	36.	508.8	36.1	1997.5	2350.151*
S30	136.2	1.7	0.	136.2	136.2	1997.5	2350.151*
S31	0.	213.8	36.1	216.8	36.1	1997.5	2350.151*
S32	39.9	40.7	36.1	37.6	39.9	1997.5	2350.151*
S33	39.9	40.7	36.1	37.6	39.9	1997.5	2350.151*
S34	39.9	30.5	4.3	40.4	44.1	1997.5	2350.151*
S35	39.9	30.5	4.3	40.4	44.1	1997.5	2350.151*
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S37	134.2	1.7	0.	134.2	134.2	1997.5	2350.151*
S38	0.	467.7	4.3	467.7	4.3	1997.5	2350.151*
S39	134.2	1.7	0.	218.2	134.2	1997.5	2350.151*
S40	134.2	1.7	0.	218.2	134.2	1997.5	2350.151*

3.2 Report Grafico









SOMMARIO

<i>Sommario</i>	<i>1</i>
1 Premessa Generale	3
1.1 Assunti Progettuali	3
2 Relazione illustrativa	3
3 Relazione di calcolo	5
3.1 Report di calcolo	5
3.2 Report Grafico	133

1 PREMESSA GENERALE

1.1 Assunti Progettuali

Non essendo stato tutt'ora identificato da parte dell'amministrazione competente il tecnico incaricato per le indagini geologiche finalizzate all'identificazione dei parametri geotecnici di dettaglio, si è fatto riferimento a quanto noto alla geologia dell'area e si sono stimati i parametri geotecnici, proponendo una soluzione strutturale compatibile con le condizioni geotecniche mediocri. Tali parametri dovranno essere confermati da campagna analitica in sito prevista dall'amministrazione competente.

2 RELAZIONE ILLUSTRATIVA

TITOLO DEL PROGETTO

Realizzazione Scala esterna di sicurezza

COMMITTENTE

Città di Moncalieri
P.zza Vittorio Emanuele II
10024 Moncalieri (To)

PROGETTISTA

Dott. Ing. Virgilio M. CHIONO - Studio Associato POOL ENGINEERING
Vicolo Cugiano 4 - San Giorgio Can.se (To)
Ordine degli Ingegneri di Torino e Provincia al n° 8645 F

1. INDIVIDUAZIONE DEL MODELLO DI CALCOLO

1.1 DESCRIZIONE GENERALE DELL'OPERA

Oggetto della presente relazione e' l'analisi delle sollecitazioni ed il calcolo della struttura in cemento armato ordinario da realizzarsi in:

Lotto: Strada Vignotto, 21- 10024 Moncalieri (To)
Comune di: Moncalieri (To)
Proprieta

Città di Moncalieri
P.zza Vittorio Emanuele II
10024 Moncalieri (To)

Destinazione e tipologia dell'opera:

Il sito oggetto dell'intervento presenta i seguenti caratteri morfologico-geotecnici generali:

Realizzazione Scala esterna di sicurezza con opere in cemento armato normale e acciaio strutturale

La struttura e' composta dai seguenti elementi, previsti in calcestruzzo gettato in opera:

FONDAZIONI: soletta piena di fondazione in c.a.

Tale soluzione strutturale si e' adottata per diminuire i cedimenti, ed assicurare la funzionalità della struttura.

TRAVI: Profili in acciaio strutturale S235, sezioni tipo HE ed UPN

PILASTRI: Pilastri a sezione rettangolare e Profili in acciaio strutturale S235, sezioni tipo HE

1.2 NORMATIVE DI RIFERIMENTO

L'analisi della struttura in oggetto e' stata fatta utilizzando i metodi usuali della Scienza delle Costruzioni ed in conformità alle normative e leggi vigenti:

- Legge 5/11/1971 n. 1086: Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

- D.P.R. 6/6/2001 n. 380: Testo unico delle disposizioni legislative e regolamentari in materia edilizia.

- D.M. 14/1/2008: Norme tecniche per le costruzioni.

1.3 CRITERI DI ANALISI DELLA SICUREZZA

Con riferimento alle normative precedentemente citate, le strutture in oggetto sono verificate per quanto riguarda:

- verifica di resistenza;

- verifica a deformazione e fessurazione.

Calcestruzzo per le strutture in elevazione: classe C25/30

Acciaio in barre : B450C

Acciaio in Profili: S235/FE360

1.4 SCHEMATIZZAZIONE DELLA STRUTTURA E DEI VINCOLI

La struttura e' stata schematizzata escludendo il contributo degli elementi aventi rigidità e resistenza trascurabili a fronte dei principali. E' quindi stata considerata l'orditura a telaio tridimensionale, i solai ed i setti verticali ad elevata rigidità (vano ascensore, setti in cls).

Le opere di fondazione vengono assimilate a vincoli elastici di cui e' fornita la costante di rigidità. Le travi di fondazione sono schematizzate come poggianti su vincoli elastici distribuiti.

1.5 MODELLAZIONE DELLA STRUTTURA E DEI VINCOLI

La struttura e' modellata con il metodo degli elementi finiti, applicato a sistemi tridimensionali. Gli elementi utilizzati sono sia monodimensionali (trave con eventuali sconnessioni interne), che bidimensionali (piastre e membrane triangolari e quadrangolari). I vincoli sono considerati puntuali ed inseriti tramite le sei costanti di rigidità elastica, oppure come elementi asta poggianti su suolo elastico. Le sezioni oggetto di verifica nelle travi sono stampate a passo costante; dei gusci si conoscono le sollecitazioni nel baricentro dell'elemento stesso.

1.6 SCHEMATIZZAZIONE DELLE AZIONI

In accordo con le sopracitate normative, sono state considerate nei calcoli le seguenti azioni:

- pesi propri strutturali
- carichi permanenti portati dalla struttura
- carichi variabili sui solai, neve, vento.
- forze di piano simulanti il sisma, ricavate tramite analisi statica semplificata
- distorsioni termiche

Le condizioni ed i casi di carico prese in conto nei calcoli sono specificate nella stampa dei dati di input.

1.7 MODELLAZIONE DELLE AZIONI

Sono stati adottati i valori di carico come riportato in relazione e confacenti ai dettati normativi.

Carico Variabile Luoghi soggetti ad affollamento:

- 1) -400 - daN/m²

Le azioni sono state modellate tramite opportuni carichi concentrati e distribuiti su nodi ed aste.

1.8 MODELLAZIONE DEI MATERIALI

I materiali costituenti la struttura sono considerati elastici e con comportamento lineare. Le loro caratteristiche sono specificate nella stampa dei dati di input.

1.9 TIPO DI ANALISI

Le analisi strutturali condotte sono statiche in regime lineare. Il metodo di calcolo è ad elementi finiti. Il calcolo sismico è stato effettuato tramite analisi statica semplificata. La verifica delle membrature in cemento armato viene eseguita considerando tutte le caratteristiche di sollecitazione.

2 CODICE DI CALCOLO

2.1 INDIVIDUAZIONE DEL CODICE DI CALCOLO

Per il calcolo delle sollecitazioni e per la verifica di travi e pilastri in cemento armato si è fatto ricorso all'elaboratore elettronico utilizzando il seguente programma di calcolo:

DOLMEN WIN (R), versione 15.0 del 2015 prodotto, distribuito ed assistito dalla CDM DOLMEN srl, con sede in Torino, Via Drovetti 9/F.

Questa procedura è sviluppata in ambiente Windows, ed è stata scritta utilizzando i linguaggi Fortran e C. DOLMEN WIN permette l'analisi elastica lineare di strutture tridimensionali con nodi a sei gradi di libertà utilizzando un solutore ad elementi finiti. Gli elementi considerati sono la trave, con eventuali svincoli interni o rotazione attorno al proprio asse, ed il guscio, sia rettangolare che triangolare, avente comportamento di membrana e di piastra. I carichi possono essere applicati sia ai nodi, come forze o coppie concentrate, sia sulle travi, come forze distribuite, trapezie, concentrate, come coppie e come distorsioni termiche. I vincoli sono forniti tramite le sei costanti di rigidità elastica.

A supporto del programma è fornito un ampio manuale d'uso contenente fra l'altro una vasta serie di test di validazione sia su esempi classici di Scienza delle Costruzioni, sia su strutture particolarmente impegnative e reperibili nella bibliografia specializzata.

2.2 GRADO DI AFFIDABILITÀ DEL CODICE

L'affidabilità del codice di calcolo è garantita dall'esistenza di un'ampia documentazione di supporto, come indicato nel paragrafo precedente. La presenza di un modulo CAD per l'introduzione di dati permette la visualizzazione dettagliata degli elementi introdotti. È possibile inoltre ottenere rappresentazioni grafiche di deformate e sollecitazioni della struttura. Al termine dell'elaborazione viene inoltre valutata la qualità della soluzione, in base all'uguaglianza del lavoro esterno e dell'energia di deformazione.

2.3 MOTIVAZIONE DELLA SCELTA DEL CODICE

DOLMEN WIN permette in campo elastico lineare un'analisi dettagliata del comportamento dell'intera struttura, tenendo conto del comportamento irrigidente di setti anche complessi e solai considerati con la loro effettiva rigidità. È possibile inoltre scegliere il grado di affinamento dell'analisi di elementi complessi utilizzando mesh via via più dettagliate.

3. ESAME DEI RISULTATI E CONTROLLI

3.1 VALUTAZIONE DELLA CORRETTEZZA DEL MODELLO

Il modello di calcolo adottato è da ritenersi appropriato in quanto non sono state riscontrate labilità, le reazioni vincolari equilibrano i carichi applicati, la simmetria di carichi e struttura dà origine a sollecitazioni simmetriche.

4. GIUDIZIO MOTIVATO DI ACCETTABILITÀ DEI RISULTATI

L'analisi critica dei risultati e dei parametri di controllo nonché il confronto con calcolazioni di massima eseguite manualmente porta ad confermare la validità dei risultati.

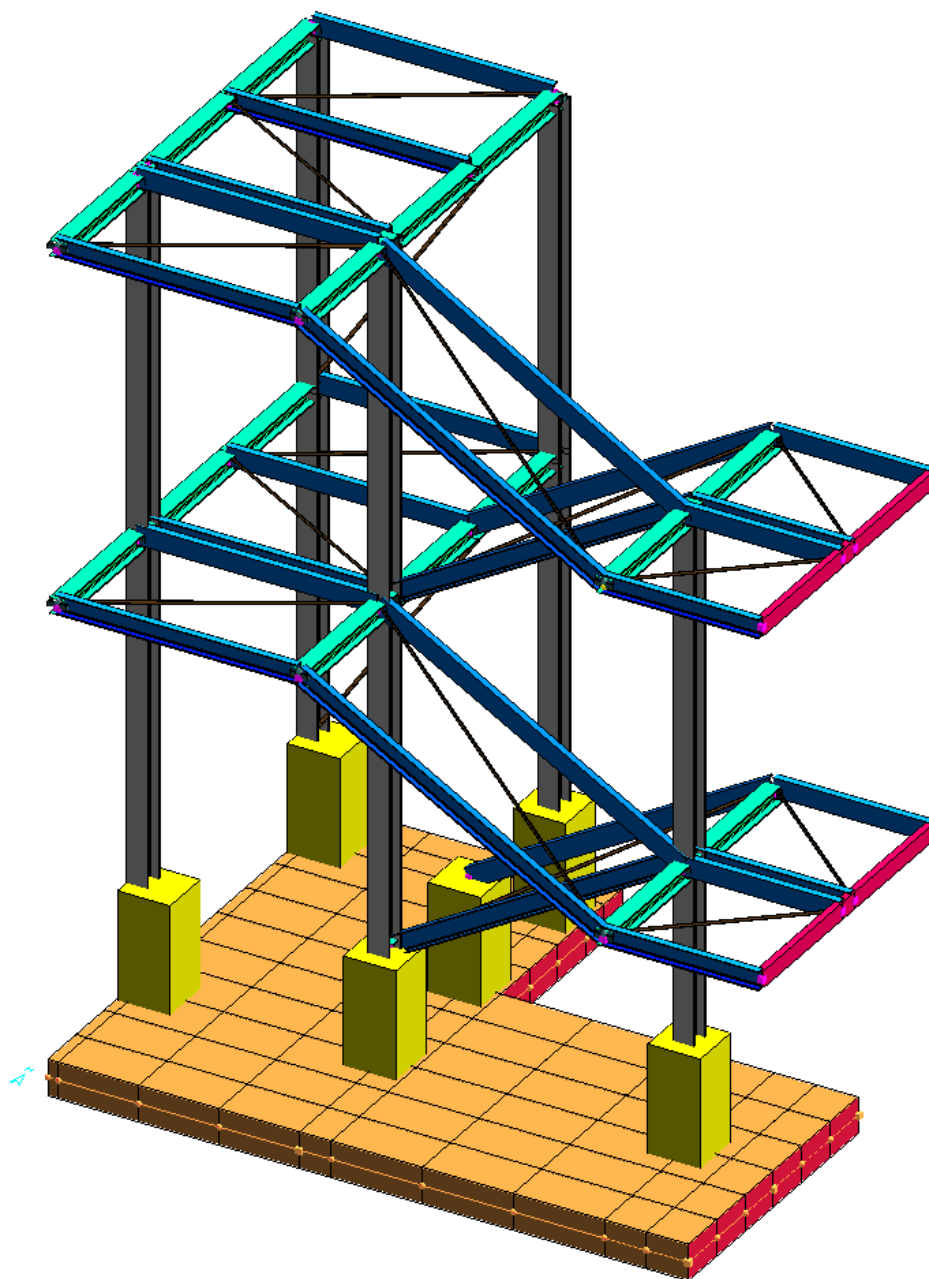
5. ALLEGATI

Alla presente relazione si allegano le seguenti stampe:

- dati di ingresso;
- sollecitazioni nelle aste e nei gusci;
- reazioni vincolari;
- verifiche di resistenza di travi e pilastri;
- diagrammi di sollecitazioni e deformazioni.

3 RELAZIONE DI CALCOLO

3.1 Report di calcolo




```
494      1      778      779      780      781
495      1      781      780      782      783
496      1      782      782      958      784
497      1      784      958      785      786
498      1      786      785      787      788
499      1      788      787      789      790

PROPRIETA' ASTE-----|-----|-----|-----|num.= 6
Nome Materiale Base Altezza Area Area tag. Y Area tag. Z
1 2 Kw vertic. 7.00 Kw orizz. 18.00 2.8000E+01 1.4400E+01 1.5400E+01
2 2 0.000000 0.000000 9.28333E+00 1.14000E+02 1.15400E+03
3 2 20.00 0.000000 5.93000E+01 2.00300E+03 5.69600E+03
4 2 36.00 0.000000 8.12000E+01 8.89000E+02 2.49200E+03
5 2 6.50 0.000000 6.20000E+01 1.20000E+01 1.36500E+01
6 2 3.00 0.000000 7.26558E+03 8.51000E+01 9.2500E+02
5 2 3.00 0.000000 3.00 2.3000E+00 1.20000E+00 1.20000E+00
6 1 50.00 0.000000 6.40000E+02 1.80000E+00 1.80000E+00
0.000000 50.00 2.50000E+03 2.0833E+03 2.0833E+03
0.000000 0.000000 8.80195E+05 5.20833E+05 5.20833E+05

PROPRIETA' GUSCI-----|-----|-----|-----|num.= 1
Nome Materiale Sp. piastra Kw
1 1 35.00 35.00 5.000000

MATERIALI-----|-----|-----|-----|num.= 2
Nome Mod. elast. Coeff. nu Mod. tang. Peso spec. D11. te.
1 3.00000E+06 1.50000E-01 1.30000E+05 2.5000E-03 1.00000E-05
2 2.10000E+06 3.00000E-01 8.50000E+05 7.85000E-03 1.00000E-05

VINCOLI-----|-----|-----|-----|num.= 6
Nodo Rigid. X Rigid. Y Rigid. Z Rigid. RX Rigid. RY Rigid. RZ
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960 bloccato bloccato libero libero libero libero
964 bloccato bloccato libero libero libero libero
967 bloccato bloccato libero libero libero libero
969 bloccato bloccato libero libero libero libero
40 bloccato bloccato libero libero libero libero

CARICHI NODI-----|-----|-----|-----|num.= 308
Nome Nodo Direzione Intensita
1 154 : Forze Statiche (Analisi Semplificata)
155 308 : Momenti Torcenti Additionali

CARICHI ASTE-----|-----|-----|-----|num.= 200
Nome Asta Dir Tip REF Parametro 1 Parametro 2 Parametro 3 Parametro 4
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310 PERM 7 2 Z RD glo -2.000
311 PERM 31 2 Z RD glo -2.000
312 PERM 23 2 Z RD glo -2.000
313 PERM 15 2 Z RD glo -2.000
314 PERM 32 2 Z RD glo -2.000
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316 PERM 16 2 Z RD glo -2.000
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320 PERM 10 2 Z RD glo -2.000
321 PERM 2 2 Z RD glo -2.000
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325 PERM 130 2 Z RD glo -2.000
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403 Vento_Y 31 Y RD glo -0.400
404 Vento_Y 32 Y RD glo -0.400

PESTI PROPRIETA' ASTE-----|-----|-----|-----|
Cond. Nome Carichi Asta
1 405-508 2 4 7-8, 10, 12, 15-17, 19, 23-25, 27, 31-36,
38-59, 91-94, 99-102, 104-112, 116-117, 119-128,
130, 132, 134, 136-138, 141-143, 145-149, 154,
156-163, 165-166, 170-176, 178

CARICHI DI LINEA-----|-----|-----|-----|num.= 0
Nome numero coordinata
inizio Fine Cond. Diraz. inizio Fine Descrizione
1 405-508 2 4 7-8, 10, 12, 15-17, 19, 23-25, 27, 31-36,
38-59, 91-94, 99-102, 104-112, 116-117, 119-128,
130, 132, 134, 136-138, 141-143, 145-149, 154,
156-163, 165-166, 170-176, 178

CONDIZIONE DI CARICO-----|-----|-----|-----|num.= 9
Nome
1 Peso proprio N. carichi: 104
Lista carichi: 405-508
2 Permanente N. carichi: 30
Lista carichi: 309-338
3 A:Var_abitazione N. carichi: 30
Lista carichi: 339-368
4 Neve_(c000n_s_m) N. carichi: 28
Lista carichi: 369-396
5 Vento_Y N. carichi: 8
Lista carichi: 397-404
6 Sigma_X N. carichi: 77
Lista carichi: 1-77
7 Sigma_Y N. carichi: 77
Lista carichi: 78-154
8 Torcente_add_X N. carichi: 77
Lista carichi: 155-231
9 Torcente_add_Y N. carichi: 77
Lista carichi: 232-308

RISULTANTI DEI CARICHI (punto di applicazione nell'origine degli assi):
cond. FX FY FZ MX MY MZ
1 0.00000E+00 0.00000E+00 -8.152057E+03 -7.291865E+05 -7.030302E+04 0.000000E+00
2 0.00000E+00 0.00000E+00 -1.348847E+04 -4.915020E+05 9.962286E+05 0.000000E+00
3 0.00000E+00 0.00000E+00 -2.360483E+04 -8.637126E+05 1.744100E+06 0.000000E+00
4 0.00000E+00 0.00000E+00 -7.757084E+02 -2.255701E+05 6.752571E+05 0.000000E+00
5 0.00000E+00 -1.484847E+03 0.00000E+00 8.177556E+05 0.000000E+00 -2.642286E+04
6 2.106702E+03 0.00000E+00 0.00000E+00 0.00000E+00 1.254815E+06 -8.433983E+04
7 0.00000E+00 2.106702E+03 0.00000E+00 -1.254815E+06 0.00000E+00 8.103980E+04
8 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 -1.533155E+02 -3.926788E+04
9 0.00000E+00 0.00000E+00 0.00000E+00 -4.875793E+01 0.000000E+00 2.260460E+04
```


DATI ANALISI SISMICA:

Analisi sismica - Statica lineare - (NTC 2008)

DATI PROGETTO

Edificio sito in localit  MONCALIERE (Long. 7,702 Lat. 45,000100)

Categoria del suolo di fondazione = C

Coeff. di amplificazione stratigrafica Ss = 1,500

Coeff. di amplificazione topografica ST = 1,000

S = 1,500

Vita nominale dell'opera VN = 50 anni

Coefficiente d'uso CU = 1,5

Periodo di riferimento VR = 75,0

PMR : probabilit  di superamento in VR = 10 %

Tempo di ritorno = 712

Coeff. di smorzamento viscoso = 5,0

Valori risultanti per :

ag 0,599 [g/10]

Tc 2,796

Tc 0,281

Edificio con struttura in acciaio :

Fattore di struttura q = 3,200

q = q0 * KR dove :

q0 = 4,00 2,00 + -1,0

KR = 0,8 (edifici non regolari in altezza)

Rapporto spettro di esercizio / spettro di progetto = 1,648

Cond. lambda = 1,0000

Sd = 0,078 per T1 = 0,36

Numero condizioni generanti carichi sismici : 3

Cond. 001 : Peso,proprio con coeff. 1,000

Cond. 002 : Permanente con coeff. 1,000

Cond. 003 : Avar.abitazione con coeff. 0,300

Condizioni di carico sisma generate:

Cond. 005 : Sisma X con coeff. 1,000

Cond. 007 : Sisma Y con coeff. 1,000

Cond. 008 : Torcente add. X con coeff. 0,300

Cond. 009 : Torcente add. Y con coeff. 0,300

Carichi sismici :

[Baric. Y]	Plan[cm]	Resi cm]	C. distr. l cm]	Forze di piano X[Torc. di piano Y]	Forze di piano Y[Torc. di piano X]	Baric. X]
[Baric. Y]	cm]	dan]	cm]	dan]	dan]	cm]
[0,1]	120,0]	3434]	0,0192]	66]	923]	1713]
[0,1]	285,0]	4482]	0,0456]	204]	2860]	1532]
[66,5]	450,0]	7996]	0,0720]	575]	12085]	6618]
[60,0]	620,0]	4439]	0,0992]	440]	6163]	3302]
[60,1]	790,0]	6496]	0,1264]	821]	17237]	9439]

ANALISI DINAMICA

PARAMETRI DI CALCOLO:

Calcolo secondo NTC 2008

Modello generale

Asci di vibrazione: X Y

Combinazione quadratica completa (CQC)

DATI PROGETTO

Edificio sito in localit  MONCALIERE (Long. 7,702 Lat. 45,000100)

Categoria del suolo di fondazione = C

Coeff. di amplificazione stratigrafica Ss = 1,500

Coeff. di amplificazione topografica ST = 1,000

S = 1,500

Vita nominale dell'opera VN = 50 anni

Coefficiente d'uso CU = 1,5

Periodo di riferimento VR = 75,0

PMR : probabilit  di superamento in VR = 10 %

Tempo di ritorno = 712

Coeff. di smorzamento viscoso = 5,0

Valori risultanti per :

ag 0,599 [g/10]

Tc 2,796

Tc 0,281

Edificio con struttura in acciaio :

Fattore di struttura q = 3,200

q = q0 * KR dove :

q0 = 4,00 2,00 + -1,0

KR = 0,8 (edifici non regolari in altezza)

Rapporto spettro di esercizio / spettro di progetto = 1,648

CONDIZIONI DI RIFERIMENTO COEFFICIENTE

PESO RISULTANTE

1. 1,000

2. 1,000

3.*** TABELLA AUTORETTORE ***

n	PERIODO [sec]	MASSA ATTIVATA [kg]	COEFFICIENTI DI CORRELAZIONE n=1 n=2 n=3 n=4 n=5 n=6 n=7
1	0,436440	0,532 71,273 0,000	0,131 0,022 0,006 0,004 0,004 0,002 0,002 0,002 0,001
2	0,322633	0,335 1,762 0,000	0,063 0,012 0,008 0,006 0,004 0,004 0,003 0,002

3	0,220435	76,743 0,155 0,000	0,041 0,022 0,017 0,009 0,008 0,006 0,004
4	0,137223	0,001 0,010 0,000	0,270 0,141 0,038 0,036 0,018 0,012
5	0,116474	0,093 9,394 0,000	0,602 0,084 0,077 0,032 0,018
6	0,107385	0,022 5,740 0,000	0,141 0,126 0,045 0,034
7	0,080424	3,055 0,636 0,000	0,975 0,192 0,067
8	0,086277	0,285 0,158 0,000	0,219 0,073
9	0,068499	1,447 0,058 0,000	0,269
10	0,058310	6,104 0,031 0,000	

MASSA TOTALE 88,537 89,497 0,000

***** AUTORETTORE N. 1 - periodo: 0,4364398

percentuale di massa attivata:

X Y Z

71,77 71,77 0,00

NODO SX SY SZ

2 0,7938E-02 0,3904E-01 0,0000E+00

3 0,1753E-01 0,8209E-01 0,0000E+00

5 0,2875E-01 0,1524E+00 0,0000E+00

11 0,6245E-02 0,2906E-01 0,0000E+00

12 0,9728E-02 0,8269E-01 0,0000E+00

14 0,1662E-01 0,1524E+00 0,0000E+00

19 0,5984E-02 0,4995E-02 0,0000E+00

20 0,6236E-02 0,3909E-01 0,0000E+00

21 0,7698E-02 0,8269E-01 0,0000E+00

23 0,1475E-01 0,1524E+00 0,0000E+00

28 0,0946E-03 0,4995E-02 0,0000E+00

30 0,4796E-02 0,8270E-01 0,0000E+00

32 0,4938E-02 0,1524E+00 0,0000E+00

37 0,9617E-03 0,4995E-02 0,0000E+00

38 0,8942E-02 0,8269E-01 0,0000E+00

39 0,1569E-01 0,1524E+00 0,0000E+00

46 0,6149E-02 0,3909E-01 0,0000E+00

42 0,1461E-01 0,1683E+00 0,0000E+00

210 0,2874E-01 0,1527E+00 0,0000E+00

111 0,1702E-01 0,1525E+00 0,0000E+00

212 0,1486E-01 0,1525E+00 0,0000E+00

213 0,5698E-02 0,1527E+00 0,0000E+00

139 0,3914E-01 0,1692E+00 0,0000E+00

340 0,1618E-01 0,1698E+00 0,0000E+00

341 0,1534E-01 0,1697E+00 0,0000E+00

342 0,5271E-02 0,1692E+00 0,0000E+00

466 0,1638E-01 0,8411E-01 0,0000E+00

467 0,9471E-02 0,8411E-01 0,0000E+00

468 0,8286E-02 0,8313E-01 0,0000E+00

469 0,4825E-02 0,8311E-01 0,0000E+00

470 0,9378E-02 0,4008E-01 0,0000E+00

471 0,7014E-02 0,4045E-01 0,0000E+00

472 0,5857E-02 0,4043E-01 0,0000E+00

473 0,1539E-01 0,4001E-01 0,0000E+00

726 0,3813E-01 0,1894E+00 0,0000E+00

727 0,5258E-02 0,1894E+00 0,0000E+00

728 0,1362E-01 0,1893E+00 0,0000E+00

729 0,1636E-01 0,1894E+00 0,0000E+00

730 0,1538E-01 0,3662E-01 0,0000E+00

731 0,6276E-02 0,3662E-01 0,0000E+00

732 0,7094E-02 0,3665E-01 0,0000E+00

733 0,9578E-02 0,3666E-01 0,0000E+00

734 0,9622E-03 0,4423E-02 0,0000E+00

735 0,1692E-02 0,6218E-01 0,0000E+00

737 0,1233E-01 0,6202E-01 0,0000E+00

738 0,1112E-01 0,1309E+00 0,0000E+00

739 0,1233E-01 0,8257E-01 0,0000E+00

740 0,1111E-01 0,1524E+00 0,0000E+00

741 0,5888E-03 0,4423E-02 0,0000E+00

742 0,2992E-03 0,4995E-02 0,0000E+00

745 0,2127E-01 0,6227E-01 0,0000E+00

746 0,8590E-02 0,6218E-01 0,0000E+00

747 0,6799E-02 0,6218E-01 0,0000E+00

748 0,9472E-02 0,6216E-01 0,0000E+00

749 0,4474E-02 0,6208E-01 0,0000E+00

750 0,7846E-02 0,6294E-01 0,0000E+00

751 0,9157E-02 0,6310E-01 0,0000E+00

752 0,1672E-01 0,6331E-01 0,0000E+00

753 0,2416E-01 0,6316E-01 0,0000E+00

754 0,1243E-01 0,8333E-01 0,0000E+00

760 0,6994E-02 0,1307E+00 0,0000E+00

951 0,1568E-01 0,1310E+00 0,0000E+00

953 0,1104E-01 0,1525E+00 0,0000E+00

961 0,1591E-01 0,1683E+00 0,0000E+00

962 0,1339E-01 0,1683E+00 0,0000E+00

963 0,3698E-02 0,1310E+00 0,0000E+00

964 0,3756E-01 0,1682E+00 0,0000E+00

967 0,1662E-01 0,1310E+00 0,0000E+00

968 0,1664E-01 0,1310E+00 0,0000E+00

969 0,1473E-01 0,1310E+00 0,0000E+00

970 0,2398E-02 0,1309E+00 0,0000E+00

972 0,1694E-01 0,1316E+00 0,0000E+00

973 0,1486E-01 0,1315E+00 0,0000E+00

975 0,1395E-01 0,1316E+00 0,0000E+00

976 0,2876E-01 0,1316E+00 0,0000E+00

978 0,9615E-02 0,5723E-02 0,0000E+00

***** AUTORETTORE N. 2 - periodo: 0,3226327

percentuale di massa attivata:

X Y Z

0,335 1,762 0,000

NODO SX SY SZ

2 0,4640E-01 0,2849E-01 0,0000E+00

3 0,3598E-01 0,2524E-01 0,0000E+00

5 0,1020E+00 0,6165E-01 0,0000E+00

11 0,1336E-01 0,2861E-01 0,0000E+00

12 0,1802E-01 0,2524E-01 0,0000E+00

14 0,3411E-01 0,6165E-01 0,0000E+00

20 0,6208E-02 0,1715E-02 0,0000E+00

20 0,8936E-02 0,2864E-01 0,0000E+00

21 0,1290E-01 0,2524E-01 0,0000E+00

23 0,3364E-01 0,6165E-01 0,0000E+00

28 0,1871E-02 0,1717E-02 0,0000E+00

29 0,4466E-02 0,2876E-01 0,0000E+00

30 0,2843E-01 0,2524E-01 0,0000E+00

32 0,4575E-02 0,6165E-01 0,0000E+00

37 0,8946E-03 0,1715E-02 0,0000E+00

38 0,1640E-01 0,2524E-01 0,0000E+00

39 0,3807E-01 0,6165E-01 0,0000E+00

41 0,1102E-01 0,2862E-01 0,0000E+00

42 0,2499E-01 0,1172E+00 0,0000E+00

210 0,1019E+00 0,6165E-01 0,0000E+00

211 0,3525E-01 0,6175E-01 0,0000E+00

212 0,2775E-01 0,6173E-01 0,0000E+00

213 0,4428E-01 0,6177E-01 0,0000E+00

139 0,1078E+00 0,1172E+00 0,0000E+00

340 0,3164E-01 0,1178E+00 0,0000E+00

341 0,1862E-01 0,1178E+00 0,0000E+00

342 0,4946E-01 0,1172E+00 0,0000E+00

466 0,5156E-01 0,2494E-01 0,0000E+00

467 0,1815E-01 0,2494E-01 0,0000E+00

468 0,1226E-01 0,2508E-01 0,0000E+00

469 0,4948E-01 0,2506E-01 0,0000E+00

470 0,4935E-01 0,2857E-01 0,0000E+00

471 0,1558E-01 0,2937E-01 0,0

964 -0.2555E-01 -0.2535E-01 0.0000E+00
967 -0.6033E-01 0.1248E-01 0.0000E+00
968 -0.3803E-01 0.2105E-01 0.0000E+00
969 -0.3607E-01 0.1245E-01 0.0000E+00
970 -0.1396E-01 0.1245E-01 0.0000E+00
971 -0.3874E-01 0.1245E-01 0.0000E+00
972 -0.3727E-01 0.1275E-01 0.0000E+00
973 -0.3317E-01 0.1267E-01 0.0000E+00
974 -0.3941E-01 0.1294E-01 0.0000E+00
975 -0.6001E-01 0.1294E-01 0.0000E+00
976 -0.6001E-01 0.2521E-01 0.0000E+00
977 -0.1447E-01 0.1490E-01 0.0000E+00
***** AUTOTETTORE N. 6 periodo: 0.037850
percentuale di massa attivata :
X
0.022 Y
5.710 Z
0.000

NDO SX SZ
2 -0.5689E-01 0.1733E-01 0.0000E+00
3 -0.4158E-01 0.1645E+00 0.0000E+00
4 -0.2429E-01 0.8838E-01 0.0000E+00
11 -0.7856E-02 0.1715E-01 0.0000E+00
12 -0.6520E-02 0.1645E+00 0.0000E+00
13 -0.1307E-01 0.8941E-01 0.0000E+00
14 -0.1587E-01 0.8840E-01 0.0000E+00
19 -0.8528E-03 0.9882E-02 0.0000E+00
20 -0.1133E-02 0.1715E-01 0.0000E+00
21 -0.3830E-02 0.1645E+00 0.0000E+00
23 -0.1307E-01 0.8941E-01 0.0000E+00
28 -0.3956E-02 0.9878E-02 0.0000E+00
29 -0.3410E-01 0.1696E-01 0.0000E+00
30 -0.1420E-01 0.1645E+00 0.0000E+00
32 -0.4313E-02 0.8847E-01 0.0000E+00
37 -0.1063E-02 0.9882E-02 0.0000E+00
38 -0.5249E-02 0.1645E+00 0.0000E+00
39 -0.1447E-01 0.8840E-01 0.0000E+00
41 -0.4441E-02 0.1714E-01 0.0000E+00
42 -0.5783E-02 0.1857E-01 0.0000E+00
210 -0.3432E-02 0.8884E-01 0.0000E+00
211 -0.1439E-02 0.8850E-01 0.0000E+00
212 -0.1344E-01 0.8849E-01 0.0000E+00
213 -0.5208E-02 0.8868E-01 0.0000E+00
339 -0.8940E-01 0.1838E-01 0.0000E+00
340 -0.3030E-01 0.1674E-01 0.0000E+00
341 -0.1886E-02 0.1978E-01 0.0000E+00
342 -0.1543E-02 0.1307E-01 0.0000E+00
466 -0.4628E-01 0.1652E+00 0.0000E+00
467 -0.6965E-02 0.1652E+00 0.0000E+00
468 -0.4000E-02 0.1644E+00 0.0000E+00
469 -0.1420E-01 0.1644E+00 0.0000E+00
470 -0.3805E-01 0.1743E-01 0.0000E+00
471 -0.8390E-02 0.1736E-01 0.0000E+00
472 -0.8412E-02 0.1736E-01 0.0000E+00
473 -0.3182E-01 0.1897E-01 0.0000E+00
726 -0.2648E-01 0.8888E-02 0.0000E+00
727 -0.1581E-02 0.8888E-02 0.0000E+00
728 -0.2658E-02 0.8890E-02 0.0000E+00
729 -0.9904E-02 0.8880E-02 0.0000E+00
730 -0.1319E-01 0.3560E-01 0.0000E+00
731 -0.1401E-02 0.3555E-01 0.0000E+00
732 -0.8501E-02 0.3557E-01 0.0000E+00
733 -0.5818E-01 0.3566E-01 0.0000E+00
734 -0.1066E-02 0.1487E-01 0.0000E+00
735 -0.2755E-02 0.1924E+00 0.0000E+00
737 -0.2250E-01 0.1934E+00 0.0000E+00
738 -0.1734E-01 0.1924E+00 0.0000E+00
739 -0.2291E-01 0.1639E+00 0.0000E+00
740 -0.1708E-01 0.8849E-01 0.0000E+00
741 -0.4989E-01 0.1487E-01 0.0000E+00
742 -0.4983E-02 0.9881E-02 0.0000E+00
745 -0.2263E-01 0.1931E+00 0.0000E+00
746 -0.3978E-02 0.1924E+00 0.0000E+00
747 -0.1545E-02 0.1924E+00 0.0000E+00
748 -0.1383E-01 0.1921E+00 0.0000E+00
749 -0.1370E-01 0.1924E+00 0.0000E+00
750 -0.3284E-02 0.1932E+00 0.0000E+00
751 -0.6589E-02 0.1932E+00 0.0000E+00
752 -0.4471E-01 0.1934E+00 0.0000E+00
753 -0.2247E-01 0.1936E+00 0.0000E+00
754 -0.2288E-01 0.1639E+00 0.0000E+00
760 -0.4851E-02 0.1139E+00 0.0000E+00
951 -0.1446E-01 0.1127E-01 0.0000E+00
953 -0.1794E-01 0.8847E-01 0.0000E+00
961 -0.7463E-02 0.1859E-01 0.0000E+00
962 -0.4313E-02 0.1853E-01 0.0000E+00
963 -0.3129E-02 0.1828E-01 0.0000E+00
964 -0.2133E-01 0.1874E-01 0.0000E+00
967 -0.3497E-01 0.1212E+00 0.0000E+00
968 -0.1572E-01 0.1210E+00 0.0000E+00
969 -0.1310E-01 0.1210E+00 0.0000E+00
970 -0.3881E-02 0.1209E+00 0.0000E+00
971 -0.1409E-01 0.1247E+00 0.0000E+00
973 -0.1347E-01 0.1240E+00 0.0000E+00
975 -0.1809E-01 0.1244E+00 0.0000E+00
976 -0.3413E-01 0.1248E+00 0.0000E+00
978 -0.1064E-02 0.3617E-02 0.0000E+00
***** AUTOTETTORE N. 7 periodo: 0.084045
percentuale di massa attivata :
X
3.055 Y
0.636 Z
0.000

NDO SX SZ
2 -0.1406E+00 0.1039E+00 0.0000E+00
3 -0.1101E+00 -0.1122E-01 0.0000E+00
4 -0.6946E-01 0.2834E-02 0.0000E+00
11 -0.5333E-01 0.1036E+00 0.0000E+00
12 -0.8172E-01 -0.1128E-01 0.0000E+00
14 -0.7803E-01 0.2823E-02 0.0000E+00
19 -0.3867E-02 0.4750E-02 0.0000E+00
20 -0.3301E-01 0.1036E+00 0.0000E+00
21 -0.8526E-01 -0.1123E-01 0.0000E+00
23 -0.8241E-01 0.2801E-02 0.0000E+00
24 -0.6977E-02 0.4753E-02 0.0000E+00
29 -0.4067E-01 0.1040E+00 0.0000E+00
30 -0.9501E-01 0.1127E-01 0.0000E+00
32 -0.1044E+00 0.2784E-02 0.0000E+00
37 -0.3605E-02 0.4750E-02 0.0000E+00
38 -0.8202E-01 0.1127E-01 0.0000E+00
39 -0.8705E-01 0.2810E-02 0.0000E+00
41 -0.4534E-01 0.1035E+00 0.0000E+00
42 -0.2262E-01 0.8752E-01 0.0000E+00
210 -0.6255E-01 0.1751E-01 0.0000E+00
211 -0.6259E-01 0.2584E-02 0.0000E+00
212 -0.8605E-01 0.2584E-02 0.0000E+00
213 -0.8608E-01 0.2501E-02 0.0000E+00
339 -0.1372E+00 -0.8002E-01 0.0000E+00
340 -0.3533E-01 0.3504E-01 0.0000E+00
341 -0.5911E-01 0.5084E-01 0.0000E+00
342 -0.4653E+00 -0.9595E-01 0.0000E+00
466 -0.1166E+00 -0.1116E-01 0.0000E+00
467 -0.5165E-01 0.1116E-01 0.0000E+00
468 -0.8240E-01 0.1074E-01 0.0000E+00
469 -0.9576E-01 0.1070E-01 0.0000E+00
470 -0.1410E+00 0.1018E+00 0.0000E+00
471 -0.6760E-01 0.1066E+00 0.0000E+00
472 -0.2344E-01 0.1053E+00 0.0000E+00
473 -0.3620E-01 0.1078E+00 0.0000E+00
726 -0.1380E+00 0.1487E+00 0.0000E+00
727 -0.2664E+00 0.1489E+00 0.0000E+00
728 -0.5541E-01 0.1484E+00 0.0000E+00
729 -0.1004E-01 0.1482E+00 0.0000E+00
730 -0.3677E-01 0.1518E-01 0.0000E+00

731 -0.2555E-01 -0.3093E-01 0.0000E+00
732 -0.6548E-01 0.3089E-01 0.0000E+00
733 -0.2401E-01 0.2105E-01 0.0000E+00
734 -0.3618E-02 -0.7245E-03 0.0000E+00
735 -0.9082E-01 0.1903E-01 0.0000E+00
737 -0.3629E-01 0.1828E-01 0.0000E+00
738 -0.1340E+00 0.3016E-01 0.0000E+00
739 -0.3317E-01 0.1154E-01 0.0000E+00
740 -0.1321E+00 0.2598E-02 0.0000E+00
741 -0.1028E-01 -0.7230E-03 0.0000E+00
742 -0.6033E-01 0.4762E-02 0.0000E+00
745 -0.7766E-01 0.1839E-01 0.0000E+00
746 -0.3048E-01 0.1904E-01 0.0000E+00
747 -0.9122E-01 0.1904E-01 0.0000E+00
748 -0.3971E-01 0.1878E-01 0.0000E+00
749 -0.9440E-01 0.1872E-01 0.0000E+00
750 -0.8534E-01 0.1878E-01 0.0000E+00
751 -0.3638E-01 0.1873E-01 0.0000E+00
752 -0.1142E+00 0.1759E-01 0.0000E+00
753 -0.6206E-01 0.1856E-01 0.0000E+00
754 -0.6398E-01 0.1192E-01 0.0000E+00
760 -0.9027E-01 0.3009E-01 0.0000E+00
951 -0.7985E-01 0.2974E-01 0.0000E+00
953 -0.1360E+00 0.3002E-02 0.0000E+00
961 -0.3545E-02 0.8749E-01 0.0000E+00
962 -0.4238E-01 0.8757E-01 0.0000E+00
963 -0.2763E+00 0.8778E-01 0.0000E+00
964 -0.1478E+00 0.8651E-01 0.0000E+00
967 -0.6408E-01 0.2963E-01 0.0000E+00
968 -0.1493E-01 0.2974E-01 0.0000E+00
969 -0.8287E-01 0.2978E-01 0.0000E+00
730 -0.1098E+00 0.3011E-01 0.0000E+00
972 -0.6793E-01 0.3005E-01 0.0000E+00
973 -0.8623E-01 0.3007E-01 0.0000E+00
975 -0.1378E+00 0.3883E-01 0.0000E+00
976 -0.6248E-01 0.2946E-01 0.0000E+00
978 -0.1591E-02 0.1178E-01 0.0000E+00
***** AUTOTETTORE N. 8 periodo: 0.082678
percentuale di massa attivata :
X
0.285 Y
0.558 Z
0.000

NDO SX SZ
2 -0.1213E+00 -0.1157E+00 0.0000E+00
3 -0.2687E-01 0.1186E+00 0.0000E+00
5 -0.8807E-01 0.6407E-01 0.0000E+00
11 -0.1806E-01 0.1153E+00 0.0000E+00
12 -0.1478E-01 0.1186E+00 0.0000E+00
14 -0.1656E-01 0.6409E-01 0.0000E+00
730 -0.1578E-02 0.6216E-02 0.0000E+00
20 -0.6845E-03 0.1159E+00 0.0000E+00
21 -0.8636E-02 0.1184E+00 0.0000E+00
23 -0.1581E-02 0.6411E-01 0.0000E+00
28 -0.7580E-02 0.6213E-02 0.0000E+00
729 -0.1404E+00 0.1164E+00 0.0000E+00
730 -0.1112E+00 0.1186E+00 0.0000E+00
32 -0.6539E-01 0.6403E-01 0.0000E+00
37 -0.5886E-02 0.6222E-02 0.0000E+00
38 -0.1828E-01 0.1186E+00 0.0000E+00
39 -0.3001E-01 0.6405E-01 0.0000E+00
41 -0.8674E-02 0.1158E+00 0.0000E+00
42 -0.1481E-02 0.2543E-01 0.0000E+00
210 -0.8787E-01 0.6477E-01 0.0000E+00
211 -0.1309E-01 0.6444E-01 0.0000E+00
212 -0.5821E-01 0.6442E-01 0.0000E+00
213 -0.6647E-01 0.6481E-01 0.0000E+00
219 -0.1037E-01 0.2028E-01 0.0000E+00
340 -0.8313E-03 0.2175E-01 0.0000E+00
341 -0.8312E-04 0.2214E-01 0.0000E+00
342 -0.7916E-01 0.2218E-01 0.0000E+00
466 -0.1643E+00 0.1215E+00 0.0000E+00
467 -0.5646E-01 0.1215E+00 0.0000E+00
468 -0.9315E-02 0.1182E+00 0.0000E+00
469 -0.1112E+00 0.1181E+00 0.0000E+00
730 -0.1193E+00 0.1144E+00 0.0000E+00
471 -0.2367E-01 0.1185E+00 0.0000E+00
472 -0.3642E-01 0.1196E+00 0.0000E+00
473 -0.1013E+00 0.1225E+00 0.0000E+00
210 -0.6208E-01 0.4187E-01 0.0000E+00
727 -0.5809E-01 0.4193E-01 0.0000E+00
728 -0.7641E-03 0.4177E-01 0.0000E+00
729 -0.5240E-02 0.4171E-01 0.0000E+00
730 -0.1027E+00 0.8286E-02 0.0000E+00
731 -0.7123E-01 0.7123E-02 0.0000E+00
732 -0.2278E-01 0.8278E-02 0.0000E+00
733 -0.1198E+00 0.8275E-02 0.0000E+00
734 -0.3576E-02 0.6371E-02 0.0000E+00
735 -0.2139E-01 0.9918E-01 0.0000E+00
737 -0.1993E+00 0.9886E-01 0.0000E+00
738 -0.1106E+00 0.6242E-01 0.0000E+00
739 -0.4012E+00 0.1178E+00 0.0000E+00
740 -0.1090E+00 0.6423E-01 0.0000E+00
741 -0.3674E-02 0.6394E-02 0.0000E+00
742 -0.5646E-02 0.6238E-02 0.0000E+00
745 -0.1533E+00 -0.9989E-01 0.0000E+00
746 -0.3801E-01 0.9903E-01 0.0000E+00
747 -0.1189E+00 0.9902E-01 0.0000E+00
748 -0.1113E+00 0.9905E-01 0.0000E+00
749 -0.1103E+00 0.9905E-01 0.0000E+00
750 -0.1018E-01 0.9917E-01 0.0000E+00
751 -0.2823E-01 0.9908E-01 0.0000E+00
752 -0.1646E+00 0.9980E-01 0.0000E+00
753 -0.1996E+00 0.9881E-01 0.0000E+00
754 -0.2015E+00 0.1177E+00 0.0000E+00
760 -0.6581E-01 0.6152E-01 0.0000E+00
951 -0.1195E-01 0.6246E-01 0.0000E+00
953 -0.1159E+00 0.6439E-01 0.0000E+00
961 -0.2403E-02 0.2444E-01 0.0000E+00
962 -0.4588E-02 0.2538E-01 0.0000E+00
963 -0.5614E-01 0.2480E-01 0.0000E+00
964 -0.5380E-01 0.1549E-01 0.0000E+00
967 -0.9013E-01 0.6246E-01 0.0000E+00
969 -0.1701E-01 0.6246E-01 0.0000E+00
970 -0.6540E-01 0.6246E-01 0.0000E+00
972 -0.1877E-01 0.6411E-01 0.0000E+00
973 -0.1847E-01 0.6383E-01 0.0000E+00
975 -0.1415E+00 0.6406E-01 0.0000E+00
976 -0.8888E-01 0.6375E-01 0.0000E+00
978 -0.3610E-02 0.6235E-02 0.0000E+00
***** AUTOTETTORE N. 9 periodo: 0.068489
percentuale di massa attivata :
X
1.447 Y
0.058 Z
0.000

NDO SX SZ
2 -0.1484E+00 0.1107E+00 0.0000E+00
3 -0.5164E-01 0.3266E-01 0.0000E+00
5 -0.7625E-01 0.1201E-01 0.0000E+00
11 -0.1395E-01 0.1115E+00 0.0000E+00
12 -0.3013E-01 0.3270E-01 0.0000E+00
14 -0.9566E-01 0.1202E-01 0.0000E+00
19 -0.1214E-01 0.3116E-02 0.0000E+00
20 -0.8295E-01 0.1116E+00 0.0000E+00
21 -0.3270E-01 0.3270E-01 0.0000E+00
22 -0.3338E-01 0.1199E-01 0.0000E+00
28 -0.6198E-02 0.3120E-02 0.0000E+00
29 -0.2714E+00 0.1120E+00 0.0000E+00
30 -0.5849E-01 0.3588E-01 0.0000E+00

32 -0.4156E-01 -0.1199E-01 0.0000E+00
37 -0.1258E-01 0.3116E-02 0.0000E+00
38 -0.2401E-01 0.2105E-01 0.0000E+00
39 -0.3156E-01 0.1199E-01 0.0000E+00
41 -0.2623E-01 0.1115E+00 0.0000E+00
42 -0.2623E-01 0.3178E-01 0.0000E+00
210 -0.2027E-01 0.1106E-01 0.0000E+00
211 -0.3319E-01 0.1154E-01 0.0000E+00
212 -0.3405E-01 0.1182E-01 0.0000E+00
213 -0.4220E-01 0.1145E-01 0.0000E+00
214 -0.1152E+00 0.2894E-01 0.0000E+00
340 -0.1554E-01 0.3900E-01 0.0000E+00
341 -0.3727E-01 0.3834E-01 0.0000E+00
342 -0.1387E+00 0.4654E-01 0.0000E+00
466 -0.3672E+00 0.3885E-01 0.0000E+00
467 -0.9440E-01 0.3683E-01 0.0000E+00
468 -0.2072E-01 0.3177E-01 0.0000E+00
469 -0.3848E-01 0.3172E-01 0.0000E+00
470 -0.1351E+00 0.1022E+00 0.0000E+00
728 -0.1698E-01 0.1134E+00 0.0000E+00
472 -0.4061E-01 0.1172E+00 0.0000E+00
473 -0.2713E-01 0.1205E+00 0.0000E+00
728 -0.1157E+00 0.1875E+00 0.0000E+00
727 -0.1395E+00 0.1673E+00 0.0000E+00
730 -0.3489E-01 0.1664E+00 0.0000E+00
739 -0.1665E-01 0.1665E+00 0.0000E+00
730 -0.2726E+00 0.1782E+00 0.0000E+00
731 -0.4070E-01 0.1772E+00 0.0000E+00
732 -0.1848E-01 0.1770E+00 0.0000E+00
733 -0.1788E-01 0.1788E+00 0.0000E+00
734 -0.1258E-01 0.7492E-02 0.0000E+00
735 -0.3623E-01 0.9008E-01 0.0000E+00
737 -0.1453E+00 0.9135E-01 0.0000E+00
738 -0.1571E-01 0.5533E-02 0.0000E+00
975 -0.1378E+00 0.3883E-01 0.0000E+00
740 -0.1542E-01 0.1186E-01 0.0000E+00
741 -0.1344E-01 0.7495E-02 0.0000E+00
742 -0.2918E-03 0.3115E-02 0.0000E+00
745 -0.9931E-01 0.8861E-01 0.0000E+00
746 -0.4127E-01 0.8806E-01 0.0000E+00
747 -0.3094E-01 0.9101E-01 0.0000E+00
748 -0.4638E-01 0.9106E-01 0.0000E+00
749 -0.4136E-01 0.9129E-01 0.0000E+00
750 -0.2687E-01 0.9106E-01 0.0000E+00
751 -0.3128E-01 0.9000E-01 0.0000E+00
752 -0.4186E-01 0.8817E-01 0.0000E+00
730 -0.1457E+00 0.1140E+00 0.0000E+00
754 -0.1449E+00 0.1361E-01 0.0000E+00
760 -0.4127E+00 0.1516E-02 0.0000E+00
973 -0.3134E-01 0.6215E-02 0.0000E+00
953 -0.1915E-01 0.1184E-01 0.0000E+00
962 -0.3053E-01 0.6222E-02 0.0000E+00
963 -0.3662E-01 0.3725E-01 0.0000E+00
964 -0.1478E+00 0.1164E+00 0.0000E+00
966 -0.1112E+00 0.3672E-01 0.0000E+00
967 -0.1881E-01 0.6270E-02 0.0000E+00
968 -0.2053E-01 0.6270E-02 0.0000E+00
969 -0.3235E-01 0.6182E-02 0.0000E+00
970 -0.3001E-01 0.6274E-02 0.0000E+00
972 -0.3323E-01 0.7728E-02 0.0000E+00
97

[illegible][illegible][illegible]

42	-0.005064	-0.01864	0.000407	-0.000028	-0.000063	0.000122
43	0.000000	0.000000	0.000379	0.000004	-0.000017	0.000000
44	0.000000	0.000000	0.000000	0.000000	-0.000002	0.000000
168	0.000000	0.000000	0.000693	-0.000002	-0.000002	0.000000
169	-0.019921	-0.002377	-0.000000	-0.000000	-0.000000	0.000000
211	-0.007110	-0.002233	-0.000549	0.000073	-0.000000	0.000094
212	-0.005632	-0.002323	-0.000552	-0.000000	0.000033	-0.000100
213	-0.00424	-0.002423	-0.000664	-0.000000	-0.000004	0.000000
339	-0.019951	-0.018729	-0.002140	0.000537	-0.000095	-0.000094
340	-0.005415	-0.015674	-0.000000	-0.000000	-0.000000	0.000000
431	-0.003787	-0.018174	-0.000618	-0.000000	0.000015	-0.000079
434	0.006517	-0.015846	-0.000000	-0.000000	-0.000000	0.000000
466	-0.010319	-0.015108	-0.000401	0.0000761	0.0000184	-0.000536
467	-0.003593	-0.011598	-0.000626	0.0000728	0.0000017	-0.000554
468	-0.003534	-0.014845	-0.000608	-0.000000	-0.000002	-0.000540
469	-0.002041	-0.004185	-0.000397	-0.000002	0.000050	-0.000564
470	-0.002851	-0.004957	-0.000398	-0.000000	-0.000000	-0.000564
471	-0.002858	-0.005003	0.000126	-0.000083	-0.000049	-0.000147
472	-0.003137	-0.005013	-0.000628	-0.000010	-0.000019	-0.000176
473	-0.002789	-0.004851	-0.000331	-0.000000	-0.000000	-0.000176
476	-0.019966	-0.012347	-0.000003	-0.000002	-0.000016	-0.000094
477	-0.000000	-0.002536	-0.000000	-0.000000	-0.000000	-0.000000
478	-0.003912	-0.002555	-0.000521	-0.000004	0.000077	0.000115
479	-0.006408	-0.002545	-0.000617	-0.000000	-0.000011	0.000077
730	0.000081	-0.000000	-0.000050	-0.000004	-0.000023	-0.000138
731	-0.001448	-0.009619	0.000715	-0.000009	0.000000	-0.000576
732	-0.002946	-0.009628	-0.000000	-0.000000	-0.000000	-0.000576
733	-0.008639	-0.009630	0.000274	-0.000001	-0.000028	-0.000333
734	-0.000089	-0.000733	0.000027	-0.000000	-0.000000	-0.000333
735	-0.000734	0.011297	0.000330	-0.000028	-0.000125	-0.000575
737	0.014943	0.011278	0.000589	-0.000027	0.000070	-0.000547
738	0.000000	-0.009899	-0.000000	-0.000000	-0.000000	-0.000547
739	0.017212	-0.004452	-0.000729	0.000000	0.000029	-0.000538
740	0.002251	-0.002243	0.000796	-0.000000	-0.000000	-0.000538
741	0.000075	0.000763	-0.000546	-0.000009	0.000070	-0.000547
742	0.000075	0.000033	-0.000561	-0.000000	-0.000000	-0.000547
743	0.000097	-0.011282	-0.000000	-0.000018	0.000010	-0.000504
746	-0.002390	0.011297	0.000579	-0.000028	-0.000024	-0.000561
747	-0.000000	0.011297	-0.000159	-0.000000	-0.000000	-0.000561
748	0.001545	0.012920	0.000546	-0.000018	-0.000021	-0.000539
749	-0.003519	-0.002323	-0.000000	-0.000000	-0.000000	-0.000539
750	-0.000460	-0.000140	0.000119	-0.000001	0.000045	-0.000537
751	-0.005152	-0.014421	-0.000579	0.0000728	0.0000089	-0.000572
752	-0.010304	-0.011371	-0.002131	-0.000000	-0.000000	-0.000572
753	-0.012975	-0.014420	0.000591	-0.000028	-0.000025	-0.000537
754	-0.012862	-0.014554	-0.000			

CONFEZIONE		9 Torcanto_add_y	
UNITA di MISURA:		SV,SZ [cm]	RV,RZ [rad]
Coefficiente moltiplicativo:		1.000000	
SV	RZ	SV	RZ
1.000000	0.000000	0.000018	0.000000
0.000451	0.000000	0.000000	0.000000
0.000530	0.000000	0.000000	0.000000
0.000907	0.000000	0.000000	0.000000
0.001260	0.000000	0.000000	0.000000
0.001620	0.000000	0.000000	0.000000
0.001984	0.000000	0.000000	0.000000
0.002349	0.000000	0.000000	0.000000
0.002715	0.000000	0.000000	0.000000
0.003082	0.000000	0.000000	0.000000
0.003450	0.000000	0.000000	0.000000
0.003819	0.000000	0.000000	0.000000
0.004189	0.000000	0.000000	0.000000
0.004560	0.000000	0.000000	0.000000
0.004932	0.000000	0.000000	0.000000
0.005305	0.000000	0.000000	0.000000
0.005679	0.000000	0.000000	0.000000
0.006054	0.000000	0.000000	0.000000
0.006430	0.000000	0.000000	0.000000
0.006807	0.000000	0.000000	0.000000
0.007185	0.000000	0.000000	0.000000
0.007564	0.000000	0.000000	0.000000
0.007944	0.000000	0.000000	0.000000
0.008325	0.000000	0.000000	0.000000
0.008707	0.000000	0.000000	0.000000
0.009090	0.000000	0.000000	0.000000
0.009474	0.000000	0.000000	0.000000
0.009859	0.000000	0.000000	0.000000
0.010245	0.000000	0.000000	0.000000
0.010632	0.000000	0.000000	0.000000
0.011020	0.000000	0.000000	0.000000
0.011410	0.000000	0.000000	0.000000
0.011801	0.000000	0.000000	0.000000
0.012194	0.000000	0.000000	0.000000
0.012588	0.000000	0.000000	0.000000
0.012984	0.000000	0.000000	0.000000
0.013381	0.000000	0.000000	0.000000
0.013780	0.000000	0.000000	0.000000
0.014181	0.000000	0.000000	0.000000
0.014583	0.000000	0.000000	0.000000
0.014987	0.000000	0.000000	0.000000
0.015392	0.000000	0.000000	0.000000
0.015799	0.000000	0.000000	0.000000
0.016207	0.000000	0.000000	0.000000
0.016617	0.000000	0.000000	0.000000
0.017028	0.000000	0.000000	0.000000
0.017440	0.000000	0.000000	0.000000
0.017854	0.000000	0.000000	0.000000
0.018269	0.000000	0.000000	0.000000
0.018686	0.000000	0.000000	0.000000
0.019104	0.000000	0.000000	0.000000
0.019523	0.000000	0.000000	0.000000
0.019944	0.000000	0.000000	0.000000
0.020366	0.000000	0.000000	0.000000
0.020790	0.000000	0.000000	0.000000
0.021215	0.000000	0.000000	0.000000
0.021642	0.000000	0.000000	0.000000
0.022070	0.000000	0.000000	0.000000
0.022500	0.000000	0.000000	0.000000
0.022932	0.000000	0.000000	0.000000
0.023365	0.000000	0.000000	0.000000
0.023800	0.000000	0.000000	0.000000
0.024236	0.		

870	0.018724	0.506923	-0.001334	0.000059	0.0001851	0.0000805
872	0.039598	0.508402	0.016514	-0.001283	0.000151	0.0000594
874	0.025258	0.529496	-0.007948	0.000000	0.000000	0.000000
875	0.063676	0.597487	-0.015467	-0.001027	0.000027	0.0000565
876	0.057993	0.592330	-0.007948	0.000000	0.000000	0.000000
878	0.026360	0.014540	-0.000662	-0.000320	0.0000209	-0.0001303
879	0.000000	0.000000	0.011244	-0.000135	0.000021	0.000000
880	0.000000	0.000000	0.002468	0.000000	0.000023	0.000000
881	0.000000	0.000000	0.0009751	-0.0000572	0.0000104	0.000000
882	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
883	0.000000	0.000000	0.0006132	-0.000037	0.0000025	0.000000
884	0.000000	0.000000	0.004620	-0.000693	0.0000169	0.000000
885	0.000000	0.000000	0.003242	-0.000638	0.000000	0.000000
886	0.000000	0.000000	0.000138	-0.0000639	0.0000021	0.000000
887	0.000000	0.000000	0.000005	0.000000	0.000000	0.000000
888	0.000000	0.000000	0.000076	-0.000006	0.0000020	0.000000
889	0.000000	0.000000	-0.000505	-0.0000727	0.0000024	0.000000
890	0.000000	0.000000	-0.000542	-0.000067	0.0000024	0.000000
891	0.000000	0.000000	-0.000663	-0.000173	0.0000017	0.000000
892	0.000000	0.000000	-0.000400	-0.000040	0.000000	0.000000
893	0.000000	0.000000	0.015995	-0.000514	0.0000024	0.000000
894	0.000000	0.000000	0.015693	-0.000548	0.0000020	0.000000
895	0.000000	0.000000	0.014761	-0.000475	0.0000015	0.000000
896	0.000000	0.000000	0.012499	-0.000409	0.0000017	0.000000
897	0.000000	0.000000	0.011115	-0.000357	0.0000013	0.000000
898	0.000000	0.000000	0.010262	-0.000366	0.0000008	0.000000
899	0.000000	0.000000	0.008004	-0.000267	0.0000016	0.000000
900	0.000000	0.000000	0.007141	-0.000246	0.0000009	0.000000
1001	0.000000	0.000000	0.007479	-0.000179	0.0000016	0.000000
1002	0.000000	0.000000	0.000850	-0.000085	0.0000001	0.000000
1003	0.000000	0.000000	0.001390	-0.000177	0.0000011	0.000000
1004	0.000000	0.000000	0.000936	-0.000167	0.0000013	0.000000
1005	0.000000	0.000000	0.000946	-0.000173	0.0000012	0.000000
1006	0.000000	0.000000	-0.000340	-0.0000815	0.0000018	0.000000
1007	0.000000	0.000000	-0.000576	-0.000126	0.0000012	0.000000
1008	0.000000	0.000000	-0.000464	-0.000087	0.0000019	0.000000
1009	0.000000	0.000000	-0.000738	-0.000167	0.0000024	0.000000
1010	0.000000	0.000000	-0.000829	-0.000289	0.0000017	0.000000
1011	0.000000	0.000000	-0.000863	-0.000393	0.0000018	0.000000
1012	0.000000	0.000000	-0.000852	-0.000402	0.0000016	0.000000
1013	0.000000	0.000000	-0.011564	-0.000946	0.0000025	0.000000
1014	0.000000	0.000000	-0.012623	-0.000978	0.0000028	0.000000
1015	0.000000	0.000000	-0.010429	-0.000882	0.0000020	0.000000
1016	0.000000	0.000000	-0.016121	-0.000986	0.0000029	0.000000
1017	0.000000	0.000000	-0.012765	-0.000910	0.0000021	

771	0.000000	0.000000	0.000354	-0.000004	-0.000021	0.000000
772	0.000000	0.000000	0.000496	-0.000002	-0.000028	0.000000
773	0.000000	0.000000	0.000496	-0.000002	-0.000028	0.000000
774	0.000000	0.000000	0.000495	-0.000001	-0.000025	0.000000
775	0.000000	0.000000	0.000495	-0.000001	-0.000025	0.000000
776	0.000000	0.000000	0.000548	0.000001	-0.000024	0.000000
777	0.000000	0.000000	0.000495	-0.000009	-0.000028	0.000000
778	0.000000	0.000000	0.000495	-0.000009	-0.000028	0.000000
779	0.000000	0.000000	0.000413	-0.000000	0.000032	0.000000
780	0.000000	0.000000	0.000413	-0.000000	0.000032	0.000000
781	0.000000	0.000000	0.000493	-0.000000	0.000031	0.000000
782	0.000000	0.000000	0.000560	-0.000010	0.000036	0.000000
783	0.000000	0.000000	0.000385	-0.000000	0.000032	0.000000
784	0.000000	0.000000	0.000289	-0.000002	0.000011	0.000000
785	0.000000	0.000000	0.000278	-0.000000	0.000011	0.000000
786	0.000000	0.000000	0.000243	0.000006	0.000014	0.000000
787	0.000000	0.000000	0.000291	-0.000000	0.000024	0.000000
788	0.000000	0.000000	0.000321	-0.000002	0.000024	0.000000
789	0.000000	0.000000	0.000391	0.000024	0.000034	0.000000
790	0.000000	0.000000	0.000493	-0.000000	0.000034	0.000000
791	0.000000	0.000000	0.000590	-0.000000	0.000036	0.000000
792	0.000000	0.000000	0.000417	-0.000026	0.000048	0.000000
793	0.000000	0.000000	0.000247	-0.000000	0.000024	0.000000
794	0.000000	0.000000	-0.000248	-0.000000	0.000002	0.000000
795	0.000000	0.000000	-0.000232	-0.000000	0.000002	0.000000
801	0.000000	0.000000	-0.000257	-0.000002	-0.000002	0.000000
802	0.000000	0.000000	-0.000251	-0.000005	0.000006	0.000000
803	0.000000	0.000000	-0.000265	-0.000000	0.000002	0.000000
804	0.000000	0.000000	-0.000265	-0.000000	-0.000003	0.000000
805	0.000000	0.000000	-0.000261	-0.000000	0.000002	0.000000
806	0.000000	0.000000	-0.000273	-0.000006	0.000000	0.000000
807	0.000000	0.000000	-0.000255	-0.000000	0.000011	0.000000
808	0.000000	0.000000	0.000311	-0.000000	0.000000	0.000000
813	0.000000	0.000000	-0.000691	-0.000018	0.000049	0.000000
814	0.000000	0.000000	-0.000774	-0.000000	0.000000	0.000000
809	0.000000	0.000000	-0.000587	-0.000000	0.000051	0.000000
824	0.000000	0.000000	0.000444	-0.000000	0.000051	0.000000
800	0.000000	0.000000	0.000495	-0.000000	0.000051	0.000000
961	-0.005975	0.020709	0.000335	-0.000021	-0.000089	0.000012
962	0.022576	-0.022323	0.000800	0.000000	0.000025	0.000000
963	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
957	0.000000	0.000000	-0.000273	-0.000007	0.000000	-0.000021
958	0.000000	0.000000	0.000369	-0.000000	0.000000	0.000000
959	0.000000	0.000000	-0.000550	-0.000002	0.000053	0.000538
960	0.000000	0.000000	-0.000554	-0.000000	0.000000	0.000000
964	-0.006301	-0.018564	0.0002			

109	0.000000	0.000000	-0.000001	-0.000013	0.000007	0.000000	0.000000
108	0.000000	0.000000	-0.000035	-0.000007	0.000012	0.000000	0.000000
107	0.000000	0.000000	-0.000032	-0.000011	0.000004	0.000000	0.000000
213	0.0003548	0.0001309	0.000289	-0.000436	-0.000000	0.000000	0.000000
212	0.0002358	0.0001309	0.000289	-0.000436	-0.000000	0.000000	0.000000
211	-0.0005067	0.0001309	0.000289	-0.000436	-0.000000	0.000000	0.000000
309	0.000206	0.0001775	0.000177	-0.000400	0.000005	0.000000	0.000000
308	0.0001977	0.0001775	0.000177	-0.000400	0.000005	0.000000	0.000000
341	0.0001873	0.0001775	-0.000031	0.000366	-0.000000	0.000000	0.000000
340	0.0001941	0.0001775	-0.000031	0.000366	-0.000000	0.000000	0.000000
466	0.0005265	0.0001088	0.000385	-0.000406	-0.000004	0.000000	0.000000
465	0.0001628	0.0001088	0.000313	-0.000405	-0.000000	0.000000	0.000000
464	0.0001211	0.0001088	0.000211	-0.000404	-0.000000	0.000000	0.000000
463	-0.0003121	0.0001088	0.000265	-0.000400	-0.000000	0.000000	0.000000
462	-0.0004932	0.0001088	0.000298	-0.000400	-0.000000	0.000000	0.000000
471	0.0001457	0.0002867	-0.000409	-0.000136	0.000006	0.000000	0.000000
472	0.0000706	0.0002867	-0.000394	-0.000002	0.000000	0.000000	0.000000
473	0.0000331	0.0002777	-0.000391	-0.000000	0.000000	0.000000	0.000000
726	0.0000876	0.0001983	0.000078	-0.000010	0.000001	0.000000	0.000000
725	0.0000294	0.0001982	0.000083	-0.000000	0.000000	0.000000	0.000000
724	0.0001954	0.0001959	0.000103	-0.000000	0.000000	0.000000	0.000000
723	0.0003187	0.0001959	0.000079	0.000002	-0.000000	0.000000	0.000000
722	0.0003334	0.0001959	0.000079	0.000002	-0.000000	0.000000	0.000000
731	0.0000807	-0.0005723	-0.000400	0.000008	-0.000000	0.000000	0.000000
730	0.0001447	-0.0005728	-0.000415	0.000000	-0.000000	0.000000	0.000000
729	0.0004503	-0.0005725	-0.000407	-0.000001	0.000017	0.000000	0.000000
734	0.0000620	-0.0004010	-0.000106	0.000045	-0.000000	0.000000	0.000000
733	0.0001478	-0.0004010	-0.000106	0.000045	-0.000000	0.000000	0.000000
732	-0.0005728	-0.0004010	-0.000306	0.000010	-0.000000	0.000000	0.000000
731	-0.0001880	-0.0004010	-0.000299	0.000000	-0.000000	0.000000	0.000000
730	-0.0006683	-0.0004004	-0.000304	0.000000	-0.000000	0.000000	0.000000
729	-0.0001387	-0.0004010	-0.000419	-0.000000	-0.000000	0.000000	0.000000
728	-0.0004042	-0.0004010	-0.000388	-0.000000	-0.000000	0.000000	0.000000
742	-0.0004622	-0.000000	0.000299	-0.000000	-0.000000	0.000000	0.000000
741	-0.0001613	-0.000000	0.000184	-0.000000	-0.000000	0.000000	0.000000
740	0.0001800	-0.000000	-0.000321	0.000000	-0.000000	0.000000	0.000000
747	0.0001444	-0.0005626	-0.000005	0.000018	0.000000	0.000000	0.000000
746	0.0000293	-0.0005626	-0.000005	0.000018	0.000000	0.000000	0.000000
745	-0.0003608	-0.0005626	-0.000029	0.000000	0.000000</		

[illegible]

972	-0.007094	0.002783	0.005652	0.0000729	0.0000567	0.0001004
973	-0.005934	0.002769	0.005623	0.0000729	0.0000567	0.0001004
974	0.002748	0.000776	0.005566	0.0000760	0.0000599	0.0001000
975	-0.005969	0.002774	0.005626	0.0000760	0.0000599	0.0001000
976	-0.000000	0.000000	-0.000023	0.0000000	0.0000000	0.0000000
977	0.000000	0.000000	-0.000023	0.0000000	0.0000000	0.0000000
978	-0.000000	0.000000	-0.000023	0.0000000	0.0000000	0.0000000
979	0.000000	0.000000	-0.000023	0.0000000	0.0000000	0.0000000
980	0.000000	0.000000	-0.000023	0.0000000	0.0000000	0.0000000
981	0.000000	0.000000	-0.000016	0.0000015	-0.0000009	0.0000000
982	0.000000	0.000000	-0.000016	0.0000015	-0.0000009	0.0000000
983	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
984	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
985	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
986	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
987	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
988	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
989	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
990	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
991	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
992	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
993	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
994	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
995	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
996	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
997	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
998	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000
999	0.000000	0.000000	-0.000017	0.0000015	-0.0000015	0.0000000

```

771 0.000000 0.000000 -0.000192 -0.000008 0.000012 0.000000
772 0.000000 0.000000 -0.000027 -0.000007 0.000007 0.000000
773 0.000000 0.000000 -0.000027 -0.000007 0.000007 0.000000
774 0.000000 0.000000 -0.000022 -0.000005 0.000014 0.000000
775 0.000000 0.000000 -0.000022 -0.000005 0.000014 0.000000
776 0.000000 0.000000 -0.000020 -0.000005 0.000013 0.000000
777 0.000000 0.000000 -0.000020 -0.000005 0.000013 0.000000
778 0.000000 0.000000 -0.000019 -0.000005 0.000017 0.000000
779 0.000000 0.000000 -0.000019 -0.000005 0.000017 0.000000
780 0.000000 0.000000 -0.000018 -0.000004 -0.000016 0.000000
781 0.000000 0.000000 -0.000018 -0.000004 -0.000016 0.000000
782 0.000000 0.000000 -0.000019 -0.000005 0.000014 0.000000
783 0.000000 0.000000 -0.000018 -0.000004 -0.000013 0.000000
784 0.000000 0.000000 -0.000018 -0.000004 -0.000015 0.000000
785 0.000000 0.000000 -0.000019 -0.000005 -0.000008 0.000000
786 0.000000 0.000000 -0.000019 -0.000005 -0.000008 0.000000
787 0.000000 0.000000 -0.000013 -0.000010 -0.000012 0.000000
788 0.000000 0.000000 -0.000013 -0.000010 -0.000012 0.000000
789 0.000000 0.000000 -0.000012 -0.000013 -0.000018 0.000000
790 0.000000 0.000000 -0.000012 -0.000013 -0.000018 0.000000
791 0.000000 0.000000 -0.000010 -0.000014 -0.000020 0.000000
795 0.000000 0.000000 -0.000010 -0.000014 -0.000021 0.000000
797 0.000000 0.000000 -0.000012 -0.000014 -0.000016 0.000000
798 0.000000 0.000000 -0.000013 -0.000015 -0.000019 0.000000
799 0.000000 0.000000 -0.000012 -0.000015 -0.000021 0.000000
800 0.000000 0.000000 -0.000012 -0.000015 -0.000021 0.000000

```


472	0.050410	-0.032306	-0.149023	-0.027424	0.00191	-0.00219
473	0.067320	-0.005130	-0.680523	-0.003496	-0.00030	-0.00129
474	0.000000	-0.380010	-0.143599	-0.000000	-0.000000	-0.000000
475	0.023106	-0.580652	-0.107761	-0.000000	-0.000000	-0.002329
476	0.029863	-0.580726	-0.000000	-0.000000	-0.000005	-0.000000
477	0.000000	-0.000000	-0.000000	-0.000000	-0.000000	-0.000000
478	-0.048644	-0.808617	-0.947682	-0.000000	-0.000000	-0.000000
479	0.067122	-0.498085	-0.863450	-0.000000	0.00136	-0.00240
480	0.075021	-0.349818	-0.808739	-0.000000	0.000000	-0.000000
481	0.004432	-0.349883	-0.813332	-0.000072	0.001514	-0.000000
482	0.000000	-0.219818	-0.349818	-0.000000	0.000000	-0.001618
483	0.007781	-0.003647	-0.066524	-0.000000	0.000008	-0.000041
484	0.002299	-0.133100	-0.000000	-0.000000	0.000000	-0.000000
485	0.004111	-0.000000	-0.000000	-0.000000	0.000000	-0.000000
486	0.004111	-0.000000	-0.000000	-0.000000	0.000000	-0.000000
487	0.128037	-0.401196	-0.602958	-0.000000	-0.000000	-0.000000
488	0.007075	-0.228310	-0.000000	-0.000000	0.000000	-0.000000
489	0.000000	-0.502138	-0.000000	-0.000000	0.000000	-0.000000
490	0.000000	-0.000000	-0.000000	-0.000000	0.000000	-0.000000
491	0.000000	-0.000000	-0.000000	-0.000000	0.000000	-0.000000
492	0.005923	-0.000000	-0.047562	-0.000000	0.000000	-0.000000
493	-0.054672	-0.132796	-0.339910	-0.000000	-0.000000	-0.000000
494	0.000000	-0.000000	-0.133103	-0.048634	-0.000000	-0.000000
495	0.000000	-0.000000	-0.133103	-0.079771	-0.000000	-0.000000
496	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
497	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
498	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
499	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
500	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
501	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
502	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
503	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
504	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
505	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
506	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
507	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
508	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
509	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
510	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
511	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
512	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
513	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
514	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
515	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
516	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
517	0.000000	-0.000000	-0.133103			

1017	0.000000	0.000000	-0.046561	0.00003	0.00001	0.00000
1018	0.000000	0.000000	-0.049626	0.00003	0.00007	0.00000
1019	0.000000	0.000000	-0.049368	0.00004	0.00004	0.00000
1020	0.000000	0.000000	-0.048304	0.00004	0.00007	0.00000
1021	0.000000	0.000000	-0.048200	0.00004	0.00007	0.00000
1022	0.000000	0.000000	-0.049803	0.00003	0.00005	0.00000
1023	0.000000	0.000000	-0.058958	0.00001	0.00006	0.00000
1024	0.000000	0.000000	-0.048979	0.00003	0.00006	0.00000
1025	0.000000	0.000000	-0.048552	0.00000	0.00000	0.00000

SPOSTAMENTI NODI		
C4 DI CARICO		2
SUOLO VENTICO		

N. DI CONDIZIONE ANALISI STATICA					
1	Resil-proprietà	1	1.30		
2	Permanente	1	1.50		
3	Accvar.az.azione	1	1.50		
4	Novo. <10000	1	1.50		

		COMBINAZIONE	
1	+1.50%[0,0]	+1.50%[0,0]	+1.50%[0,0]
Unità di misura:		SK,SY,Z[mm]	KX,KY,Rad [rad]

Coefficienti moltiplicativi:		1.000000			
NO	SK	SY	Z	KX	KY
1	0.000000	0.000000	-0.057175	0.00000	0.00000
2	-0.230130	-0.094244	-0.836003	0.00669	0.00027
3	-0.098313	-0.286618	-0.836003	0.00669	0.00027
4	-0.049447	-0.502093	-0.836003	0.001296	0.00027
11	0.000000	-0.043511	-0.153800	0.00000	0.00000
12	0.000000	-0.238796	-0.165077	0.001800	0.00116
14	0.005292	-0.801016	-0.906999	0.00006	0.00027
19	0.007728	-0.501070	-0.079268	0.00000	0.00000
20	0.007444	-0.634341	-0.149573	-0.00041	0.00058
21	0.008269	-0.238800	-0.836003	0.00000	0.00000
23	0.031265	-0.501119	-0.826555	0.00061	0.00005
28	0.098837	-0.004745	-0.861100	0.00003	0.00006
29	0.573773	-0.043600	-0.836003	0.00000	0.00000
30	0.065535	-0.238777	-0.906999	-0.00019	0.00023
32	0.055646	-0.501344	-0.836003	0.00000	0.00000
37	0.007798	-0.004739	-0.078714	0.00006	0.00007
38	0.042070	-0.238796	-0.124777	0.00110	0.00002
40	0.020869	-0.501070	-0.146548	0.00000	0.00000
40	0.000000	0.000000	-0.109721	0.00001	0.00014
41	0.012617	-0.034560	-0.145987	0.00005	0.00000
42	0.038552	-0.246947	-0.179173	0.00061	0.00002
47	0.000000	0.000000	0.000000	0.00000	0.00011
49	0.000000	0.000000	-0.098392	-0.00019	0.00000
168	0.000000	0.000000	-0.098135	0.00019	0.00013
140	-0.049584	-0.292054	-0.399100	0.00013	0.00001
211	0.004119	-0.502492	-0.046062	0.00249	-0.00017
212	0.013111	-0.000000	-0.000000	-0.00000	-0.00002
213	0.066671	-0.505654	-0.178815	0.00322	-0.00014
339	-0.287729	-0.277134	-0.890268	0.00483	0.00138
340	-0.415847	-0.277134	-0.890268	0.00483	0.00138
341	0.001839	-0.249503	-0.062017	-0.00309	0.00026
342	0.000000	-0.000000	-0.000000	0.00000	0.00000

17/136

[illegible]

20/136

978	0.005043	-0.001630	-0.071794	0.000002	0.000003	-0.001444
979	0.000000	0.000000	-0.041350	-0.000000	0.000005	0.000000
980	0.000000	0.000000	-0.048584	-0.000000	0.000005	0.000000
981	0.000000	0.000000	-0.048581	-0.000000	0.000011	0.000000
982	0.000000	0.000000	-0.052573	-0.000000	0.000005	0.000000
983	0.000000	0.000000	-0.049484	-0.000000	0.000005	0.000000
984	0.000000	0.000000	-0.058021	-0.000000	0.000004	0.000000
985	0.000000	0.000000	-0.052348	-0.000000	0.000005	0.000000
986	0.000000	0.000000	-0.058984	-0.000000	0.000005	0.000000
987	0.000000	0.000000	-0.050025	-0.000000	0.000005	0.000000
988	0.000000	0.000000	-0.055329	0.000000	0.000004	0.000000
989	0.000000	0.000000	-0.047232	0.000000	0.000005	0.000000
990	0.000000	0.000000	-0.054594	0.000000	0.000005	0.000000
991	0.000000	0.000000	-0.043760	0.000008	0.000004	0.000000
992	0.000000	0.000000	-0.048689	0.000000	0.000005	0.000000
993	0.000000	0.000000	-0.035399	-0.000008	0.000000	0.000000
994	0.000000	0.000000	-0.039196	-0.000007	0.000000	0.000000
995	0.000000	0.000000	-0.036554	-0.000000	0.000000	0.000000
996	0.000000	0.000000	-0.040708	-0.000008	0.000004	0.000000
997	0.000000	0.000000	-0.042405	-0.000000	0.000005	0.000000
998	0.000000	0.000000	-0.044111	-0.000000	0.000005	0.000000
999	0.000000	0.000000	-0.042626	0.000001	0.000000	0.000000
1000	0.000000	0.000000	-0.045449	0.000000	0.000000	0.000000
1001	0.000000	0.000000	-0.034878	0.000005	0.000000	0.000000
1002	0.000000	0.000000	-0.043895	0.000005	0.000000	0.000000
1003	0.000000	0.000000	-0.038005	0.000000	0.000001	0.000000
1004	0.000000	0.000000	-0.044070	0.000000	0.000000	0.000000
1005	0.000000	0.000000	-0.036227	0.000005	0.000001	0.000000
1006	0.000000	0.000000	-0.038297	0.000000	0.000004	0.000000
1007	0.000000	0.000000	-0.034347	0.000003	0.000000	0.000000
1008	0.000000	0.000000	-0.034193	0.000000	0.000000	0.000000
1009	0.000000	0.000000	-0.036420	0.000000	0.000000	0.000000
1010	0.000000	0.000000	-0.039795	0.000002	0.000004	0.000000
1011	0.000000	0.000000	-0.033586	0.000001	0.000000	0.000000
1012	0.000000	0.000000	-0.033381	0.000001	0.000000	0.000000
1013	0.000000	0.000000	-0.033586	0.000000	0.000004	0.000000
1014	0.000000	0.000000	-0.034584	0.000000	0.000000	0.000000
1015	0.000000	0.000000	-0.032590	0.000002	0.000000	0.000000
1016	0.000000	0.000000	-0.034732	0.000002	0.000004	0.000000
1017	0.000000	0.000000	-0.032436	0.000004	0.000000	0.000000
1018	0.000000	0.000000	-0.034194	0.000002	0.000004	0.000000
1019	0.000000	0.000000	-0.032590	0.000000	0.000000	0.000000
1020	0.000000	0.000000	-0.033553	0.000002	0.000004	0.000000
1021	0.000000	0.000000	-0.039795	0.000005	0.000000	0.000000
1022	0.000000	0.000000	-0.040866	0.000000	0.000000	0.000000
1023	0.000000	0.000000	-0.040469	0.000000	0.000004	0.000000
1024	0.000000	0.000000	-0.034163	0.000000	0.000000	0.000000
1025	0.000000	0.000000	-0.033808	0.000000	0.000000	0.000000

POSTAMENTO NODI

UNITA DI CARICO : 30 Nera Vertovz

COMBINAZIONE

1	5	CONFEZIONAZIONE ANALISI STATICA																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
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339	-0.218003	-0.465367	-0.597343	0.003201	0.00108	-0.00311
	-0.166493	-0.445348	-0.488593	0.00099	0.00079	-0.00311
340	-0.034869	-0.450683	-0.131011	0.007676	0.00173	-0.00329
	0.004951	-0.112801	-0.122320	-0.003511	0.00178	-0.00351
341	0.004774	-0.226726	-0.114057	-0.003514	0.00176	-0.00407
	0.035049	-0.118146	-0.124005	-0.003061	0.00183	-0.00402
	0.019101	-0.428709	-0.389477	-0.003514	0.00176	-0.00407
	0.243169	-0.138306	-0.500870	0.003513	0.00119	-0.00409
346	-0.078322	-0.352371	-0.515150	0.000788	-0.00001	-0.00387
	-0.163092	0.021434	-0.353548	0.000788	-0.00001	-0.00387
347	-0.005160	-0.323492	-0.102628	-0.002002	-0.00010	-0.00050
	0.012786	-0.024646	-0.080846	0.006350	-0.00009	-0.00018
	-0.000132	-0.338136	-0.091301	-0.000104	-0.00004	-0.00034
	0.012139	0.033864	-0.083433	-0.003009	-0.00009	-0.00025

469	0.0401094	-0.335925	-0.123650	0.00414	0.00072	-0.00047	0.00000	0.00000	0.00000	-0.042183	-0.00012	0.00004	0.00000	1014	0.000000	0.000000	0.000000	-0.030018	0.00007	0.00003	0.00000	790	0.000000	0.000000	0.000000	-0.026170	0.00002	-0.00001	0.00000
470	0.041749	0.039398	-0.148579	-0.05661	0.00090	-0.00014	0.00000	0.00000	0.00000	-0.054178	0.00005	-0.00003	0.00000	1015	0.000000	0.000000	0.000000	-0.048349	-0.00006	0.00006	0.00000	791	0.000000	0.000000	0.000000	-0.026990	0.00000	-0.00001	0.00000
471	0.045221	0.040161	-0.041162	-0.040003	0.00000	-0.040000	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1016	0.000000	0.000000	0.000000	-0.027007	-0.00005	0.00000	0.00000	792	0.000000	0.000000	0.000000	-0.026926	0.00000	-0.00001	0.00000
472	-0.040689	-0.130906	-0.113622	0.00741	0.01041	-0.00103	0.00000	0.00000	0.00000	-0.040451	0.00002	0.00002	0.00000	1017	0.000000	0.000000	0.000000	-0.024122	-0.00008	0.00002	0.00000	793	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
473	0.026028	0.026029	-0.040023	-0.040023	0.00000	-0.040023	0.00000	0.00000	0.00000	-0.040023	0.00000	0.00000	0.00000	1018	0.000000	0.000000	0.000000	-0.027113	-0.00009	0.00000	0.00000	794	0.000000	0.000000	0.000000	-0.027827	-0.00007	0.00001	0.00000
474	0.025793	-0.009714	-0.059002	0.00115	0.01214	-0.00103	0.00000	0.00000	0.00000	-0.047504	0.00003	0.00004	0.00000	1019	0.000000	0.000000	0.000000	-0.027123	-0.00009	-0.00001	0.00000	795	0.000000	0.000000	0.000000	-0.030957	-0.00006	0.00000	0.00000
475	0.041206	0.040024	-0.060000	-0.060000	0.00000	-0.060000	0.00000	0.00000	0.00000	-0.060000	0.00000	0.00000	0.00000	1020	0.000000	0.000000	0.000000	-0.049889	-0.00009	0.00000	0.00000	796	0.000000	0.000000	0.000000	-0.026490	0.00000	-0.00001	0.00000
476	0.0215766	-0.079464	-0.400122	-0.06007	0.00006	-0.00017	0.00000	0.00000	0.00000	-0.040012	0.00002	0.00004	0.00000	1021	0.000000	0.000000	0.000000	-0.025170	-0.00009	0.00002	0.00000	797	0.000000	0.000000	0.000000	-0.033540	-0.00001	0.00001	0.00000
477	0.277421	0.071762	-0.146627	-0.036007	0.00096	-0.00046	0.00000	0.00000	0.00000	-0.046627	0.00013	0.00002	0.00000	1022	0.000000	0.000000	0.000000	-0.046619	-0.00005	0.00007	0.00000	798	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
478	0.277999	-0.423030	-0.046512	-0.046512	0.00000	-0.046512	0.00000	0.00000	0.00000	-0.046512	0.00003	0.00005	0.00000	1023	0.000000	0.000000	0.000000	-0.046619	-0.00005	0.00007	0.00000	799	0.000000	0.000000	0.000000	-0.031549	0.00000	0.00000	0.00000
479	0.168452	-0.104857	-0.693546	0.00070	0.01144	-0.00132	0.00000	0.00000	0.00000	-0.038338	0.00011	0.00001	0.00000	1024	0.000000	0.000000	0.000000	-0.040574	-0.00004	0.00001	0.00000	800	0.000000	0.000000	0.000000	-0.029540	0.00000	0.00001	0.00000
480	0.139131	-0.040727	-0.604130	-0.040727	0.00000	-0.040727	0.00000	0.00000	0.00000	-0.040727	0.00000	0.00000	0.00000	1025	0.000000	0.000000	0.000000	-0.040574	-0.00004	0.00001	0.00000	801	0.000000	0.000000	0.000000	-0.029540	0.00000	0.00001	0.00000
481	0.245170	-0.104765	-0.761935	-0.00121	0.01085	-0.00103	0.00000	0.00000	0.00000	-0.027723	0.00009	0.00002	0.00000	1026	0.000000	0.000000	0.000000	-0.040574	-0.00004	0.00001	0.00000	802	0.000000	0.000000	0.000000	-0.027955	0.00002	0.00001	0.00000
482	0.040436	-0.040436	-0.040436	-0.040436	0.00000	-0.040436	0.00000	0.00000	0.00000	-0.040436	0.00000	0.00000	0.00000	1027	0.000000	0.000000	0.000000	-0.040574	-0.00004	0.00001	0.00000	803	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
483	0.035955	-0.104839	-0.641056	-0.00039	0.00400	-0.00152	0.00000	0.00000	0.00000	-0.021678	0.00009	0.00003	0.00000	1028	0.000000	0.000000	0.000000	-0.050106	-0.00005	0.00007	0.00000	804	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
484	-0.025473	-0.671130	-0.649552	0.00000	0.00395	-0.00130	0.00000	0.00000	0.00000	-0.059451	-0.00005	0.00007	0.00000	1029	0.000000	0.000000	0.000000	-0.034100	-0.00008	0.00002	0.00000	805	0.000000	0.000000	0.000000	-0.027173	0.00001	0.00003	0.00000
485	0.026079	-0.104853	-0.635773	-0.00000	0.00395	-0.00130	0.00000	0.00000	0.00000	-0.059451	-0.00005	0.00007	0.00000	1030	0.000000	0.000000	0.000000	-0.034100	-0.00008	0.00002	0.00000	806	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
486	0.215753	-0.292246	-0.903498	-0.00003	0.00079	-0.00135	0.00000	0.00000	0.00000	-0.052945	-0.00005	0.00007	0.00000	1031	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	807	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
487	0.277427	-0.175238	-0.660294	-0.00001	0.00006	-0.00187	0.00000	0.00000	0.00000	-0.051153	-0.00002	0.00001	0.00000	1032	0.000000	0.000000	0.000000	-0.050106	-0.00005	0.00007	0.00000	808	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
488	0.025870	-0.282170	-0.330121	-0.00073	0.00346	-0.00148	0.00000	0.00000	0.00000	-0.043489	-0.00005	0.00001	0.00000	1033	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	809	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
489	0.041723	-0.175399	-0.539576	-0.00004	0.00359	-0.00167	0.00000	0.00000	0.00000	-0.022210	-0.00001	0.00000	0.00000	1034	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	810	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
490	0.043750	-0.282130	-0.547115	-0.00096	0.00359	-0.00167	0.00000	0.00000	0.00000	-0.043573	-0.00005	0.00001	0.00000	1035	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	811	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
491	0.009016	-0.175307	-0.570402	-0.00000	0.00354	-0.00154	0.00000	0.00000	0.00000	-0.043573	-0.00005	0.00001	0.00000	1036	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	812	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
492	0.145165	-0.282136	-0.327715	-0.00009	0.00086	-0.00104	0.00000	0.00000	0.00000	-0.062278	-0.00003	0.00001	0.00000	1037	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	813	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
493	-0.104981	-0.175289	-0.626217	-0.00007	0.00095	-0.00122	0.00000	0.00000	0.00000	-0.066565	-0.00009	-0.00124	0.00033	1038	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	814	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
494	0.006490	0.008103	-0.092525	-0.00008	0.00007	-0.00023	0.00000	0.00000	0.00000	-0.054552	-0.00007	0.00002	0.00001	1039	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	815	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
495	0.006634	-0.261424	-0.065248	-0.00097	-0.00004	-0.00033	0.00000	0.00000	0.00000	-0.046813	-0.00001	0.00000	0.00000	1040	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	816	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
496	0.009048	0.008459	-0.093111	0.00004	0.00021	0.00023	0.00000	0.00000	0.00000	-0.038011	0.00011	0.00002	0.00014	1041	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	817	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
497	0.062156	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.044874	-0.00003	0.00005	0.00021	1042	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	818	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
498	0.026282	0.084188	-0.049801	-0.00002	0.00038	-0.00000	0.00000	0.00000	0.00000	-0.051153	-0.00002	0.00001	-0.00033	1043	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	819	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
499	0.026282	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.044874	-0.00003	0.00005	0.00021	1044	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	820	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
500	0.026282	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.044874	-0.00003	0.00005	0.00021	1045	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	821	0.000000	0.000000	0.000000	-0.025869	0.00000	0.00000	0.00000
501	0.026282	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.044874	-0.00003	0.00005	0.00021	1046	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.00000	822	0.000000	0.000000	0.000000	-0.027768	0.00001	0.00002	0.00000
502	0.026282	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.044874	-0.00003	0.00005	0.00021	1047	0.000000	0.000000	0.000000	-0.030730	-0.00007	0.00002	0.0000								

466	-0.043855	-0.099033	-0.267709	0.00089	0.00052	-0.00020	1011	0.000000	0.000000	-0.024663	0.00000	-0.00001	0.00000	739	0.048502	-0.000298	-0.035039	0.00033	-0.00006	-0.00015	959	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
467	-0.001017	-0.099012	-0.062134	0.00000	-0.00007	-0.00021	1012	0.000000	0.000000	-0.025274	0.00000	-0.00001	0.00000	740	0.037215	-0.127890	-0.029433	0.00055	-0.00010	-0.00007	960	0.000000	0.000000	-0.028919	-0.00001	0.00003	-0.00012
468	-0.000779	-0.000013	-0.055000	0.00000	-0.00000	-0.00002	1013	0.000000	0.000000	-0.025097	0.00000	-0.00000	0.00000	741	0.001297	-0.000000	-0.025413	0.00000	-0.00000	0.00000	961	0.000000	0.000000	-0.029000	0.00002	0.00003	-0.00013
469	-0.023114	-0.000158	-0.085884	-0.00046	0.00049	-0.00018	1014	0.000000	0.000000	-0.027017	-0.00001	0.00002	0.00000	742	0.047383	-0.153828	-0.026378	0.00016	-0.00010	-0.00015	962	-0.010201	-0.151891	-0.080470	0.00046	-0.00007	-0.00090
470	-0.002057	-0.025495	-0.349599	0.00019	0.00013	-0.00079	1015	0.000000	0.000000	-0.024703	0.00000	-0.00001	0.00000	743	0.002413	-0.025243	-0.020176	0.00000	-0.00000	0.00013	963	0.000000	0.000000	-0.027013	0.00000	0.00000	-0.00000
471	-0.000057	-0.000000	-0.060700	0.00000	-0.00000	-0.00000	1016	0.000000	0.000000	-0.025244	0.00000	-0.00000	0.00000	744	0.001960	-0.000728	-0.026118	0.00000	-0.00002	-0.00006	964	0.000758	-0.151902	-0.073738	0.00000	-0.00006	-0.00001
472	-0.013713	-0.000065	-0.067312	-0.00014	0.00083	-0.00009	1017	0.000000	0.000000	-0.024618	0.00000	-0.00001	0.00000	745	0.001144	-0.004040	-0.025231	0.00000	-0.00000	0.00000	965	0.000000	0.000000	-0.025231	0.00000	0.00000	-0.00000
473	-0.125957	-0.000000	-0.183015	-0.00000	-0.00000	-0.00000	1018	0.000000	0.000000	-0.025015	0.00000	-0.00000	0.00000	746	0.001963	-0.001234	-0.030275	-0.00001	-0.00002	-0.00012	966	0.012963	-0.152016	-0.265049	-0.00003	0.00011	-0.00094
474	-0.119772	-0.232620	-0.478813	0.00077	0.00101	-0.00098	1019	0.000000	0.000000	-0.024048	0.00000	-0.00001	0.00000	747	-0.06330	-0.087139	-0.188902	0.00110	-0.01350	-0.00017	967	-0.137719	-0.040340	-0.287330	-0.00217	0.00026	-0.00097
475	-0.134406	-0.226011	-0.428132	0.00000	0.00000	-0.00000	1020	0.000000	0.000000	-0.024885	0.00001	0.00002	0.00000	748	0.001352	-0.000012	-0.031880	0.00000	-0.00000	0.00000	968	-0.124070	-0.000000	-0.000000	-0.00000	0.00000	-0.00000
476	-0.010565	-0.000000	-0.000000	0.00000	0.00000	-0.00000	1021	0.000000	0.000000	-0.027498	0.00000	0.00000	0.00000	749	-0.003952	-0.087469	-0.046412	0.00050	0.00004	-0.00018	969	-0.114601	-0.040163	-0.324019	0.00242	0.00006	-0.00084
477	-0.007701	-0.126202	-0.389948	0.00026	0.00048	-0.00000	1022	0.000000	0.000000	-0.027413	0.00000	0.00001	0.00000	750	0.000611	-0.000370	-0.027433	0.00000	-0.00000	0.00000	970	0.000000	0.000000	-0.027394	0.00000	0.00000	-0.00000
478	-0.130869	-0.000000	-0.364472	0.00000	0.00000	-0.00000	1023	0.000000	0.000000	-0.027472	0.00000	-0.00000	0.00000	751	-0.040875	-0.029257	-0.168513	0.00014	0.00008	-0.00015	971	-0.037017	-0.236507	-0.048891	0.00010	0.00006	-0.00011
479	-0.013836	-0.142075	-0.340075	0.00014	0.00221	-0.00097	1024	0.000000	0.000000	-0.025252	0.00000	-0.00001	0.00000	752	-0.000442	-0.087469	-0.033854	0.00029	-0.00028	-0.00018	972	0.000000	0.000000	-0.030274	-0.00001	0.00003	0.00000
480	-0.000563	-0.440302	-0.364636	0.00000	0.00000	-0.00000	1025	0.000000	0.000000	-0.025256	-0.00001	-0.00001	0.00000	753	0.000498	-0.000320	-0.037181	0.00000	-0.00000	0.00000	973	0.000000	0.000000	-0.032949	0.00000	0.00000	-0.00000
481	-0.020267	-0.140211	-0.452017	0.00074	0.00059	-0.00070	730	0.020282	-0.087575	-0.052737	-0.00011	0.00036	-0.00013	754	0.000000	0.000000	-0.028901	0.00000	-0.00000	0.00000	974	0.000000	0.000000	-0.028901	0.00000	-0.00001	0.00000
482	-0.002292	-0.001682	-0.031812	0.00000	0.00003	-0.00017	731	0.021250	-0.018415	-0.025622	-0.00007	0.00011	0.00015	755	-0.020278	-0.235486	-0.153662	0.00006	0.00006	-0.00002	975	-0.002028	-0.235486	-0.153662	0.00006	0.00006	-0.00002
483	-0.000628	-0.025202	-0.039648	0.00000	-0.00000	-0.00000	732	0.022106	-0.087554	-0.025622	-0.00007	0.00011	0.00015	756	0.016493	-0.100333	-0.133628	0.00000	-0.00000	0.00000	976	-0.002096	-0.235486	-0.153662	0.00006	0.00006	-0.00002
484	-0.000000	-0.000000	-0.000000	0.00000	0.00000	0.00000	733	0.023575	-0.025993	-0.030817	0.00008	0.00002	-0.00010	757	-0.002694	-0.000807	-0.025648	-0.00014	-0.00038	-0.00015	977	-0.002694	-0.235486	-0.153662	0.00006	0.00006	-0.00002
485	-0.046461	-0.167912	-0.031004	0.00000	-0.00008	-0.00010	734	0.024641	-0.000000	-0.030817	0.00008	0.00002	-0.00010	758	0.000000	-0.000000	-0.027715	-0.00006	-0.00006	0.00000	978	-0.016517	-0.194557	-0.138654	0.00009	0.00001	-0.00014
486	-0.037291	-0.091051	-0.032244	0.00046	-0.00009	-0.00010	735	0.025291	-0.030508	-0.037214	-0.00049	0.00054	-0.00014	759	0.000498	-0.000000	-0.027715	-0.00006	-0.00006	0.00000	979	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
487	-0.043712	-0.101936	-0.033437	0.00021	0.00009	-0.00015	736	0.025818	-0.089983	-0.046445	0.00006	0.00004	-0.00018	760	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	980	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
488	-0.011551	-0.001685	-0.026646	0.00002	0.00000	-0.00010	737	0.026154	-0.000000	-0.046445	0.00006	0.00004	-0.00018	761	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	981	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
489	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	738	0.026705	-0.000000	-0.046445	0.00006	0.00004	-0.00018	762	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	982	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
490	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	739	0.027205	-0.000000	-0.046445	0.00006	0.00004	-0.00018	763	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	983	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
491	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	740	0.027705	-0.000000	-0.046445	0.00006	0.00004	-0.00018	764	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	984	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
492	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	741	0.028205	-0.000000	-0.046445	0.00006	0.00004	-0.00018	765	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	985	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
493	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	742	0.028705	-0.000000	-0.046445	0.00006	0.00004	-0.00018	766	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	986	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
494	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	743	0.029205	-0.000000	-0.046445	0.00006	0.00004	-0.00018	767	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	987	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
495	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	744	0.029705	-0.000000	-0.046445	0.00006	0.00004	-0.00018	768	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	988	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
496	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	745	0.030205	-0.000000	-0.046445	0.00006	0.00004	-0.00018	769	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	989	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
497	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	746	0.030705	-0.000000	-0.046445	0.00006	0.00004	-0.00018	770	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	990	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
498	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	747	0.031205	-0.000000	-0.046445	0.00006	0.00004	-0.00018	771	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	991	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
499	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	748	0.031705	-0.000000	-0.046445	0.00006	0.00004	-0.00018	772	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	992	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
500	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	749	0.032205	-0.000000	-0.046445	0.00006	0.00004	-0.00018	773	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	993	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
501	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	750	0.032705	-0.000000	-0.046445	0.00006	0.00004	-0.00018	774	0.000000	0.000000	-0.027715	-0.00006	-0.00006	0.00000	994	0.000000	0.000000	-0.027715	0.00000	0.00000	-0.00000
502	-0.021554	-0.001683	-0.027764	0.00002	0.00000	-0.00010	751	0.033205	-0.000000	-0.046445	0.00006	0.00004	-0.00018	775	0.000000	0.000000	-0.0277										

3 A*var_abitazione___ + 0.30

1) +1.00*c001 +1.00*c002 +0.30*c009

unità di misura: SX,SY,SZ [m]; RX,RY,RZ [rad]

Coefficiente moltiplicativo: 1.000000

Nodo SX SY SZ RX RY RZ

1	0.000000	0.000000	-0.094208	-0.000000	0.000000	0.000000
2	-0.076082	-0.008318	-0.271164	0.00215	-0.00068	-0.00054
3	-0.022667	-0.069882	-0.209514	0.00241	-0.00041	-0.00028
4	-0.024724	-0.153106	-0.266570	0.00062	-0.00000	-0.00011
11	-0.000920	-0.008350	-0.053227	0.00042	-0.00008	-0.00008
12	-0.001715	-0.009939	-0.049502	0.00007	-0.00004	-0.00004
14	-0.000682	-0.155223	-0.054580	0.00030	-0.00007	-0.00011
19	0.001365	-0.000400	-0.038154	0.00000	0.00005	0.00000
20	0.013904	-0.008346	-0.050638	-0.00014	0.00020	-0.00071
21	0.000779	-0.069938	-0.044378	0.00017	-0.00040	-0.00013
23	0.001531	-0.155296	-0.090114	0.00019	0.00001	-0.00011
28	0.001096	-0.000448	-0.022884	0.00000	0.00001	-0.00024
29	0.144657	-0.008257	-0.232257	-0.00078	-0.00068	-0.00080
30	0.016744	-0.069929	-0.068717	-0.00007	0.00006	-0.00010
32	0.026244	-0.155279	-0.042386	0.00006	0.00006	-0.00011
37	0.001387	-0.000446	-0.072881	0.00000	0.00001	0.00000
38	0.000421	-0.069935	-0.043090	0.00034	-0.00001	-0.00013
39	0.000451	-0.155248	-0.020253	0.00004	0.00000	-0.00011
40	0.000000	0.000000	-0.037398	0.00000	0.00004	-0.00070
41	0.006812	-0.008352	-0.048384	0.00013	0.00003	-0.00070
42	0.000684	-0.072508	-0.057857	-0.00004	-0.00004	-0.00071
107	0.000000	0.000000	-0.039863	0.00000	0.00003	0.00000
109	0.000000	0.000000	-0.032544	-0.00007	0.00004	0.00000
168	0.000000	0.000000	-0.033827	0.00006	0.00004	0.00000
210	-0.043499	-0.157813	-0.126593	0.00073	0.00032	-0.00012
211	-0.001026	-0.155648	-0.054641	0.00078	-0.00008	-0.00012
212	0.001613	-0.155640	-0.049180	0.00000	-0.00052	-0.00011
213	0.016529	-0.156678	-0.042421	0.00000	-0.00064	-0.00012
339	-0.093625	-0.082711	-0.262786	0.00139	-0.00048	-0.00062
340	-0.096659	-0.074739	-0.062123	0.00000	-0.00000	-0.00000
341	0.007586	-0.072110	-0.059562	-0.00000	0.00090	-0.00069
342	0.104123	-0.064388	-0.217753	-0.00216	0.00052	-0.00074
466	-0.024714	-0.076029	-0.209582	0.00069	-0.00000	-0.00015
467	0.000115	-0.075993	-0.049634	0.00077	-0.00007	-0.00016
468	0.001325	-0.069115	-0.044647	0.00007	0.00013	-0.00003
469	0.017053	-0.069081	-0.068782	-0.00036	0.00037	-0.00014
470	-0.027674	-0.039060	-0.271254	0.00012	-0.00012	-0.00000
471	-0.002507	-0.094063	-0.053520	0.00133	0.00074	-0.00062
472	0.014967	-0.007533	-0.050750	-0.00090	-0.00066	-0.00062
473	0.117858	0.000646	-0.233541	0.00113	0.00104	-0.00071
726	-0.093629	-0.178862	-0.178011	0.00060	0.00081	-0.00065
727	-0.104123	-0.178967	-0.180095	0.00000	-0.00005	-0.00007
728	-0.007489	-0.178950	-0.313242	0.00008	0.00136	-0.00072
729	-0.006759	-0.178964	-0.310022	0.00020	0.00196	-0.00071
730	-0.117852	-0.110336	-0.290413	-0.00025	-0.00050	-0.00078
731	-0.015040	-0.110335	-0.271795	0.00011	0.00175	-0.00077
732	-0.000106	-0.110303	-0.275127	0.00000	0.00022	-0.00000
733	-0.072697	-0.110295	-0.335911	0.00057	0.00049	-0.00054
734	0.001380	-0.000923	-0.026913	0.00001	0.00002	-0.00013
745	-0.001194	-0.040463	-0.033279	-0.00024	-0.00001	-0.00013
737	0.026595	-0.040514	-0.027267	0.00022	0.00016	-0.00007
738	0.032254	-0.139358	-0.029143	0.00000	0.00031	-0.00000
739	0.027808	-0.069798	-0.027286	0.00036	-0.00008	-0.00007
740	0.021540	-0.155581	-0.028275	0.00016	0.00006	-0.00011
741	0.000817	-0.000625	-0.023618	0.00001	0.00001	-0.00007
742	0.000820	-0.000447	-0.023637	0.00001	0.00001	-0.00007
745	-0.018521	-0.040109	-0.127760	0.00078	-0.00126	-0.00012
746	-0.002466	-0.040461	-0.036671	0.00032	0.00027	-0.00013
747	0.000081	-0.040461	-0.033938	0.00016	-0.00019	-0.00013
748	0.015578	-0.040518	-0.044395	-0.00008	0.00018	-0.00010
749	0.016494	-0.040158	-0.044416	-0.00036	0.00028	-0.00012
750	-0.000895	-0.041283	-0.033864	-0.00021	0.00042	-0.00011
751	-0.000981	-0.042060	-0.036696	0.00077	0.00042	-0.00014
752	-0.033362	-0.040451	-0.127783	0.00049	0.00067	-0.00013
753	0.027423	-0.041615	-0.027307	0.00022	0.00017	-0.00010
754	0.027396	-0.071555	-0.027319	0.00035	-0.00009	-0.00009
760	0.016488	-0.129402	-0.054633	0.00001	0.00053	-0.00012
761	0.000000	0.000000	-0.028804	-0.00007	0.00005	0.00000
762	0.000000	0.000000	-0.038814	-0.00007	0.00005	0.00000
763	0.000000	0.000000	-0.034165	-0.00007	0.00004	0.00000
764	0.000000	0.000000	-0.032300	-0.00007	0.00005	0.00000
765	0.000000	0.000000	-0.035818	-0.00007	0.00004	0.00000
766	0.000000	0.000000	-0.037158	-0.00005	0.00004	0.00000
767	0.000000	0.000000	-0.035111	-0.00006	0.00005	0.00000
768	0.000000	0.000000	-0.038586	-0.00005	0.00004	0.00000
769	0.000000	0.000000	-0.038641	-0.00005	0.00004	0.00000
770	0.000000	0.000000	-0.037564	0.00004	0.00004	0.00000
771	0.000000	0.000000	-0.039598	0.00005	0.00005	0.00000
772	0.000000	0.000000	-0.038958	0.00004	0.00004	0.00000
773	0.000000	0.000000	-0.039041	0.00006	0.00004	0.00000
774	0.000000	0.000000	-0.032773	0.00006	0.00005	0.00000
775	0.000000	0.000000	-0.036618	0.00006	0.00004	0.00000
776	0.000000	0.000000	-0.032022	0.00006	0.00004	0.00000
777	0.000000	0.000000	-0.039458	0.00006	0.00005	0.00000
778	0.000000	0.000000	-0.020659	-0.00005	-0.00002	0.00000
779	0.000000	0.000000	-0.030462	-0.00005	-0.00002	0.00000
780	0.000000	0.000000	-0.022993	-0.00005	-0.00002	0.00000
781	0.000000	0.000000	-0.023205	-0.00005	-0.00002	0.00000
782	0.000000	0.000000	-0.025264	-0.00004	-0.00002	0.00000
783	0.000000	0.000000	-0.025485	-0.00004	-0.00002	0.00000
784	0.000000	0.000000	-0.026467	0.00000	-0.00001	0.00000
785	0.000000	0.000000	-0.025370	0.00003	-0.00002	0.00000
786	0.000000	0.000000	-0.025545	0.00003	-0.00002	0.00000
787	0.000000	0.000000	-0.023779	0.00003	-0.00001	0.00000
788	0.000000	0.000000	-0.023922	0.00003	-0.00001	0.00000
789	0.000000	0.000000	-0.022615	0.00002	-0.00001	0.00000
790	0.000000	0.000000	-0.022737	0.00002	-0.00001	0.00000
791	0.000000	0.000000	-0.023176	0.00000	-0.00001	0.00000
795	0.000000	0.000000	-0.023176	0.00000	-0.00001	0.00000
797	0.000000	0.000000	-0.023252	0.00000	-0.00001	0.00000
798	0.000000	0.000000	-0.019549	-0.00006	0.00000	0.00000
799	0.000000	0.000000	-0.023126	-0.00006	0.00000	0.00000
800	0.000000	0.000000	-0.022225	-0.00006	0.00001	0.00000
801	0.000000	0.000000	-0.034897	-0.00005	0.00000	0.00000
802	0.000000	0.000000	-0.024885	-0.00005	0.00001	0.00000
803	0.000000	0.000000	-0.026960	-0.00001	-0.00001	0.00000
804	0.000000	0.000000	-0.025739	-0.00003	0.00001	0.00000
805	0.000000	0.000000	-0.025521	0.00003	0.00001	0.00000
806	0.000000	0.000000	-0.024003	0.00003	0.00001	0.00000
807	0.000000	0.000000	-0.023918	0.00003	0.00001	0.00000
808	0.000000	0.000000	-0.022568	0.00002	0.00000	0.00000
813	0.000000	0.000000	-0.023703	-0.00001	0.00001	0.00000
814	0.000000	0.000000	-0.023716	0.00000	0.00002	0.00000
909	0.000000	0.000000	-0.023269	0.00000	0.00002	0.00000
924	0.000000	0.000000	-0.023224	0.00000	-0.00001	0.00000
943	0.000000	0.000000	-0.023159	0.00000	-0.00001	0.00000
951	0.000399	-0.130367	-0.036578	0.00022	0.00001	-0.00011
953	0.021863	-0.155746	-0.028322	-0.00073	-0.00059	-0.00010
954	0.000000	0.000000	-0.026534	0.00000	0.00001	0.00000
957	0.000000	0.000000	-0.022797	0.00001	0.00001	-0.00024
958	0.000000	0.000000	-0.026130	0.00000	-0.00001	-0.00013
959	0.000000	0.000000	-0.023271	0.00000	0.00001	-0.00007
960	0.000000	0.000000	-0.023271	0.00000	-0.00001	-0.00007
961	-0.006365	-0.077536	-0.063101	0.00044	0.00006	-0.00070
962	-0.007784	-0.027513	-0.059456	-0.00008	-0.00004	-0.00071
963	-0.103398	-0.025738	-0.115722	-0.00164	-0.00014	-0.00075
964	-0.094350	-0.077481	-0.262708	0.00035	0.00014	-0.00066
965	0.000000	0.000000	-0.023198	0.00000	0.00002	0.00000
966	0.000000	0.000000	-0.023107	0.00000	-0.00001	0.00000
967	-0.014440	-0.130358	-0.116973	0.00071	0.00003	-0.00010
968	-0.000744	-0.133367	-0.038672	0.00029	-0.00003	-0.00011

969	0.001543	-0.130367	-0.035659	0.00013	0.00001	-0.00011
970	0.016514	-0.130367	-0.054801	-0.00009	-0.00001	-0.00011
972	-0.000028	-0.131812	-0.039684	0.00078	0.00004	-0.00010
973	0.001603	-0.131026	-0.035691	0.00000	0.00004	-0.00011
975	0.013911	-0.131916	-0.029075	-0.00073	0.00008	-0.00010
976	-0.014395	-0.133886	-0.116993	0.00073	0.00021	-0.00010
978	0.001396	0.000162	-0.038664	0.00000	0.00000	-0.00070
979	0.000000	0.000000	-0.020449	-0.00006	0.00002	0.00000
980	0.000000	0.000000	-0.023024	-0.00005	0.00002	0.00000
981	0.000000	0.000000	-0.025886	-0.00006	0.00002	0.00000
982	0.000000	0.000000	-0.026854	-0.00006	0.00002	0.00000
983	0.000000	0.000000	-0.025106	-0.00003	0.00002	0.00000
984	0.000000	0.000000	-0.025066	-0.00004	0.00007	0.00000
985	0.000000	0.000000	-0.026151	-0.00001	0.00002	0.00000
986	0.000000	0.000000	-0.024932	-0.00001	0.00007	0.00000
987	0.000000	0.000000	-0.025873	0.00002	0.00000	0.00000
988	0.000000	0.000000	-0.026887	0.00003	0.00007	0.00000
989	0.000000	0.000000	-0.024696	0.00003	0.00002	0.00000
990	0.000000	0.000000	-0.028154	0.00004	0.00006	0.00000
991	0.000000	0.000000	-0.023180	-0.00003	-0.00001	0.00000
992	0.000000	0.000000	-0.026022	0.00005	0.00005	0.00000
993	0.000000	0.000000	-0.019149	-0.00005	-0.00001	0.00000
994	0.000000	0.000000	-0.021257	-0.00005	-0.00001	0.00000
995	0.000000	0.000000	-0.018984	-0.00005	-0.00001	0.00000
996	0.000000	0.000000	-0.021430	-0.00005	0.00002	0.00000
997	0.000000	0.000000	-0.023484	-0.00003	-0.00002	0.00000
998	0.000000	0.000000	-0.023536	-0.00004	0.00001	0.00000
999	0.000000	0.000000	-0.024371	0.00000	-0.00001	0.00000
1000	0.000000	0.000000	-0.024540	-0.00001	0.00002	0.00000
1001	0.000000	0.000000	-0.023809	0.00002	-0.00001	0.00000
1002	0.000000	0.000000	-0.024098	0.00002	-0.00001	0.00000
1003	0.000000	0.000000	-0.022746	0.00002	-0.00001	0.00000
1004	0.000000	0.000000	-0.022914	0.00003	0.00001	0.00000
1005	0.000000	0.000000	-0.022743	0.00002	-0.00001	0.00000
1006	0.000000	0.000000	-0.021881	0.00002	0.00001	0.00000
1007	0.000000	0.000000	-0.021151	0.00000	-0.00001	0.00000
1008	0.000000	0.000000	-0.022313	0.00000	-0.00001	0.00000
1009	0.000000	0.000000	-0.021415	0.00000	0.00001	0.00000
1010	0.000000	0.000000	-0.022448	0.00000	0.00001	0.00000
1011	0.000000	0.000000	-0.021475	-0.00001	-0.00001	0.00000
1012	0.000000	0.000000	-0.022782	-0.00002	-0.00001	0.00000
1013	0.000000	0.000000	-0.021478	0.00000	0.00000	0.00000
1014	0.000000	0.000000	-0.022727	-0.00001	0.00001	0.00000
1015	0.000000	0.000000	-0.021727	0.00000	0.00000	0.00000
1016	0.000000	0.000000	-0.021701	0.00000	0.00001	0.00000
1017	0.000000	0.000000	-0.021885	0.00000	-0.00001	0.00000
1018	0.000000	0.000000	-0.021768	0.00000	0.00000	0.00000
1019	0.000000	0.000000	-0.021788	0.00000	-0.00001	0.00000
1020	0.000000	0.000000	-0.021764	0.00000	0.00000	0.00000
1021	0.000000	0.000000	-0.021762	0.00000	0.00002	0.00000
1022	0.000000	0.000000	-0.021737	0.00001	0.00001	0.00000
1023	0.000000	0.000000	-0.021313	-0.00001	0.00000	0.00000
1024	0.000000	0.000000	-0.022442	0.00000	-0.00001	0.00000
1025	0.000000	0.000000	-0.020929	-0.00001	-0.00001	0.00000

25/136

Nodo	959	SX	SY	SZ	RX	RY	RZ
		378.3	-42.9	0.0	0.0	0.0	0.0
Nodo	960	SX	SY	SZ	RX	RY	RZ
		-518.3	147.1	0.0	0.0	0.0	0.0

REAZIONI VINCOLARI

CASO DI CARICO : 13 Frequente Vento

COMBINAZIONE

N. 5 CONDIZIONI ANALISI STATICA

- 1 Peso_proprio_____+ 1.00
- 2 Permanente_____+ 1.00
- 3 A'Var_abitazione_____+ 0.50
- 4 NiveL(-1000n_sln)_____+ 0.20
- 5 Vento_y_____+ 0.20

- 1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004 +0.20*c005
- 2) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004 -0.20*c005

Unità di misura: SX,SY,SZ [dm];RX,RY,RZ [dm/cm]

Coefficiente moltiplicativo:		1.000000					
Nodo	40	SX	SY	SZ	RX	RY	RZ
		1057.9	110.4	0.0	0.0	0.0	0.0
		1051.4	-12.9	0.0	0.0	0.0	0.0
Nodo	954	SX	SY	SZ	RX	RY	RZ
		-57.4	148.2	0.0	0.0	0.0	0.0
		-57.4	-4.9	0.0	0.0	0.0	0.0
Nodo	957	SX	SY	SZ	RX	RY	RZ
		-24.9	-184.3	0.0	0.0	0.0	0.0
		-29.9	-467.8	0.0	0.0	0.0	0.0
Nodo	958	SX	SY	SZ	RX	RY	RZ
		-842.0	156.3	0.0	0.0	0.0	0.0
		-817.8	46.5	0.0	0.0	0.0	0.0
Nodo	959	SX	SY	SZ	RX	RY	RZ
		362.2	-71.4	0.0	0.0	0.0	0.0
		394.4	-14.5	0.0	0.0	0.0	0.0
Nodo	960	SX	SY	SZ	RX	RY	RZ
		-495.8	137.7	0.0	0.0	0.0	0.0
		-540.7	156.6	0.0	0.0	0.0	0.0

REAZIONI VINCOLARI

CASO DI CARICO : 14 Quasi Perm

COMBINAZIONE

N. 3 CONDIZIONI ANALISI STATICA

- 1 Peso_proprio_____+ 1.00
- 2 Permanente_____+ 1.00
- 3 A'Var_abitazione_____+ 0.30

- 1) +1.00*c001 +1.00*c002 +0.30*c003

Unità di misura: SX,SY,SZ [dm];RX,RY,RZ [dm/cm]

Coefficiente moltiplicativo:		1.000000					
Nodo	40	SX	SY	SZ	RX	RY	RZ
		888.8	17.5	0.0	0.0	0.0	0.0
		-26.8	41.2	0.0	0.0	0.0	0.0
Nodo	954	SX	SY	SZ	RX	RY	RZ
		-14.8	-257.8	0.0	0.0	0.0	0.0
		-703.6	67.5	0.0	0.0	0.0	0.0
Nodo	958	SX	SY	SZ	RX	RY	RZ
		317.1	-6.9	0.0	0.0	0.0	0.0
		-460.8	138.5	0.0	0.0	0.0	0.0

SOLLECITAZIONI ASTE

N.	4 CONDIZIONI ANALISI STATICA	
1	Reso proprio	+ 1,30

1) +1.30⁰c001 +1.50⁰c002 +1.50⁰c00

Unità di misura: Proj e Trecce [un]; NORM, I
MZZ, MYY, TORS [daNom]

0.	-500.6	-1465.8	-0.7
42	-712.7	-1091.1	-0.7

125.	-1140.1	-341.8	-0.7
167.	-1353.3	32.9	-0.7

292.	-1992.8	1156.9	-0.7
324.	2206.0	1521.6	0.7

PROGR.	NORM	TYT	TZZ
0.	1174.4	-1567.1	-0.8

84.	733.1	-817.7	-0.8
126.	515.5	-443.1	-0.8

252.	-143.4	680.9	-0.8
294	-262.1	1055.6	-0.8

Asta	7	nodi	339
PROGR.	NORM	TYT	TZZ

38.	-3.7	-888.2	2.4
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94.	-3.7	-306.8	2.4
113.	-3.7	-113.0	2.4

190.	-3.7	274.6	2.4
Asta	8	nodh	470

19.	-27.4	-1112.6	9.3
38	-27.4	-918.8	9.3

75.	-27.4	-531.2	9.3
94.	-27.4	-337.4	9.3

150.	-27.4	244.0	9.3
151.	-27.4	244.0	9.3
152.	-27.4	244.0	9.3
153.	-27.4	244.0	9.3
154.	-27.4	244.0	9.3
155.	-27.4	244.0	9.3
156.	-27.4	244.0	9.3
157.	-27.4	244.0	9.3
158.	-27.4	244.0	9.3
159.	-27.4	244.0	9.3
160.	-27.4	244.0	9.3
161.	-27.4	244.0	9.3
162.	-27.4	244.0	9.3
163.	-27.4	244.0	9.3
164.	-27.4	244.0	9.3
165.	-27.4	244.0	9.3
166.	-27.4	244.0	9.3
167.	-27.4	244.0	9.3
168.	-27.4	244.0	9.3
169.	-27.4	244.0	9.3
170.	-27.4	244.0	9.3
171.	-27.4	244.0	9.3
172.	-27.4	244.0	9.3
173.	-27.4	244.0	9.3
174.	-27.4	244.0	9.3
175.	-27.4	244.0	9.3
176.	-27.4	244.0	9.3
177.	-27.4	244.0	9.3
178.	-27.4	244.0	9.3
179.	-27.4	244.0	9.3
180.	-27.4	244.0	9.3
181.	-27.4	244.0	9.3
182.	-27.4	244.0	9.3
183.	-27.4	244.0	9.3
184.	-27.4	244.0	9.3
185.	-27.4	244.0	9.3
186.	-27.4	244.0	9.3
187.	-27.4	244.0	9.3
188.	-27.4	244.0	9.3
189.	-27.4	244.0	9.3
190.	-27.4	244.0	9.3
191.	-27.4	244.0	9.3
192.	-27.4	244.0	9.3
193.	-27.4	244.0	9.3
194.	-27.4	244.0	9.3
195.	-27.4	244.0	9.3
196.	-27.4	244.0	9.3
197.	-27.4	244.0	9.3
198.	-27.4	244.0	9.3
199.	-27.4	244.0	9.3
200.	-27.4	244.0	9.3
201.	-27.4	244.0	9.3
202.	-27.4	244.0	9.3
203.	-27.4	244.0	9.3
204.	-27.4	244.0	9.3
205.	-27.4	244.0	9.3
206.	-27.4	244.0	9.3
207.	-27.4	244.0	9.3
208.	-27.4	244.0	9.3
209.	-27.4	244.0	9.3
210.	-27.4	244.0	9.3
211.	-27.4	244.0	9.3
212.	-27.4	244.0	9.3
213.	-27.4	244.0	9.3
214.	-27.4	244.0	9.3
215.	-27.4	244.0	9.3
216.	-27.4	244.0	9.3
217.	-27.4	244.0	9.3
218.	-27.4	244.0	9.3
219.	-27.4	244.0	9.3
220.	-27.4	244.0	9.3
221.	-27.4	244.0	9.3
222.	-27.4	244.0	9.3
223.	-27.4	244.0	9.3
224.	-27.4	244.0	9.3
225.	-27.4	244.0	9.3
226.	-27.4	244.0	9.3
227.	-27.4	244.0	9.3
228.	-27.4	244.0	9.3
229.	-27.4	244.0	9.3
230.	-27.4	244.0	9.3
231.	-27.4	244.0	9.3
232.	-27.4	244.0	9.3
233.	-27.4	244.0	9.3
234.	-27.4	244.0	9.3
235.	-27.4	244.0	9.3
236.	-27.4	244.0	9.3
237.	-27.4	244.0	9.3
238.	-27.4	244.0	9.3

0.	1526.4	1206.9	1.1
42.	1313.2	832.2	1.1

123.	886.9	82.9	1.1
167.	673.7	-291.8	1.1
222.	122.2	222.2	1.1

292.	34.2	-1415.8	1.1
334	-179.0	-1790.5	1.1

PRGR.	NRM	TY	TZ
0.	579.3	1168.2	1.2

126.	-79.6	44.2	1.2
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252.	-738.5	-1079.8	1.2
294.	-958.1	-1454.4	1.2

ASTA	15	NOOT	340
PROGR.	NORM	TYT	TZZ

38.	-134.4	1476.0	-3.7
66	-134.4	1282.2	-3.7

94.	-134.4	894.7	-3.7
113.	-134.4	700.9	-3.7

1997	1994	1993	199
Asta	16	noti	471
1997	1994	1993	199

19.	468.1	1593.6	0.5
38.	468.1	1399.8	0.5

75.	468.1	1012.2	0.5
94.	468.1	818.4	0.5

150.	468.1	237.0	0.5
Asta	17	podh	19

0.	-685.8	-1021.8	-1.6
42.	-466.2	-647.1	-1.6

168.	192.7	476.9	-1.6
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294.	851.6	1600.9	-1.6
336.	1071.3	1975.6	-1.6

PROGR.	NORM	111	122
0.	-812.9	-1177.9	-1.0

126.	-154.0	-53.9	-1.0
168	65.7	320.8	-1.0

252.	504.9	1070.1	-1.0
294.	724.6	1444.8	-1.0

ASTA	25	1001	342
PROGR.	NORM	TYT	TZZ
0	124.1	1054.4	2.7

38.	-124.1	-1466.8	3.7
56.	-124.1	-1273.0	3.7

94.	-124.1	-885.4	3.7
113.	-124.1	-691.6	3.7

4	-53.7	-680.2	-168.1	-840.7	-1153.9	-45891.0
5	-53.7	-680.3	-168.1	-840.7	-1153.9	-45891.0
6	-53.7	-680.4	-168.1	-840.7	-1153.9	-45891.0
7	-53.7	-680.5	-168.1	-840.7	-1153.9	-45891.0
8	-53.7	-680.6	-168.1	-840.7	-1153.9	-45891.0
9	-53.7	-680.7	-168.1	-840.7	-1153.9	-45891.0
10	-53.7	-680.8	-168.1	-840.7	-1153.9	-45891.0
11	-53.7	-680.9	-168.1	-840.7	-1153.9	-45891.0
12	-53.7	-681.0	-168.1	-840.7	-1153.9	-45891.0
13	-53.7	-681.1	-168.1	-840.7	-1153.9	-45891.0
14	-53.7	-681.2	-168.1	-840.7	-1153.9	-45891.0
15	-53.7	-681.3	-168.1	-840.7	-1153.9	-45891.0
16	-53.7	-681.4	-168.1	-840.7	-1153.9	-45891.0
17	-53.7	-681.5	-168.1	-840.7	-1153.9	-45891.0
18	-53.7	-681.6	-168.1	-840.7	-1153.9	-45891.0
19	-53.7	-681.7	-168.1	-840.7	-1153.9	-45891.0
20	-53.7	-681.8	-168.1	-840.7	-1153.9	-45891.0
21	-53.7	-681.9	-168.1	-840.7	-1153.9	-45891.0
22	-53.7	-682.0	-168.1	-840.7	-1153.9	-45891.0
23	-53.7	-682.1	-168.1	-840.7	-1153.9	-45891.0
24	-53.7	-682.2	-168.1	-840.7	-1153.9	-45891.0
25	-53.7	-682.3	-168.1	-840.7	-1153.9	-45891.0
26	-53.7	-682.4	-168.1	-840.7	-1153.9	-45891.0
27	-53.7	-682.5	-168.1	-840.7	-1153.9	-45891.0
28	-53.7	-682.6	-168.1	-840.7	-1153.9	-45891.0
29	-53.7	-682.7	-168.1	-840.7	-1153.9	-45891.0
30	-53.7	-682.8	-168.1	-840.7	-1153.9	-45891.0
31	-53.7	-682.9	-168.1	-840.7	-1153.9	-45891.0
32	-53.7	-683.0	-168.1	-840.7	-1153.9	-45891.0
33	-53.7	-683.1	-168.1	-840.7	-1153.9	-45891.0
34	-53.7	-683.2	-168.1	-840.7	-1153.9	-45891.0
35	-53.7	-683.3	-168.1	-840.7	-1153.9	-45891.0
36	-53.7	-683.4	-168.1	-840.7	-1153.9	-45891.0
37	-53.7	-683.5	-168.1	-840.7	-1153.9	-45891.0
38	-53.7	-683.6	-168.1	-840.7	-1153.9	-45891.0
39	-53.7	-683.7	-168.1	-840.7	-1153.9	-45891.0
40	-53.7	-683.8	-168.1	-840.7	-1153.9	-45891.0
41	-53.7	-683.9	-168.1	-840.7	-1153.9	-45891.0
42	-53.7	-684.0	-168.1	-840.7	-1153.9	-45891.0
43	-53.7	-684.1	-168.1	-840.7	-1153.9	-45891.0
44	-53.7	-684.2	-168.1	-840.7	-1153.9	-45891.0
45	-53.7	-684.3	-168.1	-840.7	-1153.9	-45891.0
46	-53.7	-684.4	-168.1	-840.7	-1153.9	-45891.0
47	-53.7	-684.5	-168.1	-840.7	-1153.9	-45891.0
48	-53.7	-684.6	-168.1	-840.7	-1153.9	-45891.0
49	-53.7	-684.7	-168.1	-840.7	-1153.9	-45891.0
50	-53.7	-684.8	-168.1	-840.7	-1153.9	-45891.0
51	-53.7	-684.9	-168.1	-840.7	-1153.9	-45891.0
52	-53.7	-685.0	-168.1	-840.7	-1153.9	-45891.0
53	-53.7	-685.1	-168.1	-840.7	-1153.9	-45891.0
54	-53.7	-685.2	-168.1	-840.7	-1153.9	-45891.0
55	-53.7	-685.3	-168.1	-840.7	-1153.9	-45891.0
56	-53.7	-685.4	-168.1	-840.7	-1153.9	-45891.0
57	-53.7	-685.5	-168.1	-840.7	-1153.9	-45891.0
58	-53.7	-685.6	-168.1	-840.7	-1153.9	-45891.0
59	-53.7	-685.7</				

1979.6	782.2	-0.7	-55.8	278.8	-16540.2
1980.6	1156.9	-0.7	-55.8	308.9	25796.6
1981.6	-200.0	0.0	-55.8	339.6	79016.6
sta	4	nodes	230		
1982.6	1174.4	-1567.1	-58.9	100.4	92844.5
1983.6	954.5	-1182.4	-0.8	-58.9	4208.6
1984.6	73.8	8.4	-0.8	-58.9	132.1
1985.6	116.5	-443.1	-0.8	-58.9	135.3
1986.6	206.6	116.6	-0.8	-58.9	2843.0
1987.6	230.0	76.2	306.3	-58.9	258.6
1988.6	-143.7	105.6	-58.9	-58.9	29.9
1989.6	-363.1	105.6	-58.9	-58.9	2304.7
1990.6	-582.7	1430.3	-58.9	353.5	75252.6
1991.6	1174.4	1174.4	722.7	TORS	MY
1992.6	-3.7	-122.7	1.2	-60.7	-5204.3
1993.6	-3.7	-1081.9	2.4	-128.0	289.4
1994.6	-3.7	-688.2	2.4	-128.0	34679.7
1995.6	-3.7	-688.2	2.4	-128.0	188.7
1996.6	-3.7	-500.6	2.4	-128.0	153.4
1997.6	-3.7	-500.6	2.4	-128.0	153.4
1998.6	-3.7	-113.0	2.4	-128.0	62.7
1999.6	-3.7	-113.0	2.4	-128.0	62.7
2000.6	-3.7	274.6	2.4	-128.0	168.5
sta	8	nodes	470	733	
2001.6	1558.4	1558.4	722.7	TORS	MY
2002.6	-27.4	-1306.4	9.3	-119.1	32.2
2003.6	-27.4	-1306.4	9.3	-119.1	32.2
2004.6	-27.4	-918.8	9.3	-119.1	264.8
2005.6	-27.4	-918.8	9.3	-119.1	264.8
2006.6	-27.4	-531.2	9.3	-119.1	375.1
2007.6	-27.4	-337.4	9.3	-119.1	549.1
2008.6	-27.4	-337.4	9.3	-119.1	549.1
2009.6	-27.4	-50.2	9.3	-119.1	88.8
2010.6	-27.4	-50.2	9.3	-119.1	88.8
2011.6	-27.4	-50.2	9.3	-119.1	88.8
2012.6	-27.4	-50.2	9.3	-119.1	88.8
2013.6	-27.4	-50.2	9.3	-119.1	88.8
2014.6	-27.4	-50.2	9.3	-119.1	88.8
2015.6	-27.4	-50.2	9.3	-119.1	88.8
2016.6	-27.4	-50.2	9.3	-119.1	88.8
2017.6	-27.4	-50.2	9.3	-119.1	88.8
2018.6	-27.4	-50.2	9.3	-119.1	88.8
2019.6	-27.4	-50.2	9.3	-119.1	88.8
2020.6	-27.4	-50.2	9.3	-119.1	88.8
2021.6	-27.4	-50.2	9.3	-119.1	88.8
2022.6	-27.4	-50.2	9.3	-119.1	88.8
2023.6	-27.4	-50.2	9.3	-119.1	88.8
2024.6	-27.4	-50.2	9.3	-119.1	88.8
2025.6	-27.4	-50.2	9.3	-119.1	88.8
2026.6	-27.4	-50.2	9.3	-119.1	88.8
2027.6	-27.4	-50.2	9.3	-119.1	88.8
2028.6	-27.4	-50.2	9.3	-119.1	88.8
2029.6	-27.4	-50.2	9.3	-119.1	88.8
2030.6	-27.4	-50.2	9.3	-119.1	88.8
2031.6	-27.4	-50.2	9.3	-119.1	88.8
2032.6	-27.4	-50.2	9.3	-119.1	88.8
2033.6	-27.4	-50.2	9.3	-119.1	88.8
2034.6	-27.4	-50.2	9.3	-119.1	88.8
2035.6	-27.4	-50.2	9.3	-119.1	88.8
2036.6	-27.4	-50.2	9.3	-119.1	88.8
2037.6	-27.4	-50.2	9.3	-119.1	88.8
2038.6	-27.4	-50.2	9.3	-119.1	88.8
2039.6	-27.4	-50.2	9.3	-119.1	88.8
2040.6	-27.4	-50.2	9.3	-119.1	88.8
2041.6	-27.4	-50.2	9.3	-119.1	88.8
2042.6	-27.4	-50.2	9.3	-119.1	88.8
2043.6	-27.4	-50.2	9.3	-119.1	88.8
2044.6	-27.4	-50.2	9.3	-119.1	88.8
2045.6	-27.4	-50.2	9.3	-119.1	88.8
2046.6	-27.4	-50.2	9.3	-119.1	88.8
2047.6	-27.4	-50.2	9.3	-119.1	88.8
2048.6	-27.4	-50.2	9.3	-119.1	88.8
2049.6	-27.4	-50.2	9.3	-119.1	88.8
2050.6	-27.4	-50.2	9.3	-119.1	88.8
2051.6	-27.4	-50.2	9.3	-119.1	88.8
2052.6	-27.4	-50.2	9.3	-119.1	88.8
2053.6	-27.4	-50.2	9.3	-119.1	88.8
2054.6	-27.4	-50.2	9.3	-119.1	88.8
2055.6	-27.4	-50.2	9.3	-119.1	88.8
2056.6	-27.4	-50.2	9.3	-119.1	88.8
2057.6	-27.4	-50.2	9.3	-119.1	88.8
2058.6	-27.4	-50.2	9.3	-119.1	88.8
2059.6	-27.4	-50.2	9.3	-119.1	88.8
2060.6	-27.4	-50.2	9.3	-119.1	88.8
2061.6	-27.4	-50.2	9.3	-119.1	88.8
2062.6	-27.4	-50.2	9.3	-119.1	88.8
2063.6	-27.4	-50.2	9.3	-119.1	88.8
2064.6	-27.4	-50.2	9.3	-119.1	88.8
2065.6	-27.4	-50.2	9.3	-119.1	88.8
2066.6	-27.4	-50.2	9.3	-119.1	88.8
2067.6	-27.4	-50.2	9.3	-119.1	88.8
2068.6	-27.4	-50.2	9.3	-119.1	88.8
2069.6	-27.4	-50.2	9.3	-119.1	88.8
2070.6	-27.4	-50.2	9.3	-119.1	88.8
2071.6	-27.4	-50.2	9.3	-119.1	88.8
2072.6	-27.4	-50.2	9.3	-119.1	88.8
2073.6	-27.4	-50.2	9.3	-119.1	88.8
2074.6	-27.4	-50.2	9.3	-119.1	88.8
2075.6	-27.4	-50.2	9.3	-119.1	88.8
2076.6	-27.4	-50.2	9.3	-119.1	88.8
2077.6	-27.4	-50.2	9.3	-119.1	88.8
2078.6	-27.4	-50.2	9.3	-119.1	88.8
2079.6	-27.4	-50.2	9.3	-119.1	88.8
2080.6	-27.4	-50.2	9.3	-119.1	88.8
2081.6	-27.4	-50.2	9.3	-119.1	88.8
2082.6	-27.4	-50.2	9.3	-119.1	88.8
2083.6	-27.4	-50.2	9.3	-119.1	88.8
2084.6	-27.4	-50.2	9.3	-119.1	88.8
2085.6	-27.4	-50.2	9.3	-119.1	88.8
2086.6	-27.4	-50.2	9.3	-119.1	88.8
2087.6	-27.4	-50.2	9.3	-119.1	88.8
2088.6	-27.4	-50.2	9.3	-119.1	88.8
2089.6	-27.4	-50.2	9.3	-119.1	88.8
2090.6	-27.4	-50.2	9.3	-119.1	88.8
2091.6	-27.4	-50.2	9.3	-119.1	88.8
2092.6	-27.4	-50.2	9.3	-119.1	88.8
2093.6	-27.4	-50.2	9.3	-119.1	88.8
2094.6	-27.4	-50.2	9.3	-119.1	88.8
2095.6	-27.4	-50.2	9.3	-119.1	88.8
2096.6	-27.4	-50.2	9.3	-119.1	88.8
2097.6	-27.4	-50.2	9.3	-119.1	88.8
2098.6	-27.4	-50.2	9.3	-119.1	88.8
2099.6	-27.4	-50.2	9.3	-119.1	88.8
2100.6	-27.4	-50.2	9.3	-119.1	88.8
2101.6	-27.4	-50.2	9.3	-119.1	88.8
2102.6	-27.4	-50.2	9.3	-119.1	88.8
2103.6	-27.4	-50.2	9.3	-119.1	88.8
2104.6	-27.4	-50.2	9.3	-119.1	88.8
2105.6	-27.4	-50.2	9.3	-119.1	88.8
2106.6	-27.4	-50.2	9.3	-119.1	88.8
2107.6	-27.4	-50.2	9.3	-119.1	88.8
2108.6	-27.4	-50.2	9.3	-119.1	88.8
2109.6	-27.4	-50.2	9.3	-119.1	88.8
2110.6	-27.4	-50.2	9.3	-119.1	88.8
2111.6	-27.4	-50.2	9.3	-119.1	88.8
2112.6	-27.4	-50.2	9.3	-119.1	88.8
2113.6	-27.4	-50.2	9.3	-119.1	88.8
2114.6	-27.4	-50.2	9.3	-119.1	88.8
2115.6	-27.4	-50.2	9.3	-119.1	88.8
2116.6	-27.4	-50.2	9.3	-119.1	88.8
2117.6	-27.4	-50.2	9.3	-119.1	88.8
2118.6	-27.4	-50.2	9.3	-119.1	88.8
2119.6	-27.4	-50.2	9.3	-119.1	88.8
2120.6	-27.4	-50.2	9.3	-119.1	88.8
2121.6	-27.4	-50.2	9.3	-119.1	88.8
2122.6	-27.4	-50.2	9.3	-119.1	88.8
2123.6	-27.4	-50.2	9.3	-119.1	88.8
2124.6	-27.4	-50.2	9.3	-119.1	88.8
2125.6	-27.4	-50.2	9.3	-119.1	88.8
2126.6	-27.4	-50.2	9.3	-119.1	88.8
2127.6	-27.4	-50.2	9.3	-119.1	88.8
2128.6	-27.4	-50.2	9.3	-119.1	88.8
2129.6	-27.4	-50.2	9.3	-119.1	88.8
2130.6	-27.4	-50.2	9.3	-119.1	88.8
2131.6	-27.4	-50.2	9.3	-119.1	88.8
2132.6	-27.4	-50.2	9.3	-119.1	88.8
2133.6	-27.4	-50.2	9.3	-119.1	88.8
2134.6	-27.4	-50.2	9.3	-119.1	88.8
2135.6	-27.4	-50.2	9.3	-119.1	88.8
2136.6	-27.4	-50.2	9.3	-119.1	88.8
2137.6	-27.4	-50.2	9.3	-119.1	88.8
2138.6	-27.4	-50.2	9.3	-119.1	88.8
2139.6	-27.4	-50.2	9.3	-119.1	88.8
2140.6	-27.4	-50.2	9.3	-119.1	88.8
2141.6	-27.4	-50.2	9.3	-119.1	88.8
2142.6	-27.4	-50.2	9.3	-119.1	88.8
2143.6	-27.4	-50.2	9.3	-119.1	88.8
2144.6	-27.4	-50.2	9.3	-119.1	88.8
2145.6	-27.4	-50.2	9.3	-119.1	88.8
2146.6	-27.4	-50.2	9.3	-119.1	88.8
2147.6	-27.4	-50.2	9.3	-119.1	88.8
2148.6	-27.4	-50.2	9.3	-119.1	88.8
2149.6	-27.4	-50.2	9.3	-119.1	88.8
2150.6	-27.4	-50.2	9.3	-119.1	88.8
2151.6	-27.4	-50.2	9.3	-119.1	88.8
2152.6	-27.4	-50.2	9.3	-119.1	88.8
2153.6	-27.4	-50.2	9.3	-119.1	88.8
2154.6	-27.4	-50.2	9.3	-119.1	88.8
2155.6	-27.4	-50.2	9.3	-119.1	88.8
2156.6	-27.4	-50.2	9.3	-119.1	88.8
2157.6	-27.4	-50.2	9.3	-119.1	88.8
2158.6	-27.4	-50.2	9.3	-119.1	88.8
2159.6	-27.4	-50.2	9.3	-119.1	88.8
2160.6	-27.4	-50.2	9.3	-119.1	88.8
2161.6	-27.4	-50.2	9.3	-119.1	88.8
2162.6	-27.4	-50.2	9.3	-119.1	88.8
2163.6	-27.4	-50.2	9.3	-119.1	88.8
2164.6	-27.4	-50.2	9.3	-119.1	88.8
2165.6	-27.4	-50.2	9.3	-119.1	88.8
2166.6	-27.4	-50.2	9.3	-119.1	88.8
2167.6	-27.4	-50.2	9.3	-119.1	88.8
2168.6	-27.4	-50.2	9.3	-119.1	88.8
2169.6	-27.4	-50.2	9.3	-119.1	88.8
2170.6	-27.4	-50.2	9.3	-119.1	88.8
2171.6	-27.4	-50.2	9.3	-119.1	88.8
2172.6	-27.4	-50.2	9.3	-119.1	88.8
2173.6	-27.4	-50.2	9.3	-119.1	88.8
2174.6	-27.4	-50.2	9.3	-119.1	88.8
2175.6	-27.4	-50.2	9.3	-119.1	88.8
2176.6	-27.4	-50.2	9.3	-119.1	88.8
2177.6	-27.4	-50.2	9.3	-119.1	88.8
2178.6	-27.4	-50.2	9.3	-119.1	88.8
2179.6	-27.4	-50.2	9.3	-119.1	88.8
2180.6	-27.4	-50.2	9.3	-119.1	88.8
2181.6	-27.4	-50.2	9.3	-119.1	88.8
2182.6	-27.4	-50.2	9.3	-119.1	88.8

6.	2.0	-6240.0	716.9	3124.3	7885.7	-372206.5	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	179.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	Asta	105	nodr	12	467	MY	NZZ	
8.	2.0	-6240.7	716.9	3124.3	6989.5	-380066.9	0.	-1.3	282.1	-7.9	184.0	-587.0	-34748.6	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	
9.	2.0	-6241.0	716.9	3124.3	6989.5	-380066.9	16.	-1.3	278.2	-7.9	184.0	-458.2	-30306.3	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
10.	2.0	-6242.1	716.9	3124.3	5197.2	-395603.3	33.	-1.3	274.2	-7.9	184.0	-329.5	-25708.7	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	38	nodr	38	21	467	MY	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	324.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-115.3	12873.2	640.2	3087.1	5128.8	-339592.3	49.	-1.3	270.2	-7.9	184.0	-200.8	-12385.8	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
1.	-115.3	12873.2	640.2	3087.1	5128.8	-339592.3	81.	-1.3	262.2	-7.9	184.0	-56.7	-12634.0	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
3.	-115.3	12871.8	640.2	3087.1	3528.2	-307401.0	104.	-1.3	254.3	-7.9	184.0	314.2	-4240.8	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
4.	-115.3	12871.1	640.2	3087.1	2727.9	-231311.6	130.	-1.3	250.3	-7.9	184.0	442.9	-141.2	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
5.	-115.3	12870.4	640.2	3087.1	1852.9	-130701.1	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	45.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
6.	-115.3	12869.1	640.2	3087.1	1127.3	-25915.5	81.	-1.3	247.6	-7.9	184.0	-18.0	-41.0	0.	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
9.	-115.3	12868.4	640.2	3087.1	-471.4	-249692.9	16.	-2.4	-278.6	-3.7	-168.5	-32.5	-462.9	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
30.	-115.3	12812.7	640.2	3087.1	-1273.7	-120877.8	16.	-2.4	-278.6	-3.7	-168.5	-32.5	-462.9	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	45	nodr	21	30	467	MY	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	180.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-25.6	2061.3	-34.8	-288.1	-1247.6	-97285.5	65.	-2.4	-290.5	-3.7	-168.5	-153.6	-1306.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
16.	-25.6	2072.3	-34.8	-288.1	-708.1	-130887.8	65.	-2.4	-290.5	-3.7	-168.5	-153.6	-1306.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
31.	-25.6	2061.3	-34.8	-288.1	-142.6	-97285.5	98.	-2.4	-298.5	-3.7	-168.5	-214.1	-1895.7	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
49.	-25.6	2054.3	-34.8	-288.1	422.9	-63811.5	98.	-2.4	-298.5	-3.7	-168.5	-214.1	-1895.7	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
55.	-25.6	2045.3	-34.8	-288.1	988.4	-3022.9	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	360.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
81.	-25.6	2086.3	-34.8	-288.1	1512.9	-34929.5	0.	-114.4	6.2	-0.9	-2.6	-365.0	-3805.2	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
98.	-25.6	2027.3	-34.8	-288.1	2119.5	33655.5	0.	-114.4	6.2	-0.9	-2.6	-365.0	-3805.2	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
114.	-25.6	2008.2	-34.8	-288.1	2685.0	-68525.2	0.	-114.4	6.2	-0.9	-2.6	-365.0	-3805.2	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
130.	-25.6	2009.2	-34.8	-288.1	3250.5	101248.5	5.	-114.4	5.6	-0.9	-2.6	-362.7	-38070.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	76	nodr	964	961	30	467	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	360.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-68.4	-2869.8	24.0	120.1	0.0	341.9	10.	-114.4	4.4	-0.9	-2.6	-357.9	-38045.6	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
33.	-68.4	-2887.8	24.0	120.1	-780.9	-93270.0	13.	-114.4	3.8	-0.9	-2.6	-355.6	-38035.4	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
49.	-68.4	-2896.8	24.0	120.1	-1171.4	-140220.5	15.	-114.4	3.1	-0.9	-2.6	-353.2	-38026.8	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
65.	-68.4	-2905.8	24.0	120.1	-1561.9	-187837.3	18.	-114.4	2.5	-0.9	-2.6	-350.8	-38019.7	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
81.	-68.4	-2914.8	24.0	120.1	-1952.3	-234604.4	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	315.	210.1	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
98.	-68.4	-2923.9	24.0	120.1	-2373.3	-293685.6	0.	-115.8	8.8	-0.9	-2.6	-367.4	-38031.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
120.	-68.4	-2941.9	24.0	120.1	-3212.8	-377441.6	0.	-115.8	8.8	-0.9	-2.6	-367.4	-38031.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	47	nodr	961	42	729	MY	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	360.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-63.5	-6860.5	-19.4	-96.8	-3127.8	-377441.6	49.	-115.8	8.8	-0.9	-2.6	-367.4	-38031.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
1.	-63.5	-6861.2	-19.4	-96.8	-3099.5	-363168.2	65.	-115.8	8.8	-0.9	-2.6	-367.4	-38031.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
4.	-63.5	-6861.9	-19.4	-96.8	-3048.2	-349485.2	81.	-115.8	8.8	-0.9	-2.6	-367.4	-38031.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
4.	-63.5	-6862.6	-19.4	-96.8	-3051.1	-403623.0	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	180.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
6.	-63.5	-6864.0	-19.4	-96.8	-3056.9	-412336.1	130.	-115.8	8.8	-0.9	-2.6	-367.4	-38031.5	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
6.	-63.5	-6864.0	-19.4	-96.8	-3056.9	-412336.1	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	360.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
8.	-63.5	-6867.4	-19.4	-96.8	-2978.5	-422811.6	0.	-370.2	0.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
9.	-63.5	-6867.4	-19.4	-96.8	-2978.5	-422811.6	0.	-370.2	0.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
10.	-63.5	-6868.1	-19.4	-96.8	-2930.1	-447275.0	50.	-370.2	0.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
Asta	80	nodr	962	963	30	467	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ	360.	72.8	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
0.	-182.1	6977.7	-3.8	-19.0	-2940.0	-463106.1	99.	-370.2	0.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
1.	-182.1	6977.7	-3.8	-19.0	-2940.0	-463106.1	124.	-370.2	0.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
3.	-182.1	6977.7	-3.8	-19.0	-2940.0	-463106.1	149.	-370.2	0.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1	-3150.0	0.0
4.	-182.1	6977.7	-3.8	-19.0	-2940.0	-463106.1	174.	-370.2	0.0	0.0	0.0	0.0	0.0	0.0	943.4	0.0	0.0	0.0	0.0	0.0	0.0	1.	-4128.2	720.0	-18142.7	0.0	-907.1		

49.	-169.1	-1708.8	-23.8	-237.7	875.0	-47188.3	230.	-15.8	-1258.5	-5.9	-15.5	677.8	-43550.5	33.	32.5	1386.8	-2.8	10.4	-94.3	-71105.1	4.	-1703.3	33.9	3701.3	0.0	2313.3	-21.2	
65.	-169.1	1099.0	-23.8	237.7	1261.1	-29256.1	Asta	138	nodi	975	953			49.	32.5	1377.8	-2.8	10.4	-48.3	-48643.3	5.	-1703.1	33.9	3701.3	0.0	0.0	0.0	
81.	-169.1	1090.0	-23.8	237.7	1641.2	-31470.7	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ	
98.	-169.1	1081.0	-23.8	237.7	2033.2	6169.4			-54.4	1188.6	0.0	0.0	0.0	81.	32.5	1359.8	-2.8	10.4	-43.8	-4158.6								
114.	-169.1	1072.0	-23.8	237.7	2419.3	23865.6			-54.4	891.4	0.0	0.0	-0.1	98.	32.5	1350.8	-2.8	10.4	89.9	-2488.0								
130.	-169.1	1063.0	-23.8	237.7	2810.4	3943.7			-54.4	294.3	0.0	0.0	0.0	114.	32.5	1340.8	-2.8	10.4	136.0	-3749.9								
PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ			-54.4	29.0	0.0	0.0	-0.4	130.	32.5	1332.7	-2.8	10.4	182.0	6184.1								
0.	-8.3	297.3	24.9	5.7	2805.3	40205.3			-54.4	0.0	0.0	0.0	-0.6	115.	32.5	1327.7	-2.8	10.4	185.0	-987.8								
18.	-8.3	343.3	24.9	5.7	2368.9	44800.5			-54.4	-594.3	0.0	0.0	0.0	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ								
35.	-8.3	391.3	24.9	5.7	1915.5	48013.5			-54.4	-801.3	0.0	0.0	0.0	0.	-20.9	-762.9	8.5	42.5	0.0	104.5								
53.	-8.3	440.9	24.9	5.7	1496.1	43682.2			-54.4	-1046.1	0.0	0.0	0.0	35.	-20.9	-771.9	8.5	42.5	-136.0	-1235.6								
70.	-8.3	319.0	24.9	5.7	310.0	3940.0			-54.4	-1188.6	0.0	0.0	0.0	115.	-20.9	-780.9	8.5	42.5	-276.0	-2498.0								
88.	-8.3	473.0	24.9	5.7	63.3	32518.7			-54.4	0.0	0.0	0.0	-0.9	70.	-20.9	-789.9	8.5	42.5	-404.0	-3748.8								
105.	-8.3	527.1	24.9	5.7	384.9	3985.1			-54.4	0.0	0.0	0.0	-2.6	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ								
123.	-8.3	781.2	24.9	5.7	-249.5	10570.3			-54.4	0.0	0.0	0.0	-5.1	88.	-20.9	-798.9	8.5	42.5	-552.0	-5083.9								
140.	-8.3	855.2	24.9	5.7	-685.9	44484.4			-54.4	0.0	0.0	0.0	-7.6	114.	-20.9	-825.9	8.5	42.5	-966.0	-8029.1								
PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ			-54.4	0.0	0.0	0.0	-10.1	130.	-20.9	-854.9	8.5	42.5	-1104.0	-10733.4								
0.	-70.2	-1907.7	-15.8	2303.9	-215.0	-11749.7			-70.2	-129.4	1.6	-5.8	19.0	Asta	159	nodi	967	976										
1.	-70.2	-1908.4	-15.8	2303.9	-295.2	-118832.7			-70.2	-56.2	1.6	-5.8	123.3	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ								
3.	-70.2	-1909.1	-15.8	2303.9	-275.5	-122238.6			-70.2	-114.4	1.2	30.6	160.9	0.	-762.9	8.5	20.9	0.0	78.4	-4.0								
5.	-70.2	-1909.8	-15.8	2303.9	-253.8	-124662.4			-70.2	-168.1	1.6	-5.8	11.7	1.	-762.7	8.5	20.9	0.0	65.3	-26.5								
7.	-70.2	-1910.5	-15.8	2303.9	-236.1	-126989.0			-70.2	-217.7	1.6	-5.8	30.6	3.	-762.4	8.5	20.9	0.0	39.2	-15.9								
9.	-70.2	-1911.2	-15.8	2303.9	-216.4	-129381.5			-70.2	-267.6	1.6	-5.8	18.2	Asta	160	nodi	969	973										
11.	-70.2	-1911.8	-15.8	2303.9	-196.6	-131770.9			-70.2	-316.5	1.2	30.6	118.6	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ								
13.	-70.2	-1912.5	-15.8	2303.9	-176.9	-134162.1			-70.2	-365.7	1.2	30.6	76.3	0.	-762.7	8.5	20.9	0.0	13.1	-5.3								
15.	-70.2	-1913.2	-15.8	2303.9	-157.2	-136532.3			-70.2	-414.6	1.2	30.6	30.4	1.	-762.7	8.5	20.9	0.0	0.0	0.0								
Asta	124	nodi	735	747					-70.2	-463.6	1.2	30.6	12.9	PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ								
0.	69.2	2109.1	12.5	1500.4	-158.2	-122928.8			-70.2	-512.6	1.2	30.6	6.0	0.	-1189.0	9.4	0.0	0.0	0.0	-46.9								
1.	69.2	2108.4	12.5	1500.4	-138.5	-120029.9			-70.2	-561.7	1.2	30.6	2.9	1.	-1189.0	9.4	0.0	0.0	0.0	0.0								
3.	69.2	2107.7	12.5	1500.4	-118.5	-117657.8			-70.2	-610.7	1.2	30.6	0.0	3.	-1189.0	9.4	0.0	0.0	0.0	0.0								
5.	69.2	2107.0	12.5	1500.4	-98.5	-115037.3			-70.2	-659.7	1.2	30.6	0.0	5.	-1189.0	9.4	0.0	0.0	0.0	0.0								
7.	69.2	2106.3	12.5	1500.4	-78.5	-112416.8			-70.2	-708.7	1.2	30.6	0.0	7.	-1189.0	9.4	0.0	0.0	0.0	0.0								
9.	69.2	2105.6	12.5	1500.4	-58.5	-109797.9			-70.2	-757.7	1.2	30.6	0.0	9.	-1189.0	9.4	0.0	0.0	0.0	0.0								
11.	69.2	2104.9	12.5	1500.4	-38.5	-107179.0			-70.2	-806.7	1.2	30.6	0.0	11.	-1189.0	9.4	0.0	0.0	0.0	0.0								
13.	69.2	2104.2	12.5	1500.4	-18.5	-104560.6			-70.2	-855.7	1.2	30.6	0.0	13.	-1189.0	9.4	0.0	0.0	0.0	0.0								
15.	69.2	2103.5	12.5	1500.4	2.5	-101945.7			-70.2	-904.7	1.2	30.6	0.0	15.	-1189.0	9.4	0.0	0.0	0.0	0.0								
PROGR.	NORM	TYV	TZZ	TORS	MYV	MZZ			-70.2	-953.7	1.2	30.6	0.0	17.	-1189.0	9.4	0.0	0.0	0.0	0.0								
0.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1002.7	1.2	30.6	0.0	19.	-1189.0	9.4	0.0	0.0	0.0	0.0								
1.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1051.7	1.2	30.6	0.0	21.	-1189.0	9.4	0.0	0.0	0.0	0.0								
3.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1100.7	1.2	30.6	0.0	23.	-1189.0	9.4	0.0	0.0	0.0	0.0								
5.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1149.7	1.2	30.6	0.0	25.	-1189.0	9.4	0.0	0.0	0.0	0.0								
7.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1198.7	1.2	30.6	0.0	27.	-1189.0	9.4	0.0	0.0	0.0	0.0								
9.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1247.7	1.2	30.6	0.0	29.	-1189.0	9.4	0.0	0.0	0.0	0.0								
Asta	125	nodi	748	750					-70.2	-1296.7	1.2	30.6	0.0	31.	-1189.0	9.4	0.0	0.0	0.0	0.0								
0.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1345.7	1.2	30.6	0.0	33.	-1189.0	9.4	0.0	0.0	0.0	0.0								
1.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1394.7	1.2	30.6	0.0	35.	-1189.0	9.4	0.0	0.0	0.0	0.0								
3.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1443.7	1.2	30.6	0.0	37.	-1189.0	9.4	0.0	0.0	0.0	0.0								
5.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1492.7	1.2	30.6	0.0	39.	-1189.0	9.4	0.0	0.0	0.0	0.0								
7.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1541.7	1.2	30.6	0.0	41.	-1189.0	9.4	0.0	0.0	0.0	0.0								
9.	-765.7	48.7	-160.9	0.0	-703.7	-213.0			-70.2	-1590.7	1.2	30.6	0.0	43.	-1189.0	9.4	0.0	0.0	0.0	0.0								
Asta	126	nodi	749	750					-70.2	-1639.7	1.2	30.6	0.0	45.	-1189.0	9.4	0.0	0.0	0.0	0.0								
0.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-1688.7	1.2	30.6	0.0	47.	-1189.0	9.4	0.0	0.0	0.0	0.0								
1.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-1737.7	1.2	30.6	0.0	49.	-1189.0	9.4	0.0	0.0	0.0	0.0								
3.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-1786.7	1.2	30.6	0.0	51.	-1189.0	9.4	0.0	0.0	0.0	0.0								
5.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-1835.7	1.2	30.6	0.0	53.	-1189.0	9.4	0.0	0.0	0.0	0.0								
7.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-1884.7	1.2	30.6	0.0	55.	-1189.0	9.4	0.0	0.0	0.0	0.0								
9.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-1933.7	1.2	30.6	0.0	57.	-1189.0	9.4	0.0	0.0	0.0	0.0								
Asta	127	nodi	750	751					-70.2	-1982.7	1.2	30.6	0.0	59.	-1189.0	9.4	0.0	0.0	0.0	0.0								
0.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-2031.7	1.2	30.6	0.0	61.	-1189.0	9.4	0.0	0.0	0.0	0.0								
1.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-2080.7	1.2	30.6	0.0	63.	-1189.0	9.4	0.0	0.0	0.0	0.0								
3.	-955.8	-347.6	0.5	0.0	2.7	1738.1			-70.2	-2																		

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3.	-33.2	-856.5	-917.0	-4199.2	6679.4	7097.3	0.0	15.8	-26.3	-91.6	-505.6	81.9	-42.0	4.	34.8	627.7	-566.6	2365.4	-3713.9	-3865.2	16.1	-320.7	57.9	23	1677.8	1111.1	-952.0
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.4	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-530																					

[illegible]

PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																									
																										ASTA	PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																														
																																																					ASTA	PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
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45.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

3.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5	
50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5	
50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.							

105.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
105.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
105.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
105.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

123.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
123.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
123.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
123.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

140.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
140.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
140.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
140.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

ASTA	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
ASTA	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
ASTA	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
ASTA	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

165.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
165.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
165.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
165.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

206.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
206.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
206.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
206.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

248.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
248.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
248.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
248.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

289.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
289.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
289.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
289.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

33.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
33.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
33.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
33.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.						

49.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
49.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5
49.	50.3	-60.4	-8.6	0.0	-26.7	138.7	PROG.	NORM	TYY	TZZ	TORS	MYY	MZZ	19.7	-5.1	1.9	-26.7	32.3	413.0	3.	-6.2	-11.7	-3.0	-18.0	241.2	-178.5

5.	Asta PROGR. 0.	8.1	41.9	0.0	0.0	0.0	-26.2	76.5	8.0	0.0	0.0	3.0	686.5	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	41.5	-19.0	0.0	-35.6	-77.7				
		-6.6	-6.3	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-4.0	-915.4	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	19.0	0.0	23.7	-91.8				
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.1	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	19.0	0.0	-7.6	-44.3			
		-8.1	-41.9	0.0	0.0	0.0	0.0	-35.1	-9.1	0.1	0.0	-7.7	-1044.7	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-35.4	6.1	0.0	7.6	-44.3			
1.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	29.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8			
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8			
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8			
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8			
2.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	58.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8		
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8		
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8		
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8		
3.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	86.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8	
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8	
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8	
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8	
4.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	115.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
5.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	144.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
6.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	173.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
7.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	201.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
8.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	229.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
9.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	257.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
10.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	285.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-9.1	-5.8	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
11.	Asta PROGR. 0.	-8.0	-51.6	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	313.	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0						

	317.9	12.7	-23.4	81.6	7868.8	-1623.3			3.9	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5415.8	70.1			-3.9	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5415.7	70.1			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-317.9	-12.7	-23.4	-81.6	-7868.8	1623.3			-4.8	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	81.6	7883.4	-1615.4			3.9	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.7	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7898.1	-1712.4			3.9	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	23.4	-81.6	-7912.7	1599.5			-253.5	-6.7	0.0	0.0	-1.2	-385.7	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5437.6	72.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	317.9	12.7	-23.4	81.6	7883.4	1607.4			-253.5	-6.7	0.0	0.0	-0.6	-202.8	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5448.6	73.2			-246.6	-8.1	0.0	0.0	-1.1	-232.5	0.0
	317.9	12.7	-23.4	81.6	-7892.4	-1599.5			253.5	-6.7	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5426.3	71.2			0.0	0.0	0.0</				

	1.5	9.3	-20.8	0.0	-51.5	-23.1		-7.1	-2.6	44.3	129.4	-311.8	364.0
	-3.0	-7.2	18.5	0.0	-46.2	17.9		-7.3	-2.6	-44.3	-129.4	311.8	-364.0
	-3.0	0.0	-7.2	-18.5	0.0	-17.9		-4.3	-2.6	39.9	103.8	-249.1	286.7
	-1.5	-9.3	-20.8	0.0	51.5	23.1		5.5	-2.4	-39.9	-103.8	249.1	-286.7
3.	1.5	9.3	-20.8	0.0	-51.5	-23.1		-7.1	-2.6	44.3	129.4	-311.8	364.0
	-3.0	-7.2	18.5	0.0	-46.2	17.9		-7.3	-2.6	-44.3	-129.4	311.8	-364.0
	-3.0	0.0	-7.2	-18.5	0.0	-17.9		-4.3	-2.6	39.9	103.8	-249.1	286.7
	-1.5	-9.3	-20.8	0.0	51.5	23.1		-5.5	-2.4	-39.9	-103.8	249.1	-286.7
4.	1.5	9.3	-20.8	0.0	-51.5	-23.1		-7.1	-2.6	44.3	129.4	-311.8	364.0
	-3.0	-7.2	18.5	0.0	-46.2	17.9		-7.3	-2.6	-44.3	-129.4	311.8	-364.0
	-3.0	0.0	-7.2	-18.5	0.0	-17.9		-4.3	-2.6	39.9	103.8	-249.1	286.7
	-1.5	-9.3	-20.8	0.0	51.5	23.1		-5.5	-2.4	-39.9	-103.8	249.1	-286.7
5.	1.5	9.3	-20.8	0.0	-51.5	-23.1		-7.1	-2.6	44.3	129.4	-311.8	364.0
	-3.0	-7.2	18.5	0.0	-46.2	17.9		-7.3	-2.6	-44.3	-129.4	311.8	-364.0
	-3.0	0.0	-7.2	-18.5	0.0	-17.9		-4.3	-2.6	39.9	103.8	-249.1	286.7
	-1.5	-9.3	-20.8	0.0	51.5	23.1		-5.5	-2.4	-39.9	-103.8	249.1	-286.7
Astra	160	969	973					-7.1	-2.6	44.3	129.4	-311.8	364.0
PROG.	0.	0.0	0.0	0.0	0.0	0.0	0.0	-7.3	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	-206.8	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	225.3	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-225.3	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	206.8	0.0	7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-206.8	0.0	-7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	139.1	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-139.1	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	181.0	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-181.0	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	155.1	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-155.1	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	112.6	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-112.6	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	103.4	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-103.4	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	77.6	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-77.6	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	84.5	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-84.5	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	77.6	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-77.6	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	51.7	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-51.7	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	56.3	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-56.3	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	51.7	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-51.7	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	28.2	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-28.2	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	25.9	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-25.9	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
Astra	161	968	972					-7.1	-2.6	44.3	129.4	-311.8	364.0
PROG.	0.	0.0	0.0	0.0	0.0	0.0	0.0	-7.3	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	-206.8	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	225.3	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-225.3	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	206.8	0.0	7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-206.8	0.0	-7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	139.1	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-139.1	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	181.0	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-181.0	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	155.1	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-155.1	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	112.6	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-112.6	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	103.4	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-103.4	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	77.6	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-77.6	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	84.5	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-84.5	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	77.6	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-77.6	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	51.7	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-51.7	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	56.3	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-56.3	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	51.7	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-51.7	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	28.2	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	-28.2	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	25.9	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-25.9	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	-7.1	-2.6	44.3	129.4	-311.8	364.0
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	7.1	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	0.0	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
Astra	162	968	972					-7.1	-2.6	44.3	129.4	-311.8	364.0
PROG.	0.	0.0	0.0	0.0	0.0	0.0	0.0	-7.3	-2.6	-44.3	-129.4	311.8	-364.0
	0.0	-45.1	0.0	0.0	0.0	-206.8	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	225.3	0.0	5.5	-2.4	-39.9	-103.8	249.1	-286.7
	0.0	-45.1	0.0	0.0	0.0	-225.3	0.0	-5.5	-2.4	-39.9	-103.8	249.1	-286.7

[illegible]

131.	-8.6	-4.4	3.0	23.8	-302.3	176.2	38.	210.7	-0.9	0.2	20.6	-32.0	111.5	336.	-377.9	7.5	0.0	3.2	14.3	872.7	168.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	8.9	3.1	-3.1	-27.9	306.0	-127.2		-220.2	-0.1	-0.4	-24.8	43.1	5.4		377.9	-7.5	0.0	-3.2	-15.6	-1188.5		812.5	-4.0	0.0	1.4	-5.1	1125.7
	-8.9	-3.3	-0.1	27.9	-306.0	127.2		-220.2	0.1	0.4	24.8	-43.1	-5.4		-377.9	7.5	0.0	-3.2	15.6	-1188.5		-812.5	4.0	0.0	-1.4	5.1	-1125.7
	8.6	4.4	-3.0	-23.8	302.3	-176.2		-210.7	0.9	-0.2	-20.6	32.0	-111.5		274.4	-6.2	0.0	-1.3	-5.4	-938.7		869.6	-2.9	0.0	3.8	-13.3	1143.6
150.	-8.6	-4.4	3.0	23.8	-357.9	193.7	56.	210.7	-0.9	0.2	-20.6	-36.5	94.7	Asta PROGR. 0.	304.2	-8.0	-2.5	5.1	126.6	872.7	210.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	8.9	3.1	-3.1	-27.9	361.4	-109.7		-220.2	0.1	0.4	24.8	-49.8	-2.7		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-8.6	-4.4	3.0	23.8	-357.9	193.7		-210.7	0.9	-0.2	-20.6	-36.5	94.7		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	8.6	4.4	-3.0	-23.8	357.9	-193.7		-200.7	-0.9	0.2	-20.6	-40.8	-78.0		240.9	6.3	-2.4	1.6	39.2	-438.7		869.6	-2.9	0.0	3.8	-13.3	1143.6
Asta PROGR. 0.	-8.6	-4.4	3.0	23.8	-413.5	111.2	75.	210.7	-0.9	0.2	-20.6	-41.0	78.0	19.	304.2	-8.0	-2.5	5.1	126.6	872.7	252.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	8.9	3.1	-3.1	-27.9	420.7	-112.2		-220.2	0.1	0.4	24.8	56.5	0.1		240.9	6.3	-2.4	1.6	39.2	-438.7		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-8.6	-4.4	3.0	23.8	-413.5	111.2		-210.7	0.9	-0.2	-20.6	-41.0	78.0		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	8.6	4.4	-3.0	-23.8	413.5	-111.2		-200.7	-0.9	0.2	-20.6	-41.0	78.0		240.9	6.3	-2.4	1.6	39.2	-438.7		869.6	-2.9	0.0	3.8	-13.3	1143.6
19.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	94.	210.7	-0.9	0.2	-20.6	-45.5	-41.2	38.	304.2	-8.0	-2.5	5.1	126.6	872.7	336.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	63.3	-2.6		240.9	6.3	-2.4	1.6	39.2	-438.7		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-45.5	-41.2		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-45.5	-41.2		240.9	6.3	-2.4	1.6	39.2	-438.7		869.6	-2.9	0.0	3.8	-13.3	1143.6
38.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	113.	210.7	-0.9	0.2	-20.6	-50.0	-44.4	56.	304.2	-8.0	-2.5	5.1	126.6	872.7	19.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	24.8	70.0	-5.2		240.9	6.3	-2.4	1.6	85.1	-701.1		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-50.0	-44.4		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-50.0	-44.4		240.9	6.3	-2.4	1.6	136.6	-727.8		869.6	-2.9	0.0	3.8	-13.3	1143.6
56.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	131.	210.7	-0.9	0.2	-20.6	-54.5	-27.7	75.	304.2	-8.0	-2.5	5.1	126.6	872.7	94.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	24.8	76.7	-7.9		240.9	6.3	-2.4	1.6	175.4	-463.6		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-76.7	7.9		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-76.7	7.9		240.9	6.3	-2.4	1.6	175.4	-463.6		869.6	-2.9	0.0	3.8	-13.3	1143.6
75.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	150.	210.7	-0.9	0.2	-20.6	-59.0	-10.9	Asta PROGR. 0.	304.2	-8.0	-2.5	5.1	126.6	872.7	38.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	24.8	83.5	-10.5		240.9	6.3	-2.4	1.6	221.1	-437.4		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-83.5	-10.5		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-83.5	-10.5		240.9	6.3	-2.4	1.6	220.6	-434.9		869.6	-2.9	0.0	3.8	-13.3	1143.6
94.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	19.	210.7	-0.9	0.2	-20.6	-63.3	-2.6	113.	304.2	-8.0	-2.5	5.1	126.6	872.7	56.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	63.3	-2.6		240.9	6.3	-2.4	1.6	265.8	-226.1		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-63.3	-2.6		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-63.3	-2.6		240.9	6.3	-2.4	1.6	265.8	-226.1		869.6	-2.9	0.0	3.8	-13.3	1143.6
113.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	38.	210.7	-0.9	0.2	-20.6	-67.7	-11.8	131.	304.2	-8.0	-2.5	5.1	126.6	872.7	150.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	24.8	89.2	-12.0		240.9	6.3	-2.4	1.6	317.4	-270.0		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-89.2	-12.0		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-89.2	-12.0		240.9	6.3	-2.4	1.6	311.0	-107.3		869.6	-2.9	0.0	3.8	-13.3	1143.6
131.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	56.	210.7	-0.9	0.2	-20.6	-71.7	-14.1	75.	304.2	-8.0	-2.5	5.1	126.6	872.7	94.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	24.8	89.2	-12.0		240.9	6.3	-2.4	1.6	311.0	-107.3		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-71.7	-14.1		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-71.7	-14.1		240.9	6.3	-2.4	1.6	311.0	-107.3		869.6	-2.9	0.0	3.8	-13.3	1143.6
150.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	94.	210.7	-0.9	0.2	-20.6	-75.7	-16.5	Asta PROGR. 0.	304.2	-8.0	-2.5	5.1	126.6	872.7	38.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	24.8	109.4	-4.4		240.9	6.3	-2.4	1.6	352.8	-13.2		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-109.4	-4.4		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-109.4	-4.4		240.9	6.3	-2.4	1.6	352.8	-13.2		869.6	-2.9	0.0	3.8	-13.3	1143.6
Asta PROGR. 0.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	19.	210.7	-0.9	0.2	-20.6	-79.7	-19.5	113.	304.2	-8.0	-2.5	5.1	126.6	872.7	56.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	24.8	127.0	-6.7		240.9	6.3	-2.4	1.6	401.1	-69.1		812.5	-4.0	0.0	-1.4	5.1	-1125.7
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-210.7	0.9	-0.2	-20.6	-127.0	-6.7		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-812.5	4.0	0.0	1.4	-5.1	1125.7
	3.0	-6.8	1.8	2.2	9.3	893.0		-200.7	-0.9	0.2	-20.6	-127.0	-6.7		240.9	6.3	-2.4	1.6	401.1	-69.1		869.6	-2.9	0.0	3.8	-13.3	1143.6
42.	-3.0	-6.8	1.8	-2.2	-9.3	-893.0	38.	210.7	-0.9	0.2	-20.6	-83.7	-21.3	131.	304.2	-8.0	-2.5	5.1	126.6	872.7	150.	-869.6	2.9	0.0	-3.8	13.3	-1143.6
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	0.4	24.8	144.4	-14.4		240.9	6.3	-2.4	1.6	442.7	-15.4		812.5	-4.0	0.			

43.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	98.	53.2	-83.0	16.5	82.3	-1604.7	-6861.7	-7.1	-107.0	19.8	98.9	-6410.0	-2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	98.	53.2	-83.0	16.5	82.3	-1604.7	-6861.7	-7.1	-107.0	19.8	98.9	-6410.0	-2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	98.	53.2	-83.0	16.5	82.3	-1604.7	-6861.7	-7.1	-107.0	19.8	98.9	-6410.0	-2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
85.	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
128.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	130.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	130.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	130.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
170.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	146.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	146.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	146.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
213.	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	16.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	16.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	16.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
255.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	33.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	33.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	33.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
298.	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	65.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	65.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	65.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
340.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	81.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	81.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	81.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
382.	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	98.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	98.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	98.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
424.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	114.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
466.	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	130.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	130.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	130.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
508.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	146.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	146.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	146.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
550.	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	16.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	16.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	16.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
592.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	33.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	33.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	33.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
634.	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	65.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	65.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	454.9	-199.8	-4.6	-8.6	579.1	-1124.8	65.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
676.	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	81.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	81.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	-2097.9	81.	53.2	-83.0	-16.5	-82.3	1604.7	8861.7	-7.1	-107.0	-19.8	-98.9	6410.0	2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
718.	454.9	-199.8	-4.6	-8.6	579.1	-1124.8																				

61.	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	177.2	-52.2	126.0	-1638.5	-10821.0	-30.5	-151.7	2.3	15.4	-35.7	-1943.0	-6.3	6.7	-9.1	-5.6	-142.4	-218.7	259.3	0.0	0.0	0.0	0.0	0.0	
	180.6	-208.4	-29.9	149.4	-1456.7	9367.7	-30.5	151.4	4.4	-29.0	101.3	-16775.9	-10.6	6.4	-11.4	-5.8	355.0	-101.8	-259.3	0.0	0.0	0.0	0.0	
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
98.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	127.5	14314.9	-10.6	-6.7	-9.1	5.6	-437.7	-0.1	-259.3	0.0	0.0	0.0	0.0	0.0
114.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	111.5	-14498.9	-10.6	-6.4	-11.4	-5.8	-355.0	101.8	259.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	149.4	11899.3	-10.6	-6.4	-11.4	-5.8	-541.1	-2.4	-311.3	0.0	0.0	0.0	0.0	0.0
130.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	149.4	-11999.3	-10.6	-6.4	-11.4	-5.8	-413.5	-23.8	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
144.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	149.4	-11999.3	-10.6	-6.4	-11.4	-5.8	-413.5	-23.8	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
16.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
33.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
49.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
65.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
81.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
107.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
124.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
149.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151.4	-4.4	-29.0	31.0	-9392.8	-10.6	-6.7	-9.1	5.6	-420.7	-27.9	259.3	0.0	0.0	0.0	0.0	0.0
16.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.7	2.3	15.4	-75.6	-16934.4	-6.3	6.7	-9.1	-5.8	290.1	-109.3	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	149.4	-1456.7	-9367.7	-30.5	-151.7	-2.3	-15.4	187.3	-9441.7	-10.6	-6.7	-9.1	5.6	-273.0	-41.7	311.3	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	-10821.0	-30.5	-151.4	4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0	
	142.7	-177.2	-25.2	126.0	819.2	-5061.1	-30.5	-151																

[illegible]

2.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	41.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
3.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	83.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
4.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	124.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
5.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	165.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
6.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	206.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
7.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	248.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
8.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	289.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
9.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	330.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
10.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	371.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
11.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	412.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
12.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	453.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
13.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	494.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
14.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	535.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
15.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	576.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
16.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	617.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
17.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	658.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
18.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	699.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
19.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	740.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
20.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	781.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
21.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	822.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
22.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	863.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
23.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	904.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6
24.	176.6	25.6	-76.3	0.0	-286.0	-96.0	-48.5	-32.8	944.7	0.0	0.0	0.0	15.3	-97.3	-30.5	0.0	-76.2	243.3	945.	-701.2	313.7	-31.7	0.0	4373.3	-5711.3
																									176.6

[illegible]

126.	-283.6	195.9	-6.7	-3.1	-1449.6	-1244.5
	-297.0	-203.6	7.2	-2.6	1353.3	1002.9
	-297.0	203.6	-7.2	2.6	1353.3	1002.9
	283.6	-195.9	6.7	3.1	1449.6	1244.5
168.	-283.6	195.9	-6.7	-3.1	-1449.6	-1244.5
	-297.0	-203.6	7.2	-2.6	1353.3	1002.9
	-297.0	203.6	-7.2	2.6	1353.3	1002.9
	283.6	-195.9	6.7	3.1	1449.6	1244.5
209.	-283.6	195.9	-6.7	-3.1	-884.6	-15163.9
	-297.0	-203.6	7.2	-2.6	884.6	15163.9
	-297.0	203.6	-7.2	2.6	884.6	15163.9
	283.6	-195.9	6.7	3.1	884.6	15163.9
251.	-283.6	195.9	-6.7	-3.1	-602.1	-23368.1
	-297.0	-203.6	7.2	-2.6	602.1	23368.1
	-297.0	203.6	-7.2	2.6	602.1	23368.1
	283.6	-195.9	6.7	3.1	602.1	23368.1
293.	-283.6	195.9	-6.7	-3.1	-315.3	-315.3
	-297.0	-203.6	7.2	-2.6	315.3	315.3
	-297.0	203.6	-7.2	2.6	315.3	315.3
	283.6	-195.9	6.7	3.1	315.3	315.3
335.	-283.6	195.9	-6.7	-3.1	-37.0	39776.6
	-297.0	-203.6	7.2	-2.6	37.0	-39776.6
	-297.0	203.6	-7.2	2.6	37.0	-39776.6
	283.6	-195.9	6.7	3.1	37.0	-39776.6
Asta	154	noth	760	963	37.0	
PROG.	NOB	TYT	TZZ	TORS	MYV	MZZ
0.	-40.8	0.0	0.0	0.0	0.7	0.0
	73.2	0.0	0.0	0.0	-1.0	0.0
	-73.2	0.0	0.0	0.0	1.0	0.0
	-40.8	0.0	0.0	0.0	-0.7	0.0
34.	-40.8	0.0	0.0	0.0	0.5	0.0
	73.2	0.0	0.0	0.0	-0.7	0.0
	-73.2	0.0	0.0	0.0	0.7	0.0
	-40.8	0.0	0.0	0.0	-0.5	0.0
67.	-40.8	0.0	0.0	0.0	0.2	0.0
	73.2	0.0	0.0	0.0	-0.4	0.0
	-73.2	0.0	0.0	0.0	0.4	0.0
	-40.8	0.0	0.0	0.0	-0.2	0.0
101.	-40.8	0.0	0.0	0.0	-0.1	0.0
	73.2	0.0	0.0	0.0	0.1	0.0
	-73.2	0.0	0.0	0.0	0.1	0.0
	-40.8	0.0	0.0	0.0	0.0	0.0
135.	-40.8	0.0	0.0	0.0	-0.2	0.0
	73.2	0.0	0.0	0.0	0.2	0.0
	-73.2	0.0	0.0	0.0	-0.2	0.0
	-40.8	0.0	0.0	0.0	0.2	0.0
168.	-40.8	0.0	0.0	0.0	-0.4	0.0
	73.2	0.0	0.0	0.0	0.5	0.0
	-73.2	0.0	0.0	0.0	-0.5	0.0
	-40.8	0.0	0.0	0.0	0.4	0.0
202.	-40.8	0.0	0.0	0.0	-0.6	0.0
	73.2	0.0	0.0	0.0	0.8	0.0
	-73.2	0.0	0.0	0.0	-0.8	0.0
	-40.8	0.0	0.0	0.0	0.6	0.0
236.	-40.8	0.0	0.0	0.0	-0.8	0.0
	73.2	0.0	0.0	0.0	1.0	0.0
	-73.2	0.0	0.0	0.0	-1.1	0.0
	-40.8	0.0	0.0	0.0	0.8	0.0
269.	-40.8	0.0	0.0	0.0	-1.0	0.0
	73.2	0.0	0.0	0.0	1.4	0.0
	-73.2	0.0	0.0	0.0	-1.4	0.0
	-40.8	0.0	0.0	0.0	1.0	0.0
Asta	154	noth	973	1093	37.0	
PROG.	NOB	TYT	TZZ	TORS	MYV	MZZ
0.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
29.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
58.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
86.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
115.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
144.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
173.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
201.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
230.	-3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
	-3.9	0.0	0.0	0.0	0.0	0.0
Asta	156	noth	972	111	37.0	
PROG.	NOB	TYT	TZZ	TORS	MYV	MZZ
0.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
29.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
58.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
86.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
115.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
144.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
173.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
201.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
280.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
380.	-105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0

0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2	359	46.7	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-106.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
4.0	4.0	51.9	0.0	100.0	-7.4		13.9	21.9	0.0	0.0	1.2	630.2		106.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-13.9	-21.9	0.0	0.0	-1.2	-630.2	410.	-46.7	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		106.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-106.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		106.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-106.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		106.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-106.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		106.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-106.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7																		

[illegible]

58/136

0.7	9.4	1.5	-70.4	137.6	2214.3
-13.2	28.2	-0.1	115.2	-13.5	2393.2
-13.2	-27.5	-1.1	-98.4	137.5	2393.2
-1.3	-56.7	-0.5	92.2	-45.1	2148.7
-0.7	-51.4	1.5	-98.4	151.2	2746.9
-13.2	-27.7	-0.1	115.2	-13.5	2393.2
-1.3	-116.3	1.1	-98.3	99.5	1908.3
-13.2	-91.5	0.5	-98.4	137.5	2393.2
-13.2	-132.2	1.1	-98.3	124.8	2014.9
-13.7	-91.5	-0.1	115.2	-13.5	2393.2
-13.7	-149.1	-0.1	115.2	-13.5	2393.2
-1.3	-178.4	0.5	92.2	-45.0	1737.2
-13.2	-177.1	1.5	-98.4	151.2	2746.9
-13.2	-154.0	-0.1	115.2	-13.5	2393.2
-13.2	-159.0	0.1	115.2	-13.5	2393.2
-1.3	-239.2	0.5	92.2	-46.4	13719.2
-0.7	-213.9	1.5	-70.4	137.5	2393.2
-13.2	-200.2	-0.1	115.2	-13.5	2393.2
-13.7	-218.4	-0.1	115.2	-13.5	2393.2
-13.7	-279.6	-0.1	115.2	-13.5	2393.2
-1.3	-360.9	-0.5	92.2	-45.1	6217.5
-13.2	-360.9	1.5	-70.4	137.5	2393.2
-13.2	-360.9	-0.1	115.2	-13.5	2393.2
-13.2	-440.5	1.1	-98.4	151.2	2746.9
-1.3	-421.7	0.5	92.2	12.2	-363.2
-13.2	-421.7	1.5	-98.4	151.2	2746.9
-13.2	-397.7	-0.1	115.2	-13.5	2393.2
145	node	760	760	MY	MZ
-377.1	-40.0	19.2	0.0	96.2	199.9
-377.1	-33.9	6.3	0.0	29.6	48.6
-377.1	-33.9	6.3	0.0	31.5	169.7
-377.1	-42.9	-18.7	0.0	-93.7	-74.4
-377.1	-40.0	19.2	0.0	96.2	199.9
-377.0	36.9	-5.8	0.0	-25.4	-161.5
-377.0	36.9	-5.8	0.0	27.2	148.3
-377.0	42.9	-18.7	0.0	-82.0	-187.9
-376.9	36.9	6.3	0.0	29.6	48.6
-376.9	36.9	6.3	0.0	31.5	169.7
-376.9	36.9	6.3	0.0	23.6	127.3
-376.9	42.9	-18.7	0.0	-93.7	-181.5
-376.7	-40.0	19.2	0.0	60.1	124.9
-376.7	-40.0	19.2	0.0	60.1	124.9
-376.7	-33.9	6.3	0.0	29.6	48.6
-376.7	-33.9	6.3	0.0	31.5	169.7
-376.7	42.9	-18.7	0.0	-58.6	-146.2
-376.6	36.9	-5.8	0.0	-48.6	-9.9
-376.6	36.9	-5.8	0.0	-45.5	-92.3
-376.6	42.9	-18.7	0.0	-36.4	-135.5
-376.6	42.9	-18.7	0.0	-46.9	-107.4
-376.4	36.9	6.3	0.0	29.6	48.6
-376.4	36.9	6.3	0.0	31.5	169.7
-376.4	36.9	6.3	0.0	23.6	127.3
-376.4	42.9	-18.7	0.0	-93.7	-181.5
-376.3	-40.0	19.2	0.0	24.0	50.0
-376.3	-40.0	19.2	0.0	24.0	50.0
-376.3	-33.9	6.3	0.0	29.6	48.6
-376.3	-33.9	6.3	0.0	31.5	169.7
-376.3	42.9	-18.7	0.0	12.0	42.4
-376.2	-40.0	19.2	0.0	24.0	50.0
-376.2	36.9	-5.8	0.0	-3.6	-23.1
-376.2	36.9	-5.8	0.0	-3.7	-26.8
-376.2	42.9	-18.7	0.0	0.0	0.0
-376.0	36.9	6.3	0.0	0.0	0.0
-376.0	36.9	6.3	0.0	0.0	0.0
145	node	760	213	MY	MZ
125.2	-376.0	0.0	0.0	-0.4	0.8
125.2	-376.0	0.0	0.0	0.5	0.8
-99.1	-376.0	0.0	0.0	-0.2	0.8
146.1	-376.0	0.0	0.0	0.5	0.8
125.2	-376.0	0.0	0.0	-0.4	-948.7
125.2	-376.0	0.0	0.0	0.5	-948.7
-99.1	-376.0	0.0	0.0	-0.2	-948.7
146.1	-376.0	0.0	0.0	0.5	-948.7
125.2	-188.0	0.0	0.0	-0.3	-1621.6
125.2	-188.0	0.0	0.0	0.4	-1621.6
-99.1	-188.0	0.0	0.0	-0.1	-1621.6
146.1	-188.0	0.0	0.0	0.4	-1621.6
125.2	-94.0	0.0	0.0	-0.2	-2069.7
125.2	-94.0	0.0	0.0	0.3	-2069.7
-99.1	-94.0	0.0	0.0	-0.1	-2069.7
146.1	-94.0	0.0	0.0	0.3	-2069.7
125.2	-376.0	0.0	0.0	-0.4	-2162.1
125.2	-376.0	0.0	0.0	0.5	-2162.1
-99.1	-376.0	0.0	0.0	-0.2	-2162.1
146.1	-376.0	0.0	0.0	0.5	-2162.1
125.2	-94.0	0.0	0.0	-0.1	-2069.9
125.2	-94.0	0.0	0.0	0.2	-2069.9
-99.1	-94.0	0.0	0.0	-0.1	-2069.9
146.1	-94.0	0.0	0.0	0.2	-2069.9
125.2	-188.0	0.0	0.0	-0.1	-1621.6
125.2	-188.0	0.0	0.0	0.2	-1621.6
-99.1	-188.0	0.0	0.0	-0.0	-1621.6
146.1	-188.0	0.0	0.0	0.1	-1621.6
125.2	-376.0	0.0	0.0	-0.4	-949.3
125.2	-376.0	0.0	0.0	0.5	-949.3
-99.1	-376.0	0.0	0.0	-0.1	-949.3
146.1	-376.0	0.0	0.0	0.0	-949.3
125.2	-376.0	0.0	0.0	0.0	0.0
125.2	-376.0	0.0	0.0	0.0	0.0
-99.1	-376.0	0.0	0.0	0.0	0.0
146	node	773	754	MY	MZ
-1768.5	88.6	-66.9	317.6	17700.4	-8530.4
-613.3	56.4	-27.2	155.2	4670.6	-8767.5
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-413.5	62.1	-22.6	131.5	22578.3	-8762.2
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-612.9	56.4	-27.2	155.2	4687.6	-8767.5
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-413.1	62.1	-22.6	131.5	22774.4	-8728.4
-1767.7	88.6	-66.9	317.6	17784.1	-8416.6
-612.5	56.4	-27.2	155.2	4687.6	-8767.5
-1587.9	88.6	-66.9	317.6	17784.1	-8416.6
-1767.3	88.6	-66.9	317.6	17825.9	-8364.7
-612.5	56.4	-27.2	155.2	4721.1	-8767.5
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-412.4	62.1	-22.6	131.5	2300.7	-8650.7
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-611.8	56.4	-27.2	155.2	4738.5	-8722.4
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-412.0	62.1	-22.6	131.5	2314.8	-8611.9
-1766.5	88.6	-66.9	317.6	17909.5	-8253.5
-611.4	56.4	-27.2	155.2	4738.5	-8722.4
-1586.8	88.6	-66.9	317.6	17948.0	-8039.5
-1766.8	88.6	-66.9	317.6	17948.0	-8039.5
-1766.2	88.6	-66.9	317.6	17961.3	-8128.1
-1586.8	88.6	-66.9	317.6	17961.3	-8128.1
-1586.4	94.3	-62.2	239.9	15522.0	-8790.2
-411.2	62.1	-22.6	131.5	2343.1	-8534.3
-1586.4	94.3	-62.2	239.9	15522.0	-8790.2

		-610.6	56.4	-27.2	155.2	4789.5	-7721.6
		-1566.0	64.3	-62.4	239.9	13560.9	-8921.6
		-410.8	62.4	-31.5	76.6	2301.5	-8495.5
		-1765.4	88.6	-66.9	137.6	1803.0	-8087.4
		-610.2	56.4	-27.2	155.2	4789.5	-7721.6
		-1566.0	64.3	-62.4	239.9	13560.9	-8921.6
		-410.5	62.1	-32.6	131.5	2371.4	-8456.7
ASTR.	147						
PGC	NORM	TY	TZ	TORS	MY	MZ	
	-398.4	7.5	-5.5	11.0	-3343.0	-7675.3	
	-742.5	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-336.0	7.5	-5.5	11.0	-3343.0	-7675.3	
	-779.2	4.2	-15.1	7.6	-4132.4	-7907.6	
	-327.7	7.5	-5.5	11.0	-3343.0	-7675.3	
	-716.8	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-310.3	11.9	-7.2	-3.4	-5234.3	-7953.1	
	-753.3	4.2	-15.1	7.6	-4132.4	-7907.6	
	-347.1	7.5	-5.5	11.0	-3343.0	-7675.3	
	-691.1	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-284.6	11.9	-7.2	-3.4	-5234.3	-7953.1	
	-321.4	7.5	-5.5	11.0	-3343.0	-7675.3	
	-465.5	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-259.0	11.9	-7.2	-3.4	-5234.3	-7953.1	
	-702.2	4.2	-15.1	7.6	-4132.4	-7907.6	
	-75.7	7.5	-5.5	11.0	-3343.0	-7675.3	
	-639.8	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-233.3	11.9	-7.2	-3.4	-5234.3	-7953.1	
	-495.2	4.2	-15.1	7.6	-4132.4	-7907.6	
	-270.0	7.5	-5.5	11.0	-3343.0	-7675.3	
	-614.1	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-207.6	11.9	-7.2	-3.4	-5234.3	-7953.1	
	-650.8	4.2	-15.1	7.6	-4132.4	-7907.6	
	-244.4	7.5	-5.5	11.0	-3343.0	-7675.3	
	-588.4	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-382.0	11.9	-7.2	-3.4	-5234.3	-7953.1	
	-615.2	4.2	-15.1	7.6	-4132.4	-7907.6	
	-218.7	7.5	-5.5	11.0	-3343.0	-7675.3	
	-562.8	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-456.3	11.9	-7.2	-3.4	-5234.3	-7953.1	
	-509.5	4.2	-15.1	7.6	-4132.4	-7907.6	
	-193.0	7.5	-5.5	11.0	-3343.0	-7675.3	
	-557.1	8.6	-13.8	-6.8	-4440.6	-8893.6	
	-130.6	11.9	-7.2	-3.4	-5234.3	-7953.1	
ASTR.	148						
PGC	NORM	TY	TZ	TORS	MY	MZ	
	-5302.8	11.1	-10.6	304.1	1530.2	3227.9	
	-1575.0	0.0	30.3	161.0	-8013.2	3241.9	
	-1106.3	-3.3	-4.7	283.8	1684.6	3078.7	
	-1658.5	-3.3	-4.7	283.8	-1068.0	4768.0	
	-1022.4	11.1	-10.6	304.1	1536.8	3154.4	
	-1574.6	0.0	30.3	161.0	-8013.2	3241.9	
	-1105.9	-3.3	-4.7	283.8	1687.5	3076.6	
	-1658.1	-14.4	36.2	140.8	-1057.5	4777.0	
	-1022.0	0.0	30.3	161.0	-8013.2	3241.9	
	-1574.2	0.0	30.3	161.0	-8013.2	3241.9	
	-1105.5	-3.3	-4.7	283.8	1687.5	3076.6	
	-1657.8	-14.4	36.2	140.8	-1059.1	4768.0	
	-1021.6	0.0	30.3	161.0	-8013.2	3241.9	

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292.	97.9	-331.4	0.3	-1.9	-89.5	-10765.4	1.	486.1	38.7	-2.3	45.0	-262.7	-16055.1	0.	-284.9	-108.4	-3.2	-37.5	554.6	-79.2	94.	-13.9	103.6	4.0	-43.8	-453.9	-709.3
	16.9	-437.3	0.4	-1.8	-161.8	-23945.6	1.	411.7	34.7	1.1	6.0	315.5	-16658.0	0.	25	75	-3.8	473			94.	6.7	103.6	-2.5	-46.4	156.2	-1460.3
	29.4	-409.4	0.4	-1.7	-160.4	-23945.6	1.	411.7	34.7	1.1	6.0	315.5	-16658.0	0.	25	75	-3.8	473			94.	6.7	103.6	-2.5	-46.4	156.2	-1460.3
	64.1	-457.9	0.4	-1.7	-161.3	-23941.7	1.	411.7	34.7	1.1	6.0	315.5	-16658.0	0.	25	75	-3.8	473			94.	6.7	103.6	-2.5	-46.4	156.2	-1460.3
	30.5	-449.9	0.3	-1.9	-103.9	-27059.0	1.	535.6	157.2	-2.3	45.0	-367.8	-12936.6	0.	-1087.5	400.4	0.3	0.0	0.0	0.0	113.	-13.9	42.0	-3.2	-48.8	-529.7	658.8
334.	-50.6	-570.6	0.4	-1.8	-140.2	-3082.5	1.	347.2	289.3	-2.3	45.0	-1017.3	-5082.5	0.	0.	0.0	0.0	0.0	0.0	0.0	113.	6.7	103.6	-2.5	-46.4	156.2	-1460.3
	-84.2	-568.0	0.3	-1.7	-118.8	-48279.2	1.	443.5	157.5	-2.2	45.4	-132.1	-11305.4	0.	0.	0.0	0.0	0.0	0.0	0.0	113.	-11.5	42.0	3.3	-46.1	-453.2	670.6
	-1.3	-3.3	0.4	-1.0	-45.4	-1053.5	1.	41.0	45.4	-1.3	45.0	-1018.0	-453.5	0.	0.	0.0	0.0	0.0	0.0	0.0	131.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	-37.0	-568.0	0.3	-1.9	-118.8	-48294.2	1.	41.0	45.4	-1.3	45.0	-1018.0	-453.5	0.	0.	0.0	0.0	0.0	0.0	0.0	131.	-13.9	42.0	3.3	-46.1	-453.2	670.6
ASTA																											
PROGR.																											
	475.3	364.8	0.5	-15.8	-23.6	-16262.4	1.	515.0	272.1	-2.2	45.4	-60.4	-7299.7	0.	375.4	276.1	0.3	0.0	-11.5	1438.9	0.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	136.5	364.4	0.5	-15.8	-23.6	-16262.4	1.	515.0	272.1	-2.2	45.4	-60.4	-7299.7	0.	375.4	276.1	0.3	0.0	-11.5	1438.9	0.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	508.6	363.8	0.5	-13.6	-23.2	-16096.7	1.	515.0	272.1	-2.2	45.4	-60.4	-7299.7	0.	375.4	276.1	0.3	0.0	-11.5	1438.9	0.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	101.2	363.4	0.5	-13.6	-23.2	-16096.7	1.	515.0	272.1	-2.2	45.4	-60.4	-7299.7	0.	375.4	276.1	0.3	0.0	-11.5	1438.9	0.	-13.9	42.0	3.3	-46.1	-453.2	670.6
42.	405.9	246.2	0.5	-13.8	-44.8	-3406.1	1.	612.1	312.2	-2.3	45.4	-116.3	-3002.8	0.	444.2	312.2	0.3	0.0	-11.5	1438.9	0.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	-206.0	245.9	0.2	-26.1	-55.6	-3462.0	1.	612.1	312.2	-2.3	45.4	-116.3	-3002.8	0.	444.2	312.2	0.3	0.0	-11.5	1438.9	0.	-13.9	42.0	3.3	-46.1	-453.2	670.6
	172.7	244.9	0.3	-26.1	-55.6	-3462.0	1.	612.1	312.2	-2.3	45.4	-116.3	-3002.8	0.	444.2	312.2											

Asta	PROGR.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	12.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.	26.	27.	28.	29.	30.	31.	32.	33.	34.	35.	36.	37.	38.	39.	40.	41.	42.	43.	44.	45.	46.	47.	48.	49.	50.	51.	52.	53.	54.	55.	56.	57.	58.	59.	60.	61.	62.	63.	64.	65.	66.	67.	68.	69.	70.	71.	72.	73.	74.	75.	76.	77.	78.	79.	80.	81.	82.	83.	84.	85.	86.	87.	88.	89.	90.	91.	92.	93.	94.	95.	96.	97.	98.	99.	100.	101.	102.	103.	104.	105.	106.	107.	108.	109.	110.	111.	112.	113.	114.	115.	116.	117.	118.	119.	120.	121.	122.	123.	124.	125.	126.	127.	128.	129.	130.	131.	132.	133.	134.	135.	136.	137.	138.	139.	140.	141.	142.	143.	144.	145.	146.	147.	148.	149.	150.	151.	152.	153.	154.	155.	156.	157.	158.	159.	160.	161.	162.	163.	164.	165.	166.	167.	168.	169.	170.	171.	172.	173.	174.	175.	176.	177.	178.	179.	180.	181.	182.	183.	184.	185.	186.	187.	188.	189.	190.	191.	192.	193.	194.	195.	196.	197.	198.	199.	200.	201.	202.	203.	204.	205.	206.	207.	208.	209.	210.	211.	212.	213.	214.	215.	216.	217.	218.	219.	220.	221.	222.	223.	224.	225.	226.	227.	228.	229.	230.
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25.	122.8	0.0	0.0	0.0	0.0	4.	-869.9	3.5	-4148.2	0.0	-5185.2	-4.4	0.	-6083.5	20.1	14.9	0.0	3316.4	13564.5	3.	-595.5	-272.0	290.5	0.0	469.6	510.0
50.	122.8	0.0	0.0	0.0	0.0	4.	-869.7	3.5	-4148.2	0.0	-2592.6	-2.2	41.	-6082.2	20.1	14.9	0.0	2700.3	14391.8	4.	-595.3	-272.0	290.5	0.0	313.1	340.0
74.	122.8	0.0	0.0	0.0	0.0	5.	-869.6	3.5	-4148.2	0.0	-6032.9	0.0	85.	-6032.9	20.1	14.9	0.0	2064.2	15202.0	5.	-595.2	-272.0	290.5	0.0	156.5	170.0
99.	122.8	0.0	0.0	0.0	0.0	Asta	99	ndi	964	339	MY	MZZ	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	5.	-595.1	-272.0	290.5	0.0	0.0	0.0
124.	122.8	0.0	0.0	0.0	0.0	PROGR.	124	ndi	964	339	MY	MZZ	165.	-5982.3	20.1	14.9	0.0	852.1	16871.8	Asta	130	ndi	752	468	MY	MZZ
149.	122.8	0.0	0.0	0.0	0.0	0.	-1923.2	16.2	45.7	0.0	-1923.2	-81.0	206.	-5957.0	20.1	14.9	0.0	2700.1	15202.0	PROGR.	130	ndi	752	468	MY	MZZ
174.	122.8	0.0	0.0	0.0	0.0	1.	-1923.1	16.2	45.7	0.0	200.1	-70.9	248.	-5931.7	20.1	14.9	0.0	-380.1	18528.4	0.	-714.5	-595.1	-0.3	0.0	0.0	
198.	122.8	0.0	0.0	0.0	0.0	2.	-1923.0	16.2	45.7	0.0	171.5	-60.7	289.	-5906.4	20.1	14.9	0.0	-586.0	19131.3	1.	-714.5	-595.1	-0.3	0.0	0.0	
Asta	75	ndi	760	212	MY	2.	-1922.8	16.2	45.7	0.0	140.9	-50.6	330.	-5881.2	20.1	14.9	0.0	-1612.2	20183.1	2.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	75	ndi	760	212	MY	3.	-1922.7	16.2	45.7	0.0	118.4	-40.5	Asta	116	ndi	741	737	86.	-714.5	1.8	-0.3	0.0	28.5	-25586.4		
33.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.6	16.2	45.7	0.0	85.7	-30.4	PROGR.	116	ndi	741	737	116.	-714.5	1.8	-0.3	0.0	28.5	-25586.4		
39.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.4	16.2	45.7	0.0	57.2	-20.2	0.	-3793.3	-15.6	11.9	0.0	-2215.2	17264.7	0.	-714.5	-595.1	-0.3	0.0	0.0	
66.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.3	16.2	45.7	0.0	27.6	-10.1	4.	-3793.3	-15.6	11.9	0.0	-2215.2	17264.7	1.	-714.5	-595.1	-0.3	0.0	0.0	
99.	-13.8	0.0	0.0	0.0	0.0	5.	-1922.1	16.2	45.7	0.0	0.0	0.0	83.	-3242.7	-15.6	11.9	0.0	-3193.0	19869.8	104.	-714.5	-595.1	-0.3	0.0	0.0	
131.	-13.8	0.0	0.0	0.0	0.0	Asta	100	ndi	760	212	MY	MZZ	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	174.	-714.5	-595.1	-0.3	0.0	0.0	
165.	-13.8	0.0	0.0	0.0	0.0	PROGR.	100	ndi	760	212	MY	MZZ	165.	-5982.3	20.1	14.9	0.0	852.1	16871.8	201.	-714.5	-595.1	-0.3	0.0	0.0	
198.	-13.8	0.0	0.0	0.0	0.0	0.	-2707.3	-29.4	-3.3	0.0	-16.4	146.8	PROGR.	116	ndi	741	737	206.	-3166.8	230.	-714.5	-595.1	-0.3	0.0	0.0	
264.	-13.8	0.0	0.0	0.0	0.0	1.	-2707.2	-29.4	-3.3	0.0	-14.4	128.5	0.	-3793.3	-15.6	11.9	0.0	-2215.2	17264.7	PROGR.	130	ndi	752	468	MY	MZZ
Asta	78	ndi	776	211	MY	1.	-2707.0	-29.4	-3.3	0.0	-12.3	110.1	289.	-3116.3	-15.6	11.9	0.0	-5637.5	12712.1	201.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	78	ndi	776	211	MY	2.	-2706.9	-29.4	-3.3	0.0	-10.3	91.8	330.	-5881.2	20.1	14.9	0.0	-1612.2	20183.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
33.	-13.8	0.0	0.0	0.0	0.0	3.	-2706.7	-29.4	-3.3	0.0	-8.2	73.4	Asta	117	ndi	742	739	330.	-5881.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
66.	-13.8	0.0	0.0	0.0	0.0	4.	-2706.6	-29.4	-3.3	0.0	-6.2	55.1	PROGR.	117	ndi	742	739	330.	-5881.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
99.	-13.8	0.0	0.0	0.0	0.0	4.	-2706.5	-29.4	-3.3	0.0	-4.1	36.7	0.	-3516.2	-45.9	11.4	0.0	-1612.2	20183.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
131.	-13.8	0.0	0.0	0.0	0.0	4.	-2706.3	-29.4	-3.3	0.0	-2.1	18.4	Asta	117	ndi	742	739	330.	-5881.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
165.	-13.8	0.0	0.0	0.0	0.0	5.	-2706.2	-29.4	-3.3	0.0	0.0	0.0	PROGR.	117	ndi	742	739	330.	-5881.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
198.	-13.8	0.0	0.0	0.0	0.0	Asta	101	ndi	962	341	MY	MZZ	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	230.	-714.5	-595.1	-0.3	0.0	0.0	
231.	-13.8	0.0	0.0	0.0	0.0	0.	-2617.0	-12.4	-3.2	0.0	-15.9	61.9	PROGR.	101	ndi	962	341	206.	-3389.8	230.	-714.5	-595.1	-0.3	0.0	0.0	
264.	-13.8	0.0	0.0	0.0	0.0	1.	-2616.8	-12.4	-3.2	0.0	-13.9	54.2	0.	-3516.2	-45.9	11.4	0.0	-1612.2	20183.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
Asta	79	ndi	749	468	MY	2.	-2616.6	-12.4	-3.2	0.0	-9.9	38.7	Asta	101	ndi	962	341	248.	-3364.5	230.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	79	ndi	749	468	MY	2.	-2616.6	-12.4	-3.2	0.0	-9.9	38.7	PROGR.	101	ndi	962	341	289.	-3189.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
33.	-50.7	0.0	0.0	0.0	0.0	3.	-2616.4	-12.4	-3.2	0.0	-6.0	23.2	0.	-3516.2	-45.9	11.4	0.0	-1612.2	20183.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
66.	-50.7	0.0	0.0	0.0	0.0	4.	-2616.3	-12.4	-3.2	0.0	-4.0	15.5	PROGR.	101	ndi	962	341	330.	-5881.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
99.	-50.7	0.0	0.0	0.0	0.0	5.	-2615.9	-12.4	-3.2	0.0	0.0	0.0	0.	-3516.2	-45.9	11.4	0.0	-1612.2	20183.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
131.	-50.7	0.0	0.0	0.0	0.0	Asta	102	ndi	962	341	MY	MZZ	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	230.	-714.5	-595.1	-0.3	0.0	0.0	
165.	-50.7	0.0	0.0	0.0	0.0	PROGR.	102	ndi	962	341	MY	MZZ	165.	-5982.3	20.1	14.9	0.0	852.1	16871.8	230.	-714.5	-595.1	-0.3	0.0	0.0	
198.	-50.7	0.0	0.0	0.0	0.0	0.	-2008.2	15.0	-125.1	0.0	-425.4	-75.2	0.	-221.3	-339.4	18.9	56.0	1189.8	230.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
231.	-50.7	0.0	0.0	0.0	0.0	1.	-2008.0	15.0	-125.1	0.0	-347.3	-65.8	88.	-221.3	-339.4	18.9	56.0	1189.8	230.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
264.	-50.7	0.0	0.0	0.0	0.0	1.	-2007.9	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-339.4	18.9	56.0	1189.8	230.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
Asta	82	ndi	852	467	MY	2.	-2007.7	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-339.4	18.9	56.0	1189.8	230.1	230.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	82	ndi	852	467	MY	3.	-2007.6	15.0	-125.1	0.0	-312.7	-37.6	Asta	120	ndi	745	746	248.	-3364.5	230.	-714.5	-595.1	-0.3	0.0	0.0	
33.	508.4	0.0	0.0	0.0	0.0	4.	-2007.5	15.0	-125.1	0.0	-156.3	-18.8	PROGR.	120	ndi	745	746	248.	-3364.5	230.	-714.5	-595.1	-0.3	0.0	0.0	
66.	508.4	0.0	0.0	0.0	0.0	5.	-2007.1	15.0	-125.1	0.0	-78.2	-9.4	0.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
99.	508.4	0.0	0.0	0.0	0.0	Asta	104	ndi	962	341	MY	MZZ	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	230.	-714.5	-595.1	-0.3	0.0	0.0	
131.	508.4	0.0	0.0	0.0	0.0	0.	-1683.4	-61.8	3997.8	0.0	17988.8	319.1	16.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
165.	508.4	0.0	0.0	0.0	0.0	1.	-1683.2	-61.8	3997.8	0.0	15740.2	279.2	81.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
198.	508.4	0.0	0.0	0.0	0.0	2.	-1683.1	-61.8	3997.8	0.0	13401.6	239.3	98.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
231.	508.4	0.0	0.0	0.0	0.0	3.	-1682.9	-61.8	3997.8	0.0	11243.0	199.4	130.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
264.	508.4	0.0	0.0	0.0	0.0	Asta	104	ndi	962	341	MY	MZZ	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	230.	-714.5	-595.1	-0.3	0.0	0.0	
Asta	83	ndi	467	470	MY	3.	-1682.8	-61.8	3997.8	0.0	11243.0	199.4	PROGR.	104	ndi	962	341	248.	-3364.5	230.	-714.5	-595.1	-0.3	0.0	0.0	
PROGR.	83	ndi	467	470	MY	4.	-1682.7	-61.8	3997.8	0.0	8994.5	159.5	0.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
33.	632.7	0.0	0.0	0.0	0.0	1.	-1682.7	-61.8	3997.8	0.0	6745.8	119.7	0.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
66.	632.7	0.0	0.0	0.0	0.0	2.	-1682.5	-61.8	3997.8	0.0	4497.2	79.8	0.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
99.	632.7	0.0	0.0	0.0	0.0	3.	-1682.4	-61.8	3997.8	0.0	240.5	39.9	33.	-113.6	73.9	-15.9	-159.2	-362.1	173.	-714.5	-595.1	-0.3	0.0	0.0		
131.	632.7	0.0	0.0	0.0	0.0	4.	-1682.3	-61.8	3997.8	0.0	0.0	0.0	49.	-475.2	-590.2	1.7	-1359.9	0.0	125.2	230.	-714.5	-595.1	-0.3	0.0	0.0	
165.	632.7	0.0																								

[illegible]

-118.0	MMY	MZZ
-118.0	286.1	10806.0
-118.0	239.5	8635.8
-118.0	192.8	66832.0
-118.0	146.2	49931.1
-118.0	99.5	34796.8
-118.0	52.2	24413.6
-118.0	6.2	12472.6
-118.0	-40.4	4964.6
-118.0	-67.1	-131.7
731		
-109.7	MMY	MZZ
-109.7	292.5	110748.9
-109.7	333.3	88572.9
-109.7	374.8	67017.9
-109.7	414.8	50919.1
-109.7	455.6	35841.3
-109.7	496.4	23136.3
-109.7	537.1	12363.9
-109.7	577.7	3920.4
-109.7	618.7	-142.5
473		
TORS	MMY	MZZ
0.0	0.0	0.0
0.0	-23.5	30264.5
0.0	-46.9	49988.8
0.0	-70.4	59172.9
0.0	-93.8	57816.7
0.0	-117.3	45503.2
0.0	-140.7	23483.5
0.0	-164.2	-9893.4
0.0	-187.7	-53010.6
342		
TORS	MMY	MZZ
48.7	-83.0	45568.3
48.7	-105.6	28631.5
48.7	-128.2	15638.1
48.7	-150.8	19271.4
48.7	-173.4	29221.4
48.7	-196.0	22913.3
48.7	-218.6	8948.9
48.7	-241.2	-15555.8
48.7	-263.8	-50060.7
727		
TORS	MMY	MZZ
-91.4	-252.2	-50067.7
-91.4	-205.7	-33774.6
-91.4	-159.3	-23342.4
-91.4	-112.8	-13420.8
-91.4	-66.4	-5802.9
-91.4	-19.9	-97.0
-91.4	26.5	1864.5
-91.4	73.0	2094.1
-91.4	119.4	-109.0
730		
TORS	MMY	MZZ
-94.9	-161.9	-53010.6
-94.9	-128.7	-37087.1
-94.9	-195.5	-25192.4
-94.9	-112.4	-14692.4
-94.9	-229.2	-7305.1
-94.9	-246.0	-1710.6
-94.9	-262.8	-178.5
-94.9	-279.7	1780.2
-94.9	-296.5	1381.5
38		
TORS	MMY	MZZ
43.6	2464.8	38665.6
43.6	2029.6	35132.8
43.6	1594.1	31542.8
43.6	1159.1	28607.3
43.6	723.8	2354.5
43.6	288.5	2190.8
43.6	-146.5	18549.0
43.6	-582.0	15196.2
43.6	-1017.3	11843.5
39		
TORS	MMY	MZZ
-2.4	-1016.9	-25583.2
-2.4	-842.6	-21070.7
-2.4	-668.3	-16538.2
-2.4	-494.1	-12045.8
-2.4	-319.8	-7533.3
-2.4	-145.6	-3020.9
-2.4	28.7	1491.6
-2.4	202.9	604.1
-2.4	377.4	10016.5
41		
TORS	MMY	MZZ
0.0	-5064.5	19900.6
0.0	-4822.6	13297.9
0.0	-2960.6	5050.8
0.0	-1958.7	17607.9
0.0	-896.8	2047.1
0.0	145.2	22686.2
0.0	167.1	2523.3
0.0	2229.1	27764.4
0.0	-1324.2	48596.9
0.0	303.3	50303.5
42		
TORS	MMY	MZZ
6.3	3576.2	55582.8
6.3	3135.7	14594.2
6.3	2695.3	11001.3
6.3	2254.8	7408.4
6.3	1814.4	3815.5
6.3	1373.9	222.6
6.3	93.5	-3370.3
6.3	693.0	-6963.2
6.3	52.6	-10556.1
314.5		
TORS	MMY	MZZ
314.5	0.0	314.7
314.5	-102.2	35627.8
314.5	-204.4	71882.8
314.5	-306.6	107050.4
314.5	-408.8	144130.6
314.5	-510.4	189257.3
314.5	-613.2	217038.8
314.5	-715.6	253646.4
314.5	-817.6	290306.8
29		
TORS	MMY	MZZ
-203.7	-5296.7	-274910.1
-203.7	-4634.6	-240343.2
-203.7	-3972.7	-206017.7
-203.7	-3310.4	-171247

5.	146.3	4902.0	-174.2	-871.0	-6167.7	-29940.0	Asta	53	nodi	23	32		99.	28.3	0.0	0.0	0.0	0.0	0.0	0.0	5.	-2706.2	-29.4	-3.3	0.0	0.0	0.0
6.	146.3	4901.4	-174.2	-871.0	-5950.0	-29329.8	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	132.	28.3	0.0	0.0	0.0	0.0	0.0	Asta	201	nodi	962	341		
8.	146.3	4900.0	-174.2	-871.0	-5740.0	-28745.2	0.	-44.0	421.7	-2.4	-21.3	-157.5	-37674.2	165.	28.3	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ
9.	146.3	4900.4	-174.2	-871.0	-5514.5	-28104.6	16.	-44.0	421.7	-2.4	-21.3	-117.9	-30764.7	198.	28.3	0.0	0.0	0.0	0.0	0.0	0.	-2617.0	-12.4	-3.2	0.0	-15.9	61.9
10.	146.3	4899.8	-174.2	-871.0	-5296.7	-27493.4	33.	-44.0	414.8	-2.4	-21.3	-78.3	-27867.8	231.	28.3	0.0	0.0	0.0	0.0	0.0	1.	-2616.8	-12.4	-3.2	0.0	-13.9	54.2
Asta	51	nodi	962	341			49.	-44.0	407.9	-2.4	-21.3	-38.9	-24751.4	264.	28.3	0.0	0.0	0.0	0.0	0.0	2.	-2616.7	-12.4	-3.2	0.0	-11.9	46.4
PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	65.	-44.0	401.0	-2.4	-21.3	0.9	-10711.6	Asta	79	nodi	749	668			3.	-2616.6	-12.4	-3.2	0.0	-9.9	38.7
0.	-42.6	-4565.2	-113.2	-565.8	-8317.7	-29037.9	81.	-44.0	394.0	-2.4	-21.3	-151.0	-35101.2	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	4.	-2616.4	-12.4	-3.2	0.0	-7.9	30.0
1.	-62.6	-4565.7	-113.2	-565.8	-8035.2	-29608.5	98.	-44.0	387.1	-2.4	-21.3	-80.1	-2094.4	0.	-50.7	0.0	0.0	0.0	0.0	0.0	5.	-2616.3	-12.4	-3.2	0.0	-6.0	23.2
2.	-62.6	-4566.2	-113.2	-565.8	-7893.7	-30178.9	114.	-44.0	380.2	-2.4	-21.3	-119.7	-828.5	33.	-50.7	0.0	0.0	0.0	0.0	0.0	6.	-2616.1	-12.4	-3.2	0.0	-4.0	-4.4
3.	-62.6	-4566.8	-113.2	-565.8	-7725.0	-30742.2	130.	-44.0	373.0	-2.4	-21.3	-159.3	-1401.1	66.	-50.7	0.0	0.0	0.0	0.0	0.0	7.	-2616.0	-12.4	-3.2	0.0	-2.0	15.5
4.	-62.6	-4567.3	-113.2	-565.8	-7610.8	-31320.9	Asta	54	nodi	733	732			99.	-50.7	0.0	0.0	0.0	0.0	0.0	8.	-2615.9	-12.4	-3.2	0.0	0.0	0.0
5.	-62.6	-4567.8	-113.2	-565.8	-7462.9	-31891.2	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	127.	50.7	0.0	0.0	0.0	0.0	0.0	Asta	102	nodi	963	342		
6.	-62.6	-4568.4	-113.2	-565.8	-7327.9	-32462.9	0.	-63	-162.2	18.4	-121.6	721.0	-80.1	165.	-50.7	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ
7.	-62.6	-4568.9	-113.2	-565.8	-7198.9	-33034.2	16.	-63	-162.2	18.4	-121.6	721.0	-80.1	165.	-50.7	0.0	0.0	0.0	0.0	0.0	1.	-2008.2	15.0	-125.1	0.0	-65.4	-4.4
8.	-62.6	-4569.4	-113.2	-565.8	-7074.0	-33605.6	33.	-63	-168.3	18.4	-121.6	121.9	-545.1	231.	-50.7	0.0	0.0	0.0	0.0	0.0	2.	-2008.0	15.0	-125.1	0.0	-547.2	-65.8
9.	-62.6	-4569.9	-113.2	-565.8	-6949.1	-34176.9	49.	-63	-171.4	18.4	-121.6	121.9	-545.1	264.	-50.7	0.0	0.0	0.0	0.0	0.0	3.	-2007.9	15.0	-125.1	0.0	-469.0	-56.4
10.	-62.6	-4569.4	-113.2	-565.8	-6824.2	-34748.2	Asta	55	nodi	732	731			PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	4.	-2007.7	15.0	-125.1	0.0	-390.4	-47.0
Asta	52	nodi	963	342			0.	-165.9	-25.6	-112.0	-19.0	-101.1	-23078.9	0.	508.4	0.0	0.0	0.0	0.0	0.0	5.	-2007.6	15.0	-125.1	0.0	-312.7	-37.6
PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	11.	-165.9	-26.6	-112.0	-19.0	-101.1	-23094.4	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	6.	-2007.5	15.0	-125.1	0.0	-234.7	-18.8
0.	-98.7	-1361.6	-63.8	-319.1	0.0	17988.8	81.	-63	-177.5	18.4	-121.6	776.7	-13880.7	231.	508.4	0.0	0.0	0.0	0.0	0.0	7.	-2007.4	15.0	-125.1	0.0	-156.3	-18.8
1.	-98.7	-1362.1	-63.8	-319.1	0.0	17988.8	114.	-63	-183.6	18.4	-121.6	1375.7	-1949.1	264.	508.4	0.0	0.0	0.0	0.0	0.0	8.	-2007.3	15.0	-125.1	0.0	-78.2	-9.4
2.	-98.7	-1362.6	-63.8	-319.1	0.0	17988.8	130.	-63	-186.7	18.4	-121.6	1675.2	-27578.0	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	9.	-2007.2	15.0	-125.1	0.0	0.0	0.0
3.	-98.7	-1363.1	-63.8	-319.1	0.0	17988.8	0.	-165.9	-25.6	-112.0	-19.0	-101.1	-23078.9	0.	508.4	0.0	0.0	0.0	0.0	0.0	Asta	104	nodi	963	342		
4.	-98.7	-1363.6	-63.8	-319.1	0.0	17988.8	3.	-165.9	-26.1	-112.0	-19.0	-173.1	-22943.6	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	0.	-1683.4	-63.8	3597.8	0.0	17988.8	319.1
5.	-98.7	-1364.1	-63.8	-319.1	0.0	17988.8	15.	-165.9	-28.5	-112.0	-19.0	-331.8	-23048.5	0.	632.7	0.0	0.0	0.0	0.0	0.0	1.	-1683.2	-63.8	3597.8	0.0	15740.2	279.2
6.	-98.7	-1364.6	-63.8	-319.1	0.0	17988.8	18.	-165.9	-28.9	-112.0	-19.0	-611.7	-23216.0	0.	632.7	0.0	0.0	0.0	0.0	0.0	2.	-1683.1	-63.8	3597.8	0.0	13491.6	239.3
7.	-98.7	-1365.1	-63.8	-319.1	0.0	17988.8	20.	-165.9	-29.4	-112.0	-19.0	-891.6	-23344.6	0.	632.7	0.0	0.0	0.0	0.0	0.0	3.	-1683.0	-63.8	3597.8	0.0	11243.0	199.4
8.	-98.7	-1365.6	-63.8	-319.1	0.0	17988.8	Asta	56	nodi	731	730			0.	632.7	0.0	0.0	0.0	0.0	0.0	4.	-1682.9	-63.8	3597.8	0.0	8994.4	159.5
9.	-98.7	-1366.1	-63.8	-319.1	0.0	17988.8	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	134.	632.7	0.0	0.0	0.0	0.0	0.0	5.	-1682.8	-63.8	3597.8	0.0	2248.6	39.9
10.	-98.7	-1366.6	-63.8	-319.1	0.0	17988.8	0.	-9	190.9	-5.3	123.5	-390.7	-23319.4	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	0.	-1683.4	-63.8	3597.8	0.0	0.0	0.0
Asta	57	nodi	964	343			16.	-9	187.8	-5.3	123.5	-389.9	-20352.2	0.	632.7	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ
PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	33.	-9	184.8	-5.3	123.5	-389.9	-17248.8	0.	632.7	0.0	0.0	0.0	0.0	0.0	1.	-1683.4	-63.8	3597.8	0.0	-249.9	-9.9
0.	-77.4	8634.3	431.7	2081.8	3462.8	-22782.4	49.	-9	181.7	-5.3	123.5	-133.0	-14237.1	33.	632.7	0.0	0.0	0.0	0.0	0.0	2.	-1683.4	-63.8	3597.8	0.0	-1800.7	-150.5
1.	-77.4	8634.8	431.7	2081.8	3462.8	-22782.4	81.	-9	177.6	-5.3	123.5	38.8	-8431.0	66.	632.7	0.0	0.0	0.0	0.0	0.0	3.	-1683.4	-63.8	3597.8	0.0	-1200.4	-60.2
2.	-77.4	8635.3	431.7	2081.8	3462.8	-22782.4	98.	-9	173.5	-5.3	123.5	-47.3	-11309.2	99.	632.7	0.0	0.0	0.0	0.0	0.0	4.	-1683.4	-63.8	3597.8	0.0	-589.4	-38.2
3.	-77.4	8635.8	431.7	2081.8	3462.8	-22782.4	114.	-9	169.5	-5.3	123.5	226.5	-94.9	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	5.	-1683.4	-63.8	3597.8	0.0	0.0	0.0
4.	-77.4	8636.3	431.7	2081.8	3462.8	-22782.4	Asta	58	nodi	728	728			0.	632.7	0.0	0.0	0.0	0.0	0.0	Asta	106	nodi	964	343		
5.	-77.4	8636.8	431.7	2081.8	3462.8	-22782.4	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	135.	49.6	0.0	0.0	0.0	0.0	0.0	0.	-6511.1	-455.0	6200.0	0.0	3109.8	2275.0
6.	-77.4	8637.3	431.7	2081.8	3462.8	-22782.4	0.	-16.1	-185.8	2.5	-113.1	-103.1	-12861.2	180.	49.6	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ
7.	-77.4	8637.8	431.7	2081.8	3462.8	-22782.4	16.	-16.1	-185.8	2.5	-113.1	-103.1	-12861.2	270.	49.6	0.0	0.0	0.0	0.0	0.0	1.	-6511.0	-455.0	6200.0	0.0	2713.9	1137.5
8.	-77.4	8638.3	431.7	2081.8	3462.8	-22782.4	33.	-16.1	-191.9	2.5	-113.1	-103.1	-9217.8	360.	49.6	0.0	0.0	0.0	0.0	0.0	2.	-6510.8	-455.0	6200.0	0.0	2357.3	1706.2
9.	-77.4	8638.8	431.7	2081.8	3462.8	-22782.4	49.	-16.1	-195.0	2.5	-113.1	-103.1	-12861.2	Asta	88	nodi	468	462			3.	-6510.7	-455.0	6200.0	0.0	1988.1	1421.9
10.	-77.4	8639.3	431.7	2081.8	3462.8	-22782.4	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	127.	49.6	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ
Asta	59	nodi	728	728			0.	-16.1	-198.0	2.5	-113.1	-103.1	-12861.2	0.	140.6	0.0	0.0	0.0	0.0	0.0	1.	-6510.6	-455.0	6200.0	0.0	1504.4	1137.5
PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	12.	-16.1	-201.1	2.5	-113.1	-103.1	-12861.2	90.	140.6	0.0	0.0	0.0	0.0	0.0	2.	-6510.4	-455.0	6200.0	0.0	1162.8	853.1
0.	-45.7	-1392.2	16.2	81.0	0.0	228.7	98.	-16.1	-201.1	2.5	-113.1	-103.1	-12861.2	135.	140.6	0.0	0.0	0.0	0.0	0.0	3.	-6510.2	-455.0	6200.0	0.0	3876.2	284.4
1.	-45.7	-1392.7	16.2	81.0	0.0	228.7	Asta	60	nodi	729	729			140.	140.6	0.0	0.0	0.0	0.0	0.0	4.	-6510.0	-455.0	6200.0	0.0	0.0	0.0
2.	-45.7	-1393.2	16.2	81.0	0.0	228.7	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ	15.	140.6	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZZ	TORS	MY	NZZ
3.	-45.7	-1393.7	16.2	81.0	0.0	228.7	0.	-76.3	4.8	-0.8	-1.7	-248.8	-25568.8	135.	140.6	0.0	0.0	0.0	0.0	0.0	1.	-1634.2	49.9	1813.0	0.0	904.9	-249.6
4.	-45.7	-1394.2	16.2	81.0	0.0	228.7	16.	-76.3	3.4	-0.8	-1.7	-245.1	-25547.1	225.	140.6	0.0	0.0	0.0	0.0	0.0	2.	-1634.1	49.9	1813.0	0.0	679.8	-187.2
5.	-45.7	-1394																									

67.	-4.7	0.0	0.0	0.9	0.1	1.5	
68.	-4.7	0.0	0.0	0.9	0.2	1.5	
101.	-4.7	0.0	0.0	0.9	0.3	1.5	
125.	-4.7	0.0	0.0	0.9	0.4	1.5	
168.	-4.7	0.0	0.0	0.9	0.5	1.5	
202.	-4.7	0.0	0.0	0.9	0.5	1.5	
236.	-4.7	0.0	0.0	0.9	0.6	1.5	
269.	-4.7	0.0	0.0	0.9	0.6	1.5	
Asta	154	nodi	973	712			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	6.2	-795.8	0.0	0.0	0.0	0.0	
29.	6.2	-596.8	0.0	0.0	0.0	-2010.8	
38.	6.2	-397.9	0.0	0.0	0.0	-3437.9	
62.	6.2	-198.9	0.0	0.0	0.0	-4289.4	
85.	6.2	0.0	0.0	0.0	0.0	-4787.2	
144.	6.2	-198.9	0.0	0.0	0.0	-4289.4	
164.	6.2	-397.9	0.0	0.0	0.0	-3437.9	
201.	6.2	-596.8	0.0	0.0	0.0	-2010.8	
230.	6.2	-795.8	0.0	0.0	0.0	0.0	
Asta	156	nodi	972	711			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-58.6	6.4	0.4	0.0	62.0	0.0	
29.	-58.6	445.7	0.4	0.0	-10.1	15673.0	
38.	-58.6	246.7	0.4	0.0	-20.0	25606.4	
62.	-58.6	47.8	0.4	0.0	-30.3	39860.2	
115.	-58.6	-151.2	0.4	0.0	-40.4	26374.3	
144.	-58.6	-350.1	0.4	0.0	-50.7	21169.7	
173.	-58.6	-549.0	0.4	0.0	-60.5	8243.5	
201.	-58.6	-748.0	0.4	0.0	-70.4	-3014.4	
230.	-58.6	-946.9	0.4	0.0	-80.7	-34765.9	
Asta	157	nodi	969	970			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	21.3	948.6	0.0	7.0	-124.5	-78409.6	
16.	21.3	941.7	0.0	7.0	-61.9	-620.8	
31.	21.3	934.8	-1.9	7.0	-62.5	-47804.6	
43.	21.3	927.8	-1.9	7.0	-62.5	-47804.6	
65.	21.3	920.9	-1.9	7.0	-0.4	-1969.9	
81.	21.3	914.0	-1.9	7.0	30.6	-2741.3	
104.	21.3	907.1	-1.9	7.0	61.2	-2741.3	
114.	21.3	900.1	-1.9	7.0	92.6	26738.1	
140.	21.3	893.2	-1.9	7.0	123.6	41308.9	
Asta	158	nodi	967	968			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-14.2	-510.6	5.7	28.3	0.0	0.0	
16.	-14.2	-517.5	5.7	28.3	-92.0	-82.0	
31.	-14.2	-524.4	5.7	28.3	-183.1	-82.0	
49.	-14.2	-531.3	5.7	28.3	-275.9	-25356.8	
61.	-14.2	-538.2	5.7	28.3	-367.8	-45138.3	
81.	-14.2	-545.2	5.7	28.3	-459.8	-45271.7	
98.	-14.2	-552.2	5.7	28.3	-551.8	-45271.7	
114.	-14.2	-559.1	5.7	28.3	-643.7	-6067.7	
130.	-14.2	-566.0	5.7	28.3	-735.7	-69098.1	
Asta	159	nodi	966	967			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-510.6	5.7	14.2	0.0	71.2	-28.3	
1.	-510.5	5.7	14.2	0.0	62.3	62.8	
2.	-510.2	5.7	14.2	0.0	53.4	-17.7	
3.	-510.0	5.7	14.2	0.0	35.5	-14.1	
4.	-509.9	5.7	14.2	0.0	26.6	-10.6	
4.	-509.8	5.7	14.2	0.0	17.8	-7.1	
4.	-509.6	5.7	14.2	0.0	8.9	-3.5	
5.	-509.5	5.7	14.2	0.0	0.0	0.0	
Asta	160	nodi	969	973			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-796.9	6.2	0.0	0.0	0.0	-31.1	
1.	-796.7	6.2	0.0	0.0	0.0	-27.2	
2.	-796.6	6.2	0.0	0.0	0.0	-23.3	
12.	-796.5	6.2	0.0	0.0	0.0	-19.4	
13.	-796.4	6.2	0.0	0.0	0.0	-15.5	
23.	-796.2	6.2	0.0	0.0	0.0	-11.6	
4.	-796.1	6.2	0.0	0.0	0.0	-7.7	
4.	-795.9	6.2	0.0	0.0	0.0	-3.9	
5.	-795.8	6.2	0.0	0.0	0.0	0.0	
Asta	161	nodi	968	972			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-645.7	-58.6	0.4	0.0	0.0	292.8	
1.	-645.6	-58.6	0.4	0.0	1.3	236.2	
1.	-645.4	-58.6	0.4	0.0	1.3	219.6	
3.	-645.3	-58.6	0.4	0.0	1.3	183.0	
3.	-645.2	-58.6	0.4	0.0	0.9	146.4	
3.	-645.0	-58.6	0.4	0.0	0.0	110.0	
4.	-644.9	-58.6	0.4	0.0	0.4	73.2	
4.	-644.8	-58.6	0.4	0.0	0.0	36.6	
5.	-644.6	-58.6	0.4	0.0	0.0	0.0	
Asta	162	nodi	968	951			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-14.6	-1211.7	-52.9	-264.5	-735.7	-69906.3	
1.	-14.6	-1212.3	-52.9	-264.5	-669.7	-69906.3	
3.	-14.6	-1212.8	-52.9	-264.5	-603.4	-74933.0	
4.	-14.6	-1213.3	-52.9	-264.5	-537.3	-79571.0	
5.	-14.6	-1213.9	-52.9	-264.5	-471.9	-84209.0	
6.	-14.6	-1214.4	-52.9	-264.5	-405.0	-77488.0	
12.	-14.6	-1214.9	-52.9	-264.5	-339.4	-70767.0	
9.	-14.6	-1215.5	-52.9	-264.5	-272.8	-65025.3	
10.	-14.6	-1216.0	-52.9	-264.5	-206.6	-60084.9	
Asta	163	nodi	951	969			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	21.3	1748.8	-8.1	-24.0	-80.7	-8204.9	
1.	21.3	1748.2	-8.1	-24.0	-195.5	-93639.0	
3.	21.3	1748.7	-8.1	-24.0	-185.9	-93639.0	
4.	21.3	1748.8	-8.1	-24.0	-175.2	-89327.3	
5.	21.3	1747.6	-8.1	-24.0	-165.1	-87142.4	
17.	21.3	1747.1	-8.1	-24.0	-154.9	-84967.4	
8.	21.3	1746.6	-8.1	-24.0	-144.8	-82774.7	
10.	21.3	1746.0	-8.1	-24.0	-134.7	-80582.0	
10.	21.3	1745.5	-8.1	-24.0	-124.5	-78409.6	
Asta	165	nodi	970	974			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-18.9	-590.5	-0.3	0.0	0.0	0.0	
29.	-18.9	-310.6	-0.3	0.0	9.8	-11789.2	
58.	-18.9	-111.6	-0.3	0.0	19.6	-1876.8	
87.	-18.9	17.3	-0.3	0.0	29.1	-1805.7	
114.	-18.9	286.3	-0.3	0.0	39.1	-1285.0	
145.	-18.9	485.2	-0.3	0.0	48.9	-174.6	
175.	-18.9	684.2	-0.3	0.0	58.7	-8965.2	
201.	-18.9	883.3	-0.3	0.0	68.5	37395.1	
230.	-18.9	1082.1	-0.3	0.0	78.0	66014.4	
Asta	166	nodi	735	951			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-3171.4	-73.2	-3.9	-0.9	-1071.7	11031.0	
43.	-3145.3	-73.2	-3.9	-0.9	-907.7	8321.0	
72.	-3119.3	-73.2	-3.9	-0.9	-743.6	681.0	
128.	-3093.2	-73.2	-3.9	-0.9	-579.6	1704.0	
175.	-3067.1	-73.2	-3.9	-0.9	-415.5	-1405.0	
213.	-3041.1	-73.2	-3.9	-0.9	-251.6	-4514.0	
255.	-3015.0	-73.2	-3.9	-0.9	-87.6	-7623.0	
282.	-2982.0	-73.2	-3.9	-0.9	78.0	-13841.0	
Asta	167	nodi	749	754			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-257.0	0.0	0.0	0.0	0.0	0.0	
34.	-257.0	0.0	0.0	0.0	0.0	0.0	
67.	-257.0	0.0	0.0	0.0	0.0	0.0	
102.	-257.0	0.0	0.0	0.0	0.0	0.0	
135.	-257.0	0.0	0.0	0.0	0.0	0.0	
168.	-257.0	0.0	0.0	0.0	0.0	0.0	

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3.	-582.3	22.9	1698.2	0.0	3184.1	-42.9	0.0	-1921.1	28.5	2.4	0.0	7.6	-89.1	1.	-2658.5	180.5	3.3	0.0	12.3	-677.0	22.5	463.0	-10.2	17.4	-470.6	-2929.2	0.0	
4.	-633.0	3.8	1846.1	0.0	3461.5	-7.2	0.0	-2094.3	1.5	-252.6	0.0	-631.4	-3.8	2.	-2867.0	86.4	-1.1	0.0	-4.2	-323.9	24.9	1065.5	-21.7	-335.8	689.0	-9039.9	0.0	
5.	-581.9	22.9	1698.2	0.0	1061.4	-14.3	0.0	-1920.8	28.5	2.4	0.0	4.5	-53.5	3.	-2658.5	180.5	3.3	0.0	8.2	-451.3	22.5	449.2	-10.2	17.4	-480.8	-1469.1	0.0	
Asta	PROGR.	0.	-1317.5	-220.8	4916.2	0.0	6089.1	-27.4	-1920.8	28.5	2.4	0.0	1.5	-17.8	4.	-2658.5	180.5	3.3	0.0	1.4	-225.7	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0
1.	-1317.5	-220.8	4916.2	0.0	2481.2	110.0	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	5.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1317.5	-220.8	4916.2	0.0	2138.6	96.0	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	6.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1317.5	-220.8	4916.2	0.0	1343.7	-101.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	7.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1317.5	-220.8	4916.2	0.0	7149.8	-2.0	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	8.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1317.5	-220.8	4916.2	0.0	11517.8	-69.8	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	9.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1317.5	-220.8	4916.2	0.0	569.8	-72.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	10.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
3.	-1317.5	-220.8	4916.2	0.0	9598.1	-72.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	11.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
3.	-1317.5	-220.8	4916.2	0.0	1337.6	52.0	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	12.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
3.	-1317.5	-220.8	4916.2	0.0	1767.5	-72.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	13.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
3.	-1316.8	-220.8	4916.2	0.0	9218.0	41.0	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	14.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
3.	-1316.8	-220.8	4916.2	0.0	792.4	-3.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	15.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
4.	-1316.7	-220.8	4916.2	0.0	6145.3	276.0	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	16.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
4.	-1316.7	-220.8	4916.2	0.0	7952.0	-3.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	17.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
4.	-1316.6	-220.8	4916.2	0.0	307.7	138.0	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	18.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
5.	-1711.7	-23.2	3071.4	0.0	1919.6	-1.6	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	19.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
Asta	PROGR.	0.	-1317.5	-220.8	4916.2	0.0	6089.1	-27.4	-1920.8	28.5	2.4	0.0	1.5	-17.8	4.	-2658.5	180.5	3.3	0.0	1.4	-225.7	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0
1.	-1475.8	1.5	1247.4	0.0	626.8	-9.1	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	5.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1774.2	10.0	2880.0	0.0	1260.1	-43.8	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	6.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1774.2	10.0	2880.0	0.0	1080.1	-31.6	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	7.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1774.2	10.0	2880.0	0.0	900.1	-37.3	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	8.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1475.4	1.5	1247.4	0.0	898.0	-4.8	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	9.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-1475.4	1.5	1247.4	0.0	2880.0	-4.8	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	10.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
3.	-1475.3	1.5	1247.4	0.0	3118.4	-38.8	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	11.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
3.	-1475.3	1.5	1247.4	0.0	2880.0	-4.8	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	12.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
3.	-1475.1	1.5	1247.4	0.0	2338.8	-9.2	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	13.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
4.	-1475.1	1.5	1247.4	0.0	300.0	-12.5	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	14.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
4.	-1475.1	1.5	1247.4	0.0	1775.4	-4.9	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	15.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
4.	-1773.4	10.0	2880.0	0.0	180.0	-6.3	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	16.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
5.	-1773.2	10.0	2880.0	0.0	0.0	0.0	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	17.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
Asta	PROGR.	0.	-1317.5	-220.8	4916.2	0.0	6089.1	-27.4	-1920.8	28.5	2.4	0.0	1.5	-17.8	4.	-2658.5	180.5	3.3	0.0	1.4	-225.7	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0
1.	-858.7	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	5.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	6.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	7.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	8.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	9.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	10.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	11.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	12.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	13.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	14.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	15.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	16.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	17.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	18.	-2658.5	180.5	3.3	0.0	-1.4	-108.0	22.5	435.3	-10.2	17.4	-49.4	-96.0	0.0	
1.	-858.6	10.5	-3510.2	0.0	-1751.1	-52.4	0.0	-2094.3	1.5	-252.6	0.0	0.0	0.0	19.	-2658.5	180.5	3.3											

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33.	10.6	857.5	-14.3	-119.7	-55.0	-4002.8	114.	-1.0	-129.2	1.7	-69.7	-171.8	-13529.9	45.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.3	-286.4	3806.6	0.0	4758.3	358.0	
49.	10.6	850.6	-14.3	-119.7	178.0	-2614.2	130.	-1.0	-132.3	1.7	-69.7	-138.9	-15654.2	90.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.2	-286.4	3806.6	0.0	2379.1	179.0	
81.	10.6	843.2	-14.3	-119.7	41.1	-13796.0	Asta	82	10.6	843.2	-14.3	-119.7	41.1	-13796.0	729.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.0	-286.4	3806.6	0.0	729.0	0.0
89.	10.6	836.8	-14.3	-119.7	644.0	1277.5	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	180.	85.1	0.0	0.0	0.0	0.0	0.0	Asta	107	nodi	30	469	MY	NZZ	
98.	10.6	829.8	-14.3	-119.7	877.0	14815.5	0.	45.0	3.7	-1.1	-0.3	-164.3	-15737.8	225.	85.1	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	
114	110.6	822.9	-14.3	-119.7	110.6	822.9	1	45.0	3.7	-1.1	-0.3	-164.3	-15737.8	270.	85.1	0.0	0.0	0.0	0.0	0.0	1.	-990.5	30.7	1121.6	0.0	5608.0	-133.4	
130.	10.6	816.0	-14.3	-119.7	1343.0	41562.8	5.	45.0	2.8	-1.1	-0.9	-158.7	-15721.5	315.	85.1	0.0	0.0	0.0	0.0	0.0	1.	-990.5	30.7	1121.6	0.0	4907.0	-134.3	
Asta	46	nodi	964	8	6.0	2.3	360.	85.0	0.0	0.0	0.0	0.0	0.0	90.	85.0	0.0	0.0	0.0	0.0	0.0	2.	-990.5	30.7	1121.6	0.0	1121.6	-115.1	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	10.	45.0	1.9	-1.1	-0.9	-153.1	-15709.9	Asta	89	nodi	211	339	MY	NZZ	2.	-990.2	30.7	1121.6	0.0	3305.0	-95.9	
0.	-27.8	-1176.2	10.3	51.5	0.0	130.1	13.	45.0	1.4	-1.1	-0.3	-150.3	-15705.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	3.	-990.1	30.7	1121.6	0.0	2804.0	-76.7	
16.	-27.8	-1183.1	10.3	51.5	0.0	130.2	16.	45.0	1.9	-1.1	-0.3	-147.5	-15701.0	270.	85.0	0.0	0.0	0.0	0.0	0.0	1.	-990.1	30.7	1121.6	0.0	2184.9	-57.7	
33.	-27.8	-1190.0	10.3	51.5	-334.5	-3831.2	18.	45.0	0.4	-1.1	-0.9	-144.7	-15701.3	45.	-51.0	0.0	0.0	0.0	0.0	0.0	4.	-989.8	30.7	1121.6	0.0	1402.0	-38.4	
49.	-27.8	-1197.0	10.3	51.5	-634.5	-4370.5	20.	45.0	0.0	-1.1	-0.9	-141.9	-15700.8	90.	-51.0	0.0	0.0	0.0	0.0	0.0	5.	-989.5	30.7	1121.6	0.0	701.6	-19.2	
65.	-27.8	-1203.9	10.3	51.5	-669.0	-47721.3	Asta	59	nodi	728	727	MY	NZZ	135.	-51.0	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	
81.	-27.8	-1210.8	10.3	51.5	-678.8	-48108.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	225.	-51.0	0.0	0.0	0.0	0.0	0.0	1.	-1350.9	39.1	37.2	0.0	185.9	-195.5	
98.	-27.8	-1217.7	10.3	51.5	-1003.5	-116565.1	0.	1.5	132.0	-0.2	67.3	-82.7	-15628.3	270.	-51.0	0.0	0.0	0.0	0.0	0.0	1.	-1350.7	39.1	37.2	0.0	185.9	-195.5	
114.	-27.8	-1224.7	10.3	51.5	-1170.8	-136498.9	16.	1.5	129.0	-0.2	67.3	-89.9	-13507.7	360.	-51.0	0.0	0.0	0.0	0.0	0.0	1.	-1350.6	39.1	37.2	0.0	139.4	-146.6	
130.	-27.8	-1231.6	10.3	51.5	-1338.0	-156387.0	13.	1.5	125.9	-0.2	67.3	-87.1	-11486.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	2.	-1350.5	39.1	37.2	0.0	92.9	-97.7	
Asta	67	nodi	961	42	82	45	49.	1.5	122.8	-0.2	67.3	-84.3	-9415.7	0.	-51.0	0.0	0.0	0.0	0.0	0.0	3.	-1350.2	39.1	37.2	0.0	69.7	-73.3	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	65.	1.5	119.8	-0.2	67.3	-81.5	-7444.4	Asta	91	nodi	5	210	MY	NZZ	4.	-1349.8	39.1	37.2	0.0	46.7	-48.9	
0.	-25.8	-2888.1	-9.0	-45.1	-1338.0	-156377.0	81.	1.5	116.7	-0.2	67.3	-78.7	-5527.7	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	1.	-1405.8	-110.4	-0.1	0.0	-0.4	276.0	
1.	-25.8	-2888.6	-9.0	-45.1	-1326.8	-159987.5	96.	1.5	113.7	-0.2	67.3	-75.8	-3650.9	0.	-361.7	7.6	1068.2	0.0	5341.2	-37.9	0.	-1406.2	-110.4	-0.1	0.0	-0.6	483.1	
3.	-25.8	-2889.1	-9.0	-45.1	-1315.5	-163396.5	114.	1.5	110.6	-0.2	67.3	-72.0	-1828.8	1.	-361.6	7.6	1068.2	0.0	4673.5	-39.2	1.	-1405.1	-110.4	-0.1	0.0	-0.5	414.1	
4.	-25.8	-2889.7	-9.0	-45.1	-1304.2	-167210.3	130.	1.5	107.5	-0.2	67.3	-70.2	-56.4	1.	-361.3	7.6	1068.2	0.0	4005.9	-28.5	2.	-1405.9	-110.4	-0.1	0.0	-0.4	345.1	
5.	-25.8	-2890.2	-9.0	-45.1	-1291.0	-170822.7	Asta	67	nodi	473	731	MY	NZZ	3.	-361.2	7.6	1068.2	0.0	3338.2	-23.7	3.	-1405.7	-110.4	-0.1	0.0	-0.3	207.0	
6.	-25.8	-2890.7	-9.0	-45.1	-1281.7	-174455.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	3.	-361.2	7.6	1068.2	0.0	2670.6	-19.0	4.	-1405.5	-110.4	-0.1	0.0	-0.2	138.0	
7.	-25.8	-2891.3	-9.0	-45.1	-1270.4	-178049.5	25.	-154.5	0.0	0.0	0.0	0.0	0.0	4.	-360.9	7.6	1068.2	0.0	1335.3	-9.5	Asta	109	nodi	11	471	MY	NZZ	
9.	-25.8	-2891.8	-9.0	-45.1	-1259.2	-181663.9	50.	-154.5	0.0	0.0	0.0	0.0	0.0	4.	-360.8	7.6	1068.2	0.0	667.6	-4.7	0.	-1406.1	-110.4	-0.1	0.0	-0.4	276.0	
10.	-25.8	-2892.3	-9.0	-45.1	-1247.9	-185279.0	99.	-154.5	0.0	0.0	0.0	0.0	0.0	Asta	92	nodi	14	211	MY	NZZ	1.	-1406.2	-110.4	-0.1	0.0	-0.4	345.1	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	124.	-154.5	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	2.	-1405.9	-110.4	-0.1	0.0	-0.4	345.1	
0.	-76.5	2889.1	-2.3	-11.5	-1250.5	-191421.2	149.	-154.5	0.0	0.0	0.0	0.0	0.0	0.	-922.1	-56.7	2454.4	0.0	1227.2	283.3	3.	-1405.8	-110.4	-0.1	0.0	-0.3	207.0	
1.	-76.5	2888.6	-2.3	-11.5	-1247.6	-187810.1	174.	-154.5	0.0	0.0	0.0	0.0	0.0	1.	-921.9	-56.7	2454.4	0.0	1078.2	247.9	4.	-1405.5	-110.4	-0.1	0.0	-0.2	138.0	
3.	-76.5	2888.1	-2.3	-11.5	-1244.7	-184199.7	198.	-154.5	0.0	0.0	0.0	0.0	0.0	2.	-921.8	-56.7	2454.4	0.0	928.2	212.5	5.	-1405.3	-110.4	-0.1	0.0	-0.1	89.0	
5.	-76.5	2887.0	-2.3	-11.5	-1241.5	-180589.9	Asta	70	nodi	470	732	MY	NZZ	2.	-921.7	-56.7	2454.4	0.0	7670.1	177.1	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	
7.	-76.5	2886.5	-2.3	-11.5	-1239.0	-176980.8	0.	-152.0	0.0	0.0	0.0	0.0	0.0	3.	-921.5	-56.7	2454.4	0.0	6130.5	147.7	0.	-1405.7	-110.4	-0.1	0.0	0.0	0.0	
8.	-76.5	2885.9	-2.3	-11.5	-1233.3	-169764.7	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	4.	-921.3	-56.7	2454.4	0.0	4602.1	106.2	1.	-1405.5	-110.4	-0.1	0.0	-0.1	89.0	
9.	-76.5	2885.4	-2.3	-11.5	-1230.4	-166517.6	25.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-921.3	-56.7	2454.4	0.0	3068.0	70.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	
Asta	69	nodi	962	365	11	45	74.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-921.3	-56.7	2454.4	0.0	1354.0	35.4	0.	-1405.8	-110.4	-0.1	0.0	3.8	-438.4	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	99.	-152.0	0.0	0.0	0.0	0.0	0.0	Asta	92	nodi	14	211	MY	NZZ	1.	-1405.8	-110.4	-0.1	0.0	3.8	-438.4	
0.	-74.5	1281.0	-9.4	-47.2	-1227.5	-162580.8	124.	-152.0	0.0	0.0	0.0	0.0	0.0	1.	-995.9	3.2	1264.7	0.0	620.6	-15.8	2.	-1405.8	-110.4	-0.1	0.0	3.8	-438.4	
1.	-74.5	1280.5	-9.4	-47.2	-1224.6	-158100.1	149.	-152.0	0.0	0.0	0.0	0.0	0.0	1.	-995.8	3.2	1264.7	0.0	474.7	-11.8	3.	-1405.8	-110.4	-0.1	0.0	3.8	-438.4	
3.	-74.5	1276.2	-9.4	-47.2	-1201.6	-121152.1	174.	-152.0	0.0	0.0	0.0	0.0	0.0	3.	-995.4	3.2	1264.7	0.0	361.3	-7.9	4.	-1405.8	-110.4	-0.1	0.0	3.8	-438.4	
4.	-74.5	1260.3	-9.4	-47.2	-1176.2	-93016.5	198.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-995.1	3.2	1264.7	0.0	1580.9	-1.9	5.	-1405.8	-110.4	-0.1	0.0	3.8	-438.4	
65.	-74.5	1246.4	-9.4	-47.2	-1146.8	-64603.4	Asta	71	nodi	342	740	MY	NZZ	Asta	111	nodi	29	473	MY	NZZ	1.	-1270.5	24.9	89.3	0.0	446.6	-124.6	
81.	-74.5	1246.4	-9.4	-47.2	-1146.8	-64603.4	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	0.	-995.9	3.2	1264.7	0.0	5333.1	-11.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	
98.	-74.5	1246.4	-9.4	-47.2	-1146.8	-64603.4	0.	-995.9	3.2	1264.7	0.0	0.0	0.0	1.	-995.9	3.2	1264.7	0.0	5333.1	-11.8	1.	-1270.4	24.9	89.3	0.0	390.8	-109.0	
114.	-74.5	1246.4	-9.4	-47.2	-1146.8	-64603.4	25.	-99.2	0.0	0.0	0.0	0.0	0.0	4.	-995.1	3.2	1264.7	0.0	1580.9	-1.9	2.	-1270.3	24.9	89.3	0.0	390.8	-109.0	
130.	-74.5	1246.4	-9.4	-47.2	-1146.8	-64603.4	74.	-99.2	0.0	0.0	0.0	0.0	0.0	4.	-995.0	3.2	1264.7	0.0	790.4	-2.0	3.	-1270.2	24.9	89.3	0.0	390.8	-109.0	
Asta	10	nodi	5	14	34	45	99.	64.2	0.0	0.0	0.0	0.0	0.0	Asta	94	nodi	32	213	MY	NZZ	4.	-1269.7	24.9	89.3	0.0	390.8	-109.0	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	124.	64.2	0.0	0.0	0.0	0.0	0.0	0.	-530.3	2.3	-2532.6	0.0	-12663.1	-11.5	1.	-1270.1	24.9	89.3	0.0	390.8	-109.0	
0.	-29.8	-323.3	1.3	37.9	-21.2	144.6	149.	64.2	0.0	0.0	0.0	0.0	0.0	1.	-530.3	2.3	-2532.6	0.0	-12663.1	-11.5	2.	-1270.0	24.9	89.3	0.0	390.8	-109.0	
1.	-29.8	-323.3	1.3	37.9</																								

0.	-30.4	-803.9	-8.1	990	-159.0	-49431.4	88.	-315.0	-53.2	0.7	-1.3	42.4	8306.4
1.	-30.4	-804.5	-8.1	940.1	-148.9	-50436.7	100.	-315.0	-130.5	0.7	-1.3	29.4	6699.7
2.	-30.4	-804.5	-8.1	940.1	-148.9	-50436.7	120.	-315.0	-207.0	0.7	-1.3	11.0	2047.0
3.	-30.4	-804.5	-8.1	940.1	-128.6	-52449.1	140.	-315.0	-285.0	0.7	-1.3	3.5	-571.2
4.	-30.4	-806.1	-8.1	940.1	-118.5	-5346.4	Asta	142	nodi	970	738		
5.	-30.4	-806.6	-8.1	940.1	-108.6	-5446.2	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-30.4	-807.1	-8.1	940.1	-98.3	-5547.8	0.	3.2	77.4	0.6	13.5	84.3	26673.3
7.	-30.4	-807.6	-8.1	940.1	-88.3	-5648.4	1.	3.2	77.4	0.6	13.5	84.3	26673.3
8.	-30.4	-808.1	-8.1	940.1	-78.0	-5749.0	2.	3.2	77.4	0.6	13.5	84.3	26673.3
9.	-30.4	-808.2	-8.1	940.1	-68.0	-5849.6	3.	3.2	77.4	0.6	13.5	84.3	26673.3
10.	-30.4	-808.2	-8.1	940.1	-58.0	-5950.2	4.	3.2	77.4	0.6	13.5	84.3	26673.3
11.	-30.4	-808.2	-8.1	940.1	-48.0	-6050.8	5.	3.2	77.4	0.6	13.5	84.3	26673.3
12.	-30.4	-808.2	-8.1	940.1	-38.0	-6151.4	6.	3.2	77.4	0.6	13.5	84.3	26673.3
13.	-30.4	-808.2	-8.1	940.1	-28.0	-6252.0	7.	3.2	77.4	0.6	13.5	84.3	26673.3
14.	-30.4	-808.2	-8.1	940.1	-18.0	-6352.6	8.	3.2	77.4	0.6	13.5	84.3	26673.3
15.	-30.4	-808.2	-8.1	940.1	-8.0	-6453.2	9.	3.2	77.4	0.6	13.5	84.3	26673.3
16.	-30.4	-808.2	-8.1	940.1	2.0	-6553.8	10.	3.2	77.4	0.6	13.5	84.3	26673.3
17.	-30.4	-808.2	-8.1	940.1	12.0	-6654.4	11.	3.2	77.4	0.6	13.5	84.3	26673.3
18.	-30.4	-808.2	-8.1	940.1	22.0	-6755.0	12.	3.2	77.4	0.6	13.5	84.3	26673.3
19.	-30.4	-808.2	-8.1	940.1	32.0	-6855.6	13.	3.2	77.4	0.6	13.5	84.3	26673.3
20.	-30.4	-808.2	-8.1	940.1	42.0	-6956.2	14.	3.2	77.4	0.6	13.5	84.3	26673.3
21.	-30.4	-808.2	-8.1	940.1	52.0	-7056.8	15.	3.2	77.4	0.6	13.5	84.3	26673.3
22.	-30.4	-808.2	-8.1	940.1	62.0	-7157.4	16.	3.2	77.4	0.6	13.5	84.3	26673.3
23.	-30.4	-808.2	-8.1	940.1	72.0	-7258.0	17.	3.2	77.4	0.6	13.5	84.3	26673.3
24.	-30.4	-808.2	-8.1	940.1	82.0	-7358.6	18.	3.2	77.4	0.6	13.5	84.3	26673.3
25.	-30.4	-808.2	-8.1	940.1	92.0	-7459.2	19.	3.2	77.4	0.6	13.5	84.3	26673.3
26.	-30.4	-808.2	-8.1	940.1	102.0	-7559.8	20.	3.2	77.4	0.6	13.5	84.3	26673.3
27.	-30.4	-808.2	-8.1	940.1	112.0	-7660.4	21.	3.2	77.4	0.6	13.5	84.3	26673.3
28.	-30.4	-808.2	-8.1	940.1	122.0	-7761.0	22.	3.2	77.4	0.6	13.5	84.3	26673.3
29.	-30.4	-808.2	-8.1	940.1	132.0	-7861.6	23.	3.2	77.4	0.6	13.5	84.3	26673.3
30.	-30.4	-808.2	-8.1	940.1	142.0	-7962.2	24.	3.2	77.4	0.6	13.5	84.3	26673.3
31.	-30.4	-808.2	-8.1	940.1	152.0	-8062.8	25.	3.2	77.4	0.6	13.5	84.3	26673.3
32.	-30.4	-808.2	-8.1	940.1	162.0	-8163.4	26.	3.2	77.4	0.6	13.5	84.3	26673.3
33.	-30.4	-808.2	-8.1	940.1	172.0	-8264.0	27.	3.2	77.4	0.6	13.5	84.3	26673.3
34.	-30.4	-808.2	-8.1	940.1	182.0	-8364.6	28.	3.2	77.4	0.6	13.5	84.3	26673.3
35.	-30.4	-808.2	-8.1	940.1	192.0	-8465.2	29.	3.2	77.4	0.6	13.5	84.3	26673.3
36.	-30.4	-808.2	-8.1	940.1	202.0	-8565.8	30.	3.2	77.4	0.6	13.5	84.3	26673.3
37.	-30.4	-808.2	-8.1	940.1	212.0	-8666.4	31.	3.2	77.4	0.6	13.5	84.3	26673.3
38.	-30.4	-808.2	-8.1	940.1	222.0	-8767.0	32.	3.2	77.4	0.6	13.5	84.3	26673.3
39.	-30.4	-808.2	-8.1	940.1	232.0	-8867.6	33.	3.2	77.4	0.6	13.5	84.3	26673.3
40.	-30.4	-808.2	-8.1	940.1	242.0	-8968.2	34.	3.2	77.4	0.6	13.5	84.3	26673.3
41.	-30.4	-808.2	-8.1	940.1	252.0	-9068.8	35.	3.2	77.4	0.6	13.5	84.3	26673.3
42.	-30.4	-808.2	-8.1	940.1	262.0	-9169.4	36.	3.2	77.4	0.6	13.5	84.3	26673.3
43.	-30.4	-808.2	-8.1	940.1	272.0	-9270.0	37.	3.2	77.4	0.6	13.5	84.3	26673.3
44.	-30.4	-808.2	-8.1	940.1	282.0	-9370.6	38.	3.2	77.4	0.6	13.5	84.3	26673.3
45.	-30.4	-808.2	-8.1	940.1	292.0	-9471.2	39.	3.2	77.4	0.6	13.5	84.3	26673.3
46.	-30.4	-808.2	-8.1	940.1	302.0	-9571.8	40.	3.2	77.4	0.6	13.5	84.3	26673.3
47.	-30.4	-808.2	-8.1	940.1	312.0	-9672.4	41.	3.2	77.4	0.6	13.5	84.3	26673.3
48.	-30.4	-808.2	-8.1	940.1	322.0	-9773.0	42.	3.2	77.4	0.6	13.5	84.3	26673.3
49.	-30.4	-808.2	-8.1	940.1	332.0	-9873.6	43.	3.2	77.4	0.6	13.5	84.3	26673.3
50.	-30.4	-808.2	-8.1	940.1	342.0	-9974.2	44.	3.2	77.4	0.6	13.5	84.3	26673.3
51.	-30.4	-808.2	-8.1	940.1	352.0	-10074.8	45.	3.2	77.4	0.6	13.5	84.3	26673.3
52.	-30.4	-808.2	-8.1	940.1	362.0	-10175.4	46.	3.2	77.4	0.6	13.5	84.3	26673.3
53.	-30.4	-808.2	-8.1	940.1	372.0	-10276.0	47.	3.2	77.4	0.6	13.5	84.3	26673.3
54.	-30.4	-808.2	-8.1	940.1	382.0	-10376.6	48.	3.2	77.4	0.6	13.5	84.3	26673.3
55.	-30.4	-808.2	-8.1	940.1	392.0	-10477.2	49.	3.2	77.4	0.6	13.5	84.3	26673.3
56.	-30.4	-808.2	-8.1	940.1	402.0	-10577.8	50.	3.2	77.4	0.6	13.5	84.3	26673.3
57.	-30.4	-808.2	-8.1	940.1	412.0	-10678.4	51.	3.2	77.4	0.6	13.5	84.3	26673.3
58.	-30.4	-808.2	-8.1	940.1	422.0	-10779.0	52.	3.2	77.4	0.6	13.5	84.3	26673.3
59.	-30.4	-808.2	-8.1	940.1	432.0	-10879.6	53.	3.2	77.4	0.6	13.5	84.3	26673.3
60.	-30.4	-808.2	-8.1	940.1	442.0	-10980.2	54.	3.2	77.4	0.6	13.5	84.3	26673.3
61.	-30.4	-808.2	-8.1	940.1	452.0	-11080.8	55.	3.2	77.4	0.6	13.5	84.3	26673.3
62.	-30.4	-808.2	-8.1	940.1	462.0	-11181.4	56.	3.2	77.4	0.6	13.5	84.3	26673.3
63.	-30.4	-808.2	-8.1	940.1	472.0	-11282.0	57.	3.2	77.4	0.6	13.5	84.3	26673.3
64.	-30.4	-808.2	-8.1	940.1	482.0	-11382.6	58.	3.2	77.4	0.6	13.5	84.3	26673.3
65.	-30.4	-808.2	-8.1	940.1	492.0	-11483.2	59.	3.2	77.4	0.6	13.5	84.3	26673.3
66.	-30.4	-808.2	-8.1	940.1	502.0	-11583.8	60.	3.2	77.4	0.6	13.5	84.3	26673.3
67.	-30.4	-808.2	-8.1	940.1	512.0	-11684.4	61.	3.2	77.4	0.6	13.5	84.3	26673.3
68.	-30.4	-808.2	-8.1	940.1	522.0	-11785.0	62.	3.2	77.4	0.6	13.5	84.3	26673.3
69.	-30.4	-808.2	-8.1	940.1	532.0	-11885.6	63.	3.2	77.4	0.6	13.5	84.3	26673.3
70.	-30.4	-808.2	-8.1	940.1	542.0	-11986.2	64.	3.2	77.4	0.6	13.5	84.3	26673.3
71.	-30.4	-808.2	-8.1	940.1	552.0	-12086.8	65.	3.2	77.4	0.6	13.5	84.3	26673.3
72.	-30.4	-808.2	-8.1	940.1	562.0	-12187.4	66.	3.2	77.4	0.6	13.5	84.3	26673.3
73.	-30.4	-808.2	-8.1	940.1	572.0	-12288.0	67.	3.2	77.4	0.6	13.5	84.3	26673.3
74.	-30.4	-808.2	-8.1	940.1	582.0	-12388.6	68.	3.2	77.4	0.6	13.5	84.3	26673.3
75.	-30.4	-808.2	-8.1	940.1	592.0	-12489.2	69.	3.2	77.4	0.6	13.5	84.3	26673.3
76.	-30.4	-808.2	-8.1	940.1	602.0	-12589.8	70.	3.2	77.4	0.6	13.5	84.3	26673.3
77.	-30.4	-808.2	-8.1	940.1	612.0	-12690.4	71.	3.2	77.4	0.6	13.5	84.3	26673.3
78.	-30.4	-808.2	-8.1	940.1	622.0	-12791.0	72.	3.2	77.4	0.6	13.5	84.3	26673.3
79.	-30.4	-808.2	-8.1	940.1	632.0	-12891.6	73.	3.2	77.4	0.6	13.5	84.3	26673.3
80.	-30.4	-808.2	-8.1	940.1	642.0	-12992.2	74.	3.2	77.4	0.6	13.5	84.3	26673.3
81.	-30.4	-808.2	-8.1	940.1	652.0	-13092.8	75.	3.2	77.4	0.6	13.5	84.3	26673.3
82.	-30.4	-808.2	-8.1	940.1	662.0	-13193.4	76.	3.2	77.4	0.6	13.5	84.3	26673.3
83.	-30.4	-808.2	-8.1	940.1	672.0	-13294.0	77.	3.2	77.4	0.6	13.5	84.3	26673.3
84.	-30.4	-808.2	-8.1	940.1	682.0	-13394.6	78.	3.2	77.4	0.6	13.5	84.3	26673.3
85.	-30.4	-808.2	-8.1	940.1	692.0	-13495.2	79.	3.2	77.4	0.6	13.5	84.3	26673.3
86.	-30.4	-808.2	-8.1	940.1	702.0	-13595.8	80.	3.2	77.4	0.6	13.5	84.3	26673.3
87.	-30.4	-808.2	-8.1	940.1	712.0	-13696.4	81.	3.2	77.4	0.6	13.5	84.3	26673.3
88.	-30.4	-808.2	-8.1	940.1	722.0	-13797.0	82.	3.2	77.4	0.6	13.5	84.3	26673.3
89.	-30.4	-808.2	-8.1	940.1	732.0	-13897.6	83.	3.2	77.4	0.6	13.5	84.3	26673.3
90.	-30.4	-808.2	-8.1	940.1	742.0	-13998.2	84.	3.2	77.4	0.6	13.5	84.3	26673.3
91.	-30.4	-808.2	-8.1	940.1	752.0	-14098.8	85.	3.2	77.4	0.6	13.5	84.3	26673.3
92.	-30.4	-808.2	-8.1	940.1	762.0	-14199.4	86.	3.2	77.4	0.6	13.5	84.3	26673.3
93.	-30.4	-808.2	-8.1	940.1	772.0	-14299.9	87.	3.2	77.4	0.6	13.5		

200	198.2	-276.0	0.5	-21.4	-131.7	109.5	PROGR.	NORM	TY	TZZ	TORS	MY	MZZ	6	-25.8	-2890.2	-9.0	-45.1	-1281.0	-17082.7	0.0	Asta	67	north	473	731	MY	MZZ	
201	-118.2	-428.6	0.5	-21.4	-150.5	-14583.7	0.0	-4488.8	62.9	-2.4	-2.6	-593.3	-15216.1	0.0	5.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	PROGR.	TY	TZZ	TORS	MY	MZZ	
202	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	-4462.2	62.9	-2.4	-2.6	-593.3	-15216.1	0.0	6.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
334	-62.4	-733.8	0.5	-21.4	-188.1	-63064.3	0.0	85.	-4436.2	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	9.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	25.	-154.5	0.0	0.0	0.0	0.0
335	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	138.	-4401.1	62.9	-2.4	-2.6	-390.8	-9668.2	0.0	10.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	30.	-154.5	0.0	0.0	0.0	0.0
336	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	180.	-4384.1	62.9	-2.4	-2.6	-188.3	-4620.2	0.0	11.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	35.	-154.5	0.0	0.0	0.0	0.0
337	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	213.	-4368.0	62.9	-2.4	-2.6	-87.0	-1962.2	0.0	12.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	40.	-154.5	0.0	0.0	0.0	0.0
338	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	255.	-4311.9	62.9	-2.4	-2.6	-14.3	-72.2	0.0	13.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	45.	-154.5	0.0	0.0	0.0	0.0
339	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	298.	-4305.9	62.9	-2.4	-2.6	-115.5	-3601.7	0.0	14.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	50.	-154.5	0.0	0.0	0.0	0.0
340	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	340.	-4279.8	62.9	-2.4	-2.6	-216.6	-6709.7	0.0	15.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	55.	-154.5	0.0	0.0	0.0	0.0
341	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	382.	-4263.7	62.9	-2.4	-2.6	-347.9	-10817.7	0.0	16.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	60.	-154.5	0.0	0.0	0.0	0.0
342	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	424.	-4247.6	62.9	-2.4	-2.6	-479.0	-14725.7	0.0	17.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	65.	-154.5	0.0	0.0	0.0	0.0
343	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	466.	-4231.5	62.9	-2.4	-2.6	-610.1	-18633.7	0.0	18.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	70.	-154.5	0.0	0.0	0.0	0.0
344	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	508.	-4215.4	62.9	-2.4	-2.6	-741.2	-22541.7	0.0	19.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	75.	-154.5	0.0	0.0	0.0	0.0
345	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	550.	-4199.3	62.9	-2.4	-2.6	-872.3	-26449.7	0.0	20.	-2890.2	-2890.0	-9.0	-45.1	-1281.0	-17445.8	0.0	80.	-154.5	0.0	0.0	0.0	0.0
346	198.2	-27																											

[illegible]

[illegible]

128.	-4385.2	86.5	-1.8	-0.3	-347.3	-10222.8	16.	-61.2	-843.1	-36.9	-184.7	600.4	-2540.6	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		20.	-89.9	-18.6	-73.9	-11.6	239.0	-14348.6	
	-4461.1	39.3	-3.0	-4.8	-306.9	-8042.6		-59.3	-817.4	-41.6	-208.1	676.5	-2483.3		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2		-116.4	-18.1	-69.7	-11.0	95.1	-14495.2	
	-4559.1	86.5	-1.8	-0.0	-259.2	-8501.8	33.	-59.3	-850.8	-36.9	-184.7	600.4	-2540.6		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2	ASTA	-116.4	-18.1	-69.7	-11.0	95.1	-14495.2	
170.	-4435.0	39.3	-3.0	-4.8	-179.6	-6371.7		-59.3	-824.3	-41.6	-208.1	1353.0	-15797.4	16.	NORM	TYT	TZZ	TORS	MYT	MZZ		PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-4333.1	86.5	-1.8	-0.0	-196.9	-2863.8	49.	-61.2	-857.0	-36.9	-184.7	1801.2	-30367.6		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2		0.	-6.2	121.3	-3.1	76.7	-183.1	-14028.3
213.	-4409.0	39.3	-3.0	-4.8	-811.3	-808.3		-61.2	-857.0	-36.9	-184.7	1801.2	-30367.6	33.	NORM	TYT	TZZ	TORS	MYT	MZZ		PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-4307.0	86.5	-1.8	-0.3	-121.7	808.3	65.	-61.2	-863.9	-36.9	-184.7	2041.2	-44150.0		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2	16.	-6.2	121.3	-3.1	76.7	-132.2	-1237.5	
255.	-4382.9	39.3	-3.0	-4.8	-98.2	-39.3		-61.2	-863.9	-36.9	-184.7	2041.2	-44150.0	49.	NORM	TYT	TZZ	TORS	MYT	MZZ		PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-4281.0	86.5	-1.8	-0.0	-46.5	-870.8	81.	-61.2	-870.8	-36.9	-184.7	2041.2	-44150.0		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2	33.	-6.2	115.1	-3.1	76.7	-81.2	-10441.5	
298.	-4356.9	39.3	-3.0	-4.8	202.3	-1358.9		-59.3	-845.1	-41.6	-208.1	3382.4	-56980.2	65.	NORM	TYT	TZZ	TORS	MYT	MZZ		PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-4254.9	86.5	-1.8	-0.0	-46.5	-870.8	98.	-59.3	-845.1	-41.6	-208.1	3382.4	-56980.2		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2	49.	-5.2	117.0	-3.2	75.4	-171.4	-10322.6	
340.	-4330.8	39.3	-3.0	-4.8	329.6	312.7		-59.3	-852.0	-41.6	-208.1	4075.9	-70279.6	81.	NORM	TYT	TZZ	TORS	MYT	MZZ		PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-4028.9	86.5	-1.8	-0.0	-100.0	-1183.9	114.	-59.3	-852.0	-41.6	-208.1	4075.9	-70279.6		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2	65.	-5.2	114.0	-3.2	75.4	-120.1	-6818.5	
ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
0.	-11921.1	22.8	-32.2	0.0	-3314.7	16129.2	130.	-59.3	-865.9	-41.6	-208.1	5411.8	-98396.0	114.	-100.0	1219.2	-6.7	-33.7	-109.6	-1079.1		98.	-5.2	101.7	-3.2	75.4	-17.6	-5041.1	
21.	-11082.8	130.1	-36.9	0.0	-3996.5	4092.3	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-11086.5	22.8	-32.2	0.0	-1985.0	17071.2	0.	1.1	-2569.0	247.8	1258.1	4803.1	-138932.2	130.	-100.0	1219.2	-6.7	-33.7	-109.6	-1079.1		98.	-5.2	101.7	-3.2	75.4	-17.6	-5041.1	
41.	-11895.9	130.1	-36.9	0.0	-3175.4	1410.6	1.	1.1	-2569.0	247.8	1258.1	4803.1	-138932.2	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-11897.5	130.1	-36.9	0.0	-2414.3	1272.2	0.	1.1	-2569.0	247.8	1258.1	4803.1	-138932.2	0.	-30.7	-309.1	1.3	47.5	0.0	5267.2		114.	-6.2	99.8	-3.1	76.7	173.9	-1707.6	
62.	-11883.2	22.8	-32.2	0.0	-1520.1	17542.3	3.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	16.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		
	-11884.8	130.1	-36.9	0.0	-1653.3	3954.9	0.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	0.	-30.7	-316.0	1.3	47.5	-21.6	188.0		114.	-5.2	98.7	-3.2	75.4	136.3	-7.4	
83.	-11870.6	22.8	-32.2	0.0	-655.2	18013.3	4.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	33.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		
	-11872.2	130.1	-36.9	0.0	-892.2	16177.7	5.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	0.	-30.7	-323.0	1.3	47.5	-43.2	5003.8		16.	-1.4	-107.7	2.5	-71.3	61.2	-55.7	
103.	-11857.9	22.8	-32.2	0.0	9.6	18484.4	6.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	49.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		
	-11859.5	130.1	-36.9	0.0	-131.2	9230.4	8.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	0.	-30.7	-337.4	1.3	47.5	-41.4	5325.2		16.	-1.4	-107.7	2.5	-71.3	61.2	-55.7	
124.	-11845.3	22.8	-32.2	0.0	674.5	18955.4	6.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	65.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		
	-11846.9	130.1	-36.9	0.0	629.9	12003.2	8.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	0.	-30.7	-344.3	1.3	47.5	-62.1	10864.2		39.	-0.7	-114.0	0.8	-68.2	-53.1	-3654.4	
144.	-11832.6	22.8	-32.2	0.0	1339.4	19405.4	6.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	65.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		
	-11834.2	130.1	-36.9	0.0	1391.0	14685.9	8.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	0.	-30.7	-351.3	1.3	47.5	-62.1	10864.2		39.	-0.7	-114.0	0.8	-68.2	-53.1	-3654.4	
165.	-11820.0	22.8	-32.2	0.0	2004.2	19897.4	9.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	81.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		
	-11821.6	130.1	-36.9	0.0	2152.0	17388.7	9.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	0.	-30.7	-364.5	1.3	47.5	-172.8	38518.1		49.	-0.7	-117.0	0.8	-68.2	-56.6	-5351.1	
ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
0.	-5996.5	-76.3	6.5	6.0	2197.7	1510.9	1.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	81.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		
	-5977.2	-25.0	7.0	0.0	1977.2	652.2	1.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	0.	-30.7	-375.6	1.3	47.5	-151.2	32651.0		65.	-0.7	-121.9	0.8	-68.2	-80.2	-7457.6	
42.	-5970.8	-76.3	6.5	6.0	1927.0	11097.3	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-5951.6	-25.0	7.0	0.0	1807.3	5505.4	0.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	114.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		
84.	-5949.1	-76.3	6.5	6.0	1694.4	1276.3	1.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		81.	-1.4	-119.9	2.5	-71.3	-301.1	-7453.6	
	-5925.9	-25.0	7.0	0.0	1787.3	4458.6	3.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		81.	-1.4	-119.9	2.5	-71.3	-301.1	-7453.6	
126.	-5916.7	-76.3	6.5	6.0	1480.6	1480.6	3.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-5900.2	-25.0	7.0	0.0	1495.2	3411.8	3.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		15.	-0.7	-123.3	0.8	-68.2	-134.4	-15660.8	
209.	-5888.1	-76.3	6.5	6.0	844.3	-875.4	3.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		15.	-0.7	-123.3	0.8	-68.2	-134.4	-15660.8	
	-5868.9	-25.0	7.0	0.0	844.3	-875.4	3.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		15.	-0.7	-123.3	0.8	-68.2	-134.4	-15660.8	
251.	-5842.4	-76.3	6.5	6.0	573.7	-407.0	3.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-5823.2	-25.0	7.0	0.0	573.7	-407.0	3.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		15.	-0.7	-123.3	0.8	-68.2	-134.4	-15660.8	
293.	-5816.8	-76.3	6.5	6.0	303.0	-726.7	6.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		15.	-0.7	-123.3	0.8	-68.2	-134.4	-15660.8	
	-5797.5	-25.0	7.0	0.0	303.0	-726.7	6.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		15.	-0.7	-123.3	0.8	-68.2	-134.4	-15660.8	
335.	-5791.1	-76.3	6.5	6.0	326.9	-726.7	6.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
	-5771.9	-25.0	7.0	0.0	326.9	-726.7	6.	-54.7	5807.8	289.8	1394.4	2232.8	-153617.3	0.	-256.1	-2306.5	-1.9	-357.8	-148.6	-46997.5		15.	-0.7	-123.3	0.8	-68.2	-134.4	-15660.8	
ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	
0.	-45.1	-1342.9	37.4	186.8	0.0	225.3	10.	-54.7	5807.8																				

[illegible]

[illegible]

[illegible]

126.	-44.5	-11.7	-0.3	20.5	77.1	-7099.9	130.	69.8	989.4	-19.4	-97.2	0.0	-349.2	3.	-180.2	1072.2	-3.5	-21.3	-101.1	-31368.5	231.	-5.6	0.0	0.0	0.0	0.0
168.	25.0	106.9	-0.3	20.5	91.1	-5100.4	131.	69.8	989.4	-19.4	-97.2	0.0	-349.2	4.	-180.2	1071.7	-3.5	-21.3	-96.7	-3003.6	264.	-5.6	0.0	0.0	0.0	0.0
210.	94.4	137.1	-0.3	20.5	101.1	-5100.4	132.	69.8	989.4	-19.4	-97.2	0.0	-349.2	5.	-180.2	1071.2	-3.5	-21.3	-91.2	-3003.6	298.	-5.6	0.0	0.0	0.0	0.0
252.	163.9	343.9	-0.3	20.5	119.2	-13840.3	133.	69.8	989.4	-19.4	-97.2	0.0	-349.2	6.	-180.2	1070.6	-3.5	-21.3	-87.9	-2730.7	331.	-5.6	0.0	0.0	0.0	0.0
294.	233.4	462.4	-0.3	20.5	133.2	-20781.5	134.	69.8	989.4	-19.4	-97.2	0.0	-349.2	7.	-180.2	1070.1	-3.5	-21.3	-83.5	-2602.7	366.	-5.6	0.0	0.0	0.0	0.0
336.	301.9	581.0	-0.3	20.5	147.2	-27617.7	135.	69.8	989.4	-19.4	-97.2	0.0	-349.2	8.	-180.2	1069.6	-3.5	-21.3	-79.0	-2467.5	399.	-5.6	0.0	0.0	0.0	0.0
378.	370.4	699.5	-0.3	20.5	161.3	-34523.9	136.	69.8	989.4	-19.4	-97.2	0.0	-349.2	9.	-180.2	1069.1	-3.5	-21.3	-74.6	-2338.9	432.	-5.6	0.0	0.0	0.0	0.0
420.	439.9	818.0	-0.3	20.5	175.4	-41430.1	137.	69.8	989.4	-19.4	-97.2	0.0	-349.2	10.	-180.2	1068.6	-3.5	-21.3	-70.1	-2210.3	465.	-5.6	0.0	0.0	0.0	0.0
462.	509.4	936.5	-0.3	20.5	189.5	-48336.3	138.	69.8	989.4	-19.4	-97.2	0.0	-349.2	11.	-180.2	1068.1	-3.5	-21.3	-65.6	-2081.9	498.	-5.6	0.0	0.0	0.0	0.0
504.	579.9	1055.0	-0.3	20.5	203.6	-55242.5	139.	69.8	989.4	-19.4	-97.2	0.0	-349.2	12.	-180.2	1067.6	-3.5	-21.3	-61.1	-1943.5	531.	-5.6	0.0	0.0	0.0	0.0
546.	649.4	1170.5	-0.3	20.5	217.7	-62148.7	140.	69.8	989.4	-19.4	-97.2	0.0	-349.2	13.	-180.2	1067.1	-3.5	-21.3	-56.6	-1805.1	564.	-5.6	0.0	0.0	0.0	0.0
588.	719.9	1286.0	-0.3	20.5	231.8	-69054.9	141.	69.8	989.4	-19.4	-97.2	0.0	-349.2	14.	-180.2	1066.6	-3.5	-21.3	-52.1	-1666.7	597.	-5.6	0.0	0.0	0.0	0.0
630.	789.4	1401.5	-0.3	20.5	245.9	-75961.1	142.	69.8	989.4	-19.4	-97.2	0.0	-349.2	15.	-180.2	1066.1	-3.5	-21.3	-47.6	-1528.3	630.	-5.6	0.0	0.0	0.0	0.0
672.	859.9	1517.0	-0.3	20.5	260.0	-82867.3	143.	69.8	989.4	-19.4	-97.2	0.0	-349.2	16.	-180.2	1065.6	-3.5	-21.3	-43.1	-1389.9	663.	-5.6	0.0	0.0	0.0	0.0
714.	929.4	1632.5	-0.3	20.5	274.1	-89773.5	144.	69.8	989.4	-19.4	-97.2	0.0	-349.2	17.	-180.2	1065.1	-3.5	-21.3	-38.6	-1251.5	696.	-5.6	0.0	0.0	0.0	0.0
756.	999.9	1748.0	-0.3	20.5	288.2	-96679.7	145.	69.8	989.4	-19.4	-97.2	0.0	-349.2	18.	-180.2	1064.6	-3.5	-21.3	-34.1	-1113.1	729.	-5.6	0.0	0.0	0.0	0.0
798.	1069.4	1863.5	-0.3	20.5	302.3	-103585.9	146.	69.8	989.4	-19.4	-97.2	0.0	-349.2	19.	-180.2	1064.1	-3.5	-21.3	-29.6	-974.7	762.	-5.6	0.0	0.0	0.0	0.0
840.	1139.9	1979.0	-0.3	20.5	316.4	-110492.1	147.	69.8	989.4	-19.4	-97.2	0.0	-349.2	20.	-180.2	1063.6	-3.5	-21.3	-25.1	-836.3	795.	-5.6	0.0	0.0	0.0	0.0
882.	1209.4	2094.5	-0.3	20.5	330.5	-117398.3	148.	69.8	989.4	-19.4	-97.2	0.0	-349.2	21.	-180.2	1063.1	-3.5	-21.3	-20.6	-697.9	828.	-5.6	0.0	0.0	0.0	0.0
924.	1279.9	2210.0	-0.3	20.5	344.6	-124304.5	149.	69.8	989.4	-19.4	-97.2	0.0	-349.2	22.	-180.2	1062.6	-3.5	-21.3	-16.1	-559.5	861.	-5.6	0.0	0.0	0.0	0.0
966.	1349.4	2325.5	-0.3	20.5	358.7	-131210.7	150.	69.8	989.4	-19.4	-97.2	0.0	-349.2	23.	-180.2	1062.1	-3.5	-21.3	-11.6	-421.1	894.	-5.6	0.0	0.0	0.0	0.0
1008.	1419.9	2441.0	-0.3	20.5	372.8	-138116.9	151.	69.8	989.4	-19.4	-97.2	0.0	-349.2	24.	-180.2	1061.6	-3.5	-21.3	-7.1	-282.7	927.	-5.6	0.0	0.0	0.0	0.0
1050.	1489.4	2556.5	-0.3	20.5	386.9	-145023.1	152.	69.8	989.4	-19.4	-97.2	0.0	-349.2	25.	-180.2	1061.1	-3.5	-21.3	-2.6	-144.3	960.	-5.6	0.0	0.0	0.0	0.0
1092.	1559.9	2672.0	-0.3	20.5	401.0	-151929.3	153.	69.8	989.4	-19.4	-97.2	0.0	-349.2	26.	-180.2	1060.6	-3.5	-21.3	1.9	-7.7	993.	-5.6	0.0	0.0	0.0	0.0
1134.	1629.4	2787.5	-0.3	20.5	415.1	-158835.5	154.	69.8	989.4	-19.4	-97.2	0.0	-349.2	27.	-180.2	1060.1	-3.5	-21.3	7.4	91.1	1026.	-5.6	0.0	0.0	0.0	0.0
1176.	1699.9	2903.0	-0.3	20.5	429.2	-165741.7	155.	69.8	989.4	-19.4	-97.2	0.0	-349.2	28.	-180.2	1059.6	-3.5	-21.3	12.9	182.3	1059.	-5.6	0.0	0.0	0.0	0.0
1218.	1769.4	3018.5	-0.3	20.5	443.3	-172647.9	156.	69.8	989.4	-19.4	-97.2	0.0	-349.2	29.	-180.2	1059.1	-3.5	-21.3	18.4	273.5	1092.	-5.6	0.0	0.0	0.0	0.0
1260.	1839.9	3134.0	-0.3	20.5	457.4	-179554.1	157.	69.8	989.4	-19.4	-97.2	0.0	-349.2	30.	-180.2	1058.6	-3.5	-21.3	23.9	364.7	1125.	-5.6	0.0	0.0	0.0	0.0
1302.	1909.4	3249.5	-0.3	20.5	471.5	-186460.3	158.	69.8	989.4	-19.4	-97.2	0.0	-349.2	31.	-180.2	1058.1	-3.5	-21.3	29.4	455.9	1158.	-5.6	0.0	0.0	0.0	0.0
1344.	1979.9	3365.0	-0.3	20.5	485.6	-193366.5	159.	69.8	989.4	-19.4	-97.2	0.0	-349.2	32.	-180.2	1057.6	-3.5	-21.3	34.9	547.1	1191.	-5.6	0.0	0.0	0.0	0.0
1386.	2049.4	3480.5	-0.3	20.5	499.7	-200272.7	160.	69.8	989.4	-19.4	-97.2	0.0	-349.2	33.	-180.2	1057.1	-3.5	-21.3	40.4	638.3	1224.	-5.6	0.0	0.0	0.0	0.0
1428.	2119.9	3596.0	-0.3	20.5	513.8	-207178.9	161.	69.8	989.4	-19.4	-97.2	0.0	-349.2	34.	-180.2	1056.6	-3.5	-21.3	45.9	729.5	1257.	-5.6	0.0	0.0	0.0	0.0
1470.	2189.4	3711.5	-0.3	20.5	527.9	-214085.1	162.	69.8	989.4	-19.4	-97.2	0.0	-349.2	35.	-180.2	1056.1	-3.5	-21.3	51.4	820.7	1290.	-5.6	0.0	0.0	0.0	0.0
1512.	2259.9	3827.0	-0.3	20.5	542.0	-221001.3	163.	69.8	989.4	-19.4	-97.2	0.0	-349.2	36.	-180.2	1055.6	-3.5	-21.3	56.9	911.9	1323.	-5.6	0.0	0.0	0.0	0.0
1554.	2329.4	3942.5	-0.3	20.5	556.1	-227907.5	164.	69.8	989.4	-19.4	-97.2	0.0	-349.2	37.	-180.2	1055.1	-3.5	-21.3	62.4	1003.1	1356.	-5.6	0.0	0.0	0.0	0.0
1596.	2399.9	4058.0	-0.3	20.5	570.2	-234813.7	165.	69.8	989.4	-19.4	-97.2	0.0	-349.2	38.	-180.2	1054.6	-3.5	-21.3	67.9	1094.3	1389.	-5.6	0.0	0.0	0.0	0.0
1638.	2469.4	4173.5	-0.3	20.5	584.3	-241719.9	166.	69.8	989.4	-19.4	-97.2	0.0	-349.2	39.	-180.2	1054.1	-3.5	-21.3	73.4	1185.5	1422.	-5.6	0.0	0.0	0.0	0.0
1680.	2539.9	4289.0	-0.3	20.5	598.4	-248626.1	167.	69.8	989.4	-19.4	-97.2	0.0	-349.2	40.	-180.2	1053.6	-3.5	-21.3	78.9	1276.7	1455.	-5.6	0.0	0.0	0.0	0.0
1722.	2609.4	4404.5	-0.3	20.5	612.5	-255532.3	168.	69.8	989.4	-19.4	-97.2	0.0	-349.2	41.	-180.2	1053.1	-3.5	-21.3	84.4	1367.9	1488.	-5.6	0.0	0.0	0.0	0.0
1764.	2679.9	4520.0	-0.3	20.5	626.6	-262438.5	169.	69.8	989.4	-19.4	-97.2	0.0	-349.2	42.	-180.2	1052.6	-3.5	-21.3	89.9	1459.1	1521.	-5.6	0.0	0.0	0.0	0.0
1806.	2749.4	4635.5	-0.3	20.5	640.7	-269344.7	170.	69.8	989.4	-19.4	-97.2	0.0	-349.2	43.	-180.2	1052.1	-3.5	-21.3	95.4	1550.3	1554.	-5.6	0.0	0.0	0.0	0.0
1848.	2819.9	4751.0	-0.3	20.5	654.8	-276250.9	171.	69.8	989.4	-19.4	-97.2	0.0	-349.2	44.	-180.2	1051.6	-3.5	-21.3	100.9	1641.5	1587.	-5.6	0.0	0.0	0.0	0.0
1890.	2889.4	4866.5	-0.3	20.5	668.9	-283157.1	172.	69.8	989.4	-19.4	-97.2	0.0	-349.2	45.	-180.2	1051.1	-3.5	-21.3	106.4	1732.7	1620.	-5.6	0.0	0.0	0.0	0.0
1932.	2959.9	4982.0	-0.3	20.5	683.0	-290063.3	173.	69.8	989.4	-19.4	-97.2	0.0	-349.2	46.	-180.2	1050.6	-3.5	-21.3	111.9	1823.9	1653.	-5.6	0.0	0.0	0.0	0.0
1974.	3029.4	5097.5	-0.3	20.5	697.1	-296969.5	174.	69.8	989.4	-19.4	-97.2	0.0	-349.2	47.	-180.2	1050.1	-3.5	-21.3	117.4	1915.1	1686.	-5.6	0.0	0.0	0.0	0.0
2016.	3099.9	5213.0	-0.3	20.5	711.2	-303875.7	175.	69.8	989.4	-19.4	-97.2	0.0	-349.2	48.	-180.2	1049.6	-3.5	-21.3	122.9	2006.3	1719.	-5.6	0.0	0.0	0.0	0.0
2058.	3169.4	5328.5	-0.3	20.5	725.3	-310781.9	176.	69.8	989.4	-19.4	-97.2	0.0	-349.2	49.	-180.2	1049.1	-3.5	-21.3	128.4	2097.5	1752.	-5.6	0.0	0.0	0.0	0.0
2100.	3239.9	5444.0	-0.3	20.5	739.4	-317688.1	177.	69.8	989.4	-19.4	-97.2	0.0	-349.2	50.	-180.2	1048.6	-3.5	-21.3	133.9	2188.7	1785.	-5.6	0.0	0.0	0.0	0.0
2142.	3309.4	5559.5	-0.3	20.5	753.5	-324594.3	178.	69.8	989.4	-19.4	-97.2	0.0	-349.2	51.	-180.2	1048.1	-3.5	-21.3	139.4	2279.9	1818.	-5.6	0.0	0.0	0.0	0.0
2184.	3379.9	5675.0	-0.3	20.5	767.6	-331500.5	1																			

1.	-1292.0	-15.7	-1.6	0.0	-6.9	68.8	248.	-1762.5	-5.1	4.7	0.0	-2322.4	7084.3	0.	280.2	302.6	0.1	0.0	0.0	209.	-873.2	0.3	16.8	2.5	2390.2	3189.1		
1.	-1291.9	-15.7	-1.6	0.0	-5.9	58.9	289.	-1737.3	-5.1	4.7	0.0	-2317.5	6875.1	29.	280.2	208.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1	
2.	-1291.7	-15.7	-1.6	0.0	-5.9	58.9	330.	-1721.0	-5.1	4.7	0.0	-2317.0	6875.0	58.	280.2	208.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1	
3.	-1291.6	-15.7	-1.6	0.0	-3.9	39.3	Asta	117	742	739	MY	NZZ	739	86.	280.2	20.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1	
3.	-1291.5	-15.7	-1.6	0.0	-2.9	29.5	PROGR.	117	742	739	MY	NZZ	739	115.	280.2	-73.5	0.1	0.0	-17.0	13147.7	Asta	150	780	953	MY	NZZ	780	
3.	-1291.4	-15.7	-1.6	0.0	-1.9	19.5	0.	-1304.6	-31.4	-53.9	0.0	-7828.6	17780.5	144.	280.2	-107.5	0.1	0.0	-21.3	9717.7	PROGR.	150	780	953	MY	NZZ	780	
4.	-1291.2	-15.7	-1.6	0.0	-1.0	9.8	41.	-1889.3	-31.4	-53.9	0.0	-9605.9	16485.6	173.	280.2	-261.5	0.1	0.0	-25.6	3546.0	0.	-4.8	0.0	0.0	0.4	0.0	0.4	
5.	-1291.0	-15.7	-1.6	0.0	-0.3	0.7	13.	-1864.0	-31.4	-53.9	0.0	-7702.7	15393.2	201.	280.2	-355.5	0.1	0.0	-29.8	1327.5	135.	-4.8	0.0	0.0	0.4	0.0	0.4	
Asta	101	742	739	MY	NZZ	739	124.	-1838.7	-31.4	-53.9	0.0	-1160.4	13895.8	230.	280.2	-449.5	0.1	0.0	-34.1	-16893.6	301.	-4.8	0.0	0.0	0.4	0.1	0.7	
PROGR.	101	742	739	MY	NZZ	739	365.	-1813.4	-31.4	-53.9	0.0	-1062.4	12600.9	Asta	134	750	468	MY	NZZ	468	601.	-4.8	0.0	0.0	0.4	0.1	0.7	
1.	-1252.4	-5.4	-1.5	0.0	-7.5	27.0	178.	-1781.1	-31.4	-53.9	0.0	-303.5	23879.6	PROGR.	134	750	468	MY	NZZ	468	135.	-4.8	0.0	0.0	0.4	0.1	0.7	
1.	-1252.3	-5.4	-1.5	0.0	-6.5	23.6	248.	-1762.5	-31.4	-53.9	0.0	-9507.9	10011.1	0.	-110.0	-305.0	-0.2	0.0	0.0	0.0	368.	-4.8	0.0	0.0	0.4	0.2	0.7	
1.	-1252.2	-5.4	-1.5	0.0	-5.5	19.5	289.	-1737.3	-31.4	-53.9	0.0	-7702.7	15393.2	0.	-110.0	-305.0	-0.2	0.0	0.0	0.0	202.	-4.8	0.0	0.0	0.4	0.2	0.7	
2.	-1252.0	-5.4	-1.5	0.0	-4.7	16.9	330.	-1721.0	-31.4	-53.9	0.0	-9953.4	7421.3	58.	-110.0	-313.0	-0.2	0.0	10.2	-12019.9	368.	-4.8	0.0	0.0	0.4	0.3	0.7	
3.	-1251.9	-5.4	-1.5	0.0	-3.7	12.5	Asta	119	742	739	MY	NZZ	739	Asta	119	742	739	MY	NZZ	739	269.	-4.8	0.0	0.0	0.4	0.3	0.7	
3.	-1251.7	-5.4	-1.5	0.0	-2.8	10.1	PROGR.	119	742	739	MY	NZZ	739	115.	-110.0	73.0	-0.2	0.0	20.3	-13229.0	Asta	154	780	973	212	MY	NZZ	780
4.	-1251.6	-5.4	-1.5	0.0	-1.9	6.7	0.	106.7	-134.6	9.1	26.0	1052.1	36841.0	144.	-110.0	367.0	-0.2	0.0	25.4	-9779.5	PROGR.	154	780	973	212	MY	NZZ	780
4.	-1251.5	-5.4	-1.5	0.0	-0.9	3.4	18.	106.7	-134.6	9.1	26.0	1052.1	36841.0	201.	-110.0	367.0	-0.2	0.0	30.5	-3827.4	0.	-4.8	0.0	0.0	0.4	0.0	0.4	
5.	-1251.3	-5.4	-1.5	0.0	0.0	0.0	35.	106.7	-256.3	9.1	26.0	733.0	30000.8	230.	-110.0	355.0	-0.2	0.0	35.6	5277.5	29.	2.6	-282.0	0.0	0.0	-949.4	0.0	
Asta	102	742	739	MY	NZZ	739	52.	106.7	-317.1	9.1	26.0	575.4	24893.9	0.	-110.0	449.0	-0.2	0.0	40.0	16785.0	58.	2.6	-188.0	0.0	0.0	-16216.2	0.0	
PROGR.	102	742	739	MY	NZZ	739	70.	106.7	-387.9	9.1	26.0	413.8	18802.3	Asta	136	749	469	MY	NZZ	469	86.	2.6	-94.0	0.0	0.0	-20270.2	0.0	
0.	-954.3	7.5	-57.1	0.0	-283.6	-37.5	88.	106.7	-438.8	9.1	26.0	254.2	11736.1	PROGR.	136	749	469	MY	NZZ	469	115.	2.6	0.0	0.0	0.0	-2162.6	0.0	
1.	-954.2	7.5	-57.1	0.0	-249.9	-32.8	105.	106.7	-499.6	9.1	26.0	34.6	3545.3	0.	-142.9	240.9	0.0	0.0	-5.8	5573.8	144.	2.6	94.0	0.0	0.0	-20270.2	0.0	
1.	-954.1	7.5	-57.1	0.0	-214.2	-28.1	123.	106.7	-560.4	9.1	26.0	-65.0	-5730.1	29.	142.9	146.9	0.0	0.0	-11.5	8444.8	173.	2.6	188.0	0.0	0.0	-16216.2	0.0	
2.	-953.9	7.5	-57.1	0.0	-178.5	-23.4	140.	106.7	-631.3	9.1	26.0	-224.6	-16007.1	0.	142.9	146.9	0.0	0.0	-11.5	8444.8	201.	2.6	282.0	0.0	0.0	-949.4	0.0	
3.	-953.8	7.5	-57.1	0.0	-142.8	-18.7	Asta	120	745	746	MY	NZZ	746	86.	142.9	-41.1	0.2	0.0	-17.3	8613.2	230.	2.6	376.0	0.0	0.0	0.0	0.0	
4.	-953.5	7.5	-57.1	0.0	-71.4	-9.4	PROGR.	120	745	746	MY	NZZ	746	115.	142.9	-135.2	0.2	0.0	-23.0	1616.8	PROGR.	120	745	746	MY	NZZ	746	
4.	-953.4	7.5	-57.1	0.0	-35.7	-4.7	0.	-229.4	-278.1	1.1	-659.0	0.0	604.7	144.	142.9	-229.2	0.2	0.0	-28.8	841.8	PROGR.	120	745	746	MY	NZZ	746	
Asta	104	746	747	MY	NZZ	747	16.	-229.4	-285.0	1.1	-659.0	-17.2	-3971.0	173.	142.9	-323.2	0.2	0.0	-34.6	-7029.9	0.	-25.2	305.7	0.2	0.0	0.0	0.0	
PROGR.	104	746	747	MY	NZZ	747	33.	-229.4	-292.0	1.1	-659.0	-34.5	-8659.3	201.	142.9	-417.2	0.2	0.0	-40.3	-17449.3	29.	-25.2	711.7	0.2	0.0	-4.9	7486.3	
0.	-790.0	-30.8	1698.2	0.0	8490.9	153.8	49.	-229.4	-298.9	1.1	-659.0	-51.7	-13460.2	230.	142.9	-511.2	0.2	0.0	-46.1	-13085.4	58.	-25.2	117.6	0.2	0.0	-9.9	12170.0	
1.	-790.0	-30.8	1698.2	0.0	8490.9	153.8	81.	-229.4	-312.8	1.1	-659.0	-86.2	-23399.5	PROGR.	137	753	754	MY	NZZ	754	86.	-25.2	23.6	0.0	0.0	-14.8	14200.9	
2.	-789.9	-30.8	1698.2	0.0	8490.9	153.8	98.	-229.4	-319.7	1.1	-659.0	-103.4	-28338.1	0.	-6.8	352.1	-1.9	-4.6	-220.0	-8487.8	115.	-25.2	-70.4	0.2	0.0	-19.7	13529.2	
3.	-789.8	-30.8	1698.2	0.0	8490.9	153.8	115.	-229.4	-318.6	1.1	-659.0	-124.6	-33316.1	PROGR.	137	753	754	MY	NZZ	754	144.	-25.2	-164.4	0.2	0.0	-24.7	10154.7	
3.	-789.5	-30.8	1698.2	0.0	8490.9	153.8	130.	-229.4	-333.5	1.1	-659.0	-137.9	-39152.8	0.	-6.8	352.1	-1.9	-4.6	-220.0	-8487.8	173.	-25.2	-164.4	0.2	0.0	-24.7	10154.7	
Asta	121	747	747	MY	NZZ	747	Asta	121	747	747	MY	NZZ	747	58.	-6.8	164.1	-1.9	-4.6	-100.4	6315.6	201.	-25.2	-352.4	0.2	0.0	-34.6	-4702.2	
PROGR.	121	747	747	MY	NZZ	747	0.	-90.6	412.8	-7.6	-75.0	-97.9	-3539.9	115.	-6.8	-23.9	-1.9	-4.6	-1.2	10380.2	Asta	157	747	747	MY	NZZ	747	
0.	-789.3	-30.8	1698.2	0.0	8490.9	153.8	0.	-90.6	412.8	-7.6	-75.0	-97.9	-3539.9	144.	-6.8	-118.0	-1.9	-4.6	85.5	6340.5	PROGR.	157	747	747	MY	NZZ	747	
1.	-789.2	-30.8	1698.2	0.0	8490.9	153.8	33.	-90.6	398.9	-7.6	-75.0	167.1	-22200.0	173.	-6.8	-232.0	-1.9	-4.6	111.6	5208.4	0.	500.2	-1.0	3.5	-60.8	-40038.9		
5.	-789.1	-30.8	1698.2	0.0	8490.9	153.8	65.	-90.6	385.0	-7.6	-75.0	167.1	-22200.0	201.	-6.8	-306.0	-1.9	-4.6	167.1	-3847.1	16.	0.0	492.2	-1.0	3.5	-44.5	-31867.8	
Asta	106	746	746	MY	NZZ	746	88.	-90.6	362.0	-7.6	-75.0	167.1	-22200.0	PROGR.	106	746	746	MY	NZZ	746	81.	0.0	465.5	-1.0	3.5	-20.9	-908.7	
PROGR.	106	746	746	MY	NZZ	746	81.	-90.6	378.1	-7.6	-75.0	167.1	-22200.0	0.	-17.3	376.0	0.0	0.0	0.0	0.0	49.	0.0	479.4	-1.0	3.5	-11.8	-16163.1	
0.	-1311.1	218.9	-5793.2	0.0	-2896.8	-109.7	114.	-90.6	364.3	-7.6	-75.0	167.1	-22200.0	Asta	138	746	746	MY	NZZ	746	65.	0.0	472.4	-1.0	3.5	-4.6	-6429.6	
1.	-1311.0	218.9	-5793.2	0.0	-2896.8	-109.7	130.	-90.6	364.3	-7.6	-75.0	167.1	-22200.0	PROGR.	138	746	746	MY	NZZ	746	81.	0.0	465.5	-1.0	3.5	-20.9	-908.7	
2.	-1310.9	218.9	-5793.2	0.0	-2896.8	-109.7	Asta	122	748	737	MY	NZZ	737	29.	-17.3	282.0	0.0	0.0	0.0	9459.3	130.	0.0	458.6	-1.0	3.5	37.2	6699.7	
3.	-1310.8	218.9	-5793.2	0.0	-2896.8	-109.7	PROGR.	122	748	737	MY	NZZ	737	86.	-17.3	94.0	0.0	0.0	-0.1	10209.9	PROGR.	122	748	737	MY	NZZ	737	
4.	-1310.7	218.9	-5793.2	0.0	-2896.8	-109.7	0.	-17.3	94.0	0.0	0.0	-0.1	10209.9	144.	-17.3	-94.0	0.0	0.0	-0.2	10209.9	0.	-7.8	-240.7	2.5	12.5	0.0	39.2	
5.	-1310.6	218.9	-5793.2	0.0	-2896.8	-109.7	18.	3.4	115.4	8.1	3.4	908.1	14396.7	PROGR.	144	-17.3	-94.0	0.0	0.0	-0.2	10209.9	1.	-7.8	-240.7	2.5	12.5	0.0	39.2
Asta	106	746	746	MY	NZZ	746	35.	3.4	163.3	8.1	3.4	625.5	16395.3	0.	-17.3	-376.0	0.0	0.0	-0.3	-0.8	13.	-7.8	-240.7	2.5	12.5	0.0	39.2	
PROGR.	106	746	746	MY	NZZ	746	53.	3.4	-67.1	8.1	3.4	484.1	15662.7	230.	-17.3	-376.0	0.0	0.0	-0.3	-0.8	33.	-7.8	-240.7	2.5	12.5	0.0	39.2	
0.	-3129.5	-227.9	2975.2	0.0	14875.8	1139.4	88.	3.4	-388.8	8.1	3.4	201.5	111															

PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-125.8	0.0	0.0	0.0	0.0	0.0
34.	-125.8	0.0	0.0	0.0	0.0	0.0
67.	-125.8	0.0	0.0	0.0	0.0	0.0
101.	-125.8	0.0	0.0	0.0	0.0	0.0
135.	-125.8	0.0	0.0	0.0	0.0	0.0
168.	-125.8	0.0	0.0	0.0	0.0	0.0
202.	-125.8	0.0	0.0	0.0	0.0	0.0
236.	-125.8	0.0	0.0	0.0	0.0	0.0
269.	-125.8	0.0	0.0	0.0	0.0	0.0
Asta	168	noth	753	953		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	19.4	0.0	0.0	0.0	0.0	0.0
51.	19.4	0.0	0.0	0.0	0.0	0.0
103.	19.4	0.0	0.0	0.0	0.0	0.0
154.	19.4	0.0	0.0	0.0	0.0	0.0
205.	19.4	0.0	0.0	0.0	0.0	0.0
257.	19.4	0.0	0.0	0.0	0.0	0.0
308.	19.4	0.0	0.0	0.0	0.0	0.0
359.	19.4	0.0	0.0	0.0	0.0	0.0
410.	19.4	0.0	0.0	0.0	0.0	0.0
Asta	169	noth	741	754		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	142.5	0.0	0.0	0.0	0.0	0.0
51.	142.5	0.0	0.0	0.0	0.0	0.0
102.	142.5	0.0	0.0	0.0	0.0	0.0
152.	142.5	0.0	0.0	0.0	0.0	0.0
203.	142.5	0.0	0.0	0.0	0.0	0.0
254.	142.5	0.0	0.0	0.0	0.0	0.0
305.	142.5	0.0	0.0	0.0	0.0	0.0
356.	142.5	0.0	0.0	0.0	0.0	0.0
406.	142.5	0.0	0.0	0.0	0.0	0.0
Asta	170	noth	740	953		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-553.3	10.5	1202.5	0.0	6012.6	-52.7
1.	-553.2	10.5	1202.5	0.0	5261.0	-46.1
2.	-553.1	10.5	1202.5	0.0	4509.4	-39.6
3.	-552.9	10.5	1202.5	0.0	3757.9	-33.0
4.	-552.8	10.5	1202.5	0.0	3006.3	-26.4
5.	-552.7	10.5	1202.5	0.0	2254.7	-19.8
6.	-552.5	10.5	1202.5	0.0	1503.1	-13.2
7.	-552.4	10.5	1202.5	0.0	751.6	-6.6
8.	-552.2	10.5	1202.5	0.0	0.0	0.0
Asta	171	noth	738	975		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-377.1	-17.3	0.0	0.0	0.0	86.6
1.	-377.0	-17.3	0.0	0.0	0.0	75.7
2.	-376.8	-17.3	0.0	0.0	0.0	64.9
3.	-376.7	-17.3	0.0	0.0	0.0	54.1
4.	-376.6	-17.3	0.0	0.0	0.0	43.3
5.	-376.4	-17.3	0.0	0.0	0.0	32.5
6.	-376.3	-17.3	0.0	0.0	0.0	21.6
7.	-376.2	-17.3	0.0	0.0	0.0	10.8
8.	-376.0	-17.3	0.0	0.0	0.0	0.0
Asta	172	noth	40	978		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-10163.7	-888.8	-17.5	0.0	-6752.6	103550.9
15.	-10070.0	-888.8	-17.5	0.0	-6489.1	90218.3
30.	-9976.2	-888.8	-17.5	0.0	-6226.3	76885.8
45.	-9882.5	-888.8	-17.5	0.0	-5963.4	63553.2
60.	-9788.7	-888.8	-17.5	0.0	-5700.6	50220.7
75.	-9695.0	-888.8	-17.5	0.0	-5437.7	36888.1
90.	-9601.2	-888.8	-17.5	0.0	-5174.9	23555.6
105.	-9507.5	-888.8	-17.5	0.0	-4912.0	10223.0
120.	-9413.7	-888.8	-17.5	0.0	-4649.1	-3109.5
Asta	173	noth	954	37		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-8791.4	26.8	-41.2	0.0	-13995.1	-375.7
15.	-8697.6	26.8	-41.2	0.0	-13352.9	-339.8
30.	-8603.9	26.8	-41.2	0.0	-12710.6	-299.9
45.	-8510.1	26.8	-41.2	0.0	-12068.3	-260.0
60.	-8416.4	26.8	-41.2	0.0	-11426.0	-218.0
75.	-8322.6	26.8	-41.2	0.0	-10783.8	-176.1
90.	-8228.9	26.8	-41.2	0.0	-10141.5	-134.2
105.	-8135.1	26.8	-41.2	0.0	-9499.2	-92.3
120.	-8041.4	26.8	-41.2	0.0	-8856.9	-50.4
Asta	174	noth	958	734		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-4015.0	703.6	-67.5	0.0	-15330.2	-8302.4
15.	-3921.2	703.6	-67.5	0.0	-14317.6	-7247.9
30.	-3827.5	703.6	-67.5	0.0	-13305.1	-6193.4
45.	-3733.7	703.6	-67.5	0.0	-12292.5	-5137.9
60.	-3640.0	703.6	-67.5	0.0	-11279.9	-4083.4
75.	-3546.2	703.6	-67.5	0.0	-10267.4	-3028.9
90.	-3452.5	703.6	-67.5	0.0	-9254.8	-1971.4
105.	-3358.7	703.6	-67.5	0.0	-8242.2	-917.9
120.	-3265.0	703.6	-67.5	0.0	-7229.7	1395.5
Asta	175	noth	960	741		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-2546.8	460.8	-138.5	0.0	-24959.2	-5642.5
15.	-2453.0	460.8	-138.5	0.0	-22881.7	-4953.1
30.	-2359.3	460.8	-138.5	0.0	-20804.2	-4263.7
45.	-2265.5	460.8	-138.5	0.0	-18726.7	-3573.3
60.	-2171.8	460.8	-138.5	0.0	-16649.2	-2876.9
75.	-2078.0	460.8	-138.5	0.0	-14571.7	-2180.5
90.	-1984.3	460.8	-138.5	0.0	-12494.3	-1484.1
105.	-1890.5	460.8	-138.5	0.0	-10416.8	-802.7
120.	-1796.8	460.8	-138.5	0.0	-8339.3	-113.3
Asta	176	noth	959	742		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-2664.6	-317.1	6.9	0.0	-16951.0	3023.6
15.	-2570.8	-317.1	6.9	0.0	-17054.7	2546.0
30.	-2477.1	-317.1	6.9	0.0	-17158.4	2070.5
45.	-2383.3	-317.1	6.9	0.0	-17262.1	1594.0
60.	-2289.6	-317.1	6.9	0.0	-17365.8	1117.5
75.	-2195.8	-317.1	6.9	0.0	-17469.4	641.0
90.	-2102.1	-317.1	6.9	0.0	-17573.1	168.4
105.	-2008.3	-317.1	6.9	0.0	-17676.8	-307.1
120.	-1914.6	-317.1	6.9	0.0	-17780.5	-782.6
Asta	178	noth	37	19		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	0.0	380.1	0.6	-1421.6	20.0	-3827.8
1.	0.0	380.6	0.6	-1421.6	19.2	-3351.7
3.	0.0	380.1	0.6	-1421.6	18.5	-2876.6
4.	0.0	379.5	0.6	-1421.6	17.7	-2401.6
5.	0.0	379.0	0.6	-1421.6	16.9	-1927.5
6.	0.0	378.5	0.6	-1421.6	16.2	-1454.4
7.	0.0	377.9	0.6	-1421.6	15.4	-981.4
8.	0.0	377.4	0.6	-1421.6	14.6	-509.3
9.	0.0	376.9	0.6	-1421.6	13.8	-37.9
10.	0.0	376.4	0.6	-1421.6	13.0	95.5
Asta	181	noth	957	28		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-540.5	14.8	257.8	0.0	30940.0	-1778.1
15.	-540.5	14.8	257.8	0.0	2707.5	-155.8
30.	-540.5	14.8	257.8	0.0	2320.0	-133.5
45.	-540.5	14.8	257.8	0.0	1932.5	-111.1
60.	-540.5	14.8	257.8	0.0	1545.0	-88.9
75.	-540.5	14.8	257.8	0.0	1157.5	-66.6
90.	-540.5	14.8	257.8	0.0	770.0	-44.4
105.	-540.5	14.8	257.8	0.0	382.5	-22.2
120.	-540.5	14.8	257.8	0.0	0.0	0.0

[illegible]

COLLETTAZIONE		COSTI RETTANGOLARI		CONFEZIONE			
misura		9 Forcente_add_Y		9 Forcente_add_Y			
misura		9 Forcente_add_Y		9 Forcente_add_Y			
9	415	55	=	0	51	=	0
9	416	55	=	0	51	=	0
9	417	55	=	0	51	=	0
9	418	55	=	0	51	=	0
9	419	55	=	0	51	=	0
9	420	55	=	0	51	=	0
9	421	55	=	0	51	=	0
9	422	55	=	0	51	=	0
9	423	55	=	0	51	=	0
9	424	55	=	0	51	=	0
9	425	55	=	0	51	=	0
9	426	55	=	0	51	=	0
9	427	55	=	0	51	=	0
9	428	55	=	0	51	=	0
9	429	55	=	0	51	=	0
9	430	55	=	0	51	=	0
9	431	55	=	0	51	=	0
9	432	55	=	0	51	=	0
9	433	55	=	0	51	=	0
9	434	55	=	0	51	=	0
9	435	55	=	0	51	=	0
9	436	55	=	0	51	=	0
9	437	55	=	0	51	=	0
9	438	55	=	0	51	=	0
9	439	55	=	0	51	=	0
9	440	55	=	0	51	=	0
9	441	55	=	0	51	=	0
9	442	55	=	0	51	=	0
9	443	55	=	0	51	=	0
9	444	55	=	0	51	=	0
9	445	55	=	0	51	=	0
9	446	55	=	0	51	=	0
9	447	55	=	0	51	=	0
9	448	55	=	0	51	=	0
9	449	55	=	0	51	=	0
9	450	55	=	0	51	=	0
9	451	55	=	0	51	=	0
9	452	55	=	0	51	=	0
9	453	55	=	0	51	=	0
9	454	55	=	0	51	=	0
9	455	55	=	0	51	=	0

COMBINAZIONE

93/136

GUSCIO	454	SS =	11.1	SI =	11.1
GUSCIO	455	SS =	10.9	SI =	10.9
GUSCIO	456	SS =	12.8	SI =	12.8
GUSCIO	457	SS =	4.6	SI =	4.6
GUSCIO	458	SS =	5.8	SI =	5.8
GUSCIO	459	SS =	5.4	SI =	5.4
GUSCIO	460	SS =	4.1	SI =	4.1
GUSCIO	461	SS =	3.1	SI =	3.1
GUSCIO	462	SS =	6.5	SI =	6.5
GUSCIO	463	SS =	5.1	SI =	5.1
GUSCIO	464	SS =	3.8	SI =	3.8
GUSCIO	465	SS =	4.2	SI =	4.2
GUSCIO	466	SS =	3.7	SI =	3.7
GUSCIO	467	SS =	3.5	SI =	3.5
GUSCIO	468	SS =	4.5	SI =	4.5
GUSCIO	469	SS =	4.0	SI =	4.0
GUSCIO	470	SS =	4.1	SI =	4.1
GUSCIO	471	SS =	3.5	SI =	3.5
GUSCIO	472	SS =	4.4	SI =	4.4
GUSCIO	473	SS =	4.3	SI =	4.3
GUSCIO	474	SS =	4.2	SI =	4.2
GUSCIO	475	SS =	2.8	SI =	2.8
GUSCIO	476	SS =	4.1	SI =	4.1
GUSCIO	477	SS =	3.1	SI =	3.1
GUSCIO	478	SS =	2.9	SI =	2.9
GUSCIO	479	SS =	1.2	SI =	1.2
GUSCIO	480	SS =	2.9	SI =	2.9
GUSCIO	481	SS =	1.2	SI =	1.2
GUSCIO	482	SS =	5.7	SI =	5.7
GUSCIO	483	SS =	4.7	SI =	4.7
GUSCIO	484	SS =	3.7	SI =	3.7
GUSCIO	485	SS =	4.9	SI =	4.9
GUSCIO	486	SS =	4.3	SI =	4.3
GUSCIO	487	SS =	6.2	SI =	6.2
GUSCIO	488	SS =	2.2	SI =	2.2
GUSCIO	489	SS =	6.8	SI =	6.8
GUSCIO	490	SS =	21.7	SI =	21.7
GUSCIO	491	SS =	19.4	SI =	19.4
GUSCIO	492	SS =	6.0	SI =	6.0
GUSCIO	493	SS =	7.3	SI =	7.3
GUSCIO	494	SS =	1.4	SI =	1.4
GUSCIO	495	SS =	6.0	SI =	6.0
GUSCIO	496	SS =	17.3	SI =	17.3
GUSCIO	497	SS =	11.3	SI =	11.3
GUSCIO	498	SS =	2.5	SI =	2.5
GUSCIO	499	SS =	4.8	SI =	4.8
tensione max =		21.7	guscio =	490	

SOLLECITAZIONE GUSCI RETTANGOLARE
CASO DI CARICO : 3 SLU VENTOF

N. 5 CONDIZIONI ANALISI STATICA
1 peso proprio + 1.30
2 permanenti + 1.50
3 A'var. abitazione + 1.50
4 neve (<1000h/m) + 1.50
5 vento + 1.50

1) +1.30*c001 +1.50*c002 +1.50*c003 +1.50*c004 +1.50*c005
2) +1.30*c001 +1.50*c002 +1.50*c003 +1.50*c004 -1.50*c005
unità di misura: SI,SS [daN/cm2]

GUSCIO	415	SS =	3.5	SI =	3.5
		SS =	2.9	SI =	2.9
GUSCIO	416	SS =	2.6	SI =	2.6
		SS =	1.9	SI =	1.9
GUSCIO	417	SS =	9.5	SI =	9.5
		SS =	7.6	SI =	7.6
GUSCIO	418	SS =	9.6	SI =	9.6
		SS =	8.0	SI =	8.0
GUSCIO	419	SS =	24.2	SI =	24.2
		SS =	19.0	SI =	19.0
GUSCIO	420	SS =	17.6	SI =	17.6
		SS =	16.6	SI =	16.6
GUSCIO	421	SS =	18.2	SI =	18.2
		SS =	22.2	SI =	22.2
GUSCIO	422	SS =	16.6	SI =	16.6

COMBINAZIONE

		SS =	17.1	SI =	17.1
GUSCIO	423	SS =	6.9	SI =	6.9
		SS =	8.4	SI =	8.4
GUSCIO	424	SS =	7.5	SI =	7.5
		SS =	8.7	SI =	8.7
GUSCIO	425	SS =	2.4	SI =	2.4
		SS =	3.1	SI =	3.1
GUSCIO	426	SS =	1.6	SI =	1.6
		SS =	2.0	SI =	2.0
GUSCIO	427	SS =	6.6	SI =	6.6
		SS =	5.7	SI =	5.7
GUSCIO	428	SS =	8.1	SI =	8.1
		SS =	7.1	SI =	7.1
GUSCIO	429	SS =	4.7	SI =	4.7
		SS =	4.4	SI =	4.4
GUSCIO	430	SS =	10.9	SI =	10.9
		SS =	9.3	SI =	9.3
GUSCIO	431	SS =	11.8	SI =	11.8
		SS =	10.2	SI =	10.2
GUSCIO	432	SS =	9.9	SI =	9.9
		SS =	9.0	SI =	9.0
GUSCIO	433	SS =	15.5	SI =	15.5
		SS =	13.5	SI =	13.5
GUSCIO	434	SS =	15.1	SI =	15.1
		SS =	13.7	SI =	13.7
GUSCIO	435	SS =	22.4	SI =	22.4
		SS =	17.6	SI =	17.6
GUSCIO	436	SS =	14.3	SI =	14.3
		SS =	13.2	SI =	13.2
GUSCIO	437	SS =	14.6	SI =	14.6
		SS =	13.6	SI =	13.6
GUSCIO	438	SS =	17.6	SI =	17.6
		SS =	20.6	SI =	20.6
GUSCIO	439	SS =	8.8	SI =	8.8
		SS =	8.2	SI =	8.2
GUSCIO	440	SS =	10.4	SI =	10.4
		SS =	10.5	SI =	10.5
GUSCIO	441	SS =	9.2	SI =	9.2
		SS =	9.8	SI =	9.8
GUSCIO	442	SS =	5.4	SI =	5.4
		SS =	6.8	SI =	6.8
GUSCIO	443	SS =	7.3	SI =	7.3
		SS =	7.9	SI =	7.9
GUSCIO	444	SS =	4.6	SI =	4.6
		SS =	5.3	SI =	5.3
GUSCIO	445	SS =	3.7	SI =	3.7
		SS =	2.2	SI =	2.2
GUSCIO	446	SS =	5.3	SI =	5.3
		SS =	3.4	SI =	3.4
GUSCIO	447	SS =	4.0	SI =	4.0
		SS =	3.0	SI =	3.0
GUSCIO	448	SS =	7.9	SI =	7.9
		SS =	5.1	SI =	5.1
GUSCIO	449	SS =	9.3	SI =	9.3
		SS =	6.4	SI =	6.4
GUSCIO	450	SS =	9.0	SI =	9.0
		SS =	6.6	SI =	6.6
GUSCIO	451	SS =	17.1	SI =	17.1
		SS =	10.5	SI =	10.5
GUSCIO	452	SS =	12.8	SI =	12.8
		SS =	10.3	SI =	10.3
GUSCIO	453	SS =	19.6	SI =	19.6
		SS =	11.9	SI =	11.9
GUSCIO	454	SS =	11.4	SI =	11.4
		SS =	12.1	SI =	12.1
GUSCIO	455	SS =	11.8	SI =	11.8
		SS =	10.0	SI =	10.0
GUSCIO	456	SS =	12.2	SI =	12.2

		SS =	13.9	SI =	13.9
GUSCIO	457	SS =	4.2	SI =	4.2
		SS =	5.0	SI =	5.0
GUSCIO	458	SS =	5.7	SI =	5.7
		SS =	5.9	SI =	5.9
GUSCIO	459	SS =	5.4	SI =	5.4
		SS =	5.4	SI =	5.4
GUSCIO	460	SS =	3.7	SI =	3.7
		SS =	4.5	SI =	4.5
GUSCIO	461	SS =	3.0	SI =	3.0
		SS =	3.5	SI =	3.5
GUSCIO	462	SS =	3.8	SI =	3.8
		SS =	9.5	SI =	9.5
GUSCIO	463	SS =	4.1	SI =	4.1
		SS =	6.2	SI =	6.2
GUSCIO	464	SS =	3.3	SI =	3.3
		SS =	4.5	SI =	4.5
GUSCIO	465	SS =	5.4	SI =	5.4
		SS =	3.9	SI =	3.9
GUSCIO	466	SS =	2.7	SI =	2.7
		SS =	5.6	SI =	5.6
GUSCIO	467	SS =	3.1	SI =	3.1
		SS =	4.3	SI =	4.3
GUSCIO	468	SS =	3.3	SI =	3.3
		SS =	5.7	SI =	5.7
GUSCIO	469	SS =	6.3	SI =	6.3
		SS =	4.2	SI =	4.2
GUSCIO	470	SS =	3.5	SI =	3.5
		SS =	4.8	SI =	4.8
GUSCIO	471	SS =	4.1	SI =	4.1
		SS =	3.8	SI =	3.8
GUSCIO	472	SS =	3.6	SI =	3.6
		SS =	5.5	SI =	5.5
GUSCIO	473	SS =	3.6	SI =	3.6
		SS =	5.2	SI =	5.2
GUSCIO	474	SS =	3.4	SI =	3.4
		SS =	5.1	SI =	5.1
GUSCIO	475	SS =	1.9	SI =	1.9
		SS =	3.9	SI =	3.9
GUSCIO	476	SS =	2.9	SI =	2.9
		SS =	5.4	SI =	5.4
GUSCIO	477	SS =	2.1	SI =	2.1
		SS =	4.1	SI =	4.1
GUSCIO	478	SS =	1.9	SI =	1.9
		SS =	4.8	SI =	4.8
GUSCIO	479	SS =	0.4	SI =	0.4
		SS =	2.1	SI =	2.1
GUSCIO	480	SS =	2.1	SI =	2.1
		SS =	5.8	SI =	5.8
GUSCIO	481	SS =	1.2	SI =	1.2
		SS =	1.9	SI =	1.9
GUSCIO	482	SS =	6.4	SI =	6.4
		SS =	6.9	SI =	6.9
GUSCIO	483	SS =	4.0	SI =	4.0
		SS =	5.4	SI =	5.4
GUSCIO	484	SS =	5.7	SI =	5.7
		SS =	3.0	SI =	3.0
GUSCIO	485	SS =	4.2	SI =	4.2
		SS =	6.2	SI =	6.2
GUSCIO	486	SS =	2.9	SI =	2.9
		SS =	5.8	SI =	5.8
GUSCIO	487	SS =	10.3	SI =	10.3
		SS =	2.7	SI =	2.7
GUSCIO	488	SS =	2.9	SI =	2.9
		SS =	1.4	SI =	1.4
GUSCIO	489	SS =	8.2	SI =	8.2
		SS =	5.4	SI =	5.4
GUSCIO	490	SS =	26.0	SI =	26.0
		SS =	17.8	SI =	17.8

GUSCIO	491	SS =	19.3	SI =	19.3
		SS =	20.3	SI =	20.3
GUSCIO	492	SS =	6.1	SI =	6.1
		SS =	5.8	SI =	5.8
GUSCIO	493	SS =	3.8	SI =	3.8
		SS =	11.6	SI =	11.6
GUSCIO	494	SS =	1.9	SI =	1.9
		SS =	1.0	SI =	1.0
GUSCIO	495	SS =	8.3	SI =	8.3
		SS =	3.6	SI =	3.6
GUSCIO	496	SS =	24.7	SI =	24.7
		SS =	9.9	SI =	9.9
GUSCIO	497	SS =	6.1	SI =	6.1
		SS =	16.7	SI =	16.7
GUSCIO	498	SS =	2.6	SI =	2.6
		SS =	4.2	SI =	4.2
GUSCIO	499	SS =	4.2	SI =	4.2
		SS =	5.5	SI =	5.5
tensione max =		26.0	guscio =	490	

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 4 SISMAX SLU

N. 2 CONDIZIONI ANALISI STATICA
6 SISMAX + 1.00
8 Torcente_add_X + 1.00
1) +1.00*c006 +1.00*c008
2) -1.00*c006 +1.00*c008
3) +1.00*c006 -1.00*c008
4) -1.00*c006 -1.00*c008
unità di misura: SI,SS [daN/cm2]

GUSCIO	415	SS =	0.4	SI =	0.4
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.4	SI =	0.4
GUSCIO	416	SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
GUSCIO	417	SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
GUSCIO	418	SS =	0.6	SI =	0.6
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.6	SI =	0.6
GUSCIO	419	SS =	2.5	SI =	2.5
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.5	SI =	2.5
GUSCIO	420	SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
GUSCIO	421	SS =	2.7	SI =	2.7
		SS =	3.1	SI =	3.1
		SS =	3.1	SI =	3.1
		SS =	2.7	SI =	2.7
GUSCIO	422	SS =	1.9	SI =	1.9
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	1.9	SI =	1.9
GUSCIO	423	SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
GUSCIO	424	SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.6	SI =	0.6
GUSCIO	425	SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6

QJSCIO 426 SS = 0.6 SI = 0.6
SS = 0.3 SI = 0.3
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.3 SI = 0.3
QJSCIO 427 SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
QJSCIO 428 SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
QJSCIO 429 SS = 0.7 SI = 0.7
SS = 0.8 SI = 0.8
SS = 0.8 SI = 0.8
SS = 0.7 SI = 0.7
QJSCIO 430 SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
QJSCIO 431 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 432 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 433 SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.1 SI = 1.1
QJSCIO 434 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 435 SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
QJSCIO 436 SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
QJSCIO 437 SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
QJSCIO 438 SS = 2.0 SI = 2.0
SS = 2.3 SI = 2.3
SS = 2.3 SI = 2.3
SS = 2.0 SI = 2.0
QJSCIO 439 SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
QJSCIO 440 SS = 1.2 SI = 1.2
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
QJSCIO 441 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
QJSCIO 442 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2

QJSCIO 443 SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
QJSCIO 444 SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
QJSCIO 445 SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
QJSCIO 446 SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
QJSCIO 447 SS = 1.4 SI = 1.4
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.4 SI = 1.4
QJSCIO 448 SS = 1.4 SI = 1.4
SS = 1.5 SI = 1.5
SS = 1.5 SI = 1.5
SS = 1.4 SI = 1.4
QJSCIO 449 SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
QJSCIO 450 SS = 1.7 SI = 1.7
SS = 2.0 SI = 2.0
SS = 2.0 SI = 2.0
SS = 1.7 SI = 1.7
QJSCIO 451 SS = 3.4 SI = 3.4
SS = 3.7 SI = 3.7
SS = 3.7 SI = 3.7
SS = 3.4 SI = 3.4
QJSCIO 452 SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
QJSCIO 453 SS = 3.5 SI = 3.5
SS = 3.8 SI = 3.8
SS = 3.8 SI = 3.8
SS = 3.5 SI = 3.5
QJSCIO 454 SS = 2.7 SI = 2.7
SS = 3.2 SI = 3.2
SS = 3.2 SI = 3.2
SS = 2.7 SI = 2.7
QJSCIO 455 SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.2 SI = 1.2
QJSCIO 456 SS = 3.1 SI = 3.1
SS = 3.5 SI = 3.5
SS = 3.5 SI = 3.5
SS = 3.1 SI = 3.1
QJSCIO 457 SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.1 SI = 1.1
QJSCIO 458 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
QJSCIO 459 SS = 1.7 SI = 1.7
SS = 1.9 SI = 1.9
SS = 1.9 SI = 1.9
SS = 1.7 SI = 1.7

QJSCIO 460 SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
QJSCIO 461 SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
QJSCIO 462 SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
QJSCIO 463 SS = 1.3 SI = 1.3
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.3 SI = 1.3
QJSCIO 464 SS = 1.4 SI = 1.4
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.4 SI = 1.4
QJSCIO 465 SS = 1.7 SI = 1.7
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.7 SI = 1.7
QJSCIO 466 SS = 1.5 SI = 1.5
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.5 SI = 1.5
QJSCIO 467 SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
QJSCIO 468 SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
QJSCIO 469 SS = 2.1 SI = 2.1
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 2.1 SI = 2.1
QJSCIO 470 SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
QJSCIO 471 SS = 1.9 SI = 1.9
SS = 1.5 SI = 1.5
SS = 1.5 SI = 1.5
SS = 1.9 SI = 1.9
QJSCIO 472 SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
QJSCIO 473 SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
QJSCIO 474 SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
QJSCIO 475 SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
QJSCIO 476 SS = 0.4 SI = 0.4
SS = 0.5 SI = 0.5
SS = 0.5 SI = 0.5
SS = 0.4 SI = 0.4

QJSCIO 477 SS = 0.6 SI = 0.6
SS = 0.5 SI = 0.5
SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
QJSCIO 478 SS = 1.3 SI = 1.3
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.3 SI = 1.3
QJSCIO 479 SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
QJSCIO 480 SS = 1.4 SI = 1.4
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.4 SI = 1.4
QJSCIO 481 SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
QJSCIO 482 SS = 2.8 SI = 2.8
SS = 2.0 SI = 2.0
SS = 2.0 SI = 2.0
SS = 2.8 SI = 2.8
QJSCIO 483 SS = 1.0 SI = 1.0
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 1.0 SI = 1.0
QJSCIO 484 SS = 2.0 SI = 2.0
SS = 1.4 SI = 1.4
SS = 1.4 SI = 1.4
SS = 2.0 SI = 2.0
QJSCIO 485 SS = 1.3 SI = 1.3
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.3 SI = 1.3
QJSCIO 486 SS = 1.7 SI = 1.7
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.7 SI = 1.7
QJSCIO 487 SS = 2.5 SI = 2.5
SS = 1.7 SI = 1.7
SS = 1.7 SI = 1.7
SS = 2.5 SI = 2.5
QJSCIO 488 SS = 1.5 SI = 1.5
SS = 1.8 SI = 1.8
SS = 1.8 SI = 1.8
SS = 1.5 SI = 1.5
QJSCIO 489 SS = 1.9 SI = 1.9
SS = 2.1 SI = 2.1
SS = 2.1 SI = 2.1
SS = 1.9 SI = 1.9
QJSCIO 490 SS = 2.5 SI = 2.5
SS = 2.6 SI = 2.6
SS = 2.6 SI = 2.6
SS = 2.5 SI = 2.5
QJSCIO 491 SS = 1.8 SI = 1.8
SS = 1.9 SI = 1.9
SS = 1.9 SI = 1.9
SS = 1.8 SI = 1.8
QJSCIO 492 SS = 0.9 SI = 0.9
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 0.9 SI = 0.9
QJSCIO 493 SS = 2.4 SI = 2.4
SS = 1.8 SI = 1.8
SS = 1.8 SI = 1.8
SS = 2.4 SI = 2.4
QJSCIO 494 SS = 0.9 SI = 0.9

		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
QUSC10	495	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.2	SI =	2.2
QUSC10	496	SS =	3.5	SI =	3.5
		SS =	4.0	SI =	4.0
		SS =	4.0	SI =	4.0
		SS =	3.5	SI =	3.5
QUSC10	497	SS =	2.8	SI =	2.8
		SS =	3.2	SI =	3.2
		SS =	3.2	SI =	3.2
		SS =	2.8	SI =	2.8
QUSC10	498	SS =	1.4	SI =	1.4
		SS =	1.9	SI =	1.9
		SS =	1.9	SI =	1.9
		SS =	1.4	SI =	1.4
QUSC10	499	SS =	0.9	SI =	0.9
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.9	SI =	0.9
		SS =	4.0	SI =	4.0
tensione max =					
caso di carico : 5 S15WY SLU					
N. 2 CONDIZIONI ANALISI STATICA					
7 S15WY SLU					
9 Torcente_add_Y					
1) +1.00e+007 +1.00e+009					
2) -1.00e+007 +1.00e+009					
3) +1.00e+007 -1.00e+009					
4) -1.00e+007 -1.00e+009					
Unità di misura: SI,SS [daN/cm2]					
QUSC10	415	SS =	0.5	SI =	0.5
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.5	SI =	0.5
QUSC10	416	SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
QUSC10	417	SS =	1.1	SI =	1.1
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.1	SI =	1.1
QUSC10	418	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
QUSC10	419	SS =	3.5	SI =	3.5
		SS =	3.3	SI =	3.3
		SS =	3.3	SI =	3.3
		SS =	3.5	SI =	3.5
QUSC10	420	SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
QUSC10	421	SS =	3.4	SI =	3.4
		SS =	3.1	SI =	3.1
		SS =	3.1	SI =	3.1
		SS =	3.4	SI =	3.4
QUSC10	422	SS =	1.1	SI =	1.1
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.1	SI =	1.1
QUSC10	423	SS =	1.0	SI =	1.0
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	1.0	SI =	1.0
QUSC10	424	SS =	0.8	SI =	0.8
		SS =	0.6	SI =	0.6

COMBINAZIONE

		SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
QUSC10	425	SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
QUSC10	426	SS =	0.3	SI =	0.3
		SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
		SS =	0.3	SI =	0.3
QUSC10	427	SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
QUSC10	428	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	429	SS =	0.5	SI =	0.5
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.5	SI =	0.5
QUSC10	430	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	431	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	432	SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
QUSC10	433	SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
QUSC10	434	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	435	SS =	3.1	SI =	3.1
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	3.1	SI =	3.1
QUSC10	436	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSC10	437	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	438	SS =	3.0	SI =	3.0
		SS =	2.7	SI =	2.7
		SS =	2.7	SI =	2.7
		SS =	3.0	SI =	3.0
QUSC10	439	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	440	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
QUSC10	441	SS =	0.8	SI =	0.8
		SS =	0.7	SI =	0.7

		SS =	0.7	SI =	0.7
		SS =	0.8	SI =	0.8
QUSC10	442	SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
		SS =	2.2	SI =	2.2
		SS =	2.0	SI =	2.0
QUSC10	443	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
QUSC10	444	SS =	0.6	SI =	0.6
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.6	SI =	0.6
QUSC10	445	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
QUSC10	446	SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
QUSC10	447	SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
QUSC10	448	SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.5	SI =	1.5
QUSC10	449	SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
QUSC10	450	SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.4	SI =	1.4
QUSC10	451	SS =	4.5	SI =	4.5
		SS =	4.8	SI =	4.8
		SS =	4.8	SI =	4.8
		SS =	4.5	SI =	4.5
QUSC10	452	SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
QUSC10	453	SS =	4.2	SI =	4.2
		SS =	4.1	SI =	4.1
		SS =	4.1	SI =	4.1
		SS =	4.2	SI =	4.2
QUSC10	454	SS =	3.1	SI =	3.1
		SS =	3.4	SI =	3.4
		SS =	3.4	SI =	3.4
		SS =	3.1	SI =	3.1
QUSC10	455	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSC10	456	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
QUSC10	457	SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.6	SI =	0.6
QUSC10	458	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5

		SS =	0.5	SI =	0.5
QUSCID	459	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
QUSCID	460	SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
QUSCID	461	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSCID	462	SS =	3.1	SI =	3.1
		SS =	3.2	SI =	3.2
		SS =	3.2	SI =	3.2
		SS =	3.1	SI =	3.1
QUSCID	463	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSCID	464	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSCID	465	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
QUSCID	466	SS =	1.7	SI =	1.7
		SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
		SS =	1.7	SI =	1.7
QUSCID	467	SS =	1.0	SI =	1.0
		SS =	1.1	SI =	1.1
		SS =	1.1	SI =	1.1
		SS =	1.0	SI =	1.0
QUSCID	468	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSCID	469	SS =	2.6	SI =	2.6
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	2.6	SI =	2.6
QUSCID	470	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
QUSCID	471	SS =	2.4	SI =	2.4
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.4	SI =	2.4
QUSCID	472	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.1	SI =	2.1
QUSCID	473	SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
QUSCID	474	SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
QUSCID	475	SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2

		SS =	1.2	SI =	1.2
GUSCIO	476	SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
GUSCIO	477	SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
		SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
GUSCIO	478	SS =	2.2	SI =	2.2
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	479	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
GUSCIO	480	SS =	2.9	SI =	2.9
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	2.9	SI =	2.9
GUSCIO	481	SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
GUSCIO	482	SS =	2.4	SI =	2.4
		SS =	2.5	SI =	2.5
		SS =	2.5	SI =	2.5
		SS =	2.4	SI =	2.4
GUSCIO	483	SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
GUSCIO	484	SS =	2.2	SI =	2.2
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
GUSCIO	485	SS =	1.3	SI =	1.3
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
GUSCIO	486	SS =	1.9	SI =	1.9
		SS =	2.2	SI =	2.2
		SS =	2.2	SI =	2.2
		SS =	1.9	SI =	1.9
GUSCIO	487	SS =	2.9	SI =	2.9
		SS =	3.6	SI =	3.6
		SS =	3.6	SI =	3.6
		SS =	2.9	SI =	2.9
GUSCIO	488	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
GUSCIO	489	SS =	1.6	SI =	1.6
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
GUSCIO	490	SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
GUSCIO	491	SS =	3.8	SI =	3.8
		SS =	3.7	SI =	3.7
		SS =	3.7	SI =	3.7
		SS =	3.8	SI =	3.8
GUSCIO	492	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1

GUSCIO	493	SS =	4.2	SI =	4.2
		SS =	4.3	SI =	4.3
		SS =	4.3	SI =	4.3
		SS =	4.2	SI =	4.2
GUSCIO	494	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
GUSCIO	496	SS =	6.9	SI =	6.9
		SS =	7.3	SI =	7.3
		SS =	7.3	SI =	7.3
		SS =	6.9	SI =	6.9
GUSCIO	497	SS =	4.3	SI =	4.3
		SS =	5.0	SI =	5.0
		SS =	5.0	SI =	5.0
		SS =	4.3	SI =	4.3
GUSCIO	498	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.3	SI =	1.3
GUSCIO	499	SS =	0.7	SI =	0.7
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.7	SI =	0.7
tensione max = 7,3 guscio = 496					
SOLLECITAZIONE GUSCI RETTANGOLARI					
CASO DI CARICO : 6 SLU con SISMAS					
N. 3 CONDIZIONI ANALISI STATICA					
1 Peso proprio + 1.00					
2 Permanente + 1.00					
3 Avar. abbattimento + 0.30					
N. 1 CASI DI CARICO					
4 SISMAS SLU 1.00					
1) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.001					
2) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.002					
3) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.003					
4) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.004					
Unità di misura: SI,SS (kN/cm2)					
GUSCIO	415	SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.1	SI =	1.1
GUSCIO	416	SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
GUSCIO	417	SS =	3.5	SI =	3.5
		SS =	2.6	SI =	2.6
		SS =	3.4	SI =	3.4
		SS =	2.5	SI =	2.5
GUSCIO	418	SS =	3.6	SI =	3.6
		SS =	2.5	SI =	2.5
		SS =	3.5	SI =	3.5
		SS =	2.4	SI =	2.4
GUSCIO	419	SS =	9.2	SI =	9.2
		SS =	5.8	SI =	5.8
		SS =	9.0	SI =	9.0
		SS =	5.5	SI =	5.5
GUSCIO	420	SS =	7.5	SI =	7.5
		SS =	4.1	SI =	4.1
		SS =	7.6	SI =	7.6
		SS =	4.0	SI =	4.0
GUSCIO	421	SS =	9.5	SI =	9.5
		SS =	4.2	SI =	4.2
		SS =	9.9	SI =	9.9
		SS =	4.8	SI =	4.8
GUSCIO	422	SS =	7.6	SI =	7.6
		SS =	3.7	SI =	3.7
		SS =	7.7	SI =	7.7

		SS =	3.9	SI =	3.9
GUSCIO	423	SS =	3.3	SI =	3.3
		SS =	2.1	SI =	2.1
		SS =	3.5	SI =	3.5
		SS =	2.3	SI =	2.3
GUSCIO	424	SS =	3.4	SI =	3.4
		SS =	2.0	SI =	2.0
		SS =	3.6	SI =	3.6
		SS =	2.2	SI =	2.2
GUSCIO	425	SS =	1.4	SI =	1.4
		SS =	0.9	SI =	0.9
		SS =	1.4	SI =	1.4
		SS =	1.0	SI =	1.0
GUSCIO	426	SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
GUSCIO	427	SS =	2.8	SI =	2.8
		SS =	1.9	SI =	1.9
		SS =	2.9	SI =	2.9
		SS =	1.9	SI =	1.9
GUSCIO	428	SS =	3.3	SI =	3.3
		SS =	2.1	SI =	2.1
		SS =	3.4	SI =	3.4
		SS =	2.1	SI =	2.1
GUSCIO	429	SS =	2.1	SI =	2.1
		SS =	1.4	SI =	1.4
		SS =	2.2	SI =	2.2
		SS =	1.4	SI =	1.4
GUSCIO	430	SS =	3.8	SI =	3.8
		SS =	3.4	SI =	3.4
		SS =	3.9	SI =	3.9
		SS =	3.4	SI =	3.4
GUSCIO	431	SS =	4.3	SI =	4.3
		SS =	3.4	SI =	3.4
		SS =	4.4	SI =	4.4
		SS =	3.4	SI =	3.4
GUSCIO	432	SS =	3.9	SI =	3.9
		SS =	2.5	SI =	2.5
		SS =	4.0	SI =	4.0
		SS =	2.6	SI =	2.6
GUSCIO	433	SS =	5.2	SI =	5.2
		SS =	5.5	SI =	5.5
		SS =	5.3	SI =	5.3
		SS =	5.5	SI =	5.5
GUSCIO	434	SS =	5.6	SI =	5.6
		SS =	4.7	SI =	4.7
		SS =	5.7	SI =	5.7
		SS =	4.8	SI =	4.8
GUSCIO	435	SS =	7.8	SI =	7.8
		SS =	6.3	SI =	6.3
		SS =	7.6	SI =	7.6
		SS =	6.2	SI =	6.2
GUSCIO	436	SS =	4.8	SI =	4.8
		SS =	5.0	SI =	5.0
		SS =	5.0	SI =	5.0
		SS =	5.1	SI =	5.1
GUSCIO	437	SS =	5.6	SI =	5.6
		SS =	4.5	SI =	4.5
		SS =	5.7	SI =	5.7
		SS =	4.7	SI =	4.7
GUSCIO	438	SS =	7.9	SI =	7.9
		SS =	5.2	SI =	5.2
		SS =	8.4	SI =	8.4
		SS =	5.7	SI =	5.7
GUSCIO	439	SS =	3.3	SI =	3.3
		SS =	2.8	SI =	2.8
		SS =	3.5	SI =	3.5
		SS =	3.1	SI =	3.1

GUSCIO	457	SS = 1.9	SI = 1.9
		SS = 2.4	SI = 2.4
		SS = 1.7	SI = 1.7
		SS = 2.2	SI = 2.2
GUSCIO	458	SS = 2.2	SI = 2.2
		SS = 2.9	SI = 2.9
		SS = 2.2	SI = 2.2
		SS = 2.8	SI = 2.8
GUSCIO	459	SS = 1.8	SI = 1.8
		SS = 3.4	SI = 3.4
		SS = 1.9	SI = 1.9
		SS = 3.3	SI = 3.3
GUSCIO	460	SS = 1.8	SI = 1.8
		SS = 2.1	SI = 2.1
		SS = 1.8	SI = 1.8
		SS = 2.2	SI = 2.2
GUSCIO	461	SS = 1.8	SI = 1.8
		SS = 1.8	SI = 1.8
		SS = 1.7	SI = 1.7
		SS = 1.9	SI = 1.9
GUSCIO	462	SS = 2.2	SI = 2.2
		SS = 4.4	SI = 4.4
		SS = 2.0	SI = 2.0
		SS = 4.3	SI = 4.3
GUSCIO	463	SS = 2.2	SI = 2.2
		SS = 2.7	SI = 2.7
		SS = 2.1	SI = 2.1
		SS = 2.8	SI = 2.8
GUSCIO	464	SS = 2.1	SI = 2.1
		SS = 2.2	SI = 2.2
		SS = 2.0	SI = 2.0
		SS = 2.3	SI = 2.3
GUSCIO	465	SS = 2.5	SI = 2.5
		SS = 2.8	SI = 2.8
		SS = 2.2	SI = 2.2
		SS = 2.6	SI = 2.6
GUSCIO	466	SS = 2.0	SI = 2.0
		SS = 2.4	SI = 2.4
		SS = 1.6	SI = 1.6
		SS = 2.4	SI = 2.4
GUSCIO	467	SS = 2.0	SI = 2.0
		SS = 2.2	SI = 2.2
		SS = 1.9	SI = 1.9
		SS = 2.4	SI = 2.4
GUSCIO	468	SS = 2.2	SI = 2.2
		SS = 2.2	SI = 2.2
		SS = 1.9	SI = 1.9
		SS = 2.2	SI = 2.2
GUSCIO	469	SS = 2.6	SI = 2.6
		SS = 2.6	SI = 2.6
		SS = 2.5	SI = 2.5
		SS = 2.9	SI = 2.9
GUSCIO	470	SS = 2.1	SI = 2.1
		SS = 2.2	SI = 2.2
		SS = 2.1	SI = 2.1
		SS = 2.3	SI = 2.3
GUSCIO	471	SS = 2.6	SI = 2.6
		SS = 1.9	SI = 1.9
		SS = 2.5	SI = 2.5
		SS = 2.2	SI = 2.2
GUSCIO	472	SS = 2.5	SI = 2.5
		SS = 2.6	SI = 2.6
		SS = 2.4	SI = 2.4
		SS = 2.6	SI = 2.6
GUSCIO	473	SS = 2.2	SI = 2.2
		SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.4	SI = 2.4
GUSCIO	474	SS = 2.4	SI = 2.4

GUSCIO	475	SS = 1.7	SI = 1.7
		SS = 2.4	SI = 2.4
		SS = 1.9	SI = 1.9
		SS = 1.5	SI = 1.5
GUSCIO	476	SS = 1.6	SI = 1.6
		SS = 1.4	SI = 1.4
		SS = 1.7	SI = 1.7
		SS = 1.9	SI = 1.9
GUSCIO	477	SS = 2.0	SI = 2.0
		SS = 1.8	SI = 1.8
		SS = 1.2	SI = 1.2
		SS = 1.7	SI = 1.7
GUSCIO	478	SS = 2.5	SI = 2.5
		SS = 0.9	SI = 0.9
		SS = 2.2	SI = 2.2
		SS = 1.0	SI = 1.0
GUSCIO	479	SS = 0.6	SI = 0.6
		SS = 0.4	SI = 0.4
		SS = 0.6	SI = 0.6
		SS = 0.5	SI = 0.5
GUSCIO	480	SS = 1.7	SI = 1.7
		SS = 2.2	SI = 2.2
		SS = 1.2	SI = 1.2
		SS = 2.0	SI = 2.0
GUSCIO	481	SS = 1.0	SI = 1.0
		SS = 0.7	SI = 0.7
		SS = 0.9	SI = 0.9
		SS = 0.6	SI = 0.6
GUSCIO	482	SS = 4.5	SI = 4.5
		SS = 2.1	SI = 2.1
		SS = 3.6	SI = 3.6
		SS = 2.3	SI = 2.3
GUSCIO	483	SS = 2.3	SI = 2.3
		SS = 2.0	SI = 2.0
		SS = 2.0	SI = 2.0
		SS = 1.8	SI = 1.8
GUSCIO	484	SS = 3.8	SI = 3.8
		SS = 0.8	SI = 0.8
		SS = 3.3	SI = 3.3
		SS = 1.2	SI = 1.2
GUSCIO	485	SS = 2.2	SI = 2.2
		SS = 2.8	SI = 2.8
		SS = 1.9	SI = 1.9
		SS = 2.8	SI = 2.8
GUSCIO	486	SS = 2.0	SI = 2.0
		SS = 2.6	SI = 2.6
		SS = 1.7	SI = 1.7
		SS = 2.6	SI = 2.6
GUSCIO	487	SS = 2.9	SI = 2.9
		SS = 4.1	SI = 4.1
		SS = 3.0	SI = 3.0
		SS = 5.3	SI = 5.3
GUSCIO	488	SS = 1.2	SI = 1.2
		SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
		SS = 2.1	SI = 2.1
GUSCIO	489	SS = 1.6	SI = 1.6
		SS = 4.0	SI = 4.0
		SS = 1.7	SI = 1.7
		SS = 3.8	SI = 3.8
GUSCIO	490	SS = 6.4	SI = 6.4
		SS = 8.4	SI = 8.4
		SS = 6.3	SI = 6.3
		SS = 8.3	SI = 8.3
GUSCIO	491	SS = 6.1	SI = 6.1

GUSCIO	492	SS = 7.5	SI = 7.5
		SS = 5.9	SI = 5.9
		SS = 7.3	SI = 7.3
		SS = 1.8	SI = 1.8
GUSCIO	493	SS = 3.1	SI = 3.1
		SS = 1.4	SI = 1.4
		SS = 2.8	SI = 2.8
		SS = 3.8	SI = 3.8
GUSCIO	494	SS = 3.4	SI = 3.4
		SS = 3.2	SI = 3.2
		SS = 3.4	SI = 3.4
		SS = 0.8	SI = 0.8
GUSCIO	495	SS = 1.3	SI = 1.3
		SS = 0.9	SI = 0.9
		SS = 1.2	SI = 1.2
		SS = 2.3	SI = 2.3
GUSCIO	496	SS = 3.7	SI = 3.7
		SS = 2.6	SI = 2.6
		SS = 3.7	SI = 3.7
		SS = 6.2	SI = 6.2
GUSCIO	497	SS = 8.6	SI = 8.6
		SS = 7.0	SI = 7.0
		SS = 9.1	SI = 9.1
		SS = 5.2	SI = 5.2
GUSCIO	498	SS = 6.8	SI = 6.8
		SS = 4.9	SI = 4.9
		SS = 5.5	SI = 5.5
		SS = 1.1	SI = 1.1
GUSCIO	499	SS = 2.6	SI = 2.6
		SS = 1.3	SI = 1.3
		SS = 2.0	SI = 2.0
		SS = 1.9	SI = 1.9
GUSCIO	500	SS = 2.7	SI = 2.7
		SS = 1.7	SI = 1.7
		SS = 2.7	SI = 2.7
		tensione max = 9.9	guscio = 421

SOLLECITAZIONE GUSCI RETTANGOLARI			
CASO DI CARICO : 7 SLU con SISNAV			
N. 3 CONDIZIONE ANALIST STATICA			
1	Peso proprio	+	1.00
2	Permanente	+	1.00
3	Accidentalizzazione	+	0.30
N. 1 CASO DI CARICO			
5	SISNAV SLU		1.00
1)	+1.00*c001	+1.00*c002	+0.30*c003
2)	+1.00*c001	+1.00*c002	+0.30*c003
3)	+1.00*c001	+1.00*c002	+0.30*c003
4)	+1.00*c001	+1.00*c002	+0.30*c003
Unità di misura: SI,SS [daN/cm2]			
GUSCIO	415	SS = 0.9	SI = 0.9
		SS = 1.5	SI = 1.5
		SS = 0.9	SI = 0.9
		SS = 1.5	SI = 1.5
GUSCIO	416	SS = 0.4	SI = 0.4
		SS = 1.2	SI = 1.2
		SS = 0.5	SI = 0.5
		SS = 1.2	SI = 1.2
GUSCIO	417	SS = 2.0	SI = 2.0
		SS = 3.9	SI = 3.9
		SS = 2.1	SI = 2.1
		SS = 4.0	SI = 4.0
GUSCIO	418	SS = 2.1	SI = 2.1
		SS = 3.9	SI = 3.9
		SS = 2.2	SI = 2.2
		SS = 3.9	SI = 3.9
GUSCIO	419	SS = 4.8	SI = 4.8
		SS = 10.0	SI = 10.0
		SS = 4.9	SI = 4.9
		SS = 10.2	SI = 10.2
GUSCIO	420	SS = 5.3	SI = 5.3
		SS = 6.4	SI = 6.4
		SS = 5.3	SI = 5.3
		SS = 6.5	SI = 6.5
GUSCIO	421	SS = 9.6	SI = 9.6

GUSCIO	422	SS = 5.3	SI = 5.3
		SS = 9.3	SI = 9.3
		SS = 5.1	SI = 5.1
		SS = 6.2	SI = 6.2
GUSCIO	423	SS = 5.5	SI = 5.5
		SS = 6.1	SI = 6.1
		SS = 5.4	SI = 5.4
		SS = 3.7	SI = 3.7
GUSCIO	424	SS = 1.9	SI = 1.9
		SS = 3.5	SI = 3.5
		SS = 1.8	SI = 1.8
		SS = 3.6	SI = 3.6
GUSCIO	425	SS = 2.2	SI = 2.2
		SS = 3.4	SI = 3.4
		SS = 2.1	SI = 2.1
		SS = 1.4	SI = 1.4
GUSCIO	426	SS = 0.7	SI = 0.7
		SS = 1.4	SI = 1.4
		SS = 0.6	SI = 0.6
		SS = 0.9	SI = 0.9
GUSCIO	427	SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
		SS = 2.7	SI = 2.7
		SS = 1.8	SI = 1.8
GUSCIO	428	SS = 2.7	SI = 2.7
		SS = 2.2	SI = 2.2
		SS = 3.2	SI = 3.2
		SS = 3.1	SI = 3.1
GUSCIO	429	SS = 1.6	SI = 1.6
		SS = 1.8	SI = 1.8
		SS = 1.5	SI = 1.5
		SS = 1.8	SI = 1.8
GUSCIO	430	SS = 2.8	SI = 2.8
		SS = 4.4	SI = 4.4
		SS = 2.8	SI = 2.8
		SS = 4.4	SI = 4.4
GUSCIO	431	SS = 3.1	SI = 3.1
		SS = 4.6	SI = 4.6
		SS = 3.0	SI = 3.0
		SS = 4.6	SI = 4.6
GUSCIO	432	SS = 2.9	SI = 2.9
		SS = 3.7	SI = 3.7
		SS = 2.9	SI = 2.9
		SS = 3.7	SI = 3.7
GUSCIO	433	SS = 4.2	SI = 4.2
		SS = 6.5	SI = 6.5
		SS = 4.1	SI = 4.1
		SS = 6.5	SI = 6.5
GUSCIO	434	SS = 4.4	SI = 4.4
		SS = 5.8	SI = 5.8
		SS = 4.4	SI = 4.4
		SS = 5.7	SI = 5.7
GUSCIO	435	SS = 5.4	SI = 5.4
		SS = 9.4	SI = 9.4
		SS = 5.3	SI = 5.3
		SS = 9.5	SI = 9.5
GUSCIO	436	SS = 4.4	SI = 4.4
		SS = 5.4	SI = 5.4
		SS = 4.3	SI = 4.3
		SS = 5.3	SI = 5.3
GUSCIO	437	SS = 4.5	SI = 4.5
		SS = 5.4	SI = 5.4
		SS = 4.4	SI = 4.4
		SS = 5.4	SI = 5.4
GUSCIO	438	SS = 9.3	SI = 9.3

		SS = 6.1	SI = 6.1
		SS = 9.0	SI = 9.0
		SS = 6.0	SI = 6.0
QUSCIO	439	SS = 3.0	SI = 3.0
		SS = 3.3	SI = 3.3
		SS = 2.9	SI = 2.9
		SS = 3.2	SI = 3.2
QUSCIO	440	SS = 3.8	SI = 3.8
		SS = 3.6	SI = 3.6
		SS = 3.7	SI = 3.7
		SS = 3.6	SI = 3.6
QUSCIO	441	SS = 3.7	SI = 3.7
		SS = 3.0	SI = 3.0
		SS = 3.7	SI = 3.7
		SS = 3.0	SI = 3.0
QUSCIO	442	SS = 3.7	SI = 3.7
		SS = 1.9	SI = 1.9
		SS = 3.9	SI = 3.9
		SS = 1.8	SI = 1.8
QUSCIO	443	SS = 3.3	SI = 3.3
		SS = 2.4	SI = 2.4
		SS = 3.2	SI = 3.2
		SS = 2.4	SI = 2.4
QUSCIO	444	SS = 2.2	SI = 2.2
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.4	SI = 1.4
QUSCIO	445	SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
		SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
QUSCIO	446	SS = 0.8	SI = 0.8
		SS = 2.6	SI = 2.6
		SS = 0.8	SI = 0.8
		SS = 2.6	SI = 2.6
QUSCIO	447	SS = 0.8	SI = 0.8
		SS = 1.5	SI = 1.5
		SS = 0.7	SI = 0.7
		SS = 1.7	SI = 1.7
QUSCIO	448	SS = 1.2	SI = 1.2
		SS = 3.9	SI = 3.9
		SS = 1.2	SI = 1.2
		SS = 3.9	SI = 3.9
QUSCIO	449	SS = 1.5	SI = 1.5
		SS = 4.4	SI = 4.4
		SS = 1.5	SI = 1.5
		SS = 4.3	SI = 4.3
QUSCIO	450	SS = 1.5	SI = 1.5
		SS = 3.9	SI = 3.9
		SS = 1.5	SI = 1.5
		SS = 3.9	SI = 3.9
QUSCIO	451	SS = 3.3	SI = 3.3
		SS = 9.2	SI = 9.2
		SS = 3.4	SI = 3.4
		SS = 8.9	SI = 8.9
QUSCIO	452	SS = 3.2	SI = 3.2
		SS = 5.7	SI = 5.7
		SS = 3.2	SI = 3.2
		SS = 5.7	SI = 5.7
QUSCIO	453	SS = 3.3	SI = 3.3
		SS = 9.3	SI = 9.3
		SS = 3.3	SI = 3.3
		SS = 9.4	SI = 9.4
QUSCIO	454	SS = 6.1	SI = 6.1
		SS = 4.7	SI = 4.7
		SS = 6.4	SI = 6.4
		SS = 4.8	SI = 4.8
QUSCIO	455	SS = 3.2	SI = 3.2
		SS = 5.1	SI = 5.1

		SS = 3.2	SI = 3.2
		SS = 5.1	SI = 5.1
QUSCIO	456	SS = 5.8	SI = 5.8
		SS = 4.7	SI = 4.7
		SS = 5.9	SI = 5.9
		SS = 4.8	SI = 4.8
QUSCIO	457	SS = 1.9	SI = 1.9
		SS = 1.6	SI = 1.6
		SS = 2.1	SI = 2.1
		SS = 1.7	SI = 1.7
QUSCIO	458	SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.3	SI = 2.3
		SS = 2.3	SI = 2.3
QUSCIO	459	SS = 1.9	SI = 1.9
		SS = 1.9	SI = 1.9
		SS = 2.0	SI = 2.0
		SS = 1.9	SI = 1.9
QUSCIO	460	SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
		SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
QUSCIO	461	SS = 1.9	SI = 1.9
		SS = 1.4	SI = 1.4
		SS = 1.9	SI = 1.9
		SS = 1.3	SI = 1.3
QUSCIO	462	SS = 5.4	SI = 5.4
		SS = 1.9	SI = 1.9
		SS = 5.5	SI = 5.5
		SS = 1.9	SI = 1.9
QUSCIO	463	SS = 3.3	SI = 3.3
		SS = 1.3	SI = 1.3
		SS = 3.4	SI = 3.4
		SS = 1.3	SI = 1.3
QUSCIO	464	SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
		SS = 2.5	SI = 2.5
		SS = 1.2	SI = 1.2
QUSCIO	465	SS = 2.3	SI = 2.3
		SS = 3.2	SI = 3.2
		SS = 2.4	SI = 2.4
		SS = 3.4	SI = 3.4
QUSCIO	466	SS = 3.2	SI = 3.2
		SS = 1.3	SI = 1.3
		SS = 3.4	SI = 3.4
		SS = 1.0	SI = 1.0
QUSCIO	467	SS = 2.3	SI = 2.3
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.2	SI = 1.2
QUSCIO	468	SS = 2.8	SI = 2.8
		SS = 0.9	SI = 0.9
		SS = 2.9	SI = 2.9
		SS = 1.0	SI = 1.0
QUSCIO	469	SS = 2.4	SI = 2.4
		SS = 4.2	SI = 4.2
		SS = 2.7	SI = 2.7
		SS = 3.8	SI = 3.8
QUSCIO	470	SS = 2.7	SI = 2.7
		SS = 1.5	SI = 1.5
		SS = 2.6	SI = 2.6
		SS = 1.3	SI = 1.3
QUSCIO	471	SS = 2.6	SI = 2.6
		SS = 2.9	SI = 2.9
		SS = 2.5	SI = 2.5
		SS = 3.0	SI = 3.0
QUSCIO	472	SS = 3.2	SI = 3.2
		SS = 2.6	SI = 2.6

		SS = 3.4	SI = 3.4
		SS = 2.4	SI = 2.4
QUSCIO	473	SS = 3.0	SI = 3.0
		SS = 1.5	SI = 1.5
		SS = 3.0	SI = 3.0
		SS = 1.4	SI = 1.4
QUSCIO	474	SS = 3.0	SI = 3.0
		SS = 1.7	SI = 1.7
		SS = 2.9	SI = 2.9
		SS = 1.7	SI = 1.7
QUSCIO	475	SS = 2.4	SI = 2.4
		SS = 1.1	SI = 1.1
		SS = 2.4	SI = 2.4
		SS = 1.0	SI = 1.0
QUSCIO	476	SS = 3.2	SI = 3.2
		SS = 0.6	SI = 0.6
		SS = 3.2	SI = 3.2
		SS = 0.7	SI = 0.7
QUSCIO	477	SS = 2.4	SI = 2.4
		SS = 0.8	SI = 0.8
		SS = 2.4	SI = 2.4
		SS = 0.9	SI = 0.9
QUSCIO	478	SS = 3.2	SI = 3.2
		SS = 1.1	SI = 1.1
		SS = 3.2	SI = 3.2
		SS = 1.1	SI = 1.1
QUSCIO	479	SS = 1.3	SI = 1.3
		SS = 0.5	SI = 0.5
		SS = 1.3	SI = 1.3
		SS = 0.5	SI = 0.5
QUSCIO	480	SS = 3.8	SI = 3.8
		SS = 2.5	SI = 2.5
		SS = 4.1	SI = 4.1
		SS = 2.4	SI = 2.4
QUSCIO	481	SS = 1.3	SI = 1.3
		SS = 0.9	SI = 0.9
		SS = 1.4	SI = 1.4
		SS = 0.9	SI = 0.9
QUSCIO	482	SS = 3.3	SI = 3.3
		SS = 3.7	SI = 3.7
		SS = 3.6	SI = 3.6
		SS = 4.1	SI = 4.1
QUSCIO	483	SS = 2.5	SI = 2.5
		SS = 1.3	SI = 1.3
		SS = 2.7	SI = 2.7
		SS = 1.5	SI = 1.5
QUSCIO	484	SS = 1.8	SI = 1.8
		SS = 3.8	SI = 3.8
		SS = 1.9	SI = 1.9
		SS = 4.1	SI = 4.1
QUSCIO	485	SS = 3.4	SI = 3.4
		SS = 1.5	SI = 1.5
		SS = 3.5	SI = 3.5
		SS = 1.4	SI = 1.4
QUSCIO	486	SS = 3.3	SI = 3.3
		SS = 1.6	SI = 1.6
		SS = 3.4	SI = 3.4
		SS = 1.3	SI = 1.3
QUSCIO	487	SS = 1.7	SI = 1.7
		SS = 6.5	SI = 6.5
		SS = 1.9	SI = 1.9
		SS = 5.7	SI = 5.7
QUSCIO	488	SS = 0.7	SI = 0.7
		SS = 1.4	SI = 1.4
		SS = 0.5	SI = 0.5
		SS = 1.6	SI = 1.6
QUSCIO	489	SS = 0.7	SI = 0.7
		SS = 3.7	SI = 3.7
		SS = 0.8	SI = 0.8

		SS = 3.8	SI = 3.8
QUSCIO	490	SS = 4.1	SI = 4.1
		SS = 11.9	SI = 11.9
		SS = 4.2	SI = 4.2
		SS = 11.9	SI = 11.9
QUSCIO	491	SS = 8.0	SI = 8.0
		SS = 7.1	SI = 7.1
		SS = 8.1	SI = 8.1
		SS = 7.1	SI = 7.1
QUSCIO	492	SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.5	SI = 2.5
		SS = 2.3	SI = 2.3
QUSCIO	493	SS = 6.8	SI = 6.8
		SS = 1.8	SI = 1.8
		SS = 6.9	SI = 6.9
		SS = 1.9	SI = 1.9
QUSCIO	494	SS = 0.1	SI = 0.1
		SS = 0.9	SI = 0.9
		SS = 0.1	SI = 0.1
		SS = 0.9	SI = 0.9
QUSCIO	495	SS = 0.4	SI = 0.4
		SS = 4.4	SI = 4.4
		SS = 0.4	SI = 0.4
		SS = 4.3	SI = 4.3
QUSCIO	496	SS = 1.0	SI = 1.0
		SS = 13.6	SI = 13.6
		SS = 1.0	SI = 1.0
		SS = 13.3	SI = 13.3
QUSCIO	497	SS = 8.9	SI = 8.9
		SS = 1.4	SI = 1.4
		SS = 9.6	SI = 9.6
		SS = 1.4	SI = 1.4
QUSCIO	498	SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6

GUSCIO 435 SS = 13.5 SI = 13.5
GUSCIO 436 SS = 9.3 SI = 9.3
GUSCIO 437 SS = 9.5 SI = 9.5
GUSCIO 438 SS = 12.5 SI = 12.5
GUSCIO 439 SS = 5.8 SI = 5.8
GUSCIO 440 SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.4 SI = 6.4
GUSCIO 442 SS = 3.9 SI = 3.9
GUSCIO 443 SS = 5.2 SI = 5.2
GUSCIO 444 SS = 3.3 SI = 3.3
GUSCIO 445 SS = 2.0 SI = 2.0
GUSCIO 446 SS = 3.0 SI = 3.0
GUSCIO 447 SS = 2.3 SI = 2.3
GUSCIO 448 SS = 4.4 SI = 4.4
GUSCIO 449 SS = 5.3 SI = 5.3
GUSCIO 450 SS = 5.2 SI = 5.2
GUSCIO 451 SS = 8.8 SI = 8.8
GUSCIO 452 SS = 7.8 SI = 7.8
GUSCIO 453 SS = 10.6 SI = 10.6
GUSCIO 454 SS = 7.6 SI = 7.6
GUSCIO 455 SS = 7.4 SI = 7.4
GUSCIO 456 SS = 8.7 SI = 8.7
GUSCIO 457 SS = 3.1 SI = 3.1
GUSCIO 458 SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.8 SI = 2.8
GUSCIO 461 SS = 2.2 SI = 2.2
GUSCIO 462 SS = 4.4 SI = 4.4
GUSCIO 463 SS = 3.5 SI = 3.5
GUSCIO 464 SS = 2.6 SI = 2.6
GUSCIO 465 SS = 2.9 SI = 2.9
GUSCIO 466 SS = 2.6 SI = 2.6
GUSCIO 467 SS = 2.4 SI = 2.4
GUSCIO 468 SS = 3.1 SI = 3.1
GUSCIO 469 SS = 2.8 SI = 2.8
GUSCIO 470 SS = 2.9 SI = 2.9
GUSCIO 471 SS = 2.4 SI = 2.4
GUSCIO 472 SS = 3.1 SI = 3.1
GUSCIO 473 SS = 3.0 SI = 3.0
GUSCIO 474 SS = 2.9 SI = 2.9
GUSCIO 475 SS = 2.0 SI = 2.0
GUSCIO 476 SS = 2.9 SI = 2.9
GUSCIO 477 SS = 2.1 SI = 2.1
GUSCIO 478 SS = 2.0 SI = 2.0
GUSCIO 479 SS = 0.8 SI = 0.8
GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 9 Rara VentoX
N. 4 CONDIZIONI ANALISI STATICA
1 PnsL_proprio_____ + 1.00

COMBINAZIONE

2 Permanente_____ + 1.00
3 Avar_abitazione_____ + 1.00
4 Neve(<1000h_1m)_____ + 1.00
1) +1.00*c001 -1.00*c002 +1.00*c003 +1.00*c004
Unità di misura: SI,SS [daN/cm2]
GUSCIO 415 SS = 2.2 SI = 2.2
GUSCIO 416 SS = 1.5 SI = 1.5
GUSCIO 417 SS = 5.8 SI = 5.8
GUSCIO 418 SS = 5.9 SI = 5.9
GUSCIO 419 SS = 14.5 SI = 14.5
GUSCIO 420 SS = 11.5 SI = 11.5
GUSCIO 421 SS = 13.6 SI = 13.6
GUSCIO 422 SS = 11.3 SI = 11.3
GUSCIO 423 SS = 5.2 SI = 5.2
GUSCIO 424 SS = 5.5 SI = 5.5
GUSCIO 425 SS = 1.9 SI = 1.9
GUSCIO 426 SS = 1.2 SI = 1.2
GUSCIO 427 SS = 4.2 SI = 4.2
GUSCIO 428 SS = 5.1 SI = 5.1
GUSCIO 429 SS = 3.0 SI = 3.0
GUSCIO 430 SS = 6.8 SI = 6.8
GUSCIO 431 SS = 7.4 SI = 7.4
GUSCIO 432 SS = 6.3 SI = 6.3
GUSCIO 433 SS = 9.8 SI = 9.8
GUSCIO 434 SS = 9.8 SI = 9.8
GUSCIO 435 SS = 13.5 SI = 13.5
GUSCIO 436 SS = 9.3 SI = 9.3
GUSCIO 437 SS = 9.5 SI = 9.5
GUSCIO 438 SS = 12.5 SI = 12.5
GUSCIO 439 SS = 5.8 SI = 5.8
GUSCIO 440 SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.4 SI = 6.4
GUSCIO 442 SS = 3.9 SI = 3.9
GUSCIO 443 SS = 5.2 SI = 5.2
GUSCIO 444 SS = 3.3 SI = 3.3
GUSCIO 445 SS = 2.0 SI = 2.0
GUSCIO 446 SS = 3.0 SI = 3.0
GUSCIO 447 SS = 2.3 SI = 2.3
GUSCIO 448 SS = 4.4 SI = 4.4
GUSCIO 449 SS = 5.3 SI = 5.3
GUSCIO 450 SS = 5.2 SI = 5.2
GUSCIO 451 SS = 8.8 SI = 8.8
GUSCIO 452 SS = 7.8 SI = 7.8
GUSCIO 453 SS = 10.6 SI = 10.6
GUSCIO 454 SS = 7.6 SI = 7.6
GUSCIO 455 SS = 7.4 SI = 7.4
GUSCIO 456 SS = 8.7 SI = 8.7
GUSCIO 457 SS = 3.1 SI = 3.1
GUSCIO 458 SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.8 SI = 2.8
GUSCIO 461 SS = 2.2 SI = 2.2
GUSCIO 462 SS = 4.4 SI = 4.4
GUSCIO 463 SS = 3.5 SI = 3.5
GUSCIO 464 SS = 2.6 SI = 2.6
GUSCIO 465 SS = 2.9 SI = 2.9
GUSCIO 466 SS = 2.6 SI = 2.6
GUSCIO 467 SS = 2.4 SI = 2.4
GUSCIO 468 SS = 3.1 SI = 3.1
GUSCIO 469 SS = 2.8 SI = 2.8
GUSCIO 470 SS = 2.9 SI = 2.9
GUSCIO 471 SS = 2.4 SI = 2.4
GUSCIO 472 SS = 3.1 SI = 3.1
GUSCIO 473 SS = 3.0 SI = 3.0
GUSCIO 474 SS = 2.9 SI = 2.9
GUSCIO 475 SS = 2.0 SI = 2.0
GUSCIO 476 SS = 2.9 SI = 2.9
GUSCIO 477 SS = 2.1 SI = 2.1
GUSCIO 478 SS = 2.0 SI = 2.0
GUSCIO 479 SS = 0.8 SI = 0.8
GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 10 Rara VentoY

COMBINAZIONE

N. 5 CONDIZIONE ANALISI STATICA
1 PnsL_proprio_____ + 1.00
2 Permanente_____ + 1.00
3 Avar_abitazione_____ + 1.00
4 Neve(<1000h_1m)_____ + 1.00
5 Vento_Y_____ + 1.00
1) +1.00*c001 +1.00*c002 +1.00*c003 +1.00*c004 +1.00*c005
2) +1.00*c001 +1.00*c002 +1.00*c003 +1.00*c004 -1.00*c005
Unità di misura: SI,SS [daN/cm2]
GUSCIO 415 SS = 2.4 SI = 2.4
SS = 2.0 SI = 2.0
GUSCIO 416 SS = 1.8 SI = 1.8
SS = 1.3 SI = 1.3
GUSCIO 417 SS = 6.4 SI = 6.4
SS = 5.2 SI = 5.2
GUSCIO 418 SS = 6.5 SI = 6.5
SS = 5.4 SI = 5.4
GUSCIO 419 SS = 16.3 SI = 16.3
SS = 12.8 SI = 12.8
GUSCIO 420 SS = 11.8 SI = 11.8
SS = 11.2 SI = 11.2
GUSCIO 421 SS = 12.3 SI = 12.3
SS = 15.0 SI = 15.0
GUSCIO 422 SS = 11.2 SI = 11.2
SS = 11.5 SI = 11.5
GUSCIO 423 SS = 4.7 SI = 4.7
SS = 5.7 SI = 5.7
GUSCIO 424 SS = 5.1 SI = 5.1
SS = 5.8 SI = 5.8
GUSCIO 425 SS = 1.6 SI = 1.6
SS = 2.1 SI = 2.1
GUSCIO 426 SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
GUSCIO 427 SS = 4.5 SI = 4.5
SS = 3.9 SI = 3.9
GUSCIO 428 SS = 5.5 SI = 5.5
SS = 4.8 SI = 4.8
GUSCIO 429 SS = 3.2 SI = 3.2
SS = 3.0 SI = 3.0
GUSCIO 430 SS = 7.4 SI = 7.4
SS = 6.3 SI = 6.3
GUSCIO 431 SS = 7.9 SI = 7.9
SS = 6.9 SI = 6.9
GUSCIO 432 SS = 6.7 SI = 6.7
SS = 6.1 SI = 6.1
GUSCIO 433 SS = 10.5 SI = 10.5
SS = 9.2 SI = 9.2
GUSCIO 434 SS = 10.2 SI = 10.2
SS = 9.3 SI = 9.3
GUSCIO 435 SS = 15.1 SI = 15.1

SS = 11.9 SI = 11.9
GUSCIO 436 SS = 9.7 SI = 9.7
SS = 8.9 SI = 8.9
GUSCIO 437 SS = 9.8 SI = 9.8
SS = 9.2 SI = 9.2
GUSCIO 438 SS = 11.9 SI = 11.9
SS = 14.0 SI = 14.0
GUSCIO 439 SS = 6.0 SI = 6.0
SS = 5.6 SI = 5.6
GUSCIO 440 SS = 7.1 SI = 7.1
SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.3 SI = 6.3
SS = 6.6 SI = 6.6
GUSCIO 442 SS = 3.7 SI = 3.7
SS = 4.6 SI = 4.6
GUSCIO 443 SS = 5.0 SI = 5.0
SS = 5.4 SI = 5.4
GUSCIO 444 SS = 3.1 SI = 3.1
SS = 3.6 SI = 3.6
GUSCIO 445 SS = 2.5 SI = 2.5
SS = 1.5 SI = 1.5
GUSCIO 446 SS = 3.6 SI = 3.6
SS = 2.3 SI = 2.3
GUSCIO 447 SS = 2.6 SI = 2.6
SS = 2.0 SI = 2.0
GUSCIO 448 SS = 5.4 SI = 5.4
SS = 3.5 SI = 3.5
GUSCIO 449 SS = 6.3 SI = 6.3
SS = 4.4 SI = 4.4
GUSCIO 450 SS = 6.0 SI = 6.0
SS = 4.5 SI = 4.5
GUSCIO 451 SS = 11.5 SI = 11.5
SS = 7.2 SI = 7.2
GUSCIO 452 SS = 8.7 SI = 8.7
SS = 7.0 SI = 7.0
GUSCIO 453 SS = 13.2 SI = 13.2
SS = 8.1 SI = 8.1
GUSCIO 454 SS = 7.8 SI = 7.8
SS = 8.3 SI = 8.3
GUSCIO 455 SS = 8.0 SI = 8.0
SS = 6.8 SI = 6.8
GUSCIO 456 SS = 8.3 SI = 8.3
SS = 9.4 SI = 9.4
GUSCIO 457 SS = 2.9 SI = 2.9
SS = 3.4 SI = 3.4
GUSCIO 458 SS = 3.9 SI = 3.9
SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.6 SI = 2.6
SS = 3.1 SI = 3.1
GUSCIO 461 SS = 2.1 SI = 2.1
SS = 2.4 SI = 2.4
GUSCIO 462 SS = 2.6 SI = 2.6
SS = 6.5 SI = 6.5
GUSCIO 463 SS = 2.9 SI = 2.9
SS = 4.3 SI = 4.3
GUSCIO 464 SS = 2.3 SI = 2.3
SS = 3.1 SI = 3.1
GUSCIO 465 SS = 3.7 SI = 3.7
SS = 2.7 SI = 2.7
GUSCIO 466 SS = 1.9 SI = 1.9
SS = 3.8 SI = 3.8
GUSCIO 467 SS = 2.2 SI = 2.2
SS = 2.9 SI = 2.9
GUSCIO 468 SS = 2.3 SI = 2.3
SS = 3.9 SI = 3.9
GUSCIO 469 SS = 4.3 SI = 4.3

		SS =	2.9	SI =	2.9
GUSCIO	470	SS =	2.5	SI =	2.5
		SS =	3.3	SI =	3.3
GUSCIO	471	SS =	2.9	SI =	2.9
		SS =	2.6	SI =	2.6
GUSCIO	472	SS =	2.5	SI =	2.5
		SS =	3.8	SI =	3.8
GUSCIO	473	SS =	2.6	SI =	2.6
		SS =	3.6	SI =	3.6
GUSCIO	474	SS =	2.4	SI =	2.4
		SS =	3.5	SI =	3.5
GUSCIO	475	SS =	1.4	SI =	1.4
		SS =	2.7	SI =	2.7
GUSCIO	476	SS =	2.1	SI =	2.1
		SS =	3.7	SI =	3.7
GUSCIO	477	SS =	1.5	SI =	1.5
		SS =	2.8	SI =	2.8
GUSCIO	478	SS =	1.4	SI =	1.4
		SS =	3.3	SI =	3.3
GUSCIO	479	SS =	0.3	SI =	0.3
		SS =	1.4	SI =	1.4
GUSCIO	480	SS =	1.4	SI =	1.4
		SS =	4.0	SI =	4.0
GUSCIO	481	SS =	0.8	SI =	0.8
		SS =	1.3	SI =	1.3
GUSCIO	482	SS =	4.4	SI =	4.4
		SS =	4.7	SI =	4.7
GUSCIO	483	SS =	2.8	SI =	2.8
		SS =	3.7	SI =	3.7
GUSCIO	484	SS =	4.0	SI =	4.0
		SS =	2.0	SI =	2.0
GUSCIO	485	SS =	2.9	SI =	2.9
		SS =	4.3	SI =	4.3
GUSCIO	486	SS =	2.1	SI =	2.1
		SS =	4.0	SI =	4.0
GUSCIO	487	SS =	7.0	SI =	7.0
		SS =	2.0	SI =	2.0
GUSCIO	488	SS =	1.9	SI =	1.9
		SS =	0.9	SI =	0.9
GUSCIO	489	SS =	5.5	SI =	5.5
		SS =	3.6	SI =	3.6
GUSCIO	490	SS =	17.5	SI =	17.5
		SS =	12.0	SI =	12.0
GUSCIO	491	SS =	13.0	SI =	13.0
		SS =	13.7	SI =	13.7
GUSCIO	492	SS =	4.1	SI =	4.1
		SS =	3.9	SI =	3.9
GUSCIO	493	SS =	2.6	SI =	2.6
		SS =	7.8	SI =	7.8
GUSCIO	494	SS =	1.3	SI =	1.3
		SS =	0.7	SI =	0.7
GUSCIO	495	SS =	5.6	SI =	5.6
		SS =	2.5	SI =	2.5
GUSCIO	496	SS =	16.7	SI =	16.7
		SS =	6.8	SI =	6.8
GUSCIO	497	SS =	4.4	SI =	4.4
		SS =	11.4	SI =	11.4
GUSCIO	498	SS =	1.8	SI =	1.8
		SS =	2.8	SI =	2.8
GUSCIO	499	SS =	2.9	SI =	2.9
		SS =	3.8	SI =	3.8
		tensione max =	17.5	guscio =	490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 11 Frequente Ventax

N. 4 CONDIZIONI ANALISI STATICA

1	Peso proprio	_____	+	1.00
2	Permanente	_____	+	1.00
3	A'Var.abilitazione	_____	+	0.50
4	Neve (<3000m_slm)	_____	+	0.20

1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004
Unità di misura: SI,SS [daN/cm2]

GUSCIO 415 SS = 1.4 SI = 1.4

COMBINAZIONE

GUSCIO	416	SS =	1.0	SI =	1.0
GUSCIO	417	SS =	3.7	SI =	3.7
GUSCIO	418	SS =	3.8	SI =	3.8
GUSCIO	419	SS =	9.0	SI =	9.0
GUSCIO	420	SS =	7.2	SI =	7.2
GUSCIO	421	SS =	8.6	SI =	8.6
GUSCIO	422	SS =	7.2	SI =	7.2
GUSCIO	423	SS =	3.4	SI =	3.4
GUSCIO	424	SS =	3.5	SI =	3.5
GUSCIO	425	SS =	1.2	SI =	1.2
GUSCIO	426	SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
GUSCIO	429	SS =	2.0	SI =	2.0
GUSCIO	430	SS =	4.4	SI =	4.4
GUSCIO	431	SS =	4.7	SI =	4.7
GUSCIO	432	SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.3	SI =	6.3
GUSCIO	434	SS =	6.3	SI =	6.3
GUSCIO	435	SS =	8.6	SI =	8.6
GUSCIO	436	SS =	6.0	SI =	6.0
GUSCIO	437	SS =	6.1	SI =	6.1
GUSCIO	438	SS =	8.1	SI =	8.1
GUSCIO	439	SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
GUSCIO	442	SS =	2.6	SI =	2.6
GUSCIO	443	SS =	3.3	SI =	3.3
GUSCIO	444	SS =	2.1	SI =	2.1
GUSCIO	445	SS =	1.4	SI =	1.4
GUSCIO	446	SS =	2.0	SI =	2.0
GUSCIO	447	SS =	1.4	SI =	1.4
GUSCIO	448	SS =	3.0	SI =	3.0
GUSCIO	449	SS =	3.6	SI =	3.6
GUSCIO	450	SS =	3.3	SI =	3.3
GUSCIO	451	SS =	5.8	SI =	5.8
GUSCIO	452	SS =	5.2	SI =	5.2
GUSCIO	453	SS =	6.6	SI =	6.6
GUSCIO	454	SS =	5.1	SI =	5.1
GUSCIO	455	SS =	4.9	SI =	4.9
GUSCIO	456	SS =	5.7	SI =	5.7
GUSCIO	457	SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
GUSCIO	460	SS =	2.1	SI =	2.1
GUSCIO	461	SS =	1.6	SI =	1.6
GUSCIO	462	SS =	3.0	SI =	3.0
GUSCIO	463	SS =	2.6	SI =	2.6
GUSCIO	464	SS =	1.9	SI =	1.9
GUSCIO	465	SS =	2.1	SI =	2.1
GUSCIO	466	SS =	1.9	SI =	1.9
GUSCIO	467	SS =	1.8	SI =	1.8
GUSCIO	468	SS =	2.1	SI =	2.1
GUSCIO	469	SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.1	SI =	2.1
GUSCIO	471	SS =	1.8	SI =	1.8
GUSCIO	472	SS =	2.3	SI =	2.3
GUSCIO	473	SS =	2.2	SI =	2.2
GUSCIO	474	SS =	2.2	SI =	2.2
GUSCIO	475	SS =	1.4	SI =	1.4
GUSCIO	476	SS =	2.1	SI =	2.1
GUSCIO	477	SS =	1.6	SI =	1.6
GUSCIO	478	SS =	1.5	SI =	1.5
GUSCIO	479	SS =	0.6	SI =	0.6
GUSCIO	480	SS =	1.6	SI =	1.6
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.3	SI =	2.3

GUSCIO	484	SS =	2.1	SI =	2.1
GUSCIO	485	SS =	2.5	SI =	2.5
GUSCIO	486	SS =	2.2	SI =	2.2
GUSCIO	487	SS =	3.3	SI =	3.3
GUSCIO	488	SS =	0.8	SI =	0.8
GUSCIO	489	SS =	2.8	SI =	2.8
GUSCIO	490	SS =	9.1	SI =	9.1
GUSCIO	491	SS =	8.3	SI =	8.3
GUSCIO	492	SS =	2.4	SI =	2.4
GUSCIO	493	SS =	3.3	SI =	3.3
GUSCIO	494	SS =	0.6	SI =	0.6
GUSCIO	495	SS =	2.6	SI =	2.6
GUSCIO	496	SS =	7.7	SI =	7.7
GUSCIO	497	SS =	5.5	SI =	5.5
GUSCIO	498	SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.5	SI =	2.5
		tensione max =	9.1	guscio =	490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 12 Frequente Ventax

N. 4 CONDIZIONI ANALISI STATICA

1	Peso proprio	_____	+	1.00
2	Permanente	_____	+	1.00
3	A'Var.abilitazione	_____	+	0.50
4	Neve (<3000m_slm)	_____	+	0.20

1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004
Unità di misura: SI,SS [daN/cm2]

COMBINAZIONE

GUSCIO	415	SS =	1.4	SI =	1.4
GUSCIO	416	SS =	1.0	SI =	1.0
GUSCIO	417	SS =	3.7	SI =	3.7
GUSCIO	418	SS =	3.8	SI =	3.8
GUSCIO	419	SS =	9.0	SI =	9.0
GUSCIO	420	SS =	7.2	SI =	7.2
GUSCIO	421	SS =	8.6	SI =	8.6
GUSCIO	422	SS =	7.2	SI =	7.2
GUSCIO	423	SS =	3.4	SI =	3.4
GUSCIO	424	SS =	3.5	SI =	3.5
GUSCIO	425	SS =	1.2	SI =	1.2
GUSCIO	426	SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
GUSCIO	429	SS =	2.0	SI =	2.0
GUSCIO	430	SS =	4.4	SI =	4.4
GUSCIO	431	SS =	4.7	SI =	4.7
GUSCIO	432	SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.3	SI =	6.3
GUSCIO	434	SS =	6.3	SI =	6.3
GUSCIO	435	SS =	8.6	SI =	8.6
GUSCIO	436	SS =	6.0	SI =	6.0
GUSCIO	437	SS =	6.1	SI =	6.1
GUSCIO	438	SS =	8.1	SI =	8.1
GUSCIO	439	SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
GUSCIO	442	SS =	2.6	SI =	2.6
GUSCIO	443	SS =	3.3	SI =	3.3
GUSCIO	444	SS =	2.1	SI =	2.1
GUSCIO	445	SS =	1.4	SI =	1.4
GUSCIO	446	SS =	2.0	SI =	2.0
GUSCIO	447	SS =	1.4	SI =	1.4
GUSCIO	448	SS =	3.0	SI =	3.0
GUSCIO	449	SS =	3.6	SI =	3.6
GUSCIO	450	SS =	3.3	SI =	3.3
GUSCIO	451	SS =	5.8	SI =	5.8
GUSCIO	452	SS =	5.2	SI =	5.2
GUSCIO	453	SS =	6.6	SI =	6.6
GUSCIO	454	SS =	5.1	SI =	5.1
GUSCIO	455	SS =	4.9	SI =	4.9
GUSCIO	456	SS =	5.7	SI =	5.7
GUSCIO	457	SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
GUSCIO	460	SS =	2.1	SI =	2.1

GUSCIO	461	SS =	1.6	SI =	1.6
GUSCIO	462	SS =	3.0	SI =	3.0
GUSCIO	463	SS =	2.6	SI =	2.6
GUSCIO	464	SS =	1.9	SI =	1.9
GUSCIO	465	SS =	2.1	SI =	2.1
GUSCIO	466	SS =	1.9	SI =	1.9
GUSCIO	467	SS =	1.8	SI =	1.8
GUSCIO	468	SS =	2.1	SI =	2.1
GUSCIO	469	SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.1	SI =	2.1
GUSCIO	471	SS =	1.8	SI =	1.8
GUSCIO	472	SS =	2.3	SI =	2.3
GUSCIO	473	SS =	2.2	SI =	2.2
GUSCIO	474	SS =	2.2	SI =	2.2
GUSCIO	475	SS =	1.4	SI =	1.4
GUSCIO	476	SS =	2.1	SI =	2.1
GUSCIO	477	SS =	1.6	SI =	1.6
GUSCIO	478	SS =	1.5	SI =	1.5
GUSCIO	479	SS =	0.6	SI =	0.6
GUSCIO	480	SS =	1.6	SI =	1.6
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.3	SI =	2.3
GUSCIO	484	SS =	2.1	SI =	2.1
GUSCIO	485	SS =	2.5	SI =	2.5
GUSCIO	486	SS =	2.2	SI =	2.2
GUSCIO	487	SS =	3.3	SI =	3.3
GUSCIO	488	SS =	0.8	SI =	0.8
GUSCIO	489	SS =	2.8	SI =	2.8
GUSCIO	490	SS =	9.1	SI =	9.1
GUSCIO	491	SS =	8.3	SI =	8.3
GUSCIO	492	SS =	2.4	SI =	2.4
GUSCIO	493	SS =	3.3	SI =	3.3
GUSCIO	494	SS =	0.6	SI =	0.6
GUSCIO	495	SS =	2.6	SI =	2.6
GUSCIO	496	SS =	7.7	SI =	7.7
GUSCIO	497	SS =	5.5	SI =	5.5
GUSCIO	498	SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.5	SI =	2.5
		tensione max =	9.1	guscio =	490

SOLLECIT

		SS =	1.3	SI =	1.3
GUSCIO	426	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.8	SI =	2.8
		SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
		SS =	3.2	SI =	3.2
GUSCIO	429	SS =	2.0	SI =	2.0
		SS =	1.9	SI =	1.9
GUSCIO	430	SS =	4.5	SI =	4.5
		SS =	4.3	SI =	4.3
GUSCIO	431	SS =	4.8	SI =	4.8
		SS =	4.6	SI =	4.6
GUSCIO	432	SS =	4.1	SI =	4.1
		SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.4	SI =	6.4
		SS =	6.2	SI =	6.2
GUSCIO	434	SS =	6.4	SI =	6.4
		SS =	6.2	SI =	6.2
GUSCIO	435	SS =	8.9	SI =	8.9
		SS =	8.3	SI =	8.3
GUSCIO	436	SS =	6.1	SI =	6.1
		SS =	5.9	SI =	5.9
GUSCIO	437	SS =	6.1	SI =	6.1
		SS =	6.0	SI =	6.0
GUSCIO	438	SS =	7.9	SI =	7.9
		SS =	8.4	SI =	8.4
GUSCIO	439	SS =	3.8	SI =	3.8
		SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.5	SI =	4.5
		SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
		SS =	4.2	SI =	4.2
GUSCIO	442	SS =	2.6	SI =	2.6
		SS =	2.7	SI =	2.7
GUSCIO	443	SS =	3.3	SI =	3.3
		SS =	3.4	SI =	3.4
GUSCIO	444	SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	445	SS =	1.5	SI =	1.5
		SS =	1.3	SI =	1.3
GUSCIO	446	SS =	2.1	SI =	2.1
		SS =	1.9	SI =	1.9
GUSCIO	447	SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
GUSCIO	448	SS =	3.1	SI =	3.1
		SS =	2.8	SI =	2.8
GUSCIO	449	SS =	3.8	SI =	3.8
		SS =	3.4	SI =	3.4
GUSCIO	450	SS =	3.5	SI =	3.5
		SS =	3.1	SI =	3.1
GUSCIO	451	SS =	6.3	SI =	6.3
		SS =	5.4	SI =	5.4
GUSCIO	452	SS =	5.3	SI =	5.3
		SS =	5.0	SI =	5.0
GUSCIO	453	SS =	7.1	SI =	7.1
		SS =	6.1	SI =	6.1
GUSCIO	454	SS =	5.1	SI =	5.1
		SS =	5.1	SI =	5.1
GUSCIO	455	SS =	5.1	SI =	5.1
		SS =	4.8	SI =	4.8
GUSCIO	456	SS =	5.5	SI =	5.5
		SS =	5.8	SI =	5.8
GUSCIO	457	SS =	2.0	SI =	2.0
		SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
		SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3

GUSCIO	460	SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	461	SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
GUSCIO	462	SS =	2.6	SI =	2.6
		SS =	3.4	SI =	3.4
GUSCIO	463	SS =	2.4	SI =	2.4
		SS =	2.7	SI =	2.7
GUSCIO	464	SS =	1.8	SI =	1.8
		SS =	2.0	SI =	2.0
GUSCIO	465	SS =	2.3	SI =	2.3
		SS =	2.0	SI =	2.0
GUSCIO	466	SS =	1.7	SI =	1.7
		SS =	2.1	SI =	2.1
GUSCIO	467	SS =	1.7	SI =	1.7
		SS =	1.9	SI =	1.9
GUSCIO	468	SS =	1.9	SI =	1.9
		SS =	2.3	SI =	2.3
GUSCIO	469	SS =	2.4	SI =	2.4
		SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
GUSCIO	471	SS =	1.8	SI =	1.8
		SS =	1.9	SI =	1.9
GUSCIO	472	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
GUSCIO	473	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
GUSCIO	474	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
GUSCIO	475	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
GUSCIO	476	SS =	2.0	SI =	2.0
		SS =	2.3	SI =	2.3
GUSCIO	477	SS =	1.5	SI =	1.5
		SS =	1.7	SI =	1.7
GUSCIO	478	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
GUSCIO	479	SS =	0.4	SI =	0.4
		SS =	0.7	SI =	0.7
GUSCIO	480	SS =	1.2	SI =	1.2
		SS =	1.9	SI =	1.9
GUSCIO	481	SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
GUSCIO	482	SS =	2.7	SI =	2.7
		SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
GUSCIO	484	SS =	2.3	SI =	2.3
		SS =	1.8	SI =	1.8
GUSCIO	485	SS =	2.4	SI =	2.4
		SS =	2.7	SI =	2.7
GUSCIO	486	SS =	2.0	SI =	2.0
		SS =	2.4	SI =	2.4
GUSCIO	487	SS =	3.9	SI =	3.9
		SS =	2.8	SI =	2.8
GUSCIO	488	SS =	0.9	SI =	0.9
		SS =	0.7	SI =	0.7
GUSCIO	489	SS =	3.0	SI =	3.0
		SS =	2.6	SI =	2.6
GUSCIO	490	SS =	9.7	SI =	9.7
		SS =	8.6	SI =	8.6
GUSCIO	491	SS =	8.2	SI =	8.2
		SS =	8.4	SI =	8.4
GUSCIO	492	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
GUSCIO	493	SS =	2.7	SI =	2.7
		SS =	3.9	SI =	3.9

GUSCIO	494	SS =	0.7	SI =	0.7
		SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.9	SI =	2.9
		SS =	2.3	SI =	2.3
GUSCIO	496	SS =	8.7	SI =	8.7
		SS =	6.7	SI =	6.7
GUSCIO	497	SS =	4.8	SI =	4.8
		SS =	6.2	SI =	6.2
GUSCIO	498	SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.4	SI =	2.4
		SS =	2.6	SI =	2.6
tensione max =		9.7	guscio =	490	

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 14 Quasi Perm
N. 3 CONDIZIONE ANALISI STATICA
1 Peso proprio + 1.00
2 Permanente + 1.00
3 Azioni abilitazione + 0.30
1) +1.00*001 +1.00*002 +0.30*003
Unità di misura: SI,SS [dav/cm2]

GUSCIO	415	SS =	1.1	SI =	1.1
GUSCIO	416	SS =	0.8	SI =	0.8
GUSCIO	417	SS =	3.0	SI =	3.0
GUSCIO	418	SS =	3.0	SI =	3.0
GUSCIO	419	SS =	7.1	SI =	7.1
GUSCIO	420	SS =	5.8	SI =	5.8
GUSCIO	421	SS =	6.9	SI =	6.9
GUSCIO	422	SS =	5.7	SI =	5.7
GUSCIO	423	SS =	2.7	SI =	2.7
GUSCIO	424	SS =	2.8	SI =	2.8
GUSCIO	425	SS =	1.0	SI =	1.0
GUSCIO	426	SS =	0.6	SI =	0.6
GUSCIO	427	SS =	2.2	SI =	2.2
GUSCIO	428	SS =	2.6	SI =	2.6
GUSCIO	429	SS =	1.6	SI =	1.6
GUSCIO	430	SS =	3.6	SI =	3.6
GUSCIO	431	SS =	3.8	SI =	3.8
GUSCIO	432	SS =	3.2	SI =	3.2
GUSCIO	433	SS =	5.1	SI =	5.1
GUSCIO	434	SS =	5.1	SI =	5.1
GUSCIO	435	SS =	6.9	SI =	6.9
GUSCIO	436	SS =	4.8	SI =	4.8
GUSCIO	437	SS =	4.9	SI =	4.9
GUSCIO	438	SS =	6.6	SI =	6.6
GUSCIO	439	SS =	3.0	SI =	3.0
GUSCIO	440	SS =	3.7	SI =	3.7
GUSCIO	441	SS =	3.3	SI =	3.3
GUSCIO	442	SS =	2.2	SI =	2.2
GUSCIO	443	SS =	2.7	SI =	2.7
GUSCIO	444	SS =	1.7	SI =	1.7
GUSCIO	445	SS =	1.2	SI =	1.2
GUSCIO	446	SS =	1.7	SI =	1.7
GUSCIO	447	SS =	1.0	SI =	1.0
GUSCIO	448	SS =	2.4	SI =	2.4
GUSCIO	449	SS =	2.9	SI =	2.9
GUSCIO	450	SS =	2.6	SI =	2.6
GUSCIO	451	SS =	4.8	SI =	4.8
GUSCIO	452	SS =	4.3	SI =	4.3
GUSCIO	453	SS =	5.2	SI =	5.2
GUSCIO	454	SS =	4.2	SI =	4.2
GUSCIO	455	SS =	4.1	SI =	4.1
GUSCIO	456	SS =	4.6	SI =	4.6
GUSCIO	457	SS =	1.7	SI =	1.7
GUSCIO	458	SS =	2.2	SI =	2.2
GUSCIO	459	SS =	1.8	SI =	1.8
GUSCIO	460	SS =	1.9	SI =	1.9
GUSCIO	461	SS =	1.4	SI =	1.4
GUSCIO	462	SS =	2.5	SI =	2.5
GUSCIO	463	SS =	2.3	SI =	2.3
GUSCIO	464	SS =	1.7	SI =	1.7

COMBINAZIONE

GUSCIO	465	SS =	1.9	SI =	1.9
GUSCIO	466	SS =	1.6	SI =	1.6
GUSCIO	467	SS =	1.6	SI =	1.6
GUSCIO	468	SS =	1.8	SI =	1.8
GUSCIO	469	SS =	1.9	SI =	1.9
GUSCIO	470	SS =	1.9	SI =	1.9
GUSCIO	471	SS =	1.6	SI =	1.6
GUSCIO	472	SS =	2.0	SI =	2.0
GUSCIO	473	SS =	1.9	SI =	1.9
GUSCIO	474	SS =	1.9	SI =	1.9
GUSCIO	475	SS =	1.2	SI =	1.2
GUSCIO	476	SS =	1.9	SI =	1.9
GUSCIO	477	SS =	1.4	SI =	1.4
GUSCIO	478	SS =	1.3	SI =	1.3
GUSCIO	479	SS =	0.5	SI =	0.5
GUSCIO	480	SS =	1.4	SI =	1.4
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.4	SI =	2.4
GUSCIO	483	SS =	1.9	SI =	1.9
GUSCIO	484	SS =	1.9	SI =	1.9
GUSCIO	485	SS =	2.2	SI =	2.2
GUSCIO	486	SS =	1.9	SI =	1.9
GUSCIO	487	SS =	2.9	SI =	2.9
GUSCIO	488	SS =	0.6	SI =	0.6
GUSCIO	489	SS =	2.2	SI =	2.2
GUSCIO	490	SS =	7.3	SI =	7.3
GUSCIO	491	SS =	6.6	SI =	6.6
GUSCIO	492	SS =	1.9	SI =	1.9
GUSCIO	493	SS =	2.7	SI =	2.7
GUSCIO	494	SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.1	SI =	2.1
GUSCIO	496	SS =	6.3	SI =	6.3
GUSCIO	497	SS =	4.7	SI =	4.7
GUSCIO	498	SS =	1.2	SI =	1.2
GUSCIO	499	SS =	2.2	SI =	2.2
tensione max =		7.3	guscio =	490	

VERIFICA GUSCI IN C.A.:

MACROSCOPICO FONDAZ

VERIFICA ARMATURE EFFETTIVE (EFFETTO MEMBRANA + PIASTRA)

CASI DI CARICO:

Nome Descrizione
1 su VENT0
2 su VENT0
3 su VENT0
4 su su SIEWM
5 su su SIEWM
6 su su SIEWM
7 su su SIEWM

DATI:

tensione di snervamento acciaio (fyk): 4500 daN/cm2
coefficiente sicurezza acciaio: 1.15
deformazione ultima ultls: 1.97 per mille
deformazione ultima cls: 3.5 per mille
rapporto rottura/snervamento (k): 1.5
resistenza cilindrica cls (fck): 249 daN/cm2
coefficiente sicurezza cls: 1.5
coefficiente riduttivo (alfa): 0.85
copriferro inferiore (asse amatura): 3 cm
copriferro superiore (asse amatura): 3 cm
moltiplicatore sollecitazioni: 1

LEGENDA:

spess = spessore guscio, verfica effettuata su sezione Bm, con B-I cm e H="spess" cm
AF = area disposta al lembo teso, in cm2 al metro
Afc = area disposta al lembo compresso, in cm2 al metro
Mem = momento flettente (daN/cm)
Nor = sforzo normale [daN]
ecc = deformazione cls (per mille)
wfk = deformazione acciaio (per mille)

L'armatura è sufficiente se le deformazioni dei materiali sono ovunque minori delle corrispondenti deformazioni ultime.

INFERIORE ORIZZONTALE										INFERIORE VERTICALE									
GUSCI	spess	AF	Afc	Mem	Nor	ecc	of	wfk	spess	AF	Afc	Mem	Nor	ecc	of	wfk	spess	AF	Afc
415	35	4.21	4.21	1344	0	0.10	0.51	4.16	4.36	447	0	0	0	0.04	0.17				
416	35	4.21	4.21	497	0	0.04	0.19	4.16	4.36	278	0	0	0	0.02	0.11				
417	35	4.21	4.21	1815	0	0.14	0.68	4.16	4.36	1760	0	0	0	0.14	0.66				
418	35	4.21	4.21	511	0	0.04	0.19	4.16	4.36	1621	0	0	0	0.13	0.62				
419	35	4.21	4.21	2157	0	0.17	0.83	4.16	4.36	1465	0	0	0	0.17	0.83				
420	35	4.21	4.21	431	0	0.03	0.16	4.16	4.36	4386	0	0	0	0.36	1.75				
421	35	4.21	4.21	2447	0	0.17	0.85	4.16	4.36	4618	0	0	0	0.36	1.76				
422	35	4.21	4.21	347	0	0.03	0.13	4.16	4.36	4813	0	0	0	0.38	1.83				
423	35	4.21	4.21	1876	0	0.15	0.71	4.16	4.36	1819	0	0	0	0.14	0.69				
424	35	4.21	4.21	1815	0	0.03	0.05	4.16	4.36	1592	0	0	0	0.02	0.12				
425	35	4.21	4.21	1239	0	0.10	0.47	4.16	4.36	489	0	0	0	0.04	0.19				
426	35	4.21	4.21	451	0	0.04	0.17	4.16	4.36	307	0	0	0	0.02	0.12				
427	35	4.21	4.21	138	0	0.03	0.05	4.16	4.36	194	0	0	0	0.02	0.12				
428	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	319	0	0	0	0.02	0.12				
429	35	4.21	4.21	136	0	0.12	0.56	4.16	4.36	1761	0	0	0	0.14	0.67				
430	35	4.21	4.21	93	0	0.01	0.03	4.16	4.36	1073	0	0	0	0.08	0.41				
431	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	1157	0	0	0	0.09	0.44				
432	35	4.21	4.21	1530	0	0.12	0.58	4.16	4.36	2970	0	0	0	0.13	0.65				
433	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	2970	0	0	0	0.23	1.13				
434	35	4.21	4.21	303	0	0.02	0.08	4.16	4.36	618	0	0	0	0.05	0.24				
435	35	4.21	4.21	1527	0	0.12	0.57	4.16	4.36	3766	0	0	0	0.29	1.43				
436	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	324	0	0	0	0.05	0.24				
437	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	2377	0	0	0	0.19	0.90				
438	35	4.21	4.21	1307	0	0.12	0.57	4.16	4.36	3870	0	0	0	0.30	1.47				
439	35	4.21	4.21	0	0	0.02	0.11	4.16	4.36	91	0	0	0	0.01	0.03				
440	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	1074	0	0	0	0.08	0.41				
441	35	4.21	4.21	1276	0	0.10	0.48	4.16	4.36	607	0	0	0	0.03	0.12				
442	35	4.21	4.21	303	0	0.02	0.11	4.16	4.36	91	0	0	0	0.01	0.03				
443	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	321	0	0	0	0.03	0.12				
444	35	4.21	4.21	0	0	0.02	0.08	4.16	4.36	618	0	0	0	0.05	0.24				
445	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
446	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
447	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
448	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
449	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
450	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
451	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
452	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
453	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
454	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
455	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
456	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
457	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
458	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
459	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
460	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
461	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
462	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
463	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
464	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
465	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
466	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
467	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
468	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
469	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
470	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
471	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
472	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
473	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
474	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
475	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
476	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
477	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
478	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
479	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
480	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
481	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
482	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
483	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
484	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
485	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
486	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
487	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
488	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
489	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
490	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
491	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
492	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
493	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
494	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
495	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
496	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
497	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
498	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.0					

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[illegible]

107/136

[illegible]

VERIFICA PILASTRI:

VERIFICA PILASTRO IN CEMENTO ARMATO

Nome pilastro : P003a (ID=5)
Aste : 176
Metodo di verifica : stati limite - NTC08 (q=3.2)
Dettlilità : basca con gerarchia.
Unità di misura : cm; day; dan/cm; dan/cm; deform; %; 1/r Æ (permille)
Unità particolari : fessure {w}mm - ferri/mm e cm2 - sezioni:cm e derivate.
Copri-ferri (assi) : longitudoinal= 3.5 ; staffe= 2.5
Imperfetioni : M minimo = N * Æ0 ; M aggiunto = N * ei
Instabilità'ta' : rigidezza nominale {Ec2 5.8.7}; fief=3

MATERIALI

CLS : C25/30; Rck=300; fcd=249; fctd=17.91; fctm=25.58; Ecm=314472;
gc=1.5; fcd=141.1; fbd=26.86; fctd=11.94; Ecu=0.35%
ACCIAIO: B450C; ftk=5175; fyk=4500; Es=210000;
gc=1.5; fyk=3913; ftd=4500; ftd=4439.8; Eud=6.73%

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; fbd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.omegin=-15

SEZIONI UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acl=2500; i=y=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleç eoy leiz ieiy Lassi Lnet Lcr.L Cr.Si Af % am
1) 112.5 {2.5 | .4 | .4 | 120. | 120. | 0. | 0. | 0. | 26.521.0611201444616 |

CASI DI CARICO

Nome\Descrizione	Tipo	Sei
1)SLU	SLU (statico)	1
2)SLU VENTOK	SLU (statico)	1
3)SLU VENTOK	SLU (statico)	2
6)SLU con SIZMAX	SLU (statico)	4
7)SLU con SIZMAX	SLU (statico)	4
8)Rara	RARA	1
9)Rara Ventok	RARA	1
10)Rara Ventok	RARA	1
11)Frequent	FREQUENTE	1
12)Frequent Ventok	FREQUENTE	1
13)Frequent Ventok	FREQUENTE	1
14)Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI SINGOLI):
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1 C 10 -1 -204890. -1292.11 -12992.11 -0.01 -28.61 -0.005 106.61SI
1 S 6 -1 -243850. -6.21 -2438580. -6.21 -2438880. -6.21 -2438550.

TAGLI GERARCHIA:
Asi Lp C caso Veyd- caso Veyd- caso Veyd-
1120. | 6 -1 | -362.3 | 6 -1 | 0. | caso Veyd- | caso Veyd- |

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfetioni e second'ordine):
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
> 1) 3 -1 -18901. -189016.11.07 27667.11.05 -121. -28.61 -0.005 106.61SI
1 C 10 -1 -28958. -12596.11 12992.11 -0.01 -28.61 -0.005 106.61SI
1 S 1 -1 -29401. -10239.11.13 -82758.61.002 -17. -0.001 -53.21SI

INSTABILITA' - RIGIDEZZA NOMINALE V {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -125439891.120. | 58199.2 | 8.9492 | -173801. | -185580. | -186016. | .083 |

INSTABILITA' - RIGIDEZZA NOMINALE Z {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -125439891.120. | 58199.2 | 8.9492 | 264220. | 279998. | 276647. | .083 |

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -1082. -3462.3 | 53520. | 53879. | 53520. | 1.51111. | 2.4 | SI
1 C 6 -1 -1082. -3462.3 | 53464.3 | 53879. | 53464.3 | 1.51111. | 2.4 | SI
1 S 6 -1 -1082. -3462.3 | 53408.6 | 53879. | 53408.6 | 1.51111. | 2.4 | SI

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -559.21 -1789.5 | 53879. | 53879. | 53879. | 1.51111. | 2.4 | SI
1 C 13 -1 -559.21 -1789.5 | 53842.1 | 53879. | 53842.1 | 1.51111. | 2.4 | SI
1 S 7 -1 -559.21 -1789.5 | 53786.7 | 53879. | 53786.7 | 1.51111. | 2.4 | SI

NEI LIMITE (Ned < Nmx, Nmx=63% di Ncls; Ncls=rcfAc) {7.4.4.2.2.1};
Asta Caso Ned Nmx Ncls % NclsIVE
1) 3 -1 -1350. -22087.5 | -352750. | 1.31SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -19901.1 | -114806.4 | 181115.9 | -19. | 55.71SI
1 C 10 -1 -19536. | -87676. | 88802.1 | -13.7 | 13.51SI
1 S 10 -1 -19151.1 | -67646.9 | -3530.1 | -4.7 | -67.91SI

FREQUENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -1313.1 | -12621.1 | -28975.7 | 123627.4 | -10. | 12.71SI
1 C 13 -1 -1313.1 | -12621.1 | -28975.7 | 123627.4 | -10. | 12.71SI
1 S 13 -1 -11921.1 | -16129.2 | -3314.7 | -4.9 | -52.51SI

QUASI PERMANENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -141.1 | -10363.7 | 8522. | 103530.9 | 7.9 | 3.31SI
1 C 14 -1 -9788.7 | -5700.6 | 5020.7 | -5.6 | -23.1SI
1 S 14 -1 -9413.7 | -4649.1 | -3109.5 | -3.6 | -45.31SI

VERIFICA PILASTRO IN CEMENTO ARMATO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; fbd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.omegin=-15

SEZIONI UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acl=2500; i=y=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleç eoy leiz ieiy Lassi Lnet Lcr.L Cr.Si Af % am
1) 112.5 {2.5 | .4 | .4 | 120. | 120. | 0. | 0. | 0. | 26.521.0611201444616 |

CASI DI CARICO

Nome\Descrizione Tipo Sei
1)SLU SLU (statico) 1
2)SLU VENTOK SLU (statico) 1
3)SLU con SIZMAX SLU (statico) 4
6)SLU con SIZMAX SLU (statico) 4
7)SLU con SIZMAX SLU (statico) 4
8)Rara RARA 1
9)Rara Ventok RARA 1
10)Rara Ventok RARA 1
11)Frequent FREQUENTE 1
12)Frequent Ventok FREQUENTE 1
13)Frequent Ventok FREQUENTE 1
14)Quasi Perm QUASI PERMAN. 1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI SINGOLI):
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -2360580. -6.31 -2360510. -6.31 -2360710. -6.31 -2360860.
1 S 7 -1 -2371950. -7.31 -2371950. -7.31 -2358510. -7.31 -2358510.

TAGLI GERARCHIA:
Asi Lp C caso Veyd- caso Veyd- caso Veyd-
1120. | 6 -1 | 0. | 6 -3 | 4173.1 | 7 -2 | -1459.2 | 7 -3 | 1027.1 |

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfetioni e second'ordine):
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -10641. -187214.11.02 -217537.11.02 -0.01 -25.51 .017 346.71SI
1 C 6 -1 -10153. -138871.11 -103880.11 -0.01 -34.91 .006 121.41SI
1 S 1 -1 -9666. -100557.11.04 28054.15.28 -0.006 -8.51 .001 17.91SI

INSTABILITA' - RIGIDEZZA NOMINALE V {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -125287761.120. | 58128.6 | 8.96 | -219306. | -217352. | -217537. | .03 |

INSTABILITA' - RIGIDEZZA NOMINALE Z {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -125287761.120. | 58128.6 | 8.96 | -219306. | -217352. | -217537. | .03 |

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -1304.11 4173.1 | 53002.6 | 53879. | 53002.6 | 1.51111. | 2.4 | SI
1 C 6 -1 -1304.11 4173.1 | 53046.9 | 53879. | 53046.9 | 1.51111. | 2.4 | SI
1 S 6 -1 -1304.11 4173.1 | 52891.1 | 53879. | 52891.1 | 1.51111. | 2.4 | SI

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -456. -1459.2 | 53118.3 | 53879. | 53118.3 | 1.51111. | 2.4 | SI
1 C 7 -1 -456. -1459.2 | 53062.6 | 53879. | 53062.6 | 1.51111. | 2.4 | SI
1 S 7 -1 -456. -1459.2 | 53006.9 | 53879. | 53006.9 | 1.51111. | 2.4 | SI

NEI LIMITE (Ned < Nmx, Nmx=63% di Ncls; Ncls=rcfAc) {7.4.4.2.2.1};
Asta Caso Ned Nmx Ncls % NclsIVE
1) 7 -1 -4756.71 -229287.5 | -352750. | 1.31SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -7306.11 -12263.7 | -14659.6 | -17.3 | 219.71SI
1 C 10 -1 -6931.1 -10469.7 | 74158.8 | -10.2 | 79.41SI
1 S 10 -1 -6556.1 -6463.7 | 3521.9 | -5.1 | -3.1SI

FREQUENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -131.11 -4840. -3084. -93007.9 | -8.7 | 95.11SI
1 C 13 -1 -4465. -28933.2 | -48590.6 | -4.8 | 21.31SI
1 S 13 -1 -4090. -19122.5 | 1506.8 | -2.2 | -30.81SI

QUASI PERMANENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -141.1 -4015. -15330.2 | -63032.4 | -6.3 | 64.41SI
1 C 14 -1 -3649. -11279.9 | -49038.4 | -3.4 | 3.41SI
1 S 14 -1 -3649. -7729.7 | 1395.5 | -1.5 | -12.81SI

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfetioni e second'ordine):
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
> 1) 3 -2 -1991. 21366.11. -15412.11.05 -0.01 .45. .021 430.81SI
1) 3 -2 -1991. 11020.11. -7388.11.005 -0.006 -8.71 .006 120.31SI
1) 3 -2 -1991. 5775.1999.1. 5775.1999.1.001 -1.110. -4.61SI

INSTABILITA' - RIGIDEZZA NOMINALE V {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -2 -12521779.120. | 58096.1 | 8.965 | -14614. | -15450. | -15412. | .006 |

INSTABILITA' - RIGIDEZZA NOMINALE Z {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -2 -12521779.120. | 58096.1 | 8.965 | -14614. | -15450. | -15412. | .006 |

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -576.5 | 1844.9 | 52756.6 | 52756.6 | 53274.5 | 1.51111. | 2.35 | SI
1 C 6 -1 -576.5 | 1844.9 | 52756.6 | 52756.6 | 53274.5 | 1.51111. | 2.35 | SI
1 S 6 -1 -576.5 | 1844.9 | 52756.6 | 52756.6 | 53274.5 | 1.51111. | 2.35 | SI

TAGLI Z:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -1292.6 | 4136.3 | 52756.6 | 52756.6 | 53323.3 | 1.51111. | 2.35 | SI
1 C 7 -1 -1292.6 | 4136.3 | 52756.6 | 52756.6 | 53323.3 | 1.51111. | 2.35 | SI
1 S 7 -1 -1292.6 | 4136.3 | 52756.6 | 52756.6 | 53323.3 | 1.51111. | 2.35 | SI

NEI LIMITE (Ned < Nmx, Nmx=63% di Ncls; Ncls=rcfAc) {7.4.4.2.2.1};
Asta Caso Ned Nmx Ncls % NclsIVE
1) 7 -1 -895.4 | -229287.5 | -352750. | 1.25SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -1332.3 | 147499.7 | -9442. -10.1 | 285.41SI
1 C 10 -1 -1332.3 | 147499.7 | -9442. -10.1 | 285.41SI
1 S 10 -1 -1332.3 | 147499.7 | -9442. -10.1 | 285.41SI

FREQUENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -723.5 | 50336.1 | -3388. -3.9 | 100.1SI
1 C 13 -1 -723.5 | 50336.1 | -3388. -3.9 | 100.1SI
1 S 13 -1 -723.5 | 50336.1 | -3388. -3.9 | 100.1SI

QUASI PERMANENTE:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -141.1 -540.5 | 30940. | -188.1 | -2.1 | 49.91SI
1 C 14 -1 -540.5 | 30940. | -188.1 | -2.1 | 49.91SI
1 S 14 -1 -540.5 | 30940. | -188.1 | -2.1 | 49.91SI

VERIFICA PILASTRO IN CEMENTO ARMATO

Nome pilastro : P003b (ID=5)
Aste : 176
Metodo di verifica : stati limite - NTC08 (q=3.2)
Dettlilità : basca con gerarchia.
Unità di misura : cm; day; dan/cm; dan/cm; deform; %; 1/r Æ (permille)
Unità particolari : fessure {w}mm - ferri/mm e cm2 - sezioni:cm e derivate.
Copri-ferri (assi) : longitudoinal= 3.5 ; staffe= 2.5
Imperfetioni : M minimo = N * Æ0 ; M aggiunto = N * ei
Instabilità'ta' : rigidezza nominale {Ec2 5.8.7}; fief=3

CLS : C25/30; Rck=300; fcd=249; fctd=17.91; fctm=25.58; Ecm=314472;
gc=1.5; fcd=141.1; fbd=26.86; fctd=11.94; Ecu=0.35%
ACCIAIO: B450C; ftk=5175; fyk=4500; Es=210000;
gc=1.5; fyk=3913; ftd=4500; ftd=4439.8; Eud=6.73%

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; fbd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.omegin=-15

SEZIONI UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acl=2500; i=y=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleç eoy leiz ieiy Lassi Lnet Lcr.L Cr.Si Af % am
1) 112.5 {2.5 | .4 | .4 | 120. | 120. | 0. | 0. | 0. | 26.521.0611201444616 |

CASI DI CARICO

Nome\Descrizione	Tipo	Sei
1)SLU	SLU (statico)	1
2)SLU VENTOK	SLU (statico)	1
3)SLU VENTOK	SLU (statico)	1
6)SLU con SIZMAX	SLU (statico)	4
7)SLU con SIZMAX	SLU (statico)	4
8)Rara	RARA	1
9)Rara Ventok	RARA	1
10)Rara Ventok	RARA	1
11)Frequent	FREQUENTE	1
12)Frequent Ventok	FREQUENTE	1
13)Frequent Ventok	FREQUENTE	1
14)Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI SINGOLI):
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -2351940. -7.21 -2351940. -7.21 -2337120. -7.21 -2337120.
1 S 7 -1 -2337780. -7.21 -2337810. -7.21 -2336930.

TAGLI GERARCHIA:
Asi Lp C caso Veyd- caso Veyd- caso Veyd-
1120. | 7 -1 | 1484.8 | 6 -1 | 7 -3 | -769.9 | 7 -2 | 814.1 |

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfetioni e second'ordine):
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
> 1) 3 -1 -5018. -94357.11.02 58534.11.04 -0.007 -9.61 .005 106.61SI
1) 3 -1 -4531. -11876.11.11 13099.11.006 -8.71 .006 120.31SI
1) 3 -1 -4043. -148622.11.01 -27945.11.061 -0.008 -11.51 .01 209.51SI

INSTABILITA' - RIGIDEZZA NOMINALE V {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -12524228.120. | 58107.5 | 8.9633 | -146945. | -148622. | -146622. | .014 |

INSTABILITA' - RIGIDEZZA NOMINALE Z {Ec2 5.8.7};
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -12524228.120. | 58107.5 | 8.9633 | -146945. | -148622. | -146622. | .014 |

TAGLI Y:
Asta Caso Ned Meyd Mezd E cls oc E acc of IVE
1) 3 -1 -464. -1484.8 | 52969.3 | 53879. | 52969.3 | 1.51111. | 2.4 | SI
1 C 7 -1 -464. -1484.8 | 52913.6 | 53879. | 52913.6 | 1.51111. | 2.4 | SI
1 S 7 -1 -464. -1484.8 | 52857.9 | 53879. | 52857.9 | 1.51111. | 2.4 | SI

TAGLIO Z:									
Asta	Caso	Ved	Ved ger.	Ved	Vrsd	Vrzd	Asw	s	ctgttIVE
1 I	7- 2	254.4	814.1	52756.6	52756.6	53413.1	1.5111.	2.35	SI
1 C	7- 2	254.4	814.1	52756.6	52756.6	53356.5	1.5111.	2.35	SI
1 S	7- 2	254.4	814.1	52756.6	52756.6	53300.1	1.5111.	2.35	SI
NED LIMITE (Ned < Nmax ; Nmax=65% di Nc1s ; Nc1s=fcfd*Ac) [7.4.4.2.2.1]:									
Asta	Caso	Ned	Nmax	Nc1s	% Nc1sVE				
1 I	7- 3	-3838.5	-229287.5	-352750.	1.09	SI			

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	10- 1	-3521.5	-65522.6	39583.6	-6.5	68.2	SI
1 C	10- 1	-3146.5	-8045.6	10961.8	-5.9	79.3	SI
1 S	10- 1	-2771.5	-96168.7	-17660.	-7.6	135.8	SI

FREQUENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	13- 1	-2928.6	-26409.2	33187.6	-3.7	22.3	SI
1 C	13- 1	-2552.6	-2002.7	11456.7	-2.7	11.	SI
1 S	13- 1	-2178.6	-34976.2	-10274.2	-2.8	20.4	SI

QUASI PERMANENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	14- 1	-2664.6	-16951.	30223.6	-2.9	13.8	SI
1 C	14- 1	-2289.6	-17365.8	11157.5	-1.9	2.7	SI
1 S	14- 1	-1914.6	-17780.5	-7828.6	-1.7	3.4	SI

VERIFICA PILASTRO IN CEMENTO ARMATO

Nome pilastro : P03c (ID=6)
Asse : 175
Metodo di verifica : stati limite - NTC08 (q=3.2)
Durettà/ta : bassa con gerarchia.
Unità' di misura : cm; daV; daV/cm; daVcm; daV/cm2; deform. %; 1/r à6°(permille)
Unità' particolari : fessure (m)mm - ferri/mm e cm2 - sezioni/cm e derivate.
Coeff.ferri (ass): : longitudo/m1s 3.5 ; statifee 2.5
Imperfezioni : M minimo = N * e0 ; M aggiunto = N * ei
Incurvabilità : rigidizza nominale [Ec2 5.8.7]; Fief=3

MATERIALI

CLS : C25/30; Rcs=300; fcd=240; fctd=17.91; fctm=25.58; Ecm=314472;
gs=1.5; fctd141.1; ftd=26.86; fctd11.94; Ecu=8.39;
ACCIAIO: B450c; fts=5175; fyk=4500; E=2100000;
gs=1.5; fyd=3913; ftd=4500; fud=4439.8; Eud=6.79c

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; ftd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.Omgeln=15

SEZIONE UTILIZZATE

1) Rettangolare: base=50; alt.=50; ACl=2500; iy=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As SeleZ |eY |eiz |eiy |Lassi Lnet Lcr.I Lcr.S| Af % am |
1 I 1|2.5 |2.5 |.4 |.4 |120. |120. |0. |0. |26.52|1.061126|14+40|6 |

CASI DI CARICO

Nome	Descrizione	Tipo	Ses
1	SLU	SLU (statico)	1
2	SLU VENTOK	SLU (statico)	1
3	SLU VENTIOY	SLU (statico)	2
6	SLU con STEMAX	SLU (statico)	4
7	SLU con STEWAY	SLU (statico)	4
8	Rara	RARA	1
9	Rara Ventok	RARA	1
10	Rara Ventioy	RARA	2
11	Frequente	FREQUENTE	1
12	Frequente Ventok	FREQUENTE	1
13	Frequente Ventioy	FREQUENTE	2
14	Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI STATICI):

Asta	Caso	Mu+ min	Caso	Mu+ min	Caso	Mu- min	Caso	Mu+ min
1 I	6- 1	-2345700.	6- 1	2345700.	7- 2	-2339910.	7- 2	2339980.
1 S	7- 4	-2341740.	7- 4	2341740.	7- 4	-2327280.	7- 4	2327280.

TAGLI GERARCHIA:

As	Lp	caso	VEyd-	caso	VEyd+	caso	VEzd-	caso	VEzd+
1	120.	6- 1	0.	7- 3	2053.5	7- 1	-889.8	7- 4	3.4

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfezioni e second'ordine):

Asta	Caso	NEd	MEyd	MEzd	E cls	oc	E acc	of	VE
> 1	3- 1	-4744.	-124117.1 02	-102697.1 02	-0.11	-14.9	0.11	233.	SI
1	3- 1	-4257.	-112810.1 1-	-53314.1.	-0.08	-10.8	.007	156.7	SI
1	3- 1	-3769.	-104910.1 01	-10396.1 88	-0.05	-7.5	.005	109.2	SI

INSTABILITÀ - RIGIDEZZA NOMINALE Y [Ec2 5.8.7]:

Asta	Caso	NB	IO	JH	JCIS/JH	Mca1	MUEI	MED	Hu
1 I	3- 1	-12524006	120.	58106.5	8.9634	-122172.	-124070.	-124117.	.013

INSTABILITÀ - RIGIDEZZA NOMINALE Z [Ec2 5.8.7]:

Asta	Caso	NB	Io	Io	Ic1s/Io	Mca1	MEd	MEd	nu
1 I	3- 1	-12524066	120.	58106.5	8.9634	-100760.	-102658.	-102697.	.013

TAGLIO Y:

Asta	Caso	Ved	Ved ger.	Ved	Vrsd	Vrzd	Asw	s	ctgttIVE
1 I	7- 3	641.7	2053.5	52009.9	53879.	52009.9	1.5111.	2.4	SI
1 C	7- 3	641.7	2053.5	52854.2	53879.	52854.2	1.5111.	2.4	SI
1 S	7- 3	641.7	2053.5	52796.5	53879.	52796.5	1.5111.	2.4	SI

TAGLIO Z:

Asta	Caso	Ved	Ved ger.	Ved	Vrsd	Vrzd	Asw	s	ctgttIVE
1 I	7- 1	-278.1	-889.8	52921.8	53879.	52921.8	1.5111.	2.4	SI
1 C	7- 1	-278.1	-889.8	52866.1	53879.	52866.1	1.5111.	2.4	SI
1 S	7- 1	-278.1	-889.8	52810.3	53879.	52810.3	1.5111.	2.4	SI

NED LIMITE (Ned < Nmax ; Nmax=65% di Nc1s ; Nc1s=fcfd*Ac) [7.4.4.2.2.1]:

Asta	Caso	NEd	Nmax	Nc1s	% Nc1s	VE
1	7- 1	-3434.	-229287.5	-352750.	.97	SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	10- 1	-3334.6	-82947.2	-71000.1	-10.2	153.2	SI
1 C	10- 1	-2959.6	-76003.6	-37460.4	-7.4	104.3	SI
1 S	10- 1	-2504.6	-69060.	-3503.7	-4.7	65.7	SI

FREQUENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
------	------	-----	------	------	----	----	----

1 I	13- 1	-2791.1	-37501.2	-61264.1	-6.4	81.1	SI
1 C	13- 1	-2416.1	-20240.2	-31515.2	-3.8	31.7	SI
1 S	13- 1	-2041.1	-20979.2	-1766.4	-1.6	1.	SI

QUASI PERMANENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	14- 1	-2546.8	-24959.2	-56442.5	-5.2	63.6	SI
1 C	14- 1	-2171.8	-16649.2	-28796.9	-2.8	18.3	SI
1 S	14- 1	-1796.8	-8339.3	-1151.3	-1.	-4.6	SI

VERIFICA ASTE IN ACCIAIO:

VERIFICA ELEMENTI IN ACCIAIO

Numero = 15044.
Unità di misura:
Lunghezza: cm
Prop. sez.: cm
Rozze: daN
Momenti: daNm
Tensioni: daN/cm2
MATERIALE:
S235 (N 10025-2) Mod.EI = 210000000; $\rho_H = 1.050$;
fyk = 2350.0(2150.0 per sp=40 mm); fyd = 238.1(2047.6 per sp=40 mm).

CASI DI CARICO

N	Descrizione	Soll.
1	SU	1
2	SU VENTOS	1
3	SU VENTOS	2
4	SU con SISM	4
5	SU con SISM	4

CARATTERISTICHE GEOMETRICHE
P.LIN180_S001 (1)
A = 27.9857e+00 Ix= 1.3549e+03 Iy=113.3579e+00 Ix= 8.8711e+00
P.LIN180_S002 (2)
A = 78.2479e+00 Ix= 5.7065e+03 Iy= 2.0036e+03 Ix= 47.0030e+00
P.LIN180_S003 (3)
A = 54.3071e+00 Ix= 2.4964e+03 Iy=889.3628e+00 Ix= 24.5209e+00
P.LIN180_S001 (1) stato limite ultimo - ASTA (466- 470) 0.

PROGR.

SOLLECITAZIONI							
Caso		MZ	MY	MT	N	TZ	TY
3-2		71104.7	117.6	-66.9	-777.7	-0.7	-1475
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-2	si	2		-505.4	0.0	0.0	505.4
3-2	si	2	Sx	444.5	-48.0	0.0	452.3
3-2	si	5		-25.8	0.0	128.1	223.3
3-2	si	8	Ty	-500.1	47.9	0.0	507.0
			Si				

3-1	24388.9	7010.8	-323.2	-372.3	-22.2	45.7
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	506.3	0.0	0.0	506.3	
3-1	3-1	-175.3	-48.0	0.0	194.0	
3-1	3-1	60.9	-34.2	0.0	60.9	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	18332.4	8021.9	6.5	-2.6	-333.9
3-1	3-1	18486.1	7412.7	-591.1	3.0	-329.0
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	480.6	0.0	0.0	480.6	
3-1	3-1	-143.6	53.8	0.0	171.2	
3-1	3-1	104.8	0.0	56.4	143.3	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-2060.0	6755.3	-323.2	N	28.3
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	-7.3	65.8	0.0	114.1	
3-1	3-1	85.8	0.0	87.4		

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-40699.6	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	532.7	0.0	0.0	532.7	
3-1	3-1	233.5	77.8	0.0	209.6	
3-1	3-1	48.8	0.0	118.4	210.7	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-93882.6	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	769.6	0.0	0.0	769.6	
3-1	3-1	-164.0	0.0	0.0	164.0	
3-1	3-1	-6.2	0.0	149.3	258.7	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-162809.0	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	1160.8	0.0	0.0	1160.8	
3-1	3-1	1028.9	101.8	0.0	1043.9	
3-1	3-1	-79.3	0.0	180.3	322.2	

VERIFICA STABILITA' :
 Z (Lc = 336, Ro = 6.96)Im = 48.3Ncr= 248509.61aIa(c)=-0.4900(ki=0.8349)
 Y (Lc = 336, Ro = 2.01)Im = 167.0Ncr= 20791.81aIa(c)=-0.4900(ki=0.2392)
 Caso 3-1 - Nodo 3 - Asse Y
 Ned = -1470.4Mreq = -122106.7Mreq = 5964.0Ss = -1322.8 (0.591)

P.LIN180_S001 (1) stato limite ultimo - ASTA (340- 729) 15						
SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-162809.0	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	1137.3	0.0	0.0	1137.3	
3-1	3-1	1069.2	-221.7	0.0	1089.8	
3-1	3-1	-38.1	0.0	-200.6	349.5	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-1297020.4	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	906.0	0.0	0.0	906.0	
3-1	3-1	849.4	-116.6	0.0	873.1	
3-1	3-1	-33.8	0.0	-184.6	704.2	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-100265.5	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	698.9	0.0	0.0	698.9	
3-1	3-1	653.7	-113.5	0.0	681.7	
3-1	3-1	-29.4	0.0	-168.5	293.4	
3-1	3-1	-678.3	109.2	0.0	704.2	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-74444.3	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	519.6	0.0	0.0	519.6	
3-1	3-1	482.2	0.0	0.0	516.3	
3-1	3-1	-25.1	0.0	-152.5	337.9	
3-1	3-1	-506.8	104.1	0.0	537.9	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-52256.7	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	367.8	0.0	0.0	367.8	
3-1	3-1	334.8	-101.4	0.0	378.1	
3-1	3-1	-29.7	0.0	-130.5	269.3	
3-1	3-1	-359.4	99.0	0.0	398.2	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-33700.7	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	240.2	0.0	0.0	240.2	
3-1	3-1	211.6	-96.3	0.0	269.4	
3-1	3-1	-16.4	0.0	-120.5	203.9	
3-1	3-1	-236.2	93.9	0.0	286.8	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-18782.5	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	137.8	0.0	0.0	137.8	
3-1	3-1	112.5	-91.2	0.0	193.9	
3-1	3-1	-21.0	0.0	-101.4	181.3	
3-1	3-1	-137.0	88.9	0.0	206.1	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-2476.9	1929.9	78.5	-367.6	-16.1
3-1	3-1	-7495.9	272.7	78.5	-343.8	-13.7

Caso	Ve No massimi	Sx	Tz	Ty	Si	
6-3	3-1	-116.0	0.0	0.0	116.0	
3-1	3-1	-27.5	0.0	0.0	153.8	
3-1	3-1	-7.6	0.0	-88.4	153.3	
3-1	3-1	-62.1	83.8	0.0	157.8	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
6-3	3-1	2231.6	78.5	-367.6	-16.1	104.3
3-1	3-1	157.1	516.7	-343.8	-13.7	311.3
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	-113.4	0.0	0.0	113.4	
3-1	3-1	-13.3	-81.1	0.0	141.0	
3-1	3-1	-3.3	0.0	-72.4	125.4	

VERIFICA STABILITA' : Z (Lc = 150, Ro = 6.96)Im = 21.6Ncr= 1248070.31aIa(c)=-0.4900(ki=0.8650) Y (Lc = 150, Ro = 2.01)Im = 74.5Ncr= 104421.11aIa(c)=-0.4900(ki=0.6662) Caso 3-1 - Nodo 4 - Asse Y Ned = -343.8Mreq = -122106.7Mreq = -1140.5Ss = -849.2 (0.379)						
P.LIN180_S001 (1) stato limite ultimo - ASTA (471- 732) 16						
SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-150401.5	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	1078.9	0.0	0.0	1078.9	
3-1	3-1	1011.9	-117.7	0.0	1032.2	
3-1	3-1	-12.6	0.0	-102.9	334.3	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-118865.0	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	882.9	0.0	0.0	882.9	
3-1	3-1	802.4	-112.6	0.0	825.8	
3-1	3-1	-10.1	0.0	-176.9	306.5	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-90062.1	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	671.1	0.0	0.0	671.1	
3-1	3-1	617.0	-107.5	0.0	644.6	
3-1	3-1	-7.7	0.0	-160.8	278.7	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-66692.9	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	503.3	0.0	0.0	503.3	
3-1	3-1	455.3	-102.5	0.0	489.2	
3-1	3-1	-5.2	0.0	-144.8	250.9	

SOLLECITAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-46057.3	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	359.8	0.0	0.0	359.8	
3-1	3-1	318.8	-97.4	0.0	360.6	
3-1	3-1	-2.7	0.0	-128.8	223.1	

SOLLECITAZIONE							
Caso	MZ		MY	MT	N	TZ	TY
3-1	-29055.4		-770.4	507.1	359.4	-7.8	809.9
TENSIONE							
Caso	Ve No	massimi	Sx	Tz	Ty	Si	
3-1	3-1	2	240.3	0.0	0.0	240.3	
3-1	3-1	8	205.8	-92.3	0.0	260.6	
3-1	3-1	5	-0.2	0.0	-112.8	195.3	
SOLLECITAZIONE							PROGR.
							112

[illegible]

RUFIDA STABILITY : 1									
LU = 336, $\rho = 0.96$ $16 = 48.3$ $\ln \rho = 24859.0$ $6 \ln \rho / C = 40.4000$ $(16 / 0.8349)$ Z LC = 336, $\rho_0 = 2.01$ $16 = 167.0$ $\ln \rho_0 = 20791.8$ $6 \ln \rho_0 / C = 340.4000$ $(16 / 0.8349)$ N = 650, $1 \ln \rho = 6666.5$ $6 \ln \rho = 6666.5$ $16 \ln \rho = 6666.5$ $16 \ln \rho = -845.1$ (0.378)									
PJLNH0300 (1) state 11814 1010 ASTA (498 342) 27.0									
SOLLECTATION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 1	-99579.4	330.0	-1578.2	99.6	1570.0				
3 - 1	-95629.4	-577.6	338.6	-414.7	-98.0				1559.4
TENSION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 1	1181.0	-732.3	0.0	0.0	732.3				
3 - 1	1181.0	-732.3	0.0	0.0	732.3				
3 - 1	1181.0	-24.6	0.0	-139.5	277.4				
SOLLECTATION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 1	-38510.0	3009.2	338.6	-115.1	-72.8				1184.7
TENSION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 1	394.2	-394.2	0.0	0.0	394.2				
3 - 1	1181.0	245.6	-84.3	0.0	285.8				
3 - 1	1181.0	44.2	0.0	-128.5	277.0				84.0
SOLLECTATION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 1	3884.0	5536.6	338.6	24.5	-47.5				810.1
TENSION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 1	218.0	-272.7	0.0	0.0	272.7				
3 - 1	218.0	-24.9	-72.3	0.0	127.8				
3 - 1	218.0	95.0	0.0	-97.6	193.8				
SOLLECTATION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 1	30050.6	7004.6	338.6	244.2	-22.3				435.4
TENSION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 1	218.0	-504.4	0.0	0.0	504.4				
3 - 1	218.0	-190.9	-60.3	0.0	217.6				
3 - 1	218.0	127.8	0.0	-66.6	155.3				
SOLLECTATION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 2	38990.3	-7390.0	-193.4	-699.7	-1.3				71.8
3 - 2	402.8	7413.3	338.6	463.8	28.1				302.8
TENSION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 2	218.0	585.6	0.0	0.0	585.6				
3 - 2	218.0	285.4	48.8	0.0	297.7				
3 - 2	218.0	142.6	0.0	-35.6	155.3				
SOLLECTATION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 2	33537.3	-7346.5	-193.4	-480.0	-26.5				302.8
3 - 2	402.8	7413.3	338.6	603.1	28.1				311.8
TENSION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 2	218.0	535.1	0.0	0.0	535.1				
3 - 2	218.0	-209.1	57.7	0.0	231.7				
3 - 2	218.0	139.4	0.0	56.5	170.3				
SOLLECTATION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 2	13041.0	-5703.7	-193.4	-260.4	-51.7				677.5
3 - 2	402.8	7413.3	338.6	903.1	53.1				688.0
TENSION									
Caso	MZ	MT	N	TZ	SI	PRG			
3 - 2	218.0	332.6	0.0	0.0	332.6				
3 - 2	218.0	-61.3	69.7	0.0	135.3				
3 - 2	218.0	118.1	0.0	0.0	118.1				

ELECTRIZATING												
3-1	1	57290.4	MY	-144.3	MT	-526.4	N	-7.9	TZ	-24.6	TY	1113.3
TDGSION												
3-1	1	1	Sx		Tz		0.0	0.0		86.7		
3-1	1	1	2	Sx		386.7		0.0	0.0	86.7		
3-1	1	1	3	Sx		380.3		0.0	0.0	86.7		
3-1	1	1	4	Tz		-2.7	0.0	-139.6		241.8		
PROGR.												
SOLLECTIZATING												
3-1	1	1	5	MT		243.9	N	-8.0	TZ	7.0		
3-1	1	1	6	MT		398.3	-526.4	-7.9	-23.3			
TDGSION												
3-1	1	1	7	Sx		Tz		Ty				
3-1	1	1	8	Sx		287.0		0.0	0.0	287.0		
3-1	1	1	9	Tz		-25.7	-49.8	0.0	0.0	38.4		
3-1	1	1	10	Tz		6.5	0.0	-123.6		214.1		
3-1	1	1	11	Ty						214.1		
PROGR.												
SOLLECTIZATING												
3-1	1	1	12	MY		MT	N	-8.0	TZ	14.8		
3-1	1	1	13	MY		-1363.5	243.9	-7.9	-12.5			
3-1	1	1	14	MT		730.1	-526.4	-8.0	-72.1			
TDGSION												
3-1	1	1	15	Sx		Tz		Ty				
3-1	1	1	16	Sx		134.5		0.0	0.0	20.4		
3-1	1	1	17	Tz		151.2	-49.1	0.0	0.0	221.1		
3-1	1	1	18	Tz		12.1	0.0	-107.5		186.7		
3-1	1	1	19	Ty						186.7		
PROGR.												
SOLLECTIZATING												
3-1	1	1	20	MY		MT	N	-8.0	TZ	15.7		
3-1	1	1	21	MY		-1334.7	243.9	-7.9	-3.5			
3-1	1	1	22	MT		850.9	-526.4	-8.0	-0.8			
TDGSION												
3-1	1	1	23	Sx		Tz		Ty				
3-1	1	1	24	Sx		134.5		0.0	0.0	134.5		
3-1	1	1	25	Tz		72.9	-87.1	0.0	0.0	167.5		
3-1	1	1	26	Tz		15.7	-82.8	0.0	0.0	193.1		
3-1	1	1	27	Ty		-705.5	86.9	0.0	0.0	167.5		
PROGR.												
SOLLECTIZATING												
3-1	1	1	28	MY		MT	N	-8.0	TZ	10.4		
3-1	1	1	29	MY		-2859.2	243.9	-7.9	-7.7			
3-1	1	1	30	MT		760.7	-526.4	-8.0	-10.4			
TDGSION												
3-1	1	1	31	Sx		Tz		Ty				
3-1	1	1	32	Sx		80.3		0.0	0.0	80.3		
3-1	1	1	33	Tz		12.6	-82.8	0.0	0.0	144.7		
3-1	1	1	34	Tz		11.6	0.0	-75.5		131.4		
3-1	1	1	35	Ty						131.4		
PROGR.												
SOLLECTIZATING												
3-1	1	1	36	MY		MT	N	-8.0	TZ	10.0		
3-1	1	1	37	MY		-1204.5	243.9	-7.9	-7.0			
3-1	1	1	38	MT		1664.8	-526.4	-8.0	-21.7			
TDGSION												
3-1	1	1	39	Sx		Tz		Ty				
3-1	1	1	40	Sx		70.1		0.0	0.0	20.1		
3-1	1	1	41	Tz		10.8	78.7	0.0	0.0	136.8		
3-1	1	1	42	Tz		7.5	0.0	-59.5		103.3		
3-1	1	1	43	Ty						103.3		
PROGR.												
SOLLECTIZATING												
3-1	1	1	44	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	45	MY		-783.0	243.9	-7.9	-30.2			
3-1	1	1	46	MT		2829.5	-52.4	-526.4	-8.0	32.9		-49.6
TDGSION												
3-1	1	1	47	Sx		Tz		Ty				
3-1	1	1	48	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	49	Tz		-17.3	77.2	0.0	0.0	134.8		
3-1	1	1	50	Tz		-13.7	0.0	53.8		94.1		
3-1	1	1	51	Ty						94.1		
PROGR.												
SOLLECTIZATING												
3-1	1	1	52	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	53	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	54	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	55	Sx		Tz		Ty				
3-1	1	1	56	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	57	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	58	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	59	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	60	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	61	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	62	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	63	Sx		Tz		Ty				
3-1	1	1	64	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	65	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	66	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	67	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	68	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	69	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	70	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	71	Sx		Tz		Ty				
3-1	1	1	72	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	73	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	74	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	75	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	76	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	77	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	78	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	79	Sx		Tz		Ty				
3-1	1	1	80	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	81	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	82	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	83	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	84	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	85	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	86	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	87	Sx		Tz		Ty				
3-1	1	1	88	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	89	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	90	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	91	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	92	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	93	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	94	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	95	Sx		Tz		Ty				
3-1	1	1	96	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	97	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	98	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	99	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	100	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	101	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	102	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	103	Sx		Tz		Ty				
3-1	1	1	104	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	105	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	106	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	107	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	108	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	109	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	110	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	111	Sx		Tz		Ty				
3-1	1	1	112	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	113	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	114	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	115	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	116	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	117	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	118	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	119	Sx		Tz		Ty				
3-1	1	1	120	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	121	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	122	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	123	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	124	MY		MT	N	-8.0	TZ	13.2		
3-1	1	1	125	MY		-1777.2	-21.7	-31.2	8.3			-67.4
3-1	1	1	126	MT		-58.8	-775.3	-526.4	-7.9	44.2		-24.2
TDGSION												
3-1	1	1	127	Sx		Tz		Ty				
3-1	1	1	128	Sx		134.5		0.0	0.0	134.6		
3-1	1	1	129	Tz		1.0	83.3	0.0	0.0	144.2		
3-1	1	1	130	Tz		-13.5	0.0	67.6		117.9		
3-1	1	1	131	Ty						117.9		
PROGR.												
SOLLECTIZATING												
3-1	1	1	132	MY		MT	N	-8.0	T			

PUNTO		Caso		Vel	Nel	messini	Sx	Tz	0,0	0,0	Ty	Sz	416,0	0,0		
3 - 1		1	1	1	1	1	416,0	0,0	0,0	0,0	Ty	Sz	416,0	0,0		
3 - 1		1	1	1	1	1	38,8	37,6	0,0	0,0	0,0	394,3	0,0	0,0		
3 - 1		1	1	1	1	1	166,0	0,0	0,0	117,9	0,0	204,8	0,0	0,0		
VERIFICA STABILITA' : asta tesa per tutti i casi di carico.																
P_LPJN30_0001 (1) stato l'inter ultimo - ASTA (750 - 460) 134 0.																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	-563,6	Tz	-0,5	Ty	-958,2	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	20,1	0,0	0,0	0,0	0,0	0,0	48,0	0,0	0,0	
3 - 1		1	1	1	1	1	-20,1	-0,0	-25,2	0,0	0,0	0,0	137,7	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-20,1	0,0	0,0	79,2	0,0	138,7	0,0	0,0	
PROGR. 29.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-2327,4	M	15,4	0,0	N	-563,6	Tz	-0,5	Ty	-661,1
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-175,5	0,0	0,0	0,0	0,0	175,5	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-174,8	-37,4	0,0	0,0	0,0	17,3	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-19,9	0,0	0,0	54,7	0,0	96,7	0,0	0,0	
PROGR. 58.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-3801,6	M	30,8	0,0	N	-563,6	Tz	-0,5	Ty	-363,9
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-274,0	0,0	0,0	0,0	0,0	274,0	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-272,6	-9,6	0,0	0,0	0,0	23,1	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-19,6	0,0	0,0	30,1	0,0	53,7	0,0	0,0	
PROGR. 86.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-44202,8	M	46,2	0,0	N	-563,6	Tz	-0,5	Ty	-66,8
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	11,8	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-313,8	-1,8	0,0	0,0	0,0	313,8	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-19,4	0,0	0,0	5,5	0,0	21,6	0,0	0,0	
PROGR. 115.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-41859,7	M	61,6	0,0	N	-563,6	Tz	-0,5	Ty	230,4
3 - 1		1	1	1	1	1	Sx	-64,8	0,0	0,0	0,0	0,0	64,8	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-300,9	0,0	0,0	0,0	0,0	300,9	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-267,4	-6,3	0,0	0,0	0,0	267,6	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-3,6	0,0	0,0	-19,7	0,0	33,6	0,0	0,0	
PROGR. 144.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-39846,9	M	77,0	0,0	N	-563,6	Tz	-0,5	Ty	824,7
3 - 1		1	1	1	1	1	Sx	-81,0	0,0	0,0	-131,6	-0,6	535,3	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-229,2	0,0	0,0	0,0	0,0	229,2	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-189,6	-44,1	0,0	0,0	0,0	199,1	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-3,3	0,0	0,0	-44,3	0,0	76,7	0,0	0,0	
PROGR. 172.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-11517,3	M	92,4	0,0	N	-563,6	Tz	-0,5	Ty	832,4
3 - 1		1	1	1	1	1	Sx	-97,2	0,0	0,0	-131,6	-0,6	832,4	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-300,8	0,0	0,0	0,0	0,0	300,8	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-63,0	-9,9	0,0	0,0	0,0	73,5	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-3,1	0,0	0,0	-68,8	0,0	119,3	0,0	0,0	
3 - 1		1	1	1	1	1	Ne	63,0	0,0	0,0	54,7	0,0	32,0	0,0	0,0	
PROGR. 201.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-16654,1	M	107,8	0,0	N	-563,6	Tz	-0,5	Ty	1121,8
3 - 1		1	1	1	1	1	Sx	-113,4	0,0	0,0	-131,6	-0,6	1129,6	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-134,3	0,0	0,0	0,0	0,0	134,3	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-124,4	-29,7	0,0	0,0	0,0	149,6	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-9,3	0,0	0,0	-93,4	0,0	161,8	0,0	0,0	
3 - 1		1	1	1	1	1	Ne	-29,3	0,0	0,0	-74,4	0,0	162,7	0,0	0,0	
PROGR. 230.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-52988,7	M	123,2	0,0	N	-563,6	Tz	-0,5	Ty	1419,0
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-377,6	0,0	0,0	0,0	0,0	377,6	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-368,5	-37,5	0,0	0,0	0,0	374,1	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-5,5	-0,0	0,0	-39,3	0,0	204,4	0,0	0,0	
3 - 1		1	1	1	1	1	Ne	-37,5	0,0	0,0	-37,5	0,0	377,7	0,0	0,0	
PROGR. 247.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-52988,7	M	123,2	0,0	N	-563,6	Tz	-0,5	Ty	1419,0
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
PROGR. 247.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-52988,7	M	123,2	0,0	N	-563,6	Tz	-0,5	Ty	1419,0
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
PROGR. 247.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-52988,7	M	123,2	0,0	N	-563,6	Tz	-0,5	Ty	1419,0
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
PROGR. 247.																
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	-52988,7	M	123,2	0,0	N	-563,6	Tz	-0,5	Ty	1419,0
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
TENSIONI																
Caso		Vel		N		M		T		S		T		S		
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1,1	0,0	0,0	
3 - 1		1	1	1	1	1	Sx	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
3 - 1		1	1	1	1	1	Tz	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
3 - 1		1	1	1	1	1	Ty	-129,6	0,0	0,0	-131,6	-0,6	1426,7	0,0	0,0	
PROGR. 247.																
S																

3-1	11	21	Sx	Si	-27.71	0.01	0.0	271.5	
3-2	91	91	Tz		-78.7	-33.5	0.0	97.8	
3-1	91	61	Ty		16.8	0.0	58.7	103.1	201.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-2		-11333.8	2032.4	-17.21	-18.3	-337.1	-258.4	
3-1	11	21	-13946.1	1014.6	-13.8	-13.4	-309.1	-964.3	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	166.9	
3-1	91	91	Tz		-166.9	-48.0	0.0	123.6	
3-1	91	61	Ty		-4.1	0.0	85.4	112.5	PROGR.
COLLECTIVIZATION									
Caso	3-2		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		-4342.7	860.5	-12.2	-13.4	-314.7	-1225.5	
3-1	11	21	-4941.7	-8608.0	-15.8	-13.4	302.9		
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	73.3	
3-1	91	91	Tz		-73.3	0.0	0.0	73.3	
3-1	91	61	Ty		-287.6	-62.5	0.0	100.3	
3-1	91	61	Ty		69.5	0.0	112.1	206.2	PROGR.
VERIFICA STABILITA' :									
L	0	=	Z30						
Z	1	=	Z20	Ro = 6.96	=	33.1	Ncr=	530842.71	alfaFC >0.4000
Z	2	=	Z30	Ro = 2.01	lim =	114.3	Ncr=	44413.51	alfaFC >0.4000
Caso	3-1	-	Nodo	2	-	Assie	Ve		
WEd	=	-57.81	Ncr=	-32956.3	limy=			-7761.61	ss= 565.0 (0.253)
P.LINFORMO_S001 (1)									
state limite ultimo - ASTA (975, 953)									
PROGR. 0.									
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		0.0	0.0	0.0	-124.8	0.0	376.0	
3-1	11	21	-13946.1	1014.6	-13.8	-13.4	-309.1	-964.3	
3-1	91	91	Tz		0.0	-57.8	-309.1	1188.6	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	166.9	
3-1	91	91	Tz		-166.9	-48.0	0.0	123.6	
3-1	91	61	Ty		-4.1	0.0	85.4	112.5	PROGR.
COLLECTIVIZATION									
Caso	3-2		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		29900.7	7771.5	0.0	-57.8	-231.5	891.4	
3-1	11	21	-29900.7	-7771.5	0.0	-51.0	231.5	891.4	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	548.5	
3-1	91	91	Tz		548.5	0.0	0.0	548.5	
3-1	91	61	Ty		196.8	43.4	0.0	210.7	
3-1	91	61	Ty		-17.2	0.0	-79.9	139.4	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		51258.2	13312.1	0.0	-57.8	-133.9	594.3	
3-1	11	21	-51258.2	-13312.1	0.0	-51.0	133.9	594.3	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	938.3	
3-1	91	91	Tz		938.3	0.0	0.0	938.3	
3-1	91	61	Ty		338.7	28.9	0.0	362.4	
3-1	91	61	Ty		-28.1	0.0	-53.2	96.3	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		64072.6	16519.3	0.0	-57.8	-76.2	297.1	
3-1	11	21	-64072.6	-16519.3	0.0	-51.0	76.3	297.1	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	938.3	
3-1	91	91	Tz		938.3	0.0	0.0	938.3	
3-1	91	61	Ty		338.7	28.9	0.0	362.4	
3-1	91	61	Ty		-28.1	0.0	-53.2	96.3	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		64072.6	16519.3	0.0	-57.8	-76.2	297.1	
3-1	11	21	-64072.6	-16519.3	0.0	-51.0	76.3	297.1	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1171.5	
3-1	91	91	Tz		-1171.5	0.0	0.0	1171.5	
3-1	91	61	Ty		-43.4	14.8	0.0	42.8	
3-1	91	61	Ty		-5.0	0.0	-26.8	57.5	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	
3-1	91	91	Tz		-1348.0	0.0	0.0	1348.0	
3-1	91	61	Ty		-456.0	0.1	0.0	456.0	
3-1	91	61	Ty		-37.7	0.0	0.1	37.7	PROGR.
COLLECTIVIZATION									
Caso	3-1		MZ	MY	MT	N	Tz	Ty	
TENSION	3-1		68343.8	17095.6	0.0	-57.8	-1.4	0.0	
3-1	11	21	-68343.8	-17095.6	0.0	-51.0	1.4	0.0	
TENSION									
Caso	3-1	11	21	Sx	Sz	0.0	0.0	1348.0	</

3-1	2,6	-155,8	0,0	-46,4	-0,7	-1188,6
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	4	6,3	0,0	6,3		
3-1	8	3,6	31,2	0,0	44,2	
3-1	5	4,3	0,0	96,3	170,3	
3-2	5	6,3	0,0	96,3	170,4	29.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29898,7	136,5	0,0	101,7	0,7
3-1	-29898,7	-136,3	0,0	-46,4	-0,7	-891,5
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	344,6	0,0	0,0	206,6	
3-1	8	202,2	23,4	0,0	206,3	
3-1	5	-4,0	0,0	73,7	127,7	58.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51256,9	117,0	0,0	101,7	0,7
3-1	-51256,9	-116,8	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	344,1	0,0	0,0	345,2	
3-1	8	344,1	15,6	0,0	345,2	
3-1	5	-3,6	0,0	49,1	85,2	86.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64071,9	97,5	0,0	101,7	0,7
3-1	-64071,9	-97,4	0,0	-46,4	-0,7	-297,2
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	430,9	0,0	0,0	430,9	
3-1	8	429,2	7,9	0,0	429,5	
3-1	5	-3,3	0,0	24,6	42,7	115.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-68343,8	78,0	0,0	101,7	0,7
3-1	-68343,8	-78,0	0,0	-46,4	-0,7	-297,2
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	458,9	0,0	0,0	458,9	
3-1	8	457,6	0,1	0,0	457,6	
3-1	6	341,3	0,0	0,1	341,3	144.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64072,6	58,5	0,0	101,7	0,7
3-1	-64072,6	-58,5	0,0	-46,4	-0,7	-297,2
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	430,2	0,0	0,0	430,2	
3-1	8	422,0	0,9	0,0	422,2	
3-2	5	4,6	0,0	-24,6	42,8	172.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	344,8	0,0	0,0	344,8	
3-1	8	-336,9	15,6	0,0	337,9	
3-1	5	4,3	0,0	-49,1	85,2	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29900,7	19,5	0,0	101,7	0,7
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	-891,5
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	202,6	0,0	0,0	202,6	
3-1	8	-195,0	23,4	0,0	199,2	
3-1	5	4,0	0,0	-73,7	127,7	230.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	344,1	15,6	0,0	345,2	
3-1	8	344,1	15,6	0,0	345,2	
3-1	5	4,3	0,0	-49,1	85,2	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29900,7	19,5	0,0	101,7	0,7
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	-891,5
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	202,6	0,0	0,0	202,6	
3-1	8	-195,0	23,4	0,0	199,2	
3-1	5	4,0	0,0	-73,7	127,7	230.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	344,1	15,6	0,0	345,2	
3-1	8	344,1	15,6	0,0	345,2	
3-1	5	4,3	0,0	-49,1	85,2	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29900,7	19,5	0,0	101,7	0,7
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	-891,5
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	202,6	0,0	0,0	202,6	
3-1	8	-195,0	23,4	0,0	199,2	
3-1	5	4,0	0,0	-73,7	127,7	230.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	344,1	15,6	0,0	345,2	
3-1	8	344,1	15,6	0,0	345,2	
3-1	5	4,3	0,0	-49,1	85,2	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64073,5	0,0	0,0	13,8	0,0
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
3-1	-64073,5	0,0	0,0	9,4	0,0	-297,2
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	13,8	0,0	0,0	13,8	
3-1	8	13,8	0,0	0,0	13,8	
3-1	5	13,8	0,0	0,0	13,8	86.

TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	425,8	7,8	0,0	426,1	
3-1	8	425,8	7,8	0,0	426,1	
3-1	5	425,8	7,8	0,0	426,1	115.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64073,5	0,0	0,0	13,8	0,0
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
3-1	-64073,5	0,0	0,0	9,4	0,0	-297,2
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	143,9	0,0	0,0	143,9	
3-1	8	143,9	0,0	0,0	143,9	
3-1	5	143,9	0,0	0,0	143,9	144.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64073,5	0,0	0,0	13,8	0,0
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
3-1	-64073,5	0,0	0,0	9,4	0,0	-297,2
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	426,1	0,0	0,0	426,1	
3-1	8	426,1	0,0	0,0	426,1	
3-1	5	426,1	0,0	0,0	426,1	172.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,8	0,0	0,0	13,8	0,0
3-1	-51258,8	0,0	0,0	9,4	0,0	594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	341,0	0,0	0,0	341,0	
3-1	5	341,0	0,0	0,0	341,0	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29901,0	0,0	0,0	13,8	0,0
3-1	-29901,0	0,0	0,0	9,4	0,0	891,5
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	199,1	0,0	0,0	199,1	
3-1	8	199,1	0,0	0,0	199,1	
3-1	5	199,1	0,0	0,0	199,1	230.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	341,0	0,0	0,0	341,0	
3-1	5	341,0	0,0	0,0	341,0	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	341,0	0,0	0,0	341,0	
3-1	5	341,0	0,0	0,0	341,0	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	341,0	0,0	0,0	341,0	
3-1	5	341,0	0,0	0,0	341,0	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	341,0	0,0	0,0	341,0	
3-1	5	341,0	0,0	0,0	341,0	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	341,0	0,0	0,0	341,0	
3-1	5	341,0	0,0	0,0	341,0	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONE						
Caso Ve/No/massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	341,0	0,0	0,0	341,0	
3-1	5	341,0	0,0	0,0	341,0	201.

SOLLECITAZIONE	MZ	MY	MT	N
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SOLLECITAZIONI :							
Caso	MZ	MY	MT	N	TZ	TY	
3- 1	-25130.2	41.5	-19.9	-10893.1	-10.8	17.9	
3- 2	16187.1	-478.7	13.5	-10088.7	-1.6	336.1	
TENSIONE :							
Caso	Ve	No	massimi	Sx	Tz	TY	SI
3- 1	1	1	Sx	SI	-182.9	0.0	182.9
3- 2	1	6	Tz	SI	-156.8	-4.7	0.0
3- 2	1	9	TY	SI	-129.0	0.0	-21.3

PROGR. 255.

SOLLECITAZIONE :							
Caso	MZ	MY	MT	N	TZ	TY	
3- 1	-25980.4	488.5	-19.9	-10619.2	-10.8	17.9	
3- 2	30472.7	-412.4	13.5	-10054.8	-1.6	336.1	
TENSIONE :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3- 1	1	1	Sx	-186.1	0.0	0.0	186.1
3- 2	1	6	Tz	-181.4	-4.7	0.0	181.6
3- 2	1	9	Ty	-128.6	0.0	-21.3	133.8

PROGR. 298.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 2	44758.3	-946.0	MT	13.5	N	-10020.9	-1.6	TZ	TY
3- 1									336.1
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-208.2	0.0	0.0	208.2	
3- 2	1	6	Tz	SI	-206.1	-4.7	0.0	170.9	
3- 2	1	9	TY	SI	-128.1	0.0	-21.3	133.4	

PROGR. 340.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 2	59043.8	-279.7	MT	13.5	N	-9987.1	-1.6	TZ	TY
3- 1									336.1
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-208.2	0.0	0.0	208.2	
3- 2	1	6	Tz	SI	-206.1	-4.7	0.0	170.9	
3- 2	1	9	TY	SI	-127.7	0.0	-21.3	132.9	

VERIFICA STABILITA' :

[L0 = 340. ;
Z [Lc = 340. ;Ro = 8.54]Im = 39.8]Ncr= 1023125.5]a]fa(b >=0.3400)k(i=0.9165)
Y [Lc = 340. ;Ro = 5.06]Im = 66.2]Ncr= 359233.9]a]fa(c >=0.4900)k(i=0.7151)
Caso 3- 1 - NodD 2 - Asse Y
Ned = -11022.5]Mseq = -24978.2]Mseq = -897.3]Ss = -245.9 (0.110)
P.JHER002_S002 (2) stato limite ultimo - ASTA (-748 - 4) 35

P.JER200_5002 (2)		stato limite ultimo - ASTA (978- 41)					35
		----- PROG. -----					0.
SOLLECITAZIONE :							
Caso	MZ	MY	MT	N	TZ	TY	
3- 1	900763.4	-5006.5	0.0	-28470.4	-56.4	-218.8	
3- 2	-60905.4	-9669.8	0.0	-28482.5	-91.3	585.5	
TENSIONE :							
Caso	Ve	No	massimi	Sx	Tz	TY	SI
3- 2	1	1	Sx	SI	-547.9	0.0	547.9
3- 2	1	6	Tz	SI	-246.4	-9.5	247.0
3- 2	1	9	TY	SI	-366.2	0.0	371.7

PROGR. 21.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	86251.5	-3844.0	MT	0.0	N	-2843.5	-56.4	TZ	TY
3- 2	-48829.4	-7785.8	MT	0.0	N	-2846.0	-91.3	TZ	TY
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-534.0	0.0	0.0	534.0	
3- 2	1	6	Tz	SI	-529.5	-9.5	0.0	270.0	
3- 2	1	9	TY	SI	-365.5	0.0	-36.7	371.0	

PROGR. 41.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	81739.7	-2681.5	MT	0.0	N	-2843.7	-56.4	TZ	TY
3- 2	-36753.3	-5901.8	MT	0.0	N	-2844.6	-91.3	TZ	TY
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-520.1	0.0	0.0	520.1	
3- 2	1	6	Tz	SI	-520.5	-9.5	0.0	293.0	
3- 2	1	9	TY	SI	-364.9	0.0	-36.7	371.0	

PROGR. 62.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	77227.9	-1519.0	MT	0.0	N	-2842.1	-56.4	TZ	TY
3- 2	-24677.3	-4017.8	MT	0.0	N	-2843.1	-91.3	TZ	TY
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-506.1	0.0	0.0	506.1	
3- 2	1	6	Tz	SI	-515.6	-9.5	0.0	316.0	
3- 2	1	9	TY	SI	-364.3	0.0	-36.7	369.8	

PROGR. 82.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	77216.0	-1356.4	MT	0.0	N	-2840.4	-56.4	TZ	TY
3- 2	-12001.2	-2153.9	MT	0.0	N	-2841.6	-91.3	TZ	TY
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-492.2	0.0	0.0	492.2	
3- 2	1	6	Tz	SI	-503.7	-9.5	0.0	339.1	
3- 2	1	9	TY	SI	-363.6	0.0	-36.7	369.8	

PROGR. 103.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	68204.2	806.1	MT	0.0	N	-2838.2	-56.4	TZ	TY
3- 2	-255.2	-2460.9	MT	0.0	N	-2840.3	-91.3	TZ	TY
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-486.3	0.0	0.0	486.3	
3- 2	1	6	Tz	SI	-501.8	-9.5	0.0	362.1	
3- 2	1	9	TY	SI	-363.0	0.0	-36.7	369.8	

PROGR. 124.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	63692.4	2866.6	MT	0.0	N	-2837.7	-56.4	TZ	TY
3- 2	11550.9	1634.1	MT	0.0	N	-28383.8	-91.3	TZ	TY
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-484.0	0.0	0.0	484.0	
3- 2	1	6	Tz	SI	-501.8	-9.5	0.0	362.1	
3- 2	1	9	TY	SI	-362.4	0.0	-36.7	367.9	

PROGR. 144.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	59180.5	3518.1	MT	0.0	N	-2837.4	-56.4	TZ	TY
3- 2	23626.9	3518.1	MT	0.0	N	-28367.4	-91.3	TZ	TY
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-481.7	0.0	0.0	481.7	
3- 2	1	6	Tz	SI	-507.9	-9.5	0.0	367.9	
3- 2	1	9	TY	SI	-361.7	0.0	-36.7	367.3	

PROGR. 165.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	54668.7	4203.7	MT	0.0	N	-2838.9	-56.4	TZ	TY
3- 2	35703.0	5402.1	MT	0.0	N	-28350.9	-91.3	TZ	TY
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-479.4	0.0	0.0	479.4	
3- 2	1	6	Tz	SI	-431.0	-9.5	0.0	431.3	

[3- 2]si] 9] Ty | -361.1] 0.0] -36.7] 366.7]

VERIFICA STABILITA' :

[L0 = 165. ;
Z [Lc = 165. ;Ro = 8.54]Im = 19.3]Ncr= 434420.6]a]fa(b >=0.3400)k(i=0.9980)
Y [Lc = 165. ;Ro = 5.06]Im = 32.6]Ncr= 1325341.9]a]fa(c >=0.4900)k(i=0.5949)
Caso 3- 1 - NodD 1 - Asse Y
Ned = -28470.4]Mseq = 76325.5]Mseq = -2002.6]Ss = -538.2 (0.240)
P.JHER002_S002 (2) stato limite ultimo - ASTA (-41- 42) 36

P.JHER200_S02 (2)		-----					-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----		-----			
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SOLLECITAZIONE :				PROG. :			
Caso	MZ	MY	MT	N	TZ	TY	
3-2	-419700.9	-6020.3	-199.0	-63.6	-39.8	-6962.1	
6-3	-127743.4	528.0	2475.6	52.9	501.5	-2668.4	
TENSIONE :							
Caso	Ve	No	massim	Sx	Tz	Ty	Si
3-2	Si	4	Sx	-1400.3	0.0	0.0	1400.3
6-3	Si	4	Sx	402.2	196.3	0.0	0.0
3-2	Si	9	TV	-3.9	0.0	624.7	1082.0

```

VERIFICA STATISTICA :
Y      |L0 = 10. |
Z      |LC = 10. |Ro = 6.78 |Im = 1.5 |Ncr=517408865.8|alfa(b) =0.3400|ki=1.0000|
Y      |LC = 10. |Ro = 4.04 |Im = 2.5 |Ncr=184330846.8|alfa(c) =0.4900|ki=1.0000|
Caso 3 - 2 - Nodo 4 - Asse Y
Ned = -63.6 |Mreq = -463224.8 |Myeq = -6169.5 |Ss = -1541.1 ( 0.689)

```

3-1	Si	4	Sx	-1377.1	0.0	0.0	1377.1
6-3	Si	5	Tz	395.4	211.1	0.0	538.5
3-1	Si	9	Tv	-7.2	0.0	-626.2	1084.7

VERIFICA STABILITA' :

Z	L0 = 10.1								
Y	Lc = 10.1	R0 = 6.78	Im = 1.5	Ncr = 517408865.8	a fa(b) = 0.3400	ki = 1.0000			
Z	Lc = 10.1	R0 = 4.04	Im = 2.5	Ncr = 184330846.8	a fa(c) = 0.4900	ki = 1.0000			
Caseo	3- 1 + Nod0	4 - Ass0	Y						
Ned =	-384.4	Mreq = -479557.5	Mreq =	-256.9	Ss =	-1546.2	(0.691)		

TENSIONI				Sx	Tz	Ty	Sy
Caso	Ve	No	massimi	-13.0	0.0	0.0	13.0
3-	1	1	Sx	0.1	-464.2	111.3	11.0
3-	1	1	Tz	-7.0	0.0	-278.0	481.6
3-	1	1	Ty				

VERIFICA STABILITA' :

$|L_0| = 130.$

3-2	1	5	4	5x	-290.5	0.0	0.0	290.5
3-2	1	5	9	Tz	175.9	-172.3	0.0	346.5
3-1	1	5	9	Tys	-12.3	0.0	509.9	883.2

SOLLECITAZIONE

Caso	MZ	MY	MT	N	TZ	TY
3-2	-93355.6	-374.3	201.7	-565.1	-9.1	-5637.0
3-1	-65446.1	-442.6	-1485.2	-656.8	-3.2	-5195.8

TENSIONI

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-312.9	0.0	0.0	312.9
3-1	1	5	1	Tz	126.7	-172.4	0.0	307.5
3-1	1	9	1	TySi	-12.3	0.0	509.9	883.3

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-100402.2	-362.9	201.7	-565.1	-9.1	-5638.6
3-1	-71941.3	-438.5	-1485.2	-656.8	-3.2	-5196.5

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-335.4	0.0	0.0	335.4
3-1	1	5	1	Tz	127.5	-172.4	0.0	309.4
3-1	1	9	1	TySi	-12.3	0.0	510.0	883.4

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-107449.7	-351.5	201.7	-565.1	-9.1	-5638.3
3-1	-78437.3	-434.5	-1485.2	-656.8	-3.2	-5197.2

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-357.9	0.0	0.0	357.9
3-1	1	5	1	Tz	128.4	-172.4	0.0	309.0
3-1	1	9	1	TySi	-12.3	0.0	510.0	883.5

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-114498.1	-340.1	201.7	-565.1	-9.1	-5639.0
3-1	-84934.2	-430.5	-1485.2	-656.8	-3.2	-5197.8

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-380.4	0.0	0.0	380.4
3-1	1	5	1	Tz	259.2	-172.4	0.0	395.4
3-1	1	9	1	TySi	-12.3	0.0	510.1	883.6

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-121547.3	-328.7	201.7	-565.1	-9.1	-5639.7
3-1	-91431.9	-426.4	-1485.2	-656.8	-3.2	-5198.5

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-406.4	0.0	0.0	406.4
3-1	1	5	1	Tz	280.0	-172.4	0.0	409.4
3-1	1	9	1	TySi	-12.3	0.0	510.2	883.7

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-128597.4	-317.4	201.7	-565.1	-9.1	-5640.4
3-1	-97930.5	-422.4	-1485.2	-656.8	-3.2	-5199.2

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-425.4	0.0	0.0	425.4
3-1	1	5	1	Tz	300.8	-172.4	0.0	423.9
3-1	1	9	1	TySi	-12.3	0.0	510.2	883.8

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-135648.4	-306.0	201.7	-565.1	-9.1	-5641.1
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-447.8	0.0	0.0	447.8
3-1	1	5	1	Tz	321.7	-172.4	0.0	439.0
3-1	1	9	1	TySi	-12.3	0.0	510.3	883.9

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-138140.6	-298.5	201.7	-565.1	-9.1	-5641.9
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-437.7	0.0	0.0	437.7
3-1	1	5	1	Tz	411.8	-170.7	0.0	429.9
3-1	1	9	1	TySi	-11.8	0.0	510.4	884.0

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-127222.9	-381.0	201.7	-565.1	-9.1	-5642.9
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-422.7	0.0	0.0	422.7
3-1	1	5	1	Tz	396.9	-170.7	0.0	415.4
3-1	1	9	1	TySi	-11.7	0.0	510.4	884.1

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-122606.0	-363.5	201.7	-565.1	-9.1	-5643.1
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-407.7	0.0	0.0	407.7
3-1	1	5	1	Tz	380.6	-170.7	0.0	409.9
3-1	1	9	1	TySi	-11.7	0.0	510.4	884.2

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-117990.0	-346.0	201.7	-565.1	-9.1	-5644.0
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-392.8	0.0	0.0	392.8
3-1	1	5	1	Tz	367.3	-170.7	0.0	387.1
3-1	1	9	1	TySi	-11.7	0.0	510.4	884.3

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-113374.9	-328.5	201.7	-565.1	-9.1	-5644.9
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-372.8	0.0	0.0	372.8
3-1	1	5	1	Tz	352.5	-170.6	0.0	373.1
3-1	1	9	1	TySi	-11.7	0.0	510.4	884.4

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-108760.7	-311.1	201.7	-565.1	-9.1	-5645.1
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-352.9	0.0	0.0	352.9
3-1	1	5	1	Tz	337.6	-170.6	0.0	359.1
3-1	1	9	1	TySi	-11.7	0.0	510.4	884.5

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-108760.7	-311.1	201.7	-565.1	-9.1	-5645.1
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	MZ	MY	MT	N	TZ	TY
3-1	-104147.3	-293.6	201.7	-565.1	-9.1	-5646.1
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-348.0	0.0	0.0	348.0
3-1	1	5	1	Tz	322.6	-170.6	0.0	345.2
3-1	1	9	1	TySi	-11.7	0.0	510.4	884.6

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-99534.5	-276.1	201.7	-565.1	-9.1	-5647.1
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-333.0	0.0	0.0	333.0
3-1	1	5	1	Tz	308.0	-170.6	0.0	331.4
3-1	1	9	1	TySi	-11.7	0.0	510.4	884.7

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-94923.1	-258.6	201.7	-565.1	-9.1	-5648.1
3-1	-104630.0	-418.4	-1485.2	-656.8	-3.2	-5199.9

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-318.1	0.0	0.0	318.1
3-1	1	5	1	Tz	293.2	-170.6	0.0	317.7
3-1	1	9	1	TySi	-11.7	0.0	510.4	884.8

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-73407.3	-258.6	2.6	-93.8	1.1	771.8
3-1	-73407.3	-258.6	2.6	-93.8	1.1	771.8

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-239.3	0.0	0.0	239.3
3-1	1	5	1	Tz	233.0	14.6	0.0	117.5
3-1	1	9	1	TySi	-1.8	0.0	510.4	884.9

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-60939.4	-276.4	2.6	-93.8	1.1	762.7
3-1	-60939.4	-276.4	2.6	-93.8	1.1	762.7

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-199.5	0.0	0.0	199.5
3-1	1	5	1	Tz	193.0	13.5	0.0	124.5
3-1	1	9	1	TySi	-1.8	0.0	510.4	885.0

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-48617.9	-294.2	2.6	-93.8	1.1	753.7
3-1	-48617.9	-294.2	2.6	-93.8	1.1	753.7

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-169.2	0.0	0.0	169.2
3-1	1	5	1	Tz	153.4	13.7	0.0	155.3
3-1	1	9	1	TySi	-1.9	0.0	510.4	885.1

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-36442.7	-312.0	2.6	-93.8	1.1	744.7
3-1	-36442.7	-312.0	2.6	-93.8	1.1	744.7

Caso	Ve	No	mass	ini	Sx	Tz	Ty	Si
3-1	1	1	4	Sk	-123.3	0.0	0.0	123.3
3-1	1	5	1	Tz	114.4	13.6	0.0	116.8
3-1	1	9	1	TySi	-1.9	0.0	510.4	885.2

PROGR.

Caso	MZ	MY	MT	N	TZ	TY
3-1	-24413.9	-329.7	2.6	-93.8	1.1	735.7
3-1	-24413.9	-329.7	2.6	-93.8	1.1	735.7

Caso	M2	MY	MT	N	TZ	TY
3-1	-12531.3	-347.5	2.6	-93.8	1.1	726.7
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Ty
3-1	1	4	Sx	-45.0	0.0	0.0
						Si
						45.0

Case		MZ	MY	MT	N	TZ	TY
3-2	1	-5172.6	-202.4	15.6	-28.3	3.1	-816.7
3-2	1	-6955.1	-801.6	69.4	-13.5	13.9	-781.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-160.3	0.0	0.0	168.3	
3-2	1	4	160.4	18.2	0.0	163.5	
3-2	1	9	Tz	-0.6	0.0	73.0	
3-2	1	9	Si	-166.9	15.6	0.0	169.0
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-6518.9	-233.0	15.6	-28.3	3.1	-827.7
3-2	1	-6230.1	-1127.0	69.4	-13.5	13.9	-790.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-211.5	0.0	0.0	211.5	
3-2	1	4	201.8	18.3	0.0	204.3	
3-2	1	9	Tz	-0.6	0.0	73.8	
3-2	1	9	Si	-166.9	15.6	0.0	172.9
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-7860.7	-303.7	15.6	-28.3	3.1	-894.7
3-2	1	-8806.6	-1557.8	69.4	-13.5	13.9	-879.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-253.2	0.0	0.0	255.2	
3-2	1	4	248.6	18.3	0.0	245.8	
3-2	1	9	Tz	-0.7	0.0	74.6	
3-2	1	9	Si	-166.9	15.6	0.0	172.9
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-9224.4	-354.3	15.6	-28.3	3.1	-943.7
3-2	1	-10078.6	-1577.8	69.4	-13.5	13.9	-917.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-299.3	0.0	0.0	299.3	
3-2	1	4	286.9	18.7	0.0	284.2	
3-2	1	9	Tz	-0.7	0.0	75.4	
3-2	1	9	Si	-166.9	15.6	0.0	130.6
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	328.8	18.8	0.0	320.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	9	Si	-166.9	15.6	0.0	130.6
PROGR.							
VERIFICA STABILITA'							
L = 130, R0 = 6.78 m = 19.21 m → 30051.911a/fc → 0.34001 (k1.90575) L = 130, R0 = 4.78 m = 32.11 m → 30070.11a/fc → 0.40000 (k1.90975) L = 2 - Node 4 - Asse → -79520.81 mte → -303.75 mte → -258.1 (0.115) P.JERJERO_5003 (3) → 20000 mte → 195.1 mte → 195.1 mte							
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10036.5	-404.9	149.7	-26.5	29.9	-1817.4
3-2	1	-10837.0	-1803.2	944.2	-16.3	138.8	-1780.9
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	321.0	-88.6	0.0	355.8	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	9	Si	-166.9	15.6	0.0	130.6
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10036.6	-404.9	149.7	-26.5	29.9	-1818.1
3-2	1	-10937.3	-1831.1	944.2	-16.3	138.8	-1781.6
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-359.2	0.0	0.0	359.2	
3-2	1	4	336.3	-88.6	0.0	369.6	
3-2	1	9	Tz	-0.7	0.0	189.1	
3-2	1	9	Si	-221.5	0.0	179.3	
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-11285.5	-517.2	149.7	-26.5	29.9	-1819.5
3-2	1	-12044.7	-2305.1	944.2	-16.3	138.8	-1782.2
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-366.8	0.0	0.0	366.8	
3-2	1	4	341.8	-88.6	0.0	376.6	
3-2	1	9	Tz	-0.6	0.0	189.1	
3-2	1	9	Si	-226.1	0.0	179.5	
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-11570.3	-592.0	149.7	-26.5	29.9	-1820.8
3-2	1	-12760.1	-2623.0	944.2	-16.3	138.8	-1783.6
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-381.1	0.0	0.0	381.1	
3-2	1	4	359.2	-88.6	0.0	390.6	
3-2	1	9	Tz	-0.6	0.0	191.2	
3-2	1	9	Si	-239.8	0.0	179.5	
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-11945.9	-670.8	149.7	-26.5	29.9	-1821.5
3-2	1	-12832.0	-306.9	944.2	-16.3	138.8	-1784.3
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-389.7	0.0	0.0	389.7	
3-2	1	4	368.0	-88.6	0.0	397.7	
3-2	1	9	Tz	-0.7	0.0	191.2	
3-2	1	9	Si	-239.8	0.0	179.5	
PROGR.							

Case	MZ	My	MT	N	Tz	Ty
3-1	-1507.7	75.4	-4608.1	N -2.3	Tz 41.6	Ty 1522.9
Case	W	no	miss			Si
3-1	5	Sx	-49.0	0.0	Ty	49.0
3-1	5	Tz	48.4	273.7	0.0	476.5
3-1	5	Ty	0.0	0.0	-285.9	495.2
3-1	5	Ty	-0.1	0.0	-285.9	495.2
PROGR.						
1.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-15174.6	23.4	-4608.1	N -2.3	Tz 41.6	Ty 1522.9
Case	W	no	miss			Si
3-1	5	Sx	-42.5	0.0	Ty	42.5
3-1	5	Tz	42.2	273.7	0.0	475.9
3-1	5	Ty	0.0	0.0	-285.8	495.1
3-1	5	Ty	-0.1	0.0	-285.8	495.1
PROGR.						
2.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-11272.4	-28.5	-4608.1	N -2.3	Tz 41.6	Ty 1522.9
Case	W	no	miss			Si
3-1	5	Sx	-36.4	0.0	Ty	36.4
3-1	5	Tz	36.0	273.7	0.0	475.3
3-1	5	Ty	-0.1	0.0	-285.8	495.0
PROGR.						
4.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-9369.0	-80.5	-4608.1	N -2.3	Tz 41.6	Ty 1521.6
Case	W	no	miss			Si
3-1	5	Sx	-30.8	0.0	Ty	30.8
3-1	5	Tz	29.8	273.6	0.0	474.9
3-1	5	Ty	-0.1	0.0	-285.7	494.9
PROGR.						
5.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-7467.5	-132.5	-4608.1	N -2.3	Tz 41.6	Ty 1520.9
Case	W	no	miss			Si
3-1	5	Sx	-25.2	0.0	Ty	25.2
3-1	5	Tz	23.6	273.6	0.0	474.5
3-1	5	Ty	-0.1	0.0	-285.7	494.8
PROGR.						
6.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-5566.9	-184.4	-4608.1	N -2.3	Tz 41.6	Ty 1520.2
Case	W	no	miss			Si
3-1	5	Sx	-19.5	0.0	Ty	19.5
3-1	5	Tz	17.4	273.6	0.0	474.2
3-1	5	Ty	-0.1	0.0	-285.6	494.7
PROGR.						
8.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-3667.1	-236.4	-4608.1	N -2.3	Tz 41.6	Ty 1519.5
Case	W	no	miss			Si
3-1	5	Sx	-13.9	0.0	Ty	13.9
3-1	5	Tz	11.2	273.6	0.0	474.0
3-1	5	Ty	-0.1	0.0	-285.5	494.6
PROGR.						
9.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-1768.2	-288.4	-4608.1	N -2.3	Tz 41.6	Ty 1518.8
Case	W	no	miss			Si
3-1	5	Sx	-8.3	0.0	Ty	8.3
3-1	5	Tz	5.0	273.6	0.0	473.9
3-1	5	Ty	-0.2	0.0	-285.5	494.5
PROGR.						
10.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-315.6	-340.3	-4608.1	N -2.3	Tz 41.6	Ty 1518.1
Case	W	no	miss			Si
3-1	5	Sx	-5.1	0.0	Ty	5.1
3-1	5	Tz	-1.2	273.6	0.0	473.8
3-1	5	Ty	-0.2	0.0	-285.4	494.3
PROGR.						
10.						
VERIFICA STABILITA'						
Z [Lz = 10; [Ro = 6.78] Im = 1.5; [Ncr=51740885.8] a[fa]b(0) = 340; k[ic] = 1.0000						
Y [Lz = 10; [Ro = 6.04] Im = 2.5; [Ncr=184330846.8] a[fa]b(c) = 490; k[ic] = 1.0000						
Case 3-1: Node 4 - Area Y						
Nid = -2.31Mreq = -11309.01Mreq = -255.21ss = -38.6 (0.007)						

VERIFICA NODI IN ACCIAIO:

VERIFICA TENSIONALE NODI: 40 - METODO DEGLI STATI LIMITE (NTC 2008)

UNITA' DI MISURA: [daN] ; [daNcm] ; [daN/cm2] ; [mm]

GEOMETRIA NODO

Profili utilizzati

Tipi prof.:
HERDO

Piastra e fazzoletti

Num	Lz	Y	Sp
1	400	400	10
2(Y)	400	100	5
3(Z)	95	100	5

Tirafond (n° 4)									
Num	X	Y	F	Area	Num	X	Y	F	Area
1	350	50	14	115	3	350	350	14	115
2	50	50	14	115	4	50	350	14	115

Dimensioni

SALDATURE	T	l	r
300.	100.	250.	50.

SALDATURE (n° 40)									
Nome	Lung	Lato	Nome	Lung	Lato				
S1	134.	6	S21	134.	6				
S2	77.5	6	S22	77.5	6				
S3	100.	6	S23	100.	6				
S4	77.5	6	S24	100.	6				
S5	124.	6	S25	95.	6				
S6	124.	6	S26	95.	6				
S7	200.	6	S27	95.	6				
S8	77.5	6	S28	100.	6				
S9	190.	6	S29	120.	6				
S10	100.	6	S30	100.	6				
S11	100.	6	S31	100.	6				
S12	100.	6	S32	100.	6				
S13	100.	6	S33	100.	6				
S14	100.	6	S34	100.	6				
S15	95.	6	S35	100.	6				
S16	95.	6	S36	100.	6				
S17	95.	6	S37	100.	6				
S18	95.	6	S38	100.	6				
S19	190.	6	S39	100.	6				
S20	130.	6	S40	100.	6				

MATERIALI

Acciaio S 235 (re 360)

Calcestruzzo C25/30

228.1

Acciaio tirafond S 235 (re 360)

1880.

SOLLECITAZIONE AGENTI E STATO TENSIONALE

Combinazione di sollecitazioni agenti Caso 6 As. 35 nd. 40

Verifica tirafond

Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)

Co-3: Ft,Ed / Td,rd									
Num	Fv,Ed	Fv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Fb,Rd	Td,rd	Co-1	Co-2
1	14.2	1987.2	8842.1	-14.3	1980.8	11400.2	3023.8	.01	.0
2	14.2	1987.2	8842.1	-23.3	1980.8	11400.2	3023.8	.01	.01
3	14.2	1987.2	8842.1	-10.2	1980.8	11400.2	3023.8	.01	.0
4	14.2	1987.2	8842.1	-19.1	1980.8	11400.2	3023.8	.01	.01

Verifica saldature

Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.78)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Nome	S_prip	Talpa	Talpa	Seq-1	Seq-2	Seq-1	Seq-2	Ver
S1	31.3	31.3	31.3	1997.5	2350.1	1997.5	2350.1	Ver
S2	30.8	30.8	30.8	1997.5	2350.1	1997.5	2350.1	Ver
S3	38.9	38.9	38.9	1997.5	2350.1	1997.5	2350.1	Ver
S4	38.4	38.4	38.4	1997.5	2350.1	1997.5	2350.1	Ver
S5	41.6	41.6	41.6	1997.5	2350.1	1997.5	2350.1	Ver
S6	33.6	33.6	33.6	1997.5	2350.1	1997.5	2350.1	Ver
S7	33.1	33.1	33.1	1997.5	2350.1	1997.5	2350.1	Ver
S8	26	26	26	1997.5	2350.1	1997.5	2350.1	Ver
S9	39.2	39.2	39.2	1997.5	2350.1	1997.5	2350.1	Ver
S10	39.3	39.3	39.3	1997.5	2350.1	1997.5	2350.1	Ver
S11	41.6	41.6	41.6	1997.5	2350.1	1997.5	2350.1	Ver
S12	42.2	42.2	42.2	1997.5	2350.1	1997.5	2350.1	Ver
S13	33	33	33	1997.5	2350.1	1997.5	2350.1	Ver
S14	33.6	33.6	33.6	1997.5	2350.1	1997.5	2350.1	Ver
S15	44.9	44.9	44.9	1997.5	2350.1	1997.5	2350.1	Ver
S16	45.1	45.1	45.1	1997.5	2350.1	1997.5	2350.1	Ver
S17	39.5	39.5	39.5	1997.5	2350.1	1997.5	2350.1	Ver
S18	39.3	39.3	39.3	1997.5	2350.1	1997.5	2350.1	Ver
S19	25.9	25.9	25.9	1997.5	2350.1	1997.5	2350.1	Ver
S20	25.9	25.9	25.9	1997.5	2350.1	1997.5	2350.1	Ver
S21	29.5	29.5	29.5	1997.5	2350.1	1997.5	2350.1	Ver
S22	28.9	28.9	28.9	1997.5	2350.1	1997.5	2350.1	Ver
S23	20.9	20.9	20.9	1997.5	2350.1	1997.5	2350.1	Ver
S24	20.3	20.3	20.3	1997.5	2350.1	1997.5	2350.1	Ver
S25	26	26	26	1997.5	2350.1	1997.5	2350.1	Ver
S26	26.3	26.3	26.3	1997.5	2350.1	1997.5	2350.1	Ver
S27	20.6	20.6	20.6	1997.5	2350.1	1997.5	2350.1	Ver
S28	20.4	20.4	20.4	1997.5	2350.1	1997.5	2350.1	Ver
S29	60.3	60.3	60.3	1997.5	2350.1	1997.5	2350.1	Ver
S30	56.1	56.1	56.1	1997.5	2350.1	1997.5	2350.1	Ver
S31	60.3	60.3	60.3	1997.5	2350.1	1997.5	2350.1	Ver
S32	96.3	96.3	96.3	1997.5	2350.1	1997.5	2350.1	Ver
S33	96.3	96.3	96.3	1997.5	2350.1	1997.5	2350.1	Ver
S34	96.3	96.3	96.3	1997.5	2350.1	1997.5	2350.1	Ver
S35	96.3	96.3	96.3	1997.5	2350.1	1997.5	2350.1	Ver
S36	96.3	96.3	96.3	1997.5	2350.1	1997.5	2350.1	Ver
S37	96.3	96.3	96.3	1997.5	2350.1	1997.5	2350.1	Ver
S38	96.3	96.3	96.3	1997.5	2350.1	1997.5	2350.1	Ver
S39	96.3	96.3	96.3	1997.5	2350.1	1997.5	2350.1	Ver
S40	56.1	56.1	56.1	1997.5	2350.1	1997.5	2350.1	Ver

Verifica piastra

Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.78)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

N: -21268.4 Ty: 160.7 Tz: 28.3

Mx: 0 My: 5315 Mz: 60546

Verifica tirafond

Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)

Co-3: Ft,Ed / Td,rd									
Num	Fv,Ed	Fv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Fb,Rd	Td,rd	Co-1	Co-2
1	40.8	1987.2	8842.1	-63.2	1980.8	11400.2	3023.8	.01	.01
2	40.8	1987.2	8842.1	-68.6	1980.8	11400.2	3023.8	.01	.01
3	40.8	1987.2	8842.1	-124.3	1980.8	11400.2	3023.8	.01	.01
4	40.8	1987.2	8842.1	-129.7	1980.8	11400.2	3023.8	.01	.01

Verifica saldature

Seq-1, Seq-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)

Seq-2, Seq-2

S7	200.	7.	S27	144.	7.
S8	78.8	7.	S28	144.	7.
S9	124.6	7.	S29	150.	7.
S10	178.	7.	S30	150.	7.
S11	150.	7.	S31	150.	7.
S12	150.	7.	S32	150.	7.
S13	150.	7.	S33	150.	7.
S14	150.	7.	S34	150.	7.
S15	144.	7.	S35	150.	7.
S16	144.	7.	S36	150.	7.
S17	144.	7.	S37	150.	7.
S18	144.	7.	S38	150.	7.
S19	150.	7.	S39	150.	7.
S20	178.	7.	S40	150.	7.

MATERIE				
Acciaio S 235 (R 360)				
Fd 140mm				
2238.1				
Acciaio tirafond S 275 (R 430)				
Fd 2200.				

SOLLECITAZIONE AGENTI E STATO TENSIONALE

Combinazione di sollecitazioni agenti Caso 6 As. 35. Nd. 978

N: -6527.5 Ty: 23.5 Tz: 60.1

Mt: 0 My: 9575 Mz: 10090

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft,Ed / Td,Rd									
Num	Pv,Ed	Pv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Td,Rd	Co-1	Co-2
1	16.1	3240.5	13714.3	-38.1	4860.7	19543.2	3564.	0	0
2	16.1	3240.5	13714.3	-26.7	4860.7	19543.2	3564.	0	0
3	16.1	3240.5	13714.3	-26.7	4860.7	19543.2	3564.	0	0
4	16.1	3240.5	13714.3	-34.	4860.7	19543.2	3564.	0	0

Verifica saldature									
Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
	Nome	S _{pmp}	Talpa	Talpe	Seq-1	Seq-2	S _{lim-1}	S _{lim-2}	Ver
S1	38.1	7	0.	38.1	38.1	1997.5	2350.	1st	2nd
S2	31.9	7	0.	31.9	31.9	1997.5	2350.	1st	2nd
S3	35.4	7	0.	35.4	35.4	1997.5	2350.	1st	2nd
S4	35.9	7	0.	35.9	35.9	1997.5	2350.	1st	2nd
S5	38.4	7	0.	38.4	38.4	1997.5	2350.	1st	2nd
S6	42.2	7	0.	42.2	42.2	1997.5	2350.	1st	2nd
S7	42.7	7	0.	42.7	42.7	1997.5	2350.	1st	2nd
S8	38.1	7	0.	38.1	38.1	1997.5	2350.	1st	2nd
S9	40.8	7	0.	40.8	40.8	1997.5	2350.	1st	2nd
S10	42.7	7	0.	42.7	42.7	1997.5	2350.	1st	2nd
S11	35.4	7	0.	35.4	35.4	1997.5	2350.	1st	2nd
S12	35.8	7	0.	35.8	35.8	1997.5	2350.	1st	2nd
S13	48.2	7	0.	48.2	48.2	1997.5	2350.	1st	2nd
S14	48.6	7	0.	48.6	48.6	1997.5	2350.	1st	2nd
S15	40.8	7	0.	40.8	40.8	1997.5	2350.	1st	2nd
S16	40.4	7	0.	40.4	40.4	1997.5	2350.	1st	2nd
S17	47.3	7	0.	47.3	47.3	1997.5	2350.	1st	2nd
S18	47.7	7	0.	47.7	47.7	1997.5	2350.	1st	2nd
S20	35.7	7	0.	35.7	35.7	1997.5	2350.	1st	2nd
S21	28.9	7	0.	28.9	28.9	1997.5	2350.	1st	2nd
S22	28.5	7	0.	28.5	28.5	1997.5	2350.	1st	2nd
S23	41.7	7	0.	41.7	41.7	1997.5	2350.	1st	2nd
S24	41.4	7	0.	41.4	41.4	1997.5	2350.	1st	2nd
S25	28.9	7	0.	28.9	28.9	1997.5	2350.	1st	2nd
S26	28.5	7	0.	28.5	28.5	1997.5	2350.	1st	2nd
S27	35.7	7	0.	35.7	35.7	1997.5	2350.	1st	2nd
S28	35.9	7	0.	35.9	35.9	1997.5	2350.	1st	2nd
S29	0.	119.9	58.6	131.4	58.6	1997.5	2350.	1st	2nd
S30	81.7	68.7	106.8	131.8	104.4	1997.5	2350.	1st	2nd
S31	0.	185.1	58.6	194.1	58.6	1997.5	2350.	1st	2nd
S32	104.5	84.6	58.6	146.7	163.1	1997.5	2350.	1st	2nd
S33	104.5	84.6	134.4	104.5	199.5	2350.	1st	2nd	
S34	104.5	84.6	80.1	156.5	184.6	1997.5	2350.	1st	2nd
S35	104.5	84.6	134.4	104.5	199.5	2350.	1st	2nd	
S36	0.	252.5	80.1	264.9	80.1	1997.5	2350.	1st	2nd
S37	81.7	78.3	106.8	131.7	161.8	1997.5	2350.	1st	2nd
S38	0.	187.3	80.1	203.7	80.1	1997.5	2350.	1st	2nd
S39	81.7	68.7	0.	106.8	81.7	1997.5	2350.	1st	2nd
S40	81.7	68.7	0.	106.8	81.7	1997.5	2350.	1st	2nd

Verifica piastra				
Smax fdlver				
72.7 2238.11St				
Verifica nervature				
Posizione Smax fdlver				
Z 312. 2238.11St				
Y 285.5 2238.11St				

Verifica pressione sul calcestruzzo				
Smax fdlver				
3.6 141.11St				

NDO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONE AGENTI Caso 6 As. 35. Nd. 978

Combinazione di sollecitazioni agenti Caso 3 As. 35. Nd. 978

N: -28482.5 Ty: 585.5 Tz: -91.3

Mt: 0 My: -9670 Mz: -60905

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft,Ed / Td,Rd									
Num	Pv,Ed	Pv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Td,Rd	Co-1	Co-2
1	148.1	3240.5	13714.3	-142.8	4860.7	19543.2	3564.	0	0
2	148.1	3240.5	13714.3	-135.4	4860.7	19543.2	3564.	0	0
3	148.1	3240.5	13714.3	-95.3	4860.7	19543.2	3564.	0	0
4	148.1	3240.5	13714.3	-87.9	4860.7	19543.2	3564.	0	0

Verifica saldature									
Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome S_pmp Talpa Talpe Seq-1 Seq-2 S_lim-1 S_lim-2Ver									
S1	171.1	8.5	1.	171.1	171.1	1997.5	2350.	1st	2nd
S2	178.1	1.	0.	178.1	178.1	1997.5	2350.	1st	2nd
S3	181.5	1.	0.	181.5	181.5	1997.5	2350.	1st	2nd
S4	174.	1.	0.	174.	174.	1997.5	2350.	1st	2nd
S5	171.	1.	0.	171.1	171.1	1997.5	2350.	1st	2nd
S6	136.4	1.	0.	136.4	136.4	1997.5	2350.	1st	2nd
S7	127.	1.	0.	127.1	127.1	1997.5	2350.	1st	2nd
S8	140.5	1.	0.	140.5	140.5	1997.5	2350.	1st	2nd
S10	172.5	6.5	0.	172.6	172.5	1997.5	2350.	1st	2nd
S11	168.4	6.5	0.	168.4	168.4	1997.5	2350.	1st	2nd
S12	208.1	6.5	0.	208.2	208.1	1997.5	2350.	1st	2nd
S13	131.	6.5	0.	131.1	131.	1997.5	2350.	1st	2nd
S14	130.6	6.5	0.	130.8	130.6	1997.5	2350.	1st	2nd
S15	172.	1.	0.	172.	172.	1997.5	2350.	1st	2nd
S16	174.5	1.	0.	174.5	174.5	1997.5	2350.	1st	2nd
S17	132.6	1.	0.	132.6	132.6	1997.5	2350.	1st	2nd
S18	130.1	1.	0.	130.1	130.1	1997.5	2350.	1st	2nd
S20	179.8	6.5	0.	179.9	179.8	1997.5	2350.	1st	2nd
S21	215.	1.	0.	215.1	215.	1997.5	2350.	1st	2nd
S22	215.4	6.5	0.	215.5	215.4	1997.5	2350.	1st	2nd
S23	137.9	6.5	0.	137.7	137.9	1997.5	2350.	1st	2nd
S24	137.9	6.5	0.	138.	137.9	1997.5	2350.	1st	2nd

S25	184.	1.	0.	184.	184.	1997.5	2350.	1st	2nd
S26	186.5	1.	0.	186.5	186.5	1997.5	2350.	1st	2nd
S27	144.6	1.	0.	144.6	144.6	1997.5	2350.	1st	2nd
S28	142.1	1.	0.	142.1	142.1	1997.5	2350.	1st	2nd
S29	0.	1048.7	332.6	1100.2	332.6	1997.5	2350.	1st	2nd
S30	409.8	363.9	332.6	641.1	742.4	1997.5	2350.	1st	2nd
S31	0.	982.9	332.6	1037.6	332.6	1997.5	2350.	1st	2nd
S32	186.8	349.5	332.6	144.6	144.6	1997.5	2350.	1st	2nd
S33	386.8	347.8	0.	520.2	386.8	1997.5	2350.	1st	2nd
S34	386.8	347.8	241.5	573.5	628.3	1997.5	2350.	1st	2nd
S35	386.8	347.8	0.	520.2	386.8	1997.5	2350.	1st	2nd
S36	0.	575.9	241.5	643.5	241.5	1997.5	2350.	1st	2nd
S37	409.8	363.9	241.5	643.5	241.5	1997.5	2350.	1st	2nd
S38	0.	641.8	241.5	685.7	241.5	1997.5	2350.	1st	2nd
S39	409.8	363.9	0.	548.	409.8	1997.5	2350.	1st	2nd
S40	409.8	363.9	0.	548.	409.8	1997.5	2350.	1st	2nd

Verifica piastra				
Smax fdlver				
419.8 2238.11St				
Verifica nervature				
Posizione Smax fdlver				
Z 1107.1 2238.11St				
Y 1178.7 2238.11St				

Verifica pressione sul calcestruzzo				
Smax fdlver				
14.9 141.11St				

NDO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONE AGENTI Caso 3 As. 35. Nd. 978

127/136

Verifica piastra			
Smax		fdlVer	
377.5	2238.1	St'	
Verifica nervature			
Posizione		fdlVer	
Z	502	2238.1	St'
Y	437.8	2238.1	St'
Verifica pressione sul calcestruzzo			
Smax		fdlVer	
6.3	141.1	St'	

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 112 Nd. 734									
Combinazione di sollecitazioni agenti Caso 3 As. 112 Nd. 734									

N = -8956.7					Ty: 30.2		Tz: 22.5		
Mc: 0					My: 5003		Mz: 20095		

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft.Ed / Td.Rd									
Nome									
1									
2									
3									
4									

Verifica saldature									
Seq-1, Seq-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome									
S1									
S2									
S3									
S4									
S5									
S6									
S7									
S8									
S9									
S10									
S11									
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S26									
S27									
S28									
S29									
S30									
S31									
S32									
S33									
S34									
S35									
S36									
S37									
S38									
S39									
S40									

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft.Ed / Td.Rd									
Nome									
1									
2									
3									
4									

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft.Ed / Td.Rd									
Nome									
1									
2									
3									
4									

Verifica piastra			
S _{max}		f _d /v _r	
138.3		2238.1	
Verifica nervature			
Posizione	S _{max}	f _d /v _r	
Z	434.3	2238.1	
Y	379.8	2238.1	

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 1 As. 112 Nd. 734									
Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft.Ed / Td.Rd									
Nome									
1									
2									
3									
4									

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft.Ed / Td.Rd									
Nome									
1									
2									
3									
4									

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft.Ed / Td.Rd									
Nome									
1									
2									
3									
4									

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S24	166.7	6.1	0.	166.8	166.7	1997.5	2350.	[.5T]
S25	15.7	1.9	0.	15.9	15.7	1997.5	2350.	[.5T]
S26	21.3	1.1	0.	21.4	21.3	1997.5	2350.	[.5T]
S27	92.6	1.9	0.	92.6	92.6	1997.5	2350.	[.5T]
S28	98.6	1.9	0.	98.6	98.6	1997.5	2350.	[.5T]
S29	0.	274.9	0.	66.1	281.2	1997.5	2350.	[.5T]
S30	61.2	312.7	0.	66.1	325.4	1997.5	2350.	[.5T]
S31	0.	458.8	0.	66.1	462.8	1997.5	2350.	[.5T]
S32	2.	175.1	0.	68.1	187.2	1997.5	2350.	[.5T]
S33	2.	175.1	0.	68.1	187.2	1997.5	2350.	[.5T]
S34	2.	185.1	0.	69.6	198.4	1997.5	2350.	[.5T]
S35	2.	175.1	0.	69.6	198.4	1997.5	2350.	[.5T]
S36	0.	784.3	0.	784.3	784.3	1997.5	2350.	[.5T]
S37	61.2	312.7	0.	784.3	784.3	1997.5	2350.	[.5T]
S38	0.	784.3	0.	784.3	784.3	1997.5	2350.	[.5T]
S39	61.2	312.7	0.	784.3	784.3	1997.5	2350.	[.5T]
S40	61.2	312.7	0.	784.3	784.3	1997.5	2350.	[.5T]

Verifica piastra	
Smx	[.5T]
Y	1373.9
Z	2238.1
Y	1373.9
Z	2238.1

Verifica nervature	
Posizione	Smx
Y	1010.6
Z	2238.1
Y	1373.9
Z	2238.1

Verifica pressione sul calcestruzzo	
Smx	[.5T]
Y	27.7
Z	141.1
Y	27.7
Z	141.1

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 117 Nd. 742

Combinazione di sollecitazioni agenti Caso 7 As. 176 Nd. 0

N	-3003.9	Ty	464	Tz	-224.6
Mc	0	My	-76337	Mz	-2259

Verifica tirafond												
Co-1,	Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)											
Co-3:	Ft,Ed / T.ad,Rd											
Num	Pv,Ed	Pv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	T.ad,Rd	Co-1	Co-2	Co-3		
1	128.9	3240.5	13714.3	193.6	4860.7	19543.2	3564.	.07	.04	.05		
2	128.9	3240.5	13714.3	193.6	4860.7	19543.2	3564.	.04	.01	.02		
3	128.9	3240.5	13714.3	193.6	4860.7	19543.2	3564.	.07	.04	.05		
4	128.9	3240.5	13714.3	193.2	4860.7	19543.2	3564.	.04	.01	.02		

Verifica saldature									
Seq-1, Seq-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome	S.p.rp	Tau.p.a	Tau.p.e	Seq-1	Seq-2	Seq-1	Seq-2	Seq-1	Seq-2
S1	15.5	2.4	0.	11.8	11.5	1997.5	2350.	S16	83.6
S2	11.5	2.4	0.	11.8	11.5	1997.5	2350.	S17	82.1
S3	43.8	2.4	0.	43.8	43.8	1997.5	2350.	S18	82.1
S4	43.7	2.4	0.	43.7	43.7	1997.5	2350.	S19	13.1
S5	18.5	2.4	0.	18.5	18.5	1997.5	2350.	S20	8.6
S6	42.3	2.4	0.	42.4	42.3	1997.5	2350.	S21	11.5
S7	42.2	2.4	0.	42.2	42.2	1997.5	2350.	S22	11.5
S8	10.8	2.4	0.	10.8	10.8	1997.5	2350.	S23	11.5
S9	46.1	5.1	0.	46.1	46.1	1997.5	2350.	S24	14.4
S10	46.1	5.1	0.	46.1	46.1	1997.5	2350.	S25	49.2
S11	44.7	5.1	0.	44.7	44.7	1997.5	2350.	S26	49.1
S12	47.6	5.1	0.	47.6	47.6	1997.5	2350.	S27	50.6
S13	41.5	5.1	0.	41.5	41.5	1997.5	2350.	S28	50.7
S14	44.4	5.1	0.	44.7	44.4	1997.5	2350.	S29	0.
S15	83.5	2.4	0.	83.5	83.5	1997.5	2350.	S30	24.6
S16	83.6	2.4	0.	83.6	83.6	1997.5	2350.	S31	0.
S17	82.1	2.4	0.	82.1	82.1	1997.5	2350.	S32	216.1
S18	82.1	2.4	0.	82.1	82.1	1997.5	2350.	S33	216.1
S19	13.1	1.1	0.	12.6	13.1	1997.5	2350.	S34	216.1
S20	8.6	5.1	0.	8.6	8.6	1997.5	2350.	S35	216.1
S21	11.5	2.4	0.	14.1	11.5	1997.5	2350.	S36	0.
S22	11.5	2.4	0.	14.6	11.5	1997.5	2350.	S37	24.6
S23	11.5	2.4	0.	14.6	11.5	1997.5	2350.	S38	0.
S24	14.4	5.1	0.	15.3	14.4	1997.5	2350.	S39	24.6
S25	49.2	2.4	0.	49.2	49.2	1997.5	2350.	S40	24.6
S26	49.1	2.4	0.	49.1	49.1	1997.5	2350.		
S27	50.6	2.4	0.	50.7	50.6	1997.5	2350.		
S28	50.7	2.4	0.	50.8	50.7	1997.5	2350.		
S29	0.	157.5	28.2	160.1	50.8	1997.5	2350.		
S30	24.6	31.1	28.2	246.3	246.3	1997.5	2350.		
S31	0.	375.2	28.2	375.2	28.2	1997.5	2350.		
S32	216.1	123.5	246.3	216.1	216.1	1997.5	2350.		
S33	216.1	123.5	0.	248.9	216.1	1997.5	2350.		
S34	216.1	123.5	0.	248.9	216.1	1997.5	2350.		
S35	216.1	123.5	0.	248.9	216.1	1997.5	2350.		
S36	0.	359.8	11.9	360.	11.9	1997.5	2350.		
S37	24.6	27.1	11.9	360.3	36.5	1997.5	2350.		
S38	0.	172.9	11.9	173.3	11.9	1997.5	2350.		
S39	24.6	13.7	0.	28.1	24.6	1997.5	2350.		
S40	24.6	13.7	0.	28.1	24.6	1997.5	2350.		

Verifica piastra	
Smx	[.5T]
Y	583.5
Z	2238.1
Y	583.5
Z	2238.1

Verifica nervature	
Posizione	Smx
Y	467.6
Z	2238.1
Y	467.6
Z	2238.1

Verifica pressione sul calcestruzzo	
Smx	[.5T]
Y	9.6
Z	141.1
Y	9.6
Z	141.1

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 7 As. 176 Nd. 0

Combinazione di sollecitazioni agenti Caso 7 As. 117 Nd. 742

N	-3003.9	Ty	432.9	Tz	-22.5
Mc	0	My	-7259	Mz	-76337

Verifica tirafond										
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)										
Co-3: Ft,Ed / Tad,Rd										
Num	Fv,Ed	Fv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Tad,Rd	Co-1	Co-2	Co-3
1	108.4	3240.5	13714.3	-64.6	4860.7	19543.2	3564.	.03	.01	.01
2	108.4	3240.5	13714.3	-58.8	4860.7	19543.2	3564.	.03	.01	.01
3	108.4	3240.5	13714.3	208.3	4860.7	19543.2	3564.	.06	.04	.06
4	108.4	3240.5	13714.3	214.	4860.7	19543.2	3564.	.06	.04	.06

Verifica saldature							
Seq-1, Seq-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)							
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)							
Nome	S.p.rp	Tau.p.a	Tau.p.e	Seq-1	Seq-2	Seq-1	Seq-2
S1	35.6	4.8	0.	35.9	35.6	1997.5	2350.
S2	40.8	4.8	0.	40.8	40.8	1997.5	2350.
S3	45.1	4.8	0.	45.1	45.1	1997.5	2350.
S4	39.8	4.8	0.	39.8	39.8	1997.5	2350.
S5	35.5	4.8	0.	35.9	35.5	1997.5	2350.
S6	7.9	4.8	0.	7.9	7.9	1997.5	2350.
S7	12.2	4.8	0.	12.2	12.2	1997.5	2350.
S8	41.1	4.8	0.	41.1	41.1	1997.5	2350.
S9	41.1	4.8	0.	41.1	41.1	1997.5	2350.
S10	45.6	4.8	0.	45.6	45.6	1997.5	2350.
S11	85.6	4.8	0.	85.6	85.6	1997.5	2350.
S12	85.6	4.8	0.	85.6	85.6	1997.5	2350.
S13	54.3	4.8	0.	54.5	54.3	1997.5	2350.
S14	54.4	4.8	0.	54.6	54.4	1997.5	2350.
S15	40.3	4.8	0.	40.3	40.3	1997.5	2350.

S16	43.4	4.8	0.	43.4	43.4	1997.5	2350.
S17	10.2	4.8	0.	10.2	10.2	1997.5	2350.
S18	13.4	4.8	0.	13.4	13.4	1997.5	2350.
S19	42.7	4.8	0.	43.1	42.7	1997.5	2350.
S20	42.7	4.8	0.	43.1	42.7	1997.5	2350.
S21	87.2	4.8	0.	87.3	87.2	1997.5	2350.
S22	134	4.8	0.	87.4	134	1997.5	2350.
S23	52.8	4.8	0.	53.1	52.8	1997.5	2350.
S24	52.8	4.8	0.	53.1	52.8	1997.5	2350.
S25	43.1	4.8	0.	43.1	43.1	1997.5	2350.
S26	46.2	4.8	0.	46.2	46.2	1997.5	2350.
S27	7.4	4.8	0.	7.4	7.4	1997.5	2350.
S28	10.6	4.8	0.	10.6	10.6	1997.5	2350.
S29	70.9	376.7	0.	70.9	70.9	1997.5	2350.
S30	38.3	136.4	70.9	136.5	109.2	1997.5	2350.
S31	38.3	136.4	70.9	136.5	109.2	1997.5	2350.
S32	32.8	125.1	70.9	147.5	103.8	1997.5	2350.
S33	32.8	125.1	0.	129.4	32.8	1997.5	2350.
S34	32.8	125.1	0.	130.8	32.8	1997.5	2350.
S35	32.8	125.1	0.	129.4	32.8	1997.5	2350.
S36	0.	167.7	53.1	175.9	53.1	1997.5	2350.
S37	38.3	136.4	53.1	151.3	91.4	1997.5	2350.
S38	0.	151.9	53.1	140.9	53.1	1997.5	2350.
S39	38.3	136.4	0.	141.7	38.3	1997.5	2350.
S40	38.3	136.4	0.	141.7	38.3	1997.5	2350.

Verifica piastra	
Smx	[.5T]
Y	568.1
Z	2238.1
Y	568.1
Z	2238.1

Verifica nervature	
Posizione	Smx
Y	389.2
Z	2238.1
Y	568.1
Z	2238.1

Verifica pressione sul calcestruzzo	
Smx	[.5T]
Y	10.1
Z	141.1
Y	10.1
Z	141.1

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 7 As. 117 Nd. 742

Combinazione di sollecitazioni agenti Caso 1 As. 117 Nd. 742

N	-5160.4	Ty	-98.4	Tz	-166
Mc	0	My	-24032	Mz	55286

Verifica tirafondi										
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)										
Co-3: Ft,Ed / T.ad,Rd										
Num	Fv,Ed	Fv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Tad,Rd	Co-1	Co-2	Co-3
1	48,2	3240,5	13714,3	-6,1	4860,7	19543,2	3564,01	0,0	0,0	0,0
2	48,2	3240,5	13714,3	16,4	4860,7	19543,2	3564,02	0,0	0,0	0,0
3	48,2	3240,5	13714,3	-55,4	4860,7	19543,2	3564,01	0,01	0,01	0,02
4	48,2	3240,5	13714,3	-32,6	4860,7	19543,2	3564,01	0,01	0,01	0,01

Verifica saldature							
Seq-1, Seq-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)							
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)							
Nome	S.p.rp	Tau.p.a	Tau.p.e	Seq-1	Seq-2	Seq-1	Seq-2
S1	31.6	1.1	0.	31.6	31.6	1997.5	2350.'SI'
S2	19.5	1.8	0.	19.6	19.5	1997.5	2350.'SI'
S3	16.4	1.8	0.	16.5	16.4	1997.5	2350.'SI'
S4	14.5	1.4	0.	14.6	14.5	1997.5	2350.'SI'
S5	16.4	1.8	0.	16.5	16.4	1997.5	2350.'SI'
S6	14.5	1.4	0.	14.6	14.5	1997.5	2350.'SI'
S7	36.8	1.1	0.	36.8	36.8	1997.5	2350.'SI'
S8	15.7	1.7	0.	15.8	15.7	1997.5	2350.'SI'
S10	37.6	1.1	0.	37.6	37.6	1997.5	2350.'SI'
S11	15.7	1.7	0.	15.8	15.7	1997.5	2350.'SI'
S12	31.5	1.1	0.	31.5	31.5	1997.5	2350.'SI'
S13	70.8	1.1	0.	70.8	70.8	1997.5	2350.'SI'
S14	69.9	1.1	0.	69.9	69.9	1997.5	2350.'SI'
S15	10.5	1.8	0.	10.7	10.5	1997.5	2350.'SI'
S16	12.7	1.8	0.	12.9	12.7	1997.5	2350.'SI'
S17	37.3	1.8	0.	37.3	37.3	1997.5	2350.'SI'
S18	39.6	1.5	0.	39.6	39.6	1997.5	2350.'SI'
S20	55.7	1.1	0.	55.7	55.7	1997.5	2350.'SI'
S21	55.7	1.1	0.	55.7	55.7	1997.5	2350.'SI'
S22	17.7	1.1	0.	17.7	17.7	1997.5	2350.'SI'
S23	81.1	1.1	0.	81.1	81.1	1997.5	2350.'SI'
S24	88	1.8	0.	88	88	1997.5	2350.'SI'
S25	37.2	1.8	0.	37.2	37.2	1997.5	2350.'SI'
S26	29	1.8	0.	29	29	1997.5	2350.'SI'
S27	67	1.8	0.	67	67	1997.5	2350.'SI'
S28	69.6	1.8	0.	69.6	69.6	1997.5	2350.'SI'
S29	0.	46.4	10.3	47.6	10.3	1997.5	2350.'SI'
S30	99.6	150	10.3	179	10.3	1997.5	2350.'SI'
S31	10.3	150	10.3	179	10.3	1997.5	2350.'SI'
S32	41.8	89.5	10.3	99.3	52.1	1997.5	2350.'SI'
S33	41.8	89.5	10.3	99.3	41.8	1997.5	2350.'SI'
S34	41.8	106.4	115.5	163.3	157.3	1997.5	2350.'SI'
S35	41.8	106.4	115.5	163.3	41.8	1997.5	2350.'SI'
S36	0.	253.9	115.5	277.1	115.5	1997.5	2350.'SI'
S37	0.	253.9	115.5	277.1	0.	1997.5	2350.'SI'
S38	0.	414.7	115.5	430	115.5	1997.5	2350.'SI'
S39	0.	414.7	115.5	430	0.	1997.5	2350.'SI'
S40	99.6	150	10.3	179	10.3	1997.5	2350.'SI'
S41	10.3	150	10.3	179	10.3	1997.5	2350.'SI'

S51	29.61	12.51	0.	32.11	29.61	1997.51	2350.151*
S56	46.31	3.21	0.	46.41	46.31	1997.51	2350.151*
S71	46.21	3.21	0.	46.31	46.21	1997.51	2350.151*
S8	24.31	3.21	0.	24.61	24.31	1997.51	2350.151*
S10	48.31	12.51	0.	48.81	48.31	1997.51	2350.151*
S11	46.71	12.51	0.	46.81	46.71	1997.51	2350.151*
S12	48.71	12.51	0.	50.31	48.71	1997.51	2350.151*
S13	45.81	12.51	0.	45.91	45.81	1997.51	2350.151*
S14	47.81	12.51	0.	49.41	47.81	1997.51	2350.151*
S15	73.81	3.21	0.	73.91	73.81	1997.51	2350.151*
S16	73.91	3.21	0.	73.91	73.91	1997.51	2350.151*
S17	73.41	3.21	0.	73.51	73.41	1997.51	2350.151*
S18	73.41	3.21	0.	73.41	73.41	1997.51	2350.151*
S20	9.11	12.51	0.	15.41	9.11	1997.51	2350.151*
S21	11.41	12.51	0.	15.41	11.41	1997.51	2350.151*
S22	9.41	12.51	0.	15.71	9.41	1997.51	2350.151*
S23	10.51	12.51	0.	16.31	10.51	1997.51	2350.151*
S24	8.51	12.51	0.	15.11	8.51	1997.51	2350.151*
S25	16.61	3.21	0.	16.91	16.61	1997.51	2350.151*
S26	16.61	3.21	0.	16.91	16.61	1997.51	2350.151*
S27	17.11	3.21	0.	17.31	17.11	1997.51	2350.151*
S28	17.11	3.21	0.	17.41	17.11	1997.51	2350.151*
S29	0.11	26.41	53.11	59.21	0.11	1997.51	2350.151*
S30	17.51	54.61	53.11	78.11	17.51	1997.51	2350.151*
S31	0.11	307.71	53.11	332.11	0.11	1997.51	2350.151*
S32	143.71	95.51	53.11	180.51	143.71	1997.51	2350.151*
S33	143.71	95.51	53.11	172.51	143.71	1997.51	2350.151*
S34	143.71	95.51	54.61	181.11	143.71	1997.51	2350.151*
S35	143.71	95.51	0.	172.51	143.71	1997.51	2350.151*
S36	0.11	322.91	54.61	327.51	0.11	1997.51	2350.151*
S37	17.51	53.31	54.61	78.31	17.51	1997.51	2350.151*
S38	0.11	322.91	54.61	62.91	0.11	1997.51	2350.151*
S39	17.51	8.61	0.	19.51	17.51	1997.51	2350.151*
S40	17.51	8.61	0.	19.51	17.51	1997.51	2350.151*

Verifica piastra
Smax | fdlVer |
361.71 2238.1151*

Verifica nervature
Posizione | Smax | fdlVer |
Z | 361.71 2238.1151*
Y | 355.31 2238.1151*

Verifica pressione sul calcestruzzo
Smax | fdlVer |
4.61 141.1151*

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 175 Nd. 0

Combinazione di sollecitazioni agenti Caso 7 As. 175 Nd. 0

N: -2604 Ty: -641.7 Tz: -240.2
Mt: 0 Mt: 65881 Mt: 2735

Verifica tirafond
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)
Co-3: Ft,Ed / Tadm |
Num | Pv,Ed | Pv,Rd | Fb,Rd | Ft,Ed | Ft,Rd | Bp,Rd | Tadm,Rd | Co-1 | Co-2 | Co-3 | Ver |
1 | 171.31 3240.51 13714.31 | 171.11 4860.71 19543.21 | 3564.1 .08 | .04 | .05 | 151*
2 | 171.31 3240.51 13714.31 | -49.31 4860.71 19543.21 | 3564.1 .05 | .01 | .01 | 151*
3 | 171.31 3240.51 13714.31 | 164.41 4860.71 19543.21 | 3564.1 .08 | .03 | .05 | 151*
4 | 171.31 3240.51 13714.31 | -56.11 4860.71 19543.21 | 3564.1 .05 | .01 | .02 | 151*

Verifica saldature
Seq-1, SLim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)
Seq-2, SLim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)
Nome | S_pmp | Tadm_p | Tadm_p | Seq-1 | Seq-2 | SLim-1 | SLim-2 | Ver |
S1 | 13.61 1.71 | 0.11 | 15.41 | 16.61 | 1997.51 | 2350.151*
S2 | 9.51 2.61 | 0.11 | 9.81 | 9.51 | 1997.51 | 2350.151*
S3 | 36.21 2.61 | 0.11 | 36.31 | 36.21 | 1997.51 | 2350.151*
S4 | 36.31 2.61 | 0.11 | 36.41 | 36.31 | 1997.51 | 2350.151*
S5 | 16.21 2.11 | 0.11 | 17.71 | 16.21 | 1997.51 | 2350.151*
S6 | 38.11 2.61 | 0.11 | 38.11 | 38.11 | 1997.51 | 2350.151*
S7 | 38.21 2.61 | 0.11 | 38.21 | 38.21 | 1997.51 | 2350.151*
S8 | 10.21 2.61 | 0.11 | 10.61 | 10.21 | 1997.51 | 2350.151*
S10 | 40.11 7.11 | 0.11 | 40.61 | 40.11 | 1997.51 | 2350.151*
S11 | 35.61 3.51 | 0.11 | 35.61 | 35.61 | 1997.51 | 2350.151*
S12 | 38.11 7.11 | 0.11 | 38.81 | 38.11 | 1997.51 | 2350.151*
S13 | 39.11 7.11 | 0.11 | 39.71 | 39.11 | 1997.51 | 2350.151*
S14 | 41.61 7.11 | 0.11 | 41.61 | 41.61 | 1997.51 | 2350.151*
S15 | 70.61 2.61 | 0.11 | 70.71 | 70.61 | 1997.51 | 2350.151*
S16 | 70.51 2.61 | 0.11 | 70.61 | 70.51 | 1997.51 | 2350.151*
S17 | 72.41 2.61 | 0.11 | 72.41 | 72.41 | 1997.51 | 2350.151*
S18 | 72.51 2.61 | 0.11 | 72.61 | 72.51 | 1997.51 | 2350.151*
S20 | 11.51 7.11 | 0.11 | 11.51 | 11.51 | 1997.51 | 2350.151*
S21 | 10.61 7.11 | 0.11 | 12.81 | 10.61 | 1997.51 | 2350.151*
S22 | 13.11 7.11 | 0.11 | 14.91 | 13.11 | 1997.51 | 2350.151*
S23 | 7.11 7.11 | 0.11 | 10.11 | 7.11 | 1997.51 | 2350.151*
S24 | 9.61 7.11 | 0.11 | 12.11 | 9.61 | 1997.51 | 2350.151*
S25 | 43.91 2.61 | 0.11 | 44.11 | 43.91 | 1997.51 | 2350.151*
S26 | 44.11 2.61 | 0.11 | 44.11 | 44.11 | 1997.51 | 2350.151*
S27 | 42.11 2.61 | 0.11 | 42.21 | 42.11 | 1997.51 | 2350.151*
S28 | 42.11 2.61 | 0.11 | 42.11 | 42.11 | 1997.51 | 2350.151*
S29 | 0.11 35.31 | 21.11 | 35.31 | 21.11 | 1997.51 | 2350.151*
S30 | 21.11 22.91 | 21.11 | 37.41 | 21.11 | 1997.51 | 2350.151*
S31 | 0.11 306.21 | 21.11 | 306.91 | 21.11 | 1997.51 | 2350.151*
S32 | 186.41 109.91 | 21.11 | 217.41 | 207.41 | 1997.51 | 2350.151*
S33 | 186.41 109.91 | 0.11 | 216.41 | 186.41 | 1997.51 | 2350.151*
S34 | 186.41 109.91 | 16.11 | 217.11 | 207.51 | 1997.51 | 2350.151*
S35 | 186.41 109.91 | 0.11 | 216.41 | 186.41 | 1997.51 | 2350.151*
S36 | 0.11 306.91 | 16.11 | 327.31 | 16.11 | 1997.51 | 2350.151*
S37 | 21.11 27.61 | 37.41 | 37.41 | 27.61 | 1997.51 | 2350.151*
S38 | 0.11 133.81 | 16.11 | 133.81 | 16.11 | 1997.51 | 2350.151*
S39 | 21.11 11.91 | 0.11 | 21.11 | 21.11 | 1997.51 | 2350.151*
S40 | 21.11 11.91 | 0.11 | 24.11 | 21.11 | 1997.51 | 2350.151*

Verifica piastra
Smax | fdlVer |
460.11 2238.1151*

Verifica nervature
Posizione | Smax | fdlVer |
Z | 460.11 2238.1151*
Y | 425.91 2238.1151*

Verifica pressione sul calcestruzzo
Smax | fdlVer |
8.41 141.1151*

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 7 As. 175 Nd. 0

Combinazione di sollecitazioni agenti Caso 3 As. 175 Nd. 0

N: -3769.4 Ty: -791.1 Tz: -156.8
Mt: 0 Mt: -103362 Mt: -5829

Verifica tirafond
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)
Co-3: Ft,Ed / Tadm |
Num | Pv,Ed | Pv,Rd | Fb,Rd | Ft,Ed | Ft,Rd | Bp,Rd | Tadm,Rd | Co-1 | Co-2 | Co-3 | Ver |
1 | 201.61 3240.51 13714.31 | 201.71 4860.71 19543.21 | 3564.1 .08 | .01 | .03 | 151*
2 | 201.61 3240.51 13714.31 | 310.71 4860.71 19543.21 | 3564.1 .11 | .06 | .09 | 151*
3 | 201.61 3240.51 13714.31 | 74.91 4860.71 19543.21 | 3564.1 .06 | .01 | .02 | 151*
4 | 201.61 3240.51 13714.31 | 326.71 4860.71 19543.21 | 3564.1 .11 | .07 | .09 | 151*

Verifica saldature
Co-3: Ft,Ed / Tadm

Seq-1, SLim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)
Seq-2, SLim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)
Nome | S_pmp | Tadm_p | Tadm_p | Seq-1 | Seq-2 | SLim-1 | SLim-2 | Ver |
S1 | 24.11 8.81 | 0.11 | 25.71 | 24.11 | 1997.51 | 2350.151*
S2 | 58.41 1.71 | 0.11 | 58.41 | 58.41 | 1997.51 | 2350.151*
S3 | 58.71 1.71 | 0.11 | 58.71 | 58.71 | 1997.51 | 2350.151*
S4 | 14.81 1.71 | 0.11 | 14.91 | 14.81 | 1997.51 | 2350.151*
S5 | 20.11 8.81 | 0.11 | 21.91 | 20.11 | 1997.51 | 2350.151*
S6 | 17.11 1.71 | 0.11 | 17.21 | 17.11 | 1997.51 | 2350.151*
S7 | 54.41 1.71 | 0.11 | 54.51 | 54.41 | 1997.51 | 2350.151*
S8 | 54.81 1.71 | 0.11 | 54.81 | 54.81 | 1997.51 | 2350.151*
S10 | 20.31 8.81 | 0.11 | 22.11 | 20.31 | 1997.51 | 2350.151*
S11 | 12.31 8.81 | 0.11 | 15.11 | 12.31 | 1997.51 | 2350.151*
S12 | 16.31 8.81 | 0.11 | 18.51 | 16.31 | 1997.51 | 2350.151*
S13 | 19.81 8.81 | 0.11 | 21.61 | 19.81 | 1997.51 | 2350.151*
S14 | 23.71 8.81 | 0.11 | 25.31 | 23.71 | 1997.51 | 2350.151*
S15 | 67.31 1.71 | 0.11 | 67.31 | 67.31 | 1997.51 | 2350.151*
S16 | 67.11 1.71 | 0.11 | 67.11 | 67.11 | 1997.51 | 2350.151*
S17 | 71.11 1.71 | 0.11 | 71.11 | 71.11 | 1997.51 | 2350.151*
S18 | 71.31 1.71 | 0.11 | 71.31 | 71.31 | 1997.51 | 2350.151*
S20 | 61.61 8.81 | 0.11 | 62.21 | 61.61 | 1997.51 | 2350.151*
S21 | 61.11 8.81 | 0.11 | 61.61 | 61.11 | 1997.51 | 2350.151*
S22 | 65.11 8.81 | 0.11 | 65.31 | 65.11 | 1997.51 | 2350.151*
S23 | 53.61 8.81 | 0.11 | 54.31 | 53.61 | 1997.51 | 2350.151*
S24 | 51.51 8.81 | 0.11 | 52.21 | 51.51 | 1997.51 | 2350.151*
S25 | 112.41 1.71 | 0.11 | 112.41 | 112.41 | 1997.51 | 2350.151*
S26 | 112.61 1.71 | 0.11 | 112.61 | 112.61 | 1997.51 | 2350.151*
S27 | 106.61 1.71 | 0.11 | 106.61 | 106.61 | 1997.51 | 2350.151*
S28 | 108.31 1.71 | 0.11 | 108.41 | 108.31 | 1997.51 | 2350.151*
S29 | 0.11 507.51 | 36.11 | 508.81 | 36.11 | 1997.51 | 2350.151*
S30 | 134.21 172.11 | 36.11 | 221.21 | 170.31 | 1997.51 | 2350.151*
S31 | 0.11 213.81 | 36.11 | 216.81 | 36.11 | 1997.51 | 2350.151*
S32 | 39.91 40.71 | 36.11 | 67.51 | 39.91 | 1997.51 | 2350.151*
S33 | 39.91 22.81 | 0.11 | 45.91 | 39.91 | 1997.51 | 2350.151*
S34 | 39.91 30.51 | 4.31 | 50.41 | 39.91 | 1997.51 | 2350.151*
S35 | 39.91 22.81 | 0.11 | 45.91 | 39.91 | 1997.51 | 2350.151*
S36 | 0.11 253.71 | 4.31 | 253.71 | 4.31 | 1997.51 | 2350.151*
S37 | 134.21 172.11 | 4.31 | 218.31 | 138.51 | 1997.51 | 2350.151*
S38 | 0.11 467.71 | 4.31 | 467.71 | 4.31 | 1997.51 | 2350.151*
S39 | 134.21 172.11 | 0.11 | 218.21 | 134.21 | 1997.51 | 2350.151*
S40 | 134.21 172.11 | 0.11 | 218.21 | 134.21 | 1997.51 | 2350.151*

Verifica piastra
Smax | fdlVer |
826.41 2238.1151*

Verifica nervature
Posizione | Smax | fdlVer |
Z | 826.41 2238.1151*
Y | 519.91 2238.1151*

Verifica pressione sul calcestruzzo
Smax | fdlVer |
14.21 141.1151*

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 175 Nd. 0

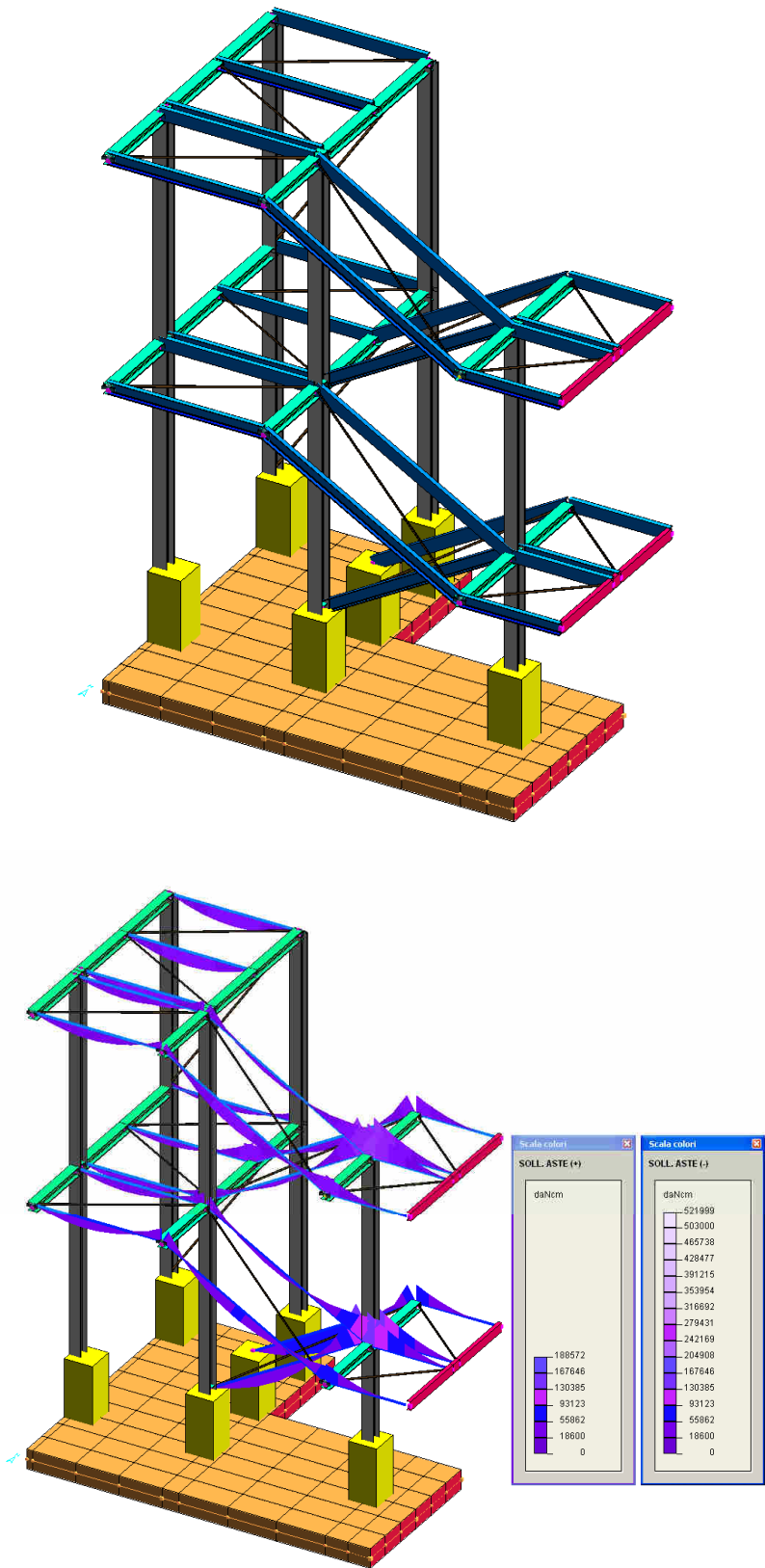
Combinazione di sollecitazioni agenti Caso 7 As. 116 Nd. 741

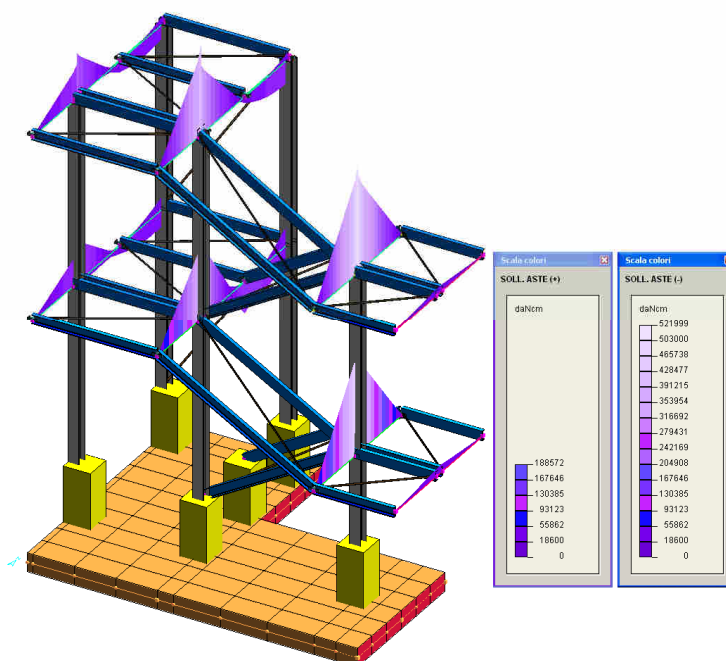
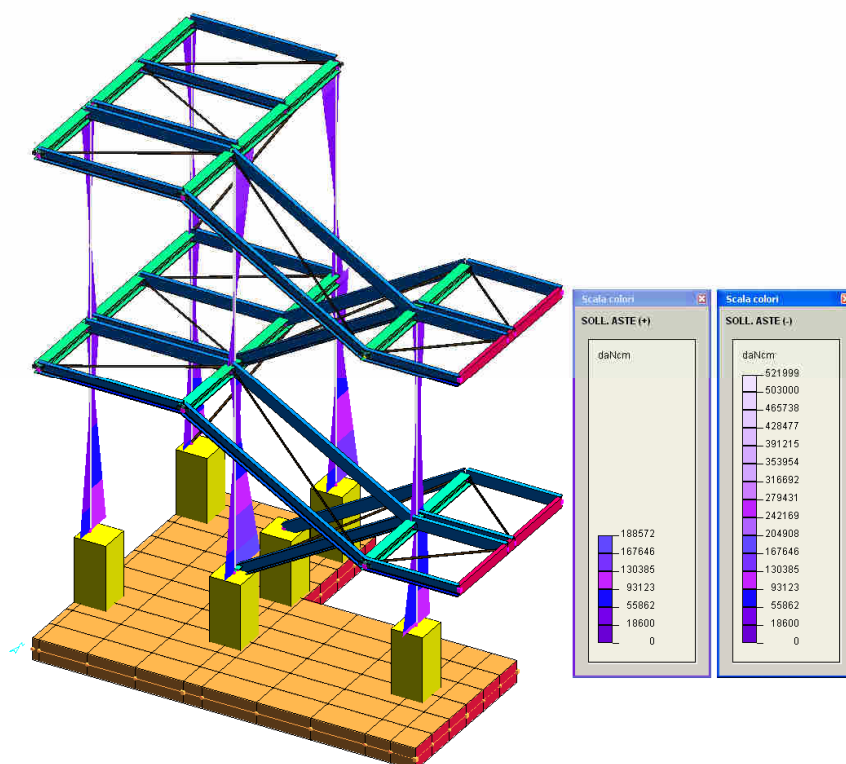
N: -4200.4 Ty: -381.3 Tz: 2.6
Mt: 0 Mt: -5829 Mt: 103362

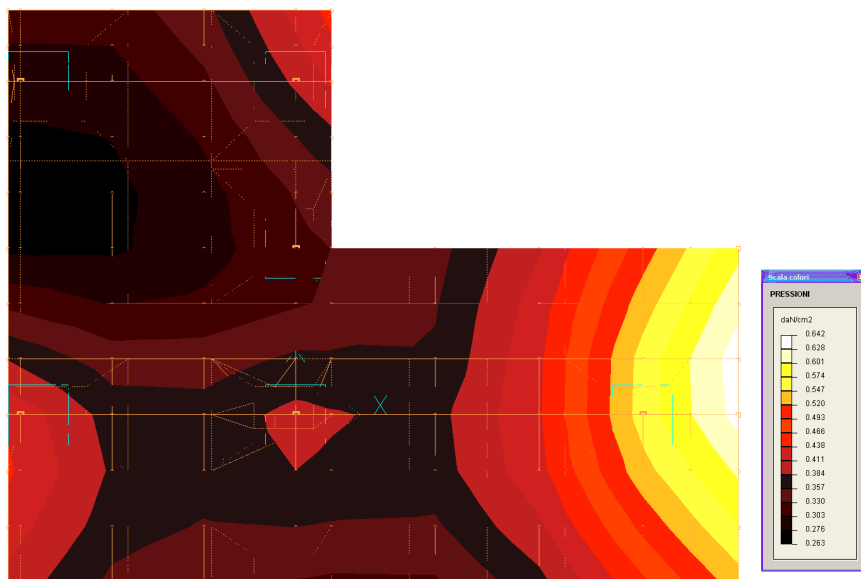
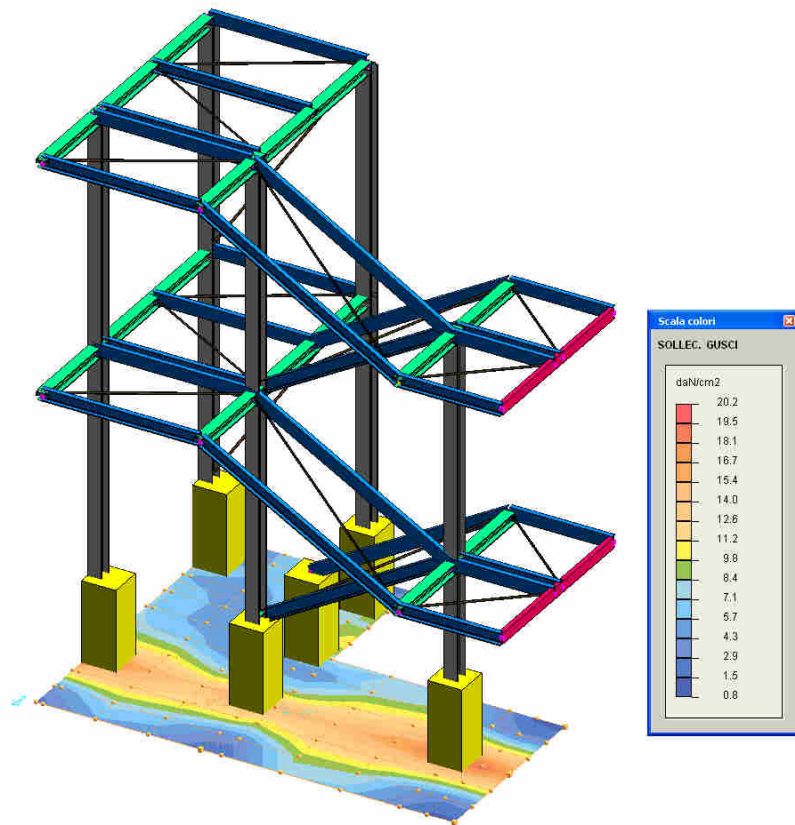
Verifica tirafond
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)
Co-3: Ft,Ed / Tadm |
Num | Pv,Ed | Pv,Rd | Fb,Rd | Ft,Ed | Ft,Rd | Bp,Rd | Tadm,Rd | Co-1 | Co-2 | Co-3 | Ver |
1 | 95.31 3240.51 13714.31 | 256.71 4860.71 19543.21 | 3564.1 .07 | .05 | .07 | 151*
2 | 95.31 3240.51 13714.31 | 271.11 4860.71 19543.21 | 3564.1 .07 | .06 | .08 | 151*
3 | 95.31 3240.51 13714.31 | -90.71 4860.71 19543.21 | 3564.1 .03 | .01 | .01 | 151*
4 | 95.31 3240.51 13714.31 | -76.41 4860.71 19543.21 | 3564.1 .03 | .01 | .02 | 151*

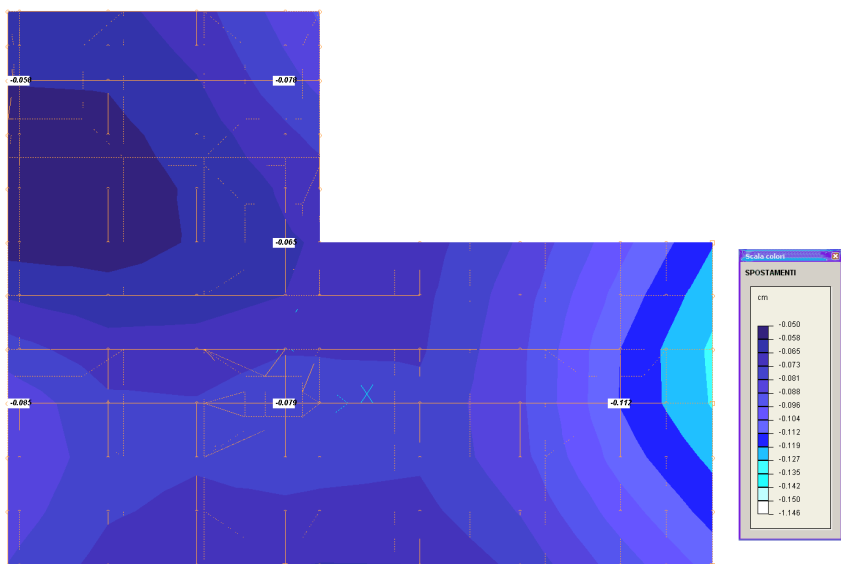
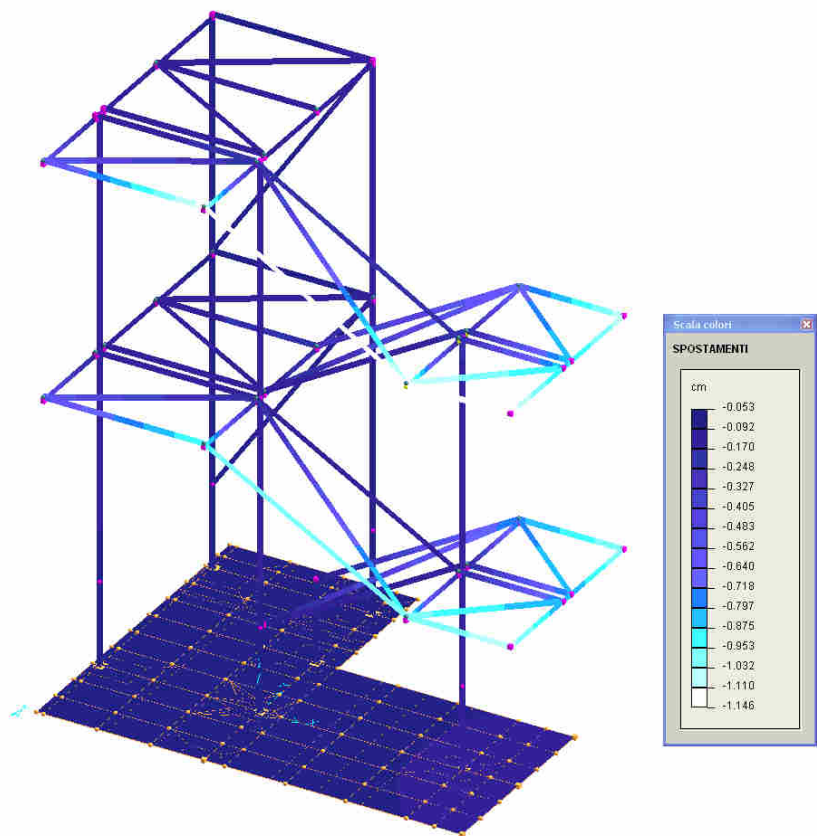
Verifica saldature
Seq-1, SLim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)
Seq-2, SLim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)
Nome | S_pmp | Tadm_p | Tadm_p | Seq-1 | Seq-2 | SLim-1 | SLim-2 | Ver |
S1 | 69.11 4.21 | 0.11 | 69.21 | 69.11 | 1997.51 | 2350.151*
S2 | 8.51 0.11 | 0.11 | 8.51 | 8.51 | 1997.51 | 2350.151*
S3 | 16.71 0.11 | 0.11 | 16.71 | 16.71 | 1997.51 | 2350.151*
S4 | 10.91 0.11 | 0.11 | 10.91 | 10.91 | 1997.51 | 2350.151*
S5 | 48.81 4.21 | 0.11 | 49.11 | 48.81 | 1997.51 | 2350.151*
S6 | 54.51 0.11 | 0.11 | 54.51 | 54.51 | 1997.51 | 2350.151*
S7 | 62.71 0.11 | 0.11 | 62.71 | 62.71 | 1997.51 | 2350.151*
S8 | 36.91 0.11 | 0.11 | 36.91 | 36.91 | 1997.51 | 2350.151*
S10 | 55.21 4.21 | 0.11 | 55.41 | 55.21 | 1997.51 | 2350.151*
S11 | 75.71 4.21 | 0.11 | 73.81 | 73.71 | 1997.51 | 2350.151*
S12 | 75.91 4.21 | 0.11 | 74.11 | 73.91 | 1997.51 | 2350.151*
S13 | 115.71 4.21 | 0.11 | 115.81 | 115.71 | 1997.51 | 2350.151*
S14 | 115.51 4.21 | 0.11 | 115.61 | 115.51 | 1997.51 | 2350.151*
S15 | 15.51 0.11 | 0.11 | 15.51 | 15.51 | 1997.51 | 2350.151*
S16 | 19.81 0.11 | 0.11 | 19.81 | 19.81 | 1997.51 | 2350.151*
S17 | 54.31 0.11 | 0.11 | 54.31 | 54.31 | 1997.51 | 2350.151*
S18 | 58.51 0.11 | 0.11 | 58.51 | 58.51 | 1997.51 | 2350.151*
S19 | 59.61 4.21 | 0.11 | 59.81 | 59.61 | 1997.51 | 2350.151*
S21 | 69.81 4.21 | 0.11 | 69.91 | 69.81 | 1997.51 | 2350.151*
S22 | 69.51 4.21 | 0.11 | 69.71 | 69.51 | 1997.51 | 2350.151*
S23 | 119.71 4.21 | 0.11 | 119.81 | 119.71 | 1997.51 | 2350.151*
S24 | 119.91 4.21 | 0.11 | 120.11 | 119.91 | 1997.51 | 2350.151*
S25 | 12.31 0.11 | 0.11 | 12.31 | 12.31 | 1997.51 | 2350.151*
S26 | 12.61 0.11 | 0.11 | 12.61 | 12.61 | 1997.51 | 2350.151*
S27 | 61.51 0.11 | 0.11 | 61.51 | 61.51 | 1997.51 | 2350.151*
S28 | 65.71 0.11 | 0.11 | 65.71 | 65.71 | 1997.51 | 2350.151*
S29 | 0.11 101.61 | 22.91 | 102.91 | 22.91 | 1997.51 | 2350.151*
S30 | 57.41 102.41 | 22.91 | 102.11 | 80.31 | 1997.51 | 2350.151*
S31 | 0.11 232.21 | 22.91 | 233.41 | 22.91 | 1997.51 | 2350.151*
S32 | 43.41 163.51 | 0.11 | 43.41 | 43.41 | 1997.51 | 2350.151*
S33 | 43.41 163.51 | 0.11 | 43.41 | 43.41 | 1997.51 | 2350.151*
S34 | 43.41 163.51 | 220.41 | 227.91 | 263.81 | 1997.51 | 2350.151*
S35 | 43.41 163.51 | 0.11 | 43.41 | 43.41 | 1997.51 | 2350.151*
S36 | 0.11 474.41 | 220.

3.2 Report Grafico









SOMMARIO

<i>Sommario</i>	<i>1</i>
1 Premessa Generale	3
1.1 Assunti Progettuali	3
2 Relazione illustrativa	3
3 Relazione di calcolo	5
3.1 Report di calcolo	5
3.2 Report Grafico	133

1 PREMESSA GENERALE

1.1 Assunti Progettuali

Non essendo stato tutt'ora identificato da parte dell'amministrazione competente il tecnico incaricato per le indagini geologiche finalizzate all'identificazione dei parametri geotecnici di dettaglio, si è fatto riferimento a quanto noto alla geologia dell'area e si sono stimati i parametri geotecnici, proponendo una soluzione strutturale compatibile con le condizioni geotecniche mediocri. Tali parametri dovranno essere confermati da campagna analitica in sito prevista dall'amministrazione competente.

2 RELAZIONE ILLUSTRATIVA

TITOLO DEL PROGETTO

Realizzazione Scala esterna di sicurezza

COMMITTENTE

Città di Moncalieri
P.zza Vittorio Emanuele II
10024 Moncalieri (To)

PROGETTISTA

Dott. Ing. Virgilio M. CHIONO - Studio Associato POOL ENGINEERING
Vicolo Cugiano 4 - San Giorgio Can.se (To)
Ordine degli Ingegneri di Torino e Provincia al n° 8645 F

1. INDIVIDUAZIONE DEL MODELLO DI CALCOLO

1.1 DESCRIZIONE GENERALE DELL'OPERA

Oggetto della presente relazione e' l'analisi delle sollecitazioni ed il calcolo della struttura in cemento armato ordinario da realizzarsi in:

Lotto: Strada Vignotto, 21- 10024 Moncalieri (To)
Comune di: Moncalieri (To)
Proprieta

Città di Moncalieri
P.zza Vittorio Emanuele II
10024 Moncalieri (To)

Destinazione e tipologia dell'opera:

Il sito oggetto dell'intervento presenta i seguenti caratteri morfologico-geotecnici generali:

Realizzazione Scala esterna di sicurezza con opere in cemento armato normale e acciaio strutturale

La struttura e' composta dai seguenti elementi, previsti in calcestruzzo gettato in opera:

FONDAZIONI: soletta piena di fondazione in c.a.

Tale soluzione strutturale si e' adottata per diminuire i cedimenti, ed assicurare la funzionalità della struttura.

TRAVI: Profili in acciaio strutturale S235, sezioni tipo HE ed UPN

PILASTRI: Pilastri a sezione rettangolare e Profili in acciaio strutturale S235, sezioni tipo HE

1.2 NORMATIVE DI RIFERIMENTO

L'analisi della struttura in oggetto e' stata fatta utilizzando i metodi usuali della Scienza delle Costruzioni ed in conformità alle normative e leggi vigenti:

- Legge 5/11/1971 n. 1086: Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

- D.P.R. 6/6/2001 n. 380: Testo unico delle disposizioni legislative e regolamentari in materia edilizia.

- D.M. 14/1/2008: Norme tecniche per le costruzioni.

1.3 CRITERI DI ANALISI DELLA SICUREZZA

Con riferimento alle normative precedentemente citate, le strutture in oggetto sono verificate per quanto riguarda:

- verifica di resistenza;

- verifica a deformazione e fessurazione.

Calcestruzzo per le strutture in elevazione: classe C25/30

Acciaio in barre : B450C

Acciaio in Profili: S235/FE360

1.4 SCHEMATIZZAZIONE DELLA STRUTTURA E DEI VINCOLI

La struttura e' stata schematizzata escludendo il contributo degli elementi aventi rigidità e resistenza trascurabili a fronte dei principali. E' quindi stata considerata l'orditura a telaio tridimensionale, i solai ed i setti verticali ad elevata rigidità (vano ascensore, setti in cls).

Le opere di fondazione vengono assimilate a vincoli elastici di cui e' fornita la costante di rigidità. Le travi di fondazione sono schematizzate come poggianti su vincoli elastici distribuiti.

1.5 MODELLAZIONE DELLA STRUTTURA E DEI VINCOLI

La struttura e' modellata con il metodo degli elementi finiti, applicato a sistemi tridimensionali. Gli elementi utilizzati sono sia monodimensionali (trave con eventuali sconnessioni interne), che bidimensionali (piastre e membrane triangolari e quadrangolari). I vincoli sono considerati puntuali ed inseriti tramite le sei costanti di rigidità elastica, oppure come elementi asta poggianti su suolo elastico. Le sezioni oggetto di verifica nelle travi sono stampate a passo costante; dei gusci si conoscono le sollecitazioni nel baricentro dell'elemento stesso.

1.6 SCHEMATIZZAZIONE DELLE AZIONI

In accordo con le sopracitate normative, sono state considerate nei calcoli le seguenti azioni:

- pesi propri strutturali
- carichi permanenti portati dalla struttura
- carichi variabili sui solai, neve, vento.
- forze di piano simulanti il sisma, ricavate tramite analisi statica semplificata
- distorsioni termiche

Le condizioni ed i casi di carico prese in conto nei calcoli sono specificate nella stampa dei dati di input.

1.7 MODELLAZIONE DELLE AZIONI

Sono stati adottati i valori di carico come riportato in relazione e confacenti ai dettati normativi.

Carico Variabile Luoghi soggetti ad affollamento:

- 1) -400 - daN/m²

Le azioni sono state modellate tramite opportuni carichi concentrati e distribuiti su nodi ed aste.

1.8 MODELLAZIONE DEI MATERIALI

I materiali costituenti la struttura sono considerati elastici e con comportamento lineare. Le loro caratteristiche sono specificate nella stampa dei dati di input.

1.9 TIPO DI ANALISI

Le analisi strutturali condotte sono statiche in regime lineare. Il metodo di calcolo è ad elementi finiti. Il calcolo sismico è stato effettuato tramite analisi statica semplificata. La verifica delle membrature in cemento armato viene eseguita considerando tutte le caratteristiche di sollecitazione.

2 CODICE DI CALCOLO

2.1 INDIVIDUAZIONE DEL CODICE DI CALCOLO

Per il calcolo delle sollecitazioni e per la verifica di travi e pilastri in cemento armato si è fatto ricorso all'elaboratore elettronico utilizzando il seguente programma di calcolo:

DOLMEN WIN (R), versione 15.0 del 2015 prodotto, distribuito ed assistito dalla CDM DOLMEN srl, con sede in Torino, Via Drovetti 9/F.

Questa procedura è sviluppata in ambiente Windows, ed è stata scritta utilizzando i linguaggi Fortran e C. DOLMEN WIN permette l'analisi elastica lineare di strutture tridimensionali con nodi a sei gradi di libertà utilizzando un solutore ad elementi finiti. Gli elementi considerati sono la trave, con eventuali svincoli interni o rotazione attorno al proprio asse, ed il guscio, sia rettangolare che triangolare, avente comportamento di membrana e di piastra. I carichi possono essere applicati sia ai nodi, come forze o coppie concentrate, sia sulle travi, come forze distribuite, trapezie, concentrate, come coppie e come distorsioni termiche. I vincoli sono forniti tramite le sei costanti di rigidità elastica.

A supporto del programma è fornito un ampio manuale d'uso contenente fra l'altro una vasta serie di test di validazione sia su esempi classici di Scienza delle Costruzioni, sia su strutture particolarmente impegnative e reperibili nella bibliografia specializzata.

2.2 GRADO DI AFFIDABILITÀ DEL CODICE

L'affidabilità del codice di calcolo è garantita dall'esistenza di un'ampia documentazione di supporto, come indicato nel paragrafo precedente. La presenza di un modulo CAD per l'introduzione di dati permette la visualizzazione dettagliata degli elementi introdotti. È possibile inoltre ottenere rappresentazioni grafiche di deformate e sollecitazioni della struttura. Al termine dell'elaborazione viene inoltre valutata la qualità della soluzione, in base all'uguaglianza del lavoro esterno e dell'energia di deformazione.

2.3 MOTIVAZIONE DELLA SCELTA DEL CODICE

DOLMEN WIN permette in campo elastico lineare un'analisi dettagliata del comportamento dell'intera struttura, tenendo conto del comportamento irrigidente di setti anche complessi e solai considerati con la loro effettiva rigidità. È possibile inoltre scegliere il grado di affinamento dell'analisi di elementi complessi utilizzando mesh via via più dettagliate.

3. ESAME DEI RISULTATI E CONTROLLI

3.1 VALUTAZIONE DELLA CORRETTEZZA DEL MODELLO

Il modello di calcolo adottato è da ritenersi appropriato in quanto non sono state riscontrate labilità, le reazioni vincolari equilibrano i carichi applicati, la simmetria di carichi e struttura dà origine a sollecitazioni simmetriche.

4. GIUDIZIO MOTIVATO DI ACCETTABILITÀ DEI RISULTATI

L'analisi critica dei risultati e dei parametri di controllo nonché il confronto con calcolazioni di massima eseguite manualmente porta ad confermare la validità dei risultati.

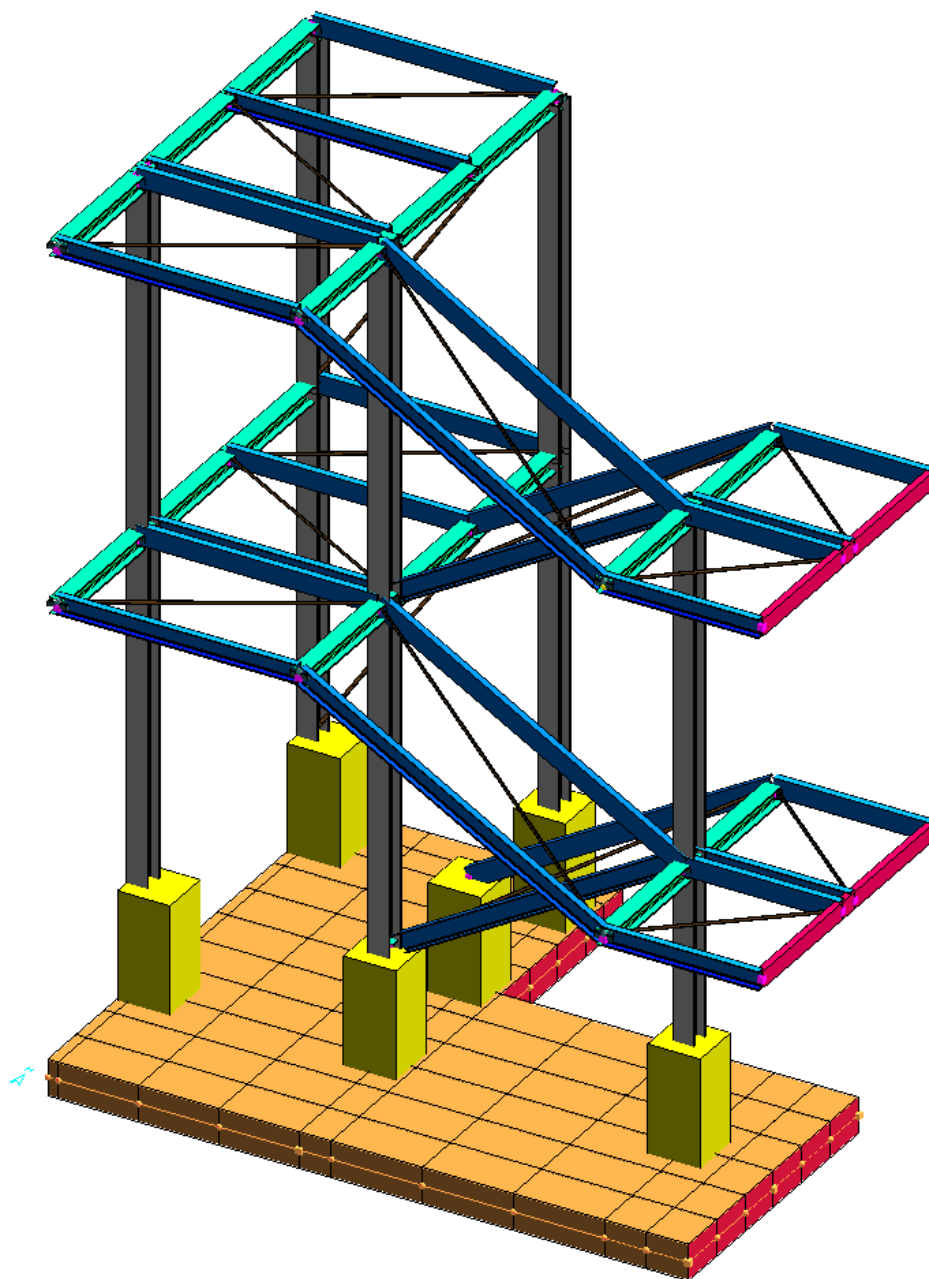
5. ALLEGATI

Alla presente relazione si allegano le seguenti stampe:

- dati di ingresso;
- sollecitazioni nelle aste e nei gusci;
- reazioni vincolari;
- verifiche di resistenza di travi e pilastri;
- diagrammi di sollecitazioni e deformazioni.

3 RELAZIONE DI CALCOLO

3.1 Report di calcolo




```
494      1      778      779      780      781
495      1      781      780      782      783
496      1      782      782      958      784
497      1      784      958      785      786
498      1      786      785      787      788
499      1      788      787      789      790

PROPRIETA' ASTE-----|-----|-----|-----|num.= 6
Nome Materiale Base Altezza Area Area tag. Y Area tag. Z
1 2 Kw vertic. 7.00 Kw orizz. 18.00 2.8000E+01 1.4400E+01 1.5400E+01
2 2 0.000000 0.000000 9.28333E+00 1.14000E+02 1.15400E+03
3 2 20.00 0.000000 5.93000E+01 2.00300E+03 5.69600E+03
4 2 36.00 0.000000 8.12000E+01 8.89000E+02 2.49200E+03
5 2 6.50 0.000000 6.20000E+01 1.20000E+01 1.36500E+01
6 2 3.00 0.000000 7.26558E+03 8.51000E+01 9.2500E+02
5 2 3.00 0.000000 3.00 2.3000E+00 1.2000E+00 1.2000E+00
6 1 50.00 0.000000 6.4000E+02 1.8000E+00 1.8000E+00
0.000000 2.000000 5.20833E+03 2.0833E+03 5.20833E+03

PROPRIETA' GUSCI-----|-----|-----|-----|num.= 1
Nome Materiale Sp. piastra Kw
1 1 35.00 35.00 5.000000

MATERIALI-----|-----|-----|-----|num.= 2
Nome Mod. elast. Coeff. nu Mod. tang. Peso spec. D11. te.
1 3.0000E+05 1.5000E+01 1.3000E+05 2.5000E-03 1.0000E-05
2 2.1000E+06 3.0000E-01 8.5000E+05 7.8500E-03 1.0000E-05

VINCOLI-----|-----|-----|-----|num.= 6
Nodo Rigid. X Rigid. Y Rigid. Z Rigid. RX Rigid. RY Rigid. RZ
958 bloccato bloccato libero libero libero libero
960 bloccato bloccato libero libero libero libero
964 bloccato bloccato libero libero libero libero
967 bloccato bloccato libero libero libero libero
969 bloccato bloccato libero libero libero libero
40 bloccato bloccato libero libero libero libero

CARICHI NODI-----|-----|-----|-----|num.= 308
Nome Nodo Direzione Intensita
1 154 : Forze Statiche (Analisi Semplificata)
155 308 : Momenti Torcenti Additional

CARICHI ASTE-----|-----|-----|-----|num.= 200
Nome Asta Dir Tip REF Parametro 1 Parametro 2 Parametro 3 Parametro 4
309 PERM 4 2 Z RD glo -2.000
310 PERM 7 2 Z RD glo -2.000
311 PERM 31 2 Z RD glo -2.000
312 PERM 23 2 Z RD glo -2.000
313 PERM 15 2 Z RD glo -2.000
314 PERM 32 2 Z RD glo -2.000
315 PERM 24 2 Z RD glo -2.000
316 PERM 16 2 Z RD glo -2.000
317 PERM 8 2 Z RD glo -2.000
318 PERM 25 2 Z RD glo -2.000
319 PERM 17 2 Z RD glo -2.000
320 PERM 10 2 Z RD glo -2.000
321 PERM 2 2 Z RD glo -2.000
322 PERM 19 2 Z RD glo -2.000
323 PERM 27 2 Z RD glo -2.000
324 PERM 12 2 Z RD glo -2.000
325 PERM 130 2 Z RD glo -2.000
326 PERM 132 2 Z RD glo -2.000
327 PERM 134 2 Z RD glo -2.000
328 PERM 136 2 Z RD glo -2.000
329 PERM 145 2 Z RD glo -2.000
330 PERM 141 2 Z RD glo -2.000
331 PERM 142 2 Z RD glo -2.000
332 PERM 119 2 Z RD glo -2.000
333 PERM 122 2 Z RD glo -2.000
334 PERM 154 2 Z RD glo -2.000
335 PERM 156 2 Z RD glo -2.000
336 PERM 165 2 Z RD glo -2.000
337 PERM 138 2 Z RD glo -2.000
338 PERM 137 2 Z RD glo -2.000
339 ACC 4 2 Z RD glo -3.500
340 ACC 7 2 Z RD glo -3.500
341 ACC 31 2 Z RD glo -3.500
342 ACC 23 2 Z RD glo -3.500
343 ACC 15 2 Z RD glo -3.500
344 ACC 32 2 Z RD glo -3.500
345 ACC 24 2 Z RD glo -3.500
346 ACC 16 2 Z RD glo -3.500
347 ACC 8 2 Z RD glo -3.500
348 ACC 25 2 Z RD glo -3.500
349 ACC 17 2 Z RD glo -3.500
350 ACC 10 2 Z RD glo -3.500
351 ACC 2 2 Z RD glo -3.500
352 ACC 19 2 Z RD glo -3.500
353 ACC 27 2 Z RD glo -3.500
354 ACC 12 2 Z RD glo -3.500
355 ACC 130 2 Z RD glo -3.500
356 ACC 132 2 Z RD glo -3.500
357 ACC 134 2 Z RD glo -3.500
358 ACC 136 2 Z RD glo -3.500
359 ACC 145 2 Z RD glo -3.500
360 ACC 122 2 Z RD glo -3.500
361 ACC 119 2 Z RD glo -3.500
362 ACC 141 2 Z RD glo -3.500
363 ACC 142 2 Z RD glo -3.500
364 ACC 154 2 Z RD glo -3.500
365 ACC 156 2 Z RD glo -3.500
366 ACC 165 2 Z RD glo -3.500
367 ACC 138 2 Z RD glo -3.500
368 ACC 137 2 Z RD glo -3.500
369 NEVE 4 2 Z RD glo -1.200
370 NEVE 7 2 Z RD glo -1.200
371 NEVE 31 2 Z RD glo -1.200
372 NEVE 23 2 Z RD glo -1.200
373 NEVE 15 2 Z RD glo -1.200
374 NEVE 32 2 Z RD glo -1.200
375 NEVE 24 2 Z RD glo -1.200
376 NEVE 16 2 Z RD glo -1.200
377 NEVE 8 2 Z RD glo -1.200
378 NEVE 25 2 Z RD glo -1.200
379 NEVE 17 2 Z RD glo -1.200
380 NEVE 10 2 Z RD glo -1.200
381 NEVE 2 2 Z RD glo -1.200
382 NEVE 19 2 Z RD glo -1.200
383 NEVE 27 2 Z RD glo -1.200
384 NEVE 12 2 Z RD glo -1.200
385 NEVE 130 2 Z RD glo -1.200
386 NEVE 132 2 Z RD glo -1.200
387 NEVE 134 2 Z RD glo -1.200
388 NEVE 136 2 Z RD glo -1.200
389 NEVE 145 2 Z RD glo -1.200
390 NEVE 141 2 Z RD glo -1.200
391 NEVE 142 2 Z RD glo -1.200
392 NEVE 154 2 Z RD glo -1.200
393 NEVE 156 2 Z RD glo -1.200
394 NEVE 165 2 Z RD glo -1.200
395 NEVE 138 2 Z RD glo -1.200
396 NEVE 137 2 Z RD glo -1.200
397 Vento_Y 137 Y RD glo -1.800
399 Vento_Y 27 Y RD glo -0.400
400 Vento_Y 15 Y RD glo -0.400
401 Vento_Y 10 Y RD glo -0.400
402 Vento_Y 12 Y RD glo -0.400
403 Vento_Y 31 Y RD glo -0.400
404 Vento_Y 32 Y RD glo -0.400

PESTI PROPRIETA' ASTE-----|-----|-----|-----|
Cond. Nome Carichi Asta
1 405-506 2 4 7-8, 10, 12, 15-17, 19, 23-25, 27, 31-36,
38-59, 91-94, 99-102, 104-112, 116-117, 119-128,
130, 132, 134, 136-138, 141-143, 145-149, 154,
156-163, 165-166, 170-176, 178

CARICHI DI LINEA-----|-----|-----|-----|num.= 0
Nome numero coordinata
inizio Fine Cond. Diraz. inizio Fine Descrizione
1 405-506 2 4 7-8, 10, 12, 15-17, 19, 23-25, 27, 31-36,
38-59, 91-94, 99-102, 104-112, 116-117, 119-128,
130, 132, 134, 136-138, 141-143, 145-149, 154,
156-163, 165-166, 170-176, 178

CONDIZIONE DI CARICO-----|-----|-----|-----|num.= 9
Nome
1 Peso proprio N. carichi: 104
Lista carichi: 405-506
2 Permanente N. carichi: 30
Lista carichi: 309-338
3 A:Var_abitazione N. carichi: 30
Lista carichi: 339-368
4 Neve_(c000n_s_m) N. carichi: 28
Lista carichi: 369-396
5 Vento_Y N. carichi: 8
Lista carichi: 397-404
6 Sigma_X N. carichi: 77
Lista carichi: 1-77
7 Sigma_Y N. carichi: 77
Lista carichi: 78-154
8 Torcente_add_X N. carichi: 77
Lista carichi: 155-231
9 Torcente_add_Y N. carichi: 77
Lista carichi: 232-308

RISULTANTI DEI CARICHI (punto di applicazione nell'origine degli assi):
cond. FX FY FZ MX MY MZ
1 0.00000E+00 0.00000E+00 -8.152057E+03 -7.291865E+05 -7.030302E+04 0.000000E+00
2 0.00000E+00 0.00000E+00 -1.348847E+04 -4.915502E+05 9.962286E+05 0.000000E+00
3 0.00000E+00 0.00000E+00 -2.360483E+04 -8.637129E+05 1.744100E+06 0.000000E+00
4 0.00000E+00 0.00000E+00 -7.757084E+02 -2.255701E+05 6.752571E+05 0.000000E+00
5 0.00000E+00 -1.484847E+03 0.00000E+00 8.177556E+05 0.000000E+00 -2.642286E+04
6 2.106702E+03 0.00000E+00 0.00000E+00 0.00000E+00 1.254815E+06 -8.433983E+04
7 0.00000E+00 2.106702E+03 0.00000E+00 -1.254815E+06 0.00000E+00 8.103980E+04
8 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 -1.533155E+02 -3.926788E+04
9 0.00000E+00 0.00000E+00 0.00000E+00 -4.875793E+01 0.000000E+00 2.260460E+04
```


964 -0.2555E-01 -0.2535E-01 0.0000E+00
967 -0.6033E-01 0.1248E-01 0.0000E+00
968 -0.3803E-01 0.2105E-01 0.0000E+00
969 -0.3607E-01 0.1245E-01 0.0000E+00
970 -0.1356E-01 0.1245E-01 0.0000E+00
971 -0.3674E-01 0.1245E-01 0.0000E+00
972 -0.3727E-01 0.1275E-01 0.0000E+00
973 -0.3317E-01 0.1267E-01 0.0000E+00
974 -0.3341E-01 0.1267E-01 0.0000E+00
975 -0.6001E-01 0.1294E-01 0.0000E+00
976 -0.6001E-01 0.2521E-01 0.0000E+00
***** AUTOTETTORE N. 6 periodo: 0.037850
percentuale di massa attivata :
X
0.022 Y
5.710 Z
0.000

NDO SX SZ
2 -0.5689E-01 0.1733E-01 0.0000E+00
3 -0.4158E-01 0.1645E+00 0.0000E+00
4 -0.2639E-01 0.8838E-01 0.0000E+00
11 -0.7856E-02 0.1715E-01 0.0000E+00
12 -0.6520E-02 0.1645E+00 0.0000E+00
13 -0.1307E-01 0.8941E-01 0.0000E+00
14 -0.1587E-01 0.8840E-01 0.0000E+00
19 -0.8528E-03 0.9882E-02 0.0000E+00
20 -0.1133E-02 0.1715E-01 0.0000E+00
21 -0.3830E-02 0.1645E+00 0.0000E+00
23 -0.1307E-01 0.8941E-01 0.0000E+00
28 0.1395E+02 0.9878E-02 0.0000E+00
29 -0.3410E-01 0.1696E-01 0.0000E+00
30 -0.1420E-01 0.1645E+00 0.0000E+00
32 -0.4313E-02 0.8847E-01 0.0000E+00
37 -0.1063E-02 0.9882E-02 0.0000E+00
38 -0.5249E-02 0.1645E+00 0.0000E+00
39 -0.1447E-01 0.8849E-01 0.0000E+00
41 -0.4441E-02 0.1714E-01 0.0000E+00
42 -0.5783E-02 0.1857E-01 0.0000E+00
210 -0.3432E-02 0.8884E-01 0.0000E+00
211 -0.1439E-02 0.8850E-01 0.0000E+00
212 -0.1344E-02 0.8849E-01 0.0000E+00
213 -0.5208E-02 0.8868E-01 0.0000E+00
339 -0.8540E-01 0.1838E-01 0.0000E+00
340 -0.1030E-01 0.1674E-01 0.0000E+00
341 -0.1886E-02 0.1978E-01 0.0000E+00
342 -0.1543E-02 0.1307E-01 0.0000E+00
466 -0.4628E-01 0.1652E+00 0.0000E+00
467 -0.6865E-02 0.1652E+00 0.0000E+00
468 -0.4000E-02 0.1644E+00 0.0000E+00
469 -0.1420E-01 0.1644E+00 0.0000E+00
470 -0.3805E-01 0.1743E-01 0.0000E+00
471 -0.8390E-02 0.1736E-01 0.0000E+00
472 -0.8412E-02 0.1736E-01 0.0000E+00
473 -0.3182E-01 0.1897E-01 0.0000E+00
726 -0.2648E-01 0.8888E-02 0.0000E+00
727 -0.1581E-02 0.8888E-02 0.0000E+00
728 -0.2658E-02 0.8890E-02 0.0000E+00
729 -0.9905E-02 0.8889E-02 0.0000E+00
730 -0.1319E-01 0.3560E-01 0.0000E+00
731 -0.1401E-02 0.3555E-01 0.0000E+00
732 -0.8501E-02 0.3557E-01 0.0000E+00
733 -0.5818E-01 0.3566E-01 0.0000E+00
734 -0.1066E-02 0.1487E-01 0.0000E+00
735 -0.2755E-02 0.1924E+00 0.0000E+00
737 -0.2250E-01 0.1783E+00 0.0000E+00
738 -0.1734E-01 0.1786E+00 0.0000E+00
739 -0.2291E-01 0.1639E+00 0.0000E+00
740 -0.1708E-01 0.8849E-01 0.0000E+00
741 -0.4989E-02 0.1487E-01 0.0000E+00
742 -0.4983E-02 0.9881E-01 0.0000E+00
745 -0.2263E-01 0.1931E+00 0.0000E+00
746 -0.3978E-02 0.1924E+00 0.0000E+00
747 -0.1545E-02 0.1924E+00 0.0000E+00
748 -0.1383E-01 0.1921E+00 0.0000E+00
749 -0.1370E-01 0.1924E+00 0.0000E+00
750 -0.3284E-02 0.1932E+00 0.0000E+00
751 -0.6589E-02 0.1932E+00 0.0000E+00
752 -0.4471E-01 0.1934E+00 0.0000E+00
753 -0.2247E-01 0.1936E+00 0.0000E+00
754 -0.2288E-01 0.1659E+00 0.0000E+00
760 -0.4851E-02 0.1139E+00 0.0000E+00
951 -0.1446E-01 0.1127E-01 0.0000E+00
953 -0.1794E-01 0.8847E-01 0.0000E+00
961 -0.7463E-02 0.1859E-01 0.0000E+00
962 -0.4313E-02 0.1853E-01 0.0000E+00
963 -0.3129E-02 0.1828E-01 0.0000E+00
964 -0.2133E-01 0.1874E-01 0.0000E+00
967 -0.3497E-01 0.1212E+00 0.0000E+00
968 -0.1572E-01 0.1210E+00 0.0000E+00
969 -0.1310E-01 0.1210E+00 0.0000E+00
970 -0.3881E-02 0.1209E+00 0.0000E+00
971 -0.1409E-01 0.1247E+00 0.0000E+00
973 -0.1347E-01 0.1240E+00 0.0000E+00
975 -0.1809E-01 0.1244E+00 0.0000E+00
976 -0.3413E-01 0.1248E+00 0.0000E+00
978 -0.1064E-02 0.3617E-02 0.0000E+00
***** AUTOTETTORE N. 7 periodo: 0.084045
percentuale di massa attivata :
X
3.055 Y
0.636 Z
0.000

NDO SX SZ
2 -0.1406E+00 0.1039E+00 0.0000E+00
3 -0.1101E+00 -0.1122E-01 0.0000E+00
4 -0.6946E-01 0.2834E-02 0.0000E+00
11 -0.5333E-01 0.1036E+00 0.0000E+00
12 -0.8172E-01 -0.1128E-01 0.0000E+00
14 -0.7803E-01 0.2823E-02 0.0000E+00
19 -0.3867E-02 0.4750E-02 0.0000E+00
20 -0.3301E-01 0.1036E+00 0.0000E+00
21 -0.8526E-01 -0.1123E-01 0.0000E+00
23 -0.8241E-01 0.2801E-02 0.0000E+00
24 -0.6977E-02 0.4753E-02 0.0000E+00
29 -0.4667E-01 0.1040E+00 0.0000E+00
30 -0.9501E-01 0.1123E-01 0.0000E+00
32 -0.1044E+00 0.2784E-02 0.0000E+00
37 -0.3605E-02 0.4750E-02 0.0000E+00
38 -0.8202E-01 0.1123E-01 0.0000E+00
39 -0.8705E-01 0.2810E-02 0.0000E+00
41 -0.4534E-01 0.1035E+00 0.0000E+00
42 -0.2262E-01 0.8752E-01 0.0000E+00
210 -0.6255E-01 0.1755E-01 0.0000E+00
211 -0.6259E-01 0.2584E-02 0.0000E+00
212 -0.8605E-01 0.2584E-02 0.0000E+00
213 -0.8608E-01 0.2501E-02 0.0000E+00
339 -0.1372E+00 -0.8002E-01 0.0000E+00
340 -0.1653E-01 0.1048E-01 0.0000E+00
341 -0.5911E-01 0.5084E-01 0.0000E+00
342 -0.4653E+00 -0.9595E-01 0.0000E+00
466 -0.1166E+00 -0.1116E-01 0.0000E+00
467 -0.5165E-01 0.1116E-01 0.0000E+00
468 -0.8240E-01 0.1074E-01 0.0000E+00
469 -0.9576E-01 0.1070E-01 0.0000E+00
470 -0.1410E+00 0.1018E+00 0.0000E+00
471 -0.6765E-01 0.1066E+00 0.0000E+00
472 -0.2344E-01 0.1053E+00 0.0000E+00
473 -0.3620E-01 0.1078E+00 0.0000E+00
726 -0.1380E+00 0.1487E+00 0.0000E+00
727 -0.2664E+00 0.1489E+00 0.0000E+00
728 -0.5541E-01 0.1484E+00 0.0000E+00
729 -0.1004E-01 0.1482E+00 0.0000E+00
730 -0.3677E-01 0.1518E-01 0.0000E+00

731 -0.2555E-01 -0.3093E-01 0.0000E+00
732 -0.6548E-01 0.3089E-01 0.0000E+00
733 -0.2401E-01 0.2105E-01 0.0000E+00
734 -0.3618E-02 -0.7245E-03 0.0000E+00
735 -0.9082E-01 0.1903E-01 0.0000E+00
737 -0.3674E-01 0.1275E-01 0.0000E+00
738 -0.1340E+00 0.3016E-01 0.0000E+00
739 -0.3341E-01 0.1267E-01 0.0000E+00
740 -0.1321E+00 0.2598E-02 0.0000E+00
741 -0.1028E-01 -0.7230E-03 0.0000E+00
742 -0.6033E-01 0.4762E-02 0.0000E+00
745 -0.7766E-01 0.1839E-01 0.0000E+00
746 -0.3048E-01 0.1904E-01 0.0000E+00
747 -0.9122E-01 0.1904E-01 0.0000E+00
748 -0.3971E-01 -0.1878E-01 0.0000E+00
749 -0.9440E-01 0.1872E-01 0.0000E+00
750 -0.8534E-01 0.1878E-01 0.0000E+00
751 -0.3638E-01 0.1873E-01 0.0000E+00
752 -0.1142E+00 -0.1759E-01 0.0000E+00
753 -0.6206E-01 0.1856E-01 0.0000E+00
754 -0.6398E-01 0.1192E-01 0.0000E+00
760 -0.5927E-01 0.3009E-01 0.0000E+00
951 -0.7985E-01 0.2974E-01 0.0000E+00
953 -0.1360E+00 0.3002E-02 0.0000E+00
961 -0.3545E-02 0.8749E-01 0.0000E+00
962 -0.4238E-01 0.8757E-01 0.0000E+00
963 -0.2763E+00 0.8778E-01 0.0000E+00
964 -0.1478E+00 0.8651E-01 0.0000E+00
967 -0.6408E-01 0.2963E-01 0.0000E+00
968 -0.1453E-01 0.2974E-01 0.0000E+00
969 -0.8287E-01 0.2978E-01 0.0000E+00
730 -0.1098E+00 0.3011E-01 0.0000E+00
972 -0.6793E-01 0.3005E-01 0.0000E+00
973 -0.8623E-01 0.3007E-01 0.0000E+00
975 -0.1378E+00 0.3883E-01 0.0000E+00
976 -0.6248E-01 0.2946E-01 0.0000E+00
978 -0.1591E-02 0.1178E-01 0.0000E+00

***** AUTOTETTORE N. 8 periodo: 0.082678
percentuale di massa attivata :
X
0.285 Y
0.558 Z
0.000

NDO SX SZ
2 -0.1213E+00 -0.1157E+00 0.0000E+00
3 -0.2687E-01 0.1186E+00 0.0000E+00
5 -0.8807E-01 0.6407E-01 0.0000E+00
11 -0.1806E-01 0.1153E+00 0.0000E+00
12 -0.1478E-01 0.1186E+00 0.0000E+00
14 -0.1656E-01 0.6409E-01 0.0000E+00
730 -0.1578E-02 0.6216E-02 0.0000E+00
20 -0.6845E-03 0.1159E+00 0.0000E+00
21 -0.8636E-02 0.1184E+00 0.0000E+00
23 -0.1581E-02 0.6411E-01 0.0000E+00
28 -0.3580E-02 0.6213E-02 0.0000E+00
729 -0.1404E+00 0.1164E+00 0.0000E+00
730 -0.1112E+00 0.1186E+00 0.0000E+00
32 -0.6539E-01 0.6403E-01 0.0000E+00
37 -0.5886E-02 0.6223E-02 0.0000E+00
38 -0.1828E-01 0.1186E+00 0.0000E+00
39 -0.3001E-01 0.6405E-01 0.0000E+00
41 -0.8674E-02 0.1158E+00 0.0000E+00
42 -0.1481E-02 0.2543E-01 0.0000E+00
210 -0.8787E-01 0.6477E-01 0.0000E+00
211 -0.1309E-01 0.6444E-01 0.0000E+00
212 -0.5821E-01 0.6442E-01 0.0000E+00
213 -0.6647E-01 0.6481E-01 0.0000E+00
219 -0.1037E-01 0.2028E-01 0.0000E+00
340 -0.8313E-03 0.2175E-01 0.0000E+00
341 -0.8312E-04 0.2214E-01 0.0000E+00
342 -0.7916E-01 0.2218E-01 0.0000E+00
466 -0.1643E+00 0.1215E+00 0.0000E+00
467 -0.5646E-01 0.1215E+00 0.0000E+00
468 -0.9315E-02 0.1182E+00 0.0000E+00
469 -0.1112E+00 0.1181E+00 0.0000E+00
730 -0.1193E+00 0.1144E+00 0.0000E+00
471 -0.2367E-01 0.1185E+00 0.0000E+00
472 -0.3642E-01 0.1196E+00 0.0000E+00
473 -0.1013E+00 0.1225E+00 0.0000E+00
210 -0.6208E-01 0.4187E-01 0.0000E+00
727 -0.5809E-01 0.4193E-01 0.0000E+00
728 -0.7641E-03 0.4177E-01 0.0000E+00
729 -0.5240E-02 0.4171E-01 0.0000E+00
730 -0.1023E+00 0.8286E-02 0.0000E+00
731 -0.7123E-01 0.7123E-02 0.0000E+00
732 -0.2278E-01 0.8278E-02 0.0000E+00
733 -0.1198E+00 0.8275E-02 0.0000E+00
734 -0.3576E-02 0.6371E-02 0.0000E+00
735 -0.2139E-01 0.9918E-01 0.0000E+00
737 -0.1993E+00 0.9886E-01 0.0000E+00
738 -0.1106E+00 0.6242E-01 0.0000E+00
739 -0.4012E+00 0.1178E+00 0.0000E+00
740 -0.1090E+00 0.6423E-01 0.0000E+00
741 -0.3674E-02 0.6394E-02 0.0000E+00
742 -0.5646E-02 0.6238E-02 0.0000E+00
745 -0.1533E+00 -0.9989E-01 0.0000E+00
746 -0.3801E-01 0.9903E-01 0.0000E+00
747 -0.1189E+00 0.9902E-01 0.0000E+00
748 -0.1113E+00 0.9905E-01 0.0000E+00
749 -0.1103E+00 0.9905E-01 0.0000E+00
750 -0.1018E-01 0.9917E-01 0.0000E+00
751 -0.2823E-01 0.9908E-01 0.0000E+00
752 -0.1646E+00 0.9980E-01 0.0000E+00
753 -0.1996E+00 0.9881E-01 0.0000E+00
754 -0.2015E+00 0.1177E+00 0.0000E+00
760 -0.6581E-01 0.6152E-01 0.0000E+00
951 -0.1195E-01 0.6246E-01 0.0000E+00
953 -0.1159E+00 0.6439E-01 0.0000E+00
961 -0.2403E-02 0.2444E-01 0.0000E+00
962 -0.4588E-02 0.2538E-01 0.0000E+00
963 -0.5614E-01 0.2480E-01 0.0000E+00
964 -0.5850E-01 0.1545E-01 0.0000E+00
967 -0.9013E-01 0.6246E-01 0.0000E+00
969 -0.1701E-01 0.6246E-01 0.0000E+00
970 -0.6540E-01 0.6246E-01 0.0000E+00
972 -0.1877E-01 0.6411E-01 0.0000E+00
973 -0.1847E-01 0.6383E-01 0.0000E+00
975 -0.1415E+00 0.6406E-01 0.0000E+00
976 -0.8888E-01 0.6375E-01 0.0000E+00
978 -0.3610E-02 0.6235E-02 0.0000E+00

***** AUTOTETTORE N. 9 periodo: 0.068489
percentuale di massa attivata :
X
1.447 Y
0.058 Z
0.000

NDO SX SZ
2 -0.1484E+00 0.1107E+00 0.0000E+00
3 -0.5164E-01 0.3266E-01 0.0000E+00
5 -0.7625E-01 0.1201E-01 0.0000E+00
11 -0.1395E-01 0.1115E+00 0.0000E+00
12 -0.3013E-01 0.3270E-01 0.0000E+00
14 -0.9566E-01 0.1202E-01 0.0000E+00
19 -0.1214E-01 0.3116E-02 0.0000E+00
20 -0.8295E-01 0.1116E+00 0.0000E+00
21 -0.1302E-01 0.3270E-01 0.0000E+00
22 -0.3338E-01 0.1199E-01 0.0000E+00
28 -0.6198E-02 0.3120E-02 0.0000E+00
29 -0.2714E+00 0.1120E+00 0.0000E+00
30 -0.5849E-01 0.3588E-01 0.0000E+00

32 -0.4156E-01 -0.1199E-01 0.0000E+00
37 -0.1258E-01 0.3116E-02 0.0000E+00
38 -0.2401E-01 0.2105E-01 0.0000E+00
39 -0.3156E-01 0.1199E-01 0.0000E+00
41 -0.2623E-01 0.1115E+00 0.0000E+00
42 -0.2623E-01 0.3178E-01 0.0000E+00
210 -0.2027E-01 0.1106E-01 0.0000E+00
211 -0.3309E-01 0.1154E-01 0.0000E+00
212 -0.3405E-01 0.1182E-01 0.0000E+00
213 -0.4220E-01 0.1145E-01 0.0000E+00
214 -0.1152E+00 0.2894E-01 0.0000E+00
340 -0.1554E-01 0.3900E-01 0.0000E+00
341 -0.3727E-01 0.3834E-01 0.0000E+00
342 -0.1387E+00 0.4654E-01 0.0000E+00
466 -0.3672E+00 0.3685E-01 0.0000E+00
467 -0.9440E-01 0.3683E-01 0.0000E+00
468 -0.2072E-01 0.3177E-01 0.0000E+00
469 -0.3848E-01 0.3172E-01 0.0000E+00
470 -0.1351E+00 0.1022E+00 0.0000E+00
728 -0.1629E-01 0.1134E+00 0.0000E+00
472 -0.4061E-01 0.1172E+00 0.0000E+00
473 -0.2713E-01 0.1205E+00 0.0000E+00
728 -0.1157E+00 0.1675E+00 0.0000E+00
727 -0.1395E+00 0.1673E+00 0.0000E+00
730 -0.3489E-01 0.1664E+00 0.0000E+00
739 -0.1665E-01 0.1665E+00 0.0000E+00
730 -0.2726E+00 0.1782E+00 0.0000E+00
731 -0.4070E-01 0.1772E+00 0.0000E+00
732 -0.1848E-01 0.1770E+00 0.0000E+00
733 -0.1788E-01 0.1788E+00 0.0000E+00
734 -0.1258E-01 0.7492E-02 0.0000E+00
735 -0.3623E-01 0.3008E-01 0.0000E+00
737 -0.1453E+00 0.9135E-01 0.0000E+00
738 -0.1571E-01 0.5533E-02 0.0000E+00
975 -0.1378E+00 0.3883E-01 0.0000E+00
740 -0.1542E-01 0.1186E-01 0.0000E+00
741 -0.1344E-02 0.7495E-02 0.0000E+00
742 -0.2918E-03 0.3115E-02 0.0000E+00
745 -0.9931E-01 0.8861E-01 0.0000E+00
746 -0.4127E-01 0.8806E-01 0.0000E+00
747 -0.3094E-01 0.9101E-01 0.0000E+00
748 -0.4639E-01 0.9106E-01 0.0000E+00
749 -0.4136E-01 0.9129E-01 0.0000E+00
750 -0.2687E-01 0.9106E-01 0.0000E+00
751 -0.3128E-01 0.9000E-01 0.0000E+00
752 -0.4186E-01 0.8817E-01 0.0000E+00
730 -0.1457E+00 0.1140E+00 0.0000E+00
754 -0.1449E+00 0.1361E-01 0.0000E+00
760 -0.4127E+00 0.1516E-02 0.0000E+00
973 -0.3134E-01 0.6215E-02 0.0000E+00
953 -0.1915E-01 0.1184E-01 0.0000E+00
962 -0.3053E-01 0.6222E-02 0.0000E+00
963 -0.3662E-01 0.3725E-01 0.0000E+00
964 -0.1478E+00 0.1164E+00 0.0000E+00
967 -0.1881E-01 0.6270E-02 0.0000E+00
968 -0.2053E-01 0.6272E-02 0.0000E+00
969 -0.3235E-01 0.6186E-02 0.0000E+00
970 -0.3001E-01 0.6274E-02 0.0000E+00
972 -0.3323E-01 0.7728E-02 0.0000E+00
973 -0.3385E-01 0

[illegible][illegible][illegible]

42	-0.005064	-0.01864	0.000407	-0.000028	-0.000063	0.000122
43	0.000000	0.000000	0.000379	0.000004	-0.000017	0.000000
44	0.000000	0.000000	0.000000	0.000000	-0.000002	0.000000
168	0.000000	0.000000	0.000693	-0.000002	-0.000002	0.000000
169	-0.019921	-0.002377	-0.000000	-0.000000	-0.000000	0.000000
211	-0.007110	-0.002233	-0.000549	0.0000719	0.000000	0.000094
212	-0.005632	-0.002123	-0.000552	-0.000000	0.000033	-0.000100
213	-0.00424	-0.00172	-0.000664	-0.000000	-0.000004	0.000000
339	-0.191951	-0.018729	-0.002140	0.000537	-0.000095	-0.000094
340	-0.000000	0.000000	-0.000000	-0.000000	-0.000000	0.000000
341	-0.003787	-0.018174	0.000618	-0.000000	0.000015	-0.000079
342	0.000000	-0.018544	-0.000000	-0.000000	-0.000000	0.000000
466	-0.010319	-0.010158	-0.000401	0.0000761	0.0000184	-0.000536
467	-0.003593	-0.011598	-0.000626	0.0000728	0.000007	-0.000554
468	-0.000000	-0.010485	-0.000000	-0.000000	-0.000002	0.000000
469	-0.00041	-0.000000	0.000397	-0.000002	0.000050	-0.000564
470	-0.003534	-0.00957	-0.000000	-0.000000	-0.000000	0.000000
471	-0.000000	0.000000	0.000126	0.000083	-0.0000049	-0.000147
472	-0.000337	-0.005013	-0.000628	0.0000110	-0.000019	-0.000076
473	-0.000789	-0.004851	-0.000331	-0.000029	-0.000000	-0.000000
474	-0.019966	-0.002347	-0.000003	-0.000002	-0.0000145	-0.000094
475	-0.000000	-0.002536	-0.000000	-0.000000	-0.000000	0.000000
476	-0.003912	-0.003255	-0.000521	-0.0000004	0.0000077	-0.000115
477	-0.000498	-0.002345	-0.000617	-0.000000	-0.000011	-0.000077
730	0.000081	-0.000000	-0.000050	-0.0000064	-0.0000023	-0.000038
731	-0.001448	-0.009619	0.000715	-0.0000009	0.0000000	-0.000576
732	-0.002946	-0.008628	-0.000000	-0.000000	-0.000000	0.000000
733	-0.008639	-0.000000	0.000274	-0.0000001	-0.0000028	-0.000033
734	-0.000089	-0.000733	0.000027	-0.000000	-0.000000	0.000000
735	-0.000734	0.011297	0.000330	-0.0000028	-0.0000125	-0.000057
737	0.010494	-0.011278	0.000589	-0.0000027	0.0000270	-0.000547
738	0.000000	-0.000899	-0.000000	-0.000000	-0.000000	0.000000
739	0.017212	-0.004452	-0.000729	0.0000000	0.0000029	-0.000038
740	0.002251	-0.002243	0.000796	-0.000000	-0.000000	0.000000
741	0.000075	0.000000	0.000546	-0.0000009	0.0000070	-0.000547
742	0.000075	0.000000	-0.000561	-0.000000	-0.000000	0.000000
743	0.000097	-0.011282	-0.000000	-0.0000184	-0.000010	-0.000004
744	-0.002390	0.011297	0.000579	-0.000000	-0.0000024	-0.000561
745	-0.000000	-0.011297	-0.00015	-0.000000	-0.000000	0.000000
746	0.001545	-0.000000	0.000546	-0.0000118	-0.0000021	-0.000559
747	-0.000000	-0.002395	-0.000000	-0.000000	-0.000000	0.000000
750	-0.000046	0.000000	0.000119	0.0000000	0.0000045	-0.000557
751	-0.005152	-0.014421	-0.000579	0.0000728	0.0000089	-0.000572
752	-0.001094	-0.011371	-0.000214	-0.000000	-0.000000	0.000000
753	-0.012975	0.000000	0.000591	-0.0000280	-0.0000025	-0.000557
754	-0.012862					

CONCENTRANTI NOXI		9 Torcento_add_y			
CONCENTRAZIONE		SU_SV_SZ [cm]; RX_RV_RZ [rad]			
UNITA' DI MISURA:					
Coefficiente moltiplicativo:		1.000000			
	ADD		RX	RV	RZ
1	0.000000	0.000000	0.000018	0.000001	0.000000
2	0.004523	0.000000	0.000289	0.000000	0.000000
3	0.005530	0.000000	0.000384	0.000078	0.000029
4	0.001997	0.000000	0.000951	-0.000007	0.000022
5	0.001260	0.000000	0.000946	0.000000	0.000028
6	0.001020	0.000000	0.000632	-0.000085	0.000015
7	0.000948	0.000000	0.000529	0.000002	0.000005
8	0.000943	-0.000016	0.000817	0.000005	0.000009
9	0.000864	0.000000	0.000494	-0.000056	0.000003
10	0.001255	0.000000	0.000021	-0.000056	0.000081
11	0.002347	0.000000	0.000075	0.000000	0.000022
12	0.000181	0.000000	0.000004	0.000000	0.000005
13	-0.000588	0.000000	-0.000004	0.000079	0.000012
14	0.001315	0.000000	0.000075	0.000000	0.000007
15	-0.000930	0.000000	0.000344	0.000000	0.000013
16	0.000000	0.000000	0.000000	0.000000	0.000007
17	0.001593	0.000000	0.000246	-0.000002	0.000031
18	0.000763	0.000000	0.000078	0.000000	0.000004
19	0.000000	0.000000	-0.000313	0.000023	0.000008

870	0.018724	0.506923	-0.001334	0.000059	0.0001851	0.0000805
872	0.039598	0.508402	0.016514	-0.0012831	0.000105	0.0000544
874	0.025258	0.529496	-0.007948	0.000000	0.000000	0.000000
875	0.063676	0.597487	-0.015467	-0.001027	0.000027	0.0000565
876	0.057993	0.592330	-0.007948	0.000000	0.000000	0.000000
878	0.063676	0.514540	-0.000662	-0.0003820	0.0000209	-0.0001303
879	0.000000	0.000000	0.011244	-0.000000	0.000021	0.000000
880	0.000000	0.000000	0.002468	0.000000	0.000023	0.000000
881	0.000000	0.000000	0.0009751	-0.0000578	0.0000104	0.000000
882	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
883	0.000000	0.000000	0.0006132	-0.000000	0.0000265	0.000000
884	0.000000	0.000000	0.004620	-0.000693	0.0000169	0.000000
885	0.000000	0.000000	0.005242	-0.000693	0.0000169	0.000000
886	0.000000	0.000000	0.000318	-0.000693	0.0000221	0.000000
887	0.000000	0.000000	0.000005	-0.000693	0.0000221	0.000000
888	0.000000	0.000000	0.000000	-0.000693	0.0000221	0.000000
889	0.000000	0.000000	-0.005076	-0.000693	0.000020	0.000000
890	0.000000	0.000000	-0.005025	-0.000727	0.000024	0.000000
891	0.000000	0.000000	-0.005042	-0.000727	0.000024	0.000000
892	0.000000	0.000000	-0.000663	-0.001073	0.000017	0.000000
893	0.000000	0.000000	-0.000040	-0.001073	0.000017	0.000000
894	0.000000	0.000000	0.015995	-0.000548	0.0000234	0.000000
895	0.000000	0.000000	0.015993	-0.000514	0.0000220	0.000000
896	0.000000	0.000000	0.016476	-0.000475	0.000021	0.000000
897	0.000000	0.000000	0.012499	-0.000497	0.0000107	0.000000
898	0.000000	0.000000	0.011115	-0.000497	0.0000107	0.000000
899	0.000000	0.000000	0.010262	-0.000566	0.0000082	0.000000
900	0.000000	0.000000	0.008004	-0.000678	0.0000165	0.000000
901	0.000000	0.000000	0.007141	-0.000678	0.0000165	0.000000
902	0.000000	0.000000	0.007479	-0.000719	0.0000106	0.000000
903	0.000000	0.000000	0.000850	-0.000757	0.0000106	0.000000
904	0.000000	0.000000	0.000190	-0.000771	0.0000116	0.000000
905	0.000000	0.000000	0.000096	-0.000767	0.0000136	0.000000
906	0.000000	0.000000	-0.000946	-0.000767	0.0000136	0.000000
907	0.000000	0.000000	-0.003340	-0.000815	0.0000189	0.000000
908	0.000000	0.000000	-0.005746	-0.000815	0.0000189	0.000000
909	0.000000	0.000000	-0.004464	-0.000807	0.0000169	0.000000
910	0.000000	0.000000	-0.007338	-0.000807	0.0000247	0.000000
911	0.000000	0.000000	-0.000829	-0.000807	0.0000247	0.000000
912	0.000000	0.000000	-0.000863	-0.000893	0.0000187	0.000000
913	0.000000	0.000000	-0.000852	-0.000912	0.0000187	0.000000
914	0.000000	0.000000	-0.011564	-0.000946	0.0000255	0.000000
915	0.000000	0.000000	-0.013262	-0.000978	0.0000248	0.000000
916	0.000000	0.000000	-0.010429	-0.000986	0.0000290	0.000000
917	0.000000	0.000000	-0.016			

771	0.000000	0.000000	0.000354	-0.000004	-0.000021	0.000000
772	0.000000	0.000000	0.000496	-0.000002	-0.000018	0.000000
773	0.000000	0.000000	0.000496	-0.000002	-0.000018	0.000000
774	0.000000	0.000000	0.000495	-0.000001	-0.000025	0.000000
775	0.000000	0.000000	0.000495	-0.000001	-0.000025	0.000000
776	0.000000	0.000000	0.000548	0.000001	-0.000024	0.000000
777	0.000000	0.000000	0.000495	-0.000009	-0.000028	0.000000
778	0.000000	0.000000	0.000495	-0.000009	-0.000028	0.000000
779	0.000000	0.000000	0.000413	-0.000000	0.000032	0.000000
780	0.000000	0.000000	0.000413	-0.000000	0.000032	0.000000
781	0.000000	0.000000	0.000493	-0.000000	0.000031	0.000000
782	0.000000	0.000000	0.000560	-0.000010	0.000036	0.000000
783	0.000000	0.000000	0.000385	-0.000000	0.000032	0.000000
784	0.000000	0.000000	0.000289	-0.000003	0.000011	0.000000
785	0.000000	0.000000	0.000278	-0.000000	0.000014	0.000000
786	0.000000	0.000000	0.000243	0.000006	0.000014	0.000000
787	0.000000	0.000000	0.000291	-0.000000	0.000024	0.000000
788	0.000000	0.000000	0.000321	-0.000002	0.000024	0.000000
789	0.000000	0.000000	0.000397	0.000024	0.000034	0.000000
790	0.000000	0.000000	0.000431	0.000000	0.000034	0.000000
791	0.000000	0.000000	0.000590	-0.000004	0.000036	0.000000
792	0.000000	0.000000	0.000417	-0.000026	0.000048	0.000000
793	0.000000	0.000000	0.000247	-0.000000	0.000024	0.000000
794	0.000000	0.000000	-0.000248	-0.000000	0.000002	0.000000
795	0.000000	0.000000	-0.000232	-0.000000	0.000002	0.000000
801	0.000000	0.000000	-0.000257	-0.000002	-0.000002	0.000000
802	0.000000	0.000000	-0.000251	-0.000005	0.000006	0.000000
803	0.000000	0.000000	-0.000265	-0.000000	0.000002	0.000000
804	0.000000	0.000000	-0.000265	-0.000000	-0.000003	0.000000
805	0.000000	0.000000	-0.000261	-0.000000	0.000002	0.000000
806	0.000000	0.000000	-0.000273	-0.000006	0.000000	0.000000
807	0.000000	0.000000	-0.000255	-0.000000	0.000011	0.000000
808	0.000000	0.000000	0.000311	-0.000000	0.000000	0.000000
813	0.000000	0.000000	-0.000697	-0.000018	0.000049	0.000000
814	0.000000	0.000000	-0.000774	-0.000000	0.000000	0.000000
909	0.000000	0.000000	-0.000587	-0.000001	0.000051	0.000000
924	0.000000	0.000000	0.000444	-0.000002	0.000051	0.000000
925	0.000000	0.000000	0.000495	-0.000000	0.000000	0.000000
961	-0.005975	0.020709	0.000335	-0.000011	-0.000089	0.000012
962	0.022576	-0.022323	0.000800	0.000000	0.000000	0.000000
963	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
964	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000031
967	0.000000	0.000000	-0.000273	-0.000007	0.000000	0.000021
968	0.000000	0.000000	0.000369	-0.000000	0.000000	0.000013
969	0.000000	0.000000	-0.000550	-0.000002	0.000053	0.000538
970	0.000000	0.000000	-0.0005			

[illegible]

UNIVERSITÀ NOCI						
INDICAZIONE : 8 Torrence_adi_xv						
UNITÀ DI MISURA: S_V,S_X [cm]; R_V,R_Z [rad]						
Coefficiente moltiplicativo: 1.000000						
	S_V	S_X	R_V	R_Z		
1	0.000000	-0.000000	-0.000000	0.000000	0.000000	0.000000
2	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
3	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
4	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
5	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
6	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
7	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
8	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
9	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
10	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
11	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
12	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
13	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
14	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
15	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
16	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
17	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
18	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
19	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
20	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
21	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
22	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
23	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
24	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
25	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
26	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
27	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
28	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
29	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
30	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
31	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
32	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
33	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
34	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
35	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
36	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
37	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
38	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
39	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
40	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
41	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
42	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
43	-0.000000	-0.000000	0.000000	0.000000	0.000000	0.000000
44	-0.000000	-0.000000	0.000000	0.		

972	-0.007094	0.002783	0.005652	0.0000729	0.0000567	0.0001004
973	-0.005934	0.002769	0.005623	0.0000729	0.0000567	0.0001004
974	0.002748	0.000773	0.005566	0.0000730	0.0000568	0.0001000
975	-0.005969	0.002774	0.005626	0.0000740	0.0000568	0.0001004
976	-0.004990	-0.000861	-0.005698	0.0000740	0.0000568	0.0001004
977	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
978	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
979	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
980	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
981	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
982	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
983	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
984	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
985	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
986	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
987	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
988	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
989	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
990	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
991	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
992	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
993	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
994	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
995	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
996	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
997	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
998	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000
999	0.000000	0.000000	-0.000235	0.0000000	0.0000000	0.0000000

```

771 0.000000 0.000000 -0.000192 -0.000008 0.000012 0.000000
772 0.000000 0.000000 -0.000027 -0.000007 0.000007 0.000000
773 0.000000 0.000000 -0.000027 -0.000007 0.000007 0.000000
774 0.000000 0.000000 -0.000022 -0.000005 0.000014 0.000000
775 0.000000 0.000000 -0.000022 -0.000005 0.000014 0.000000
776 0.000000 0.000000 -0.000020 -0.000005 0.000013 0.000000
777 0.000000 0.000000 -0.000020 -0.000005 0.000013 0.000000
778 0.000000 0.000000 -0.000019 -0.000005 0.000017 0.000000
779 0.000000 0.000000 -0.000019 -0.000005 0.000017 0.000000
780 0.000000 0.000000 -0.000014 -0.000003 -0.000016 0.000000
781 0.000000 0.000000 -0.000014 -0.000003 -0.000016 0.000000
782 0.000000 0.000000 -0.000013 -0.000003 -0.000015 0.000000
783 0.000000 0.000000 -0.000013 -0.000003 -0.000015 0.000000
784 0.000000 0.000000 -0.000013 -0.000003 -0.000015 0.000000
785 0.000000 0.000000 -0.000012 -0.000002 -0.000016 0.000000
786 0.000000 0.000000 -0.000012 -0.000002 -0.000016 0.000000
787 0.000000 0.000000 -0.000011 -0.000001 -0.000010 0.000000
788 0.000000 0.000000 -0.000011 -0.000001 -0.000010 0.000000
789 0.000000 0.000000 -0.000010 -0.000013 -0.000018 0.000000
790 0.000000 0.000000 -0.000010 -0.000013 -0.000018 0.000000
791 0.000000 0.000000 -0.000010 -0.000013 -0.000018 0.000000
792 0.000000 0.000000 -0.000010 -0.000013 -0.000018 0.000000
793 0.000000 0.000000 -0.000010 -0.000013 -0.000018 0.000000
794 0.000000 0.000000 -0.000010 -0.000013 -0.000018 0.000000
795 0.000000 0.000000 -0.000010 -0.000013 -0.000018 0.000000
796 0.000000 0.000000 -0.000012 -0.000014 -0.000016 0.000000
797 0.000000 0.000000 -0.000012 -0.000014 -0.000016 0.000000
798 0.000000 0.000000 -0.000012 -0.000014 -0.000016 0.000000
799 0.000000 0.000000 -0.000012 -0.000014 -0.000016 0.000000
800 0.000000 0.000000 -0.000012 -0.000014 -0.000016 0.000000

```


472	0.050410	-0.032306	-0.149023	-0.027424	0.00191	-0.00219
473	0.067320	-0.005130	-0.680523	-0.003496	-0.00030	-0.00129
474	0.000000	-0.380010	-0.143599	-0.000000	-0.000000	-0.000000
475	0.023106	-0.580652	-0.107761	-0.000000	-0.000000	-0.002329
476	0.029863	-0.580726	-0.000000	-0.000000	-0.000005	-0.000000
477	0.000000	-0.000000	-0.000000	-0.000000	-0.000000	-0.000000
478	-0.040614	-0.808657	-0.947682	-0.000000	-0.000000	-0.000000
479	0.000000	-0.000000	-0.000000	-0.000000	-0.000000	-0.000000
480	0.067122	-0.498085	-0.863450	-0.000000	0.00136	-0.00240
481	0.075021	-0.349818	-0.808739	-0.000000	-0.000000	-0.000000
482	0.004432	-0.349883	-0.813352	-0.000072	0.001514	-0.000000
483	0.000000	-0.219818	-0.349818	-0.000000	-0.000000	-0.000000
484	0.007781	-0.000347	-0.066524	-0.000000	0.000008	-0.000041
485	0.002299	-0.133100	-0.000000	-0.000000	-0.000000	-0.000000
486	0.004111	-0.000000	-0.000000	-0.000000	-0.000000	-0.000000
487	0.004111	-0.000000	-0.000000	-0.000000	-0.000000	-0.000000
488	0.128037	-0.401196	-0.602958	-0.000000	-0.000000	-0.000000
489	0.007075	-0.228310	-0.000000	-0.000000	-0.000000	-0.000000
490	0.000000	-0.502138	-0.000000	-0.000000	0.000002	-0.000004
491	0.000000	-0.000000	-0.000000	-0.000000	-0.000000	-0.000000
492	0.005923	-0.000000	-0.047562	-0.000000	-0.000000	-0.000004
493	0.000000	-0.126296	-0.339910	-0.000000	-0.000000	-0.000000
494	0.000000	-0.000000	-0.133103	-0.048634	-0.000000	-0.000000
495	0.000000	-0.000000	-0.133103	-0.079771	-0.000000	-0.000000
496	0.000000	-0.157060	-0.133103	-0.000000	-0.000000	-0.000000
497	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
498	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
499	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
500	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
501	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
502	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
503	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
504	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
505	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
506	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
507	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
508	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
509	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
510	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
511	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
512	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
513	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
514	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
515	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
516	0.000000	-0.000000	-0.133103	-0.000000	-0.000000	-0.000000
517	0.000000	-0.000000	-0.133103			

[illegible]

17/136

[illegible]

20/136

978	0.005043	-0.001630	-0.071794	0.000002	0.000003	-0.001044
979	0.000000	0.000000	-0.041350	-0.000000	0.000005	0.000000
980	0.000000	0.000000	-0.048584	-0.000000	0.000005	0.000000
981	0.000000	0.000000	-0.048581	-0.000011	0.000011	0.000000
982	0.000000	0.000000	-0.052573	-0.000000	0.000005	0.000000
983	0.000000	0.000000	-0.049484	-0.000000	0.000005	0.000000
984	0.000000	0.000000	-0.058021	-0.000007	0.000004	0.000000
985	0.000000	0.000000	-0.052348	-0.000000	0.000005	0.000000
986	0.000000	0.000000	-0.058984	-0.000000	0.000005	0.000000
987	0.000000	0.000000	-0.050025	-0.000000	0.000005	0.000000
988	0.000000	0.000000	-0.055329	0.000000	0.000004	0.000000
989	0.000000	0.000000	-0.047232	0.000007	0.000005	0.000000
990	0.000000	0.000000	-0.054594	0.000000	0.000005	0.000000
991	0.000000	0.000000	-0.043760	0.000008	0.000004	0.000000
992	0.000000	0.000000	-0.046889	0.000000	0.000005	0.000000
993	0.000000	0.000000	-0.035399	-0.000008	0.000000	0.000000
994	0.000000	0.000000	-0.039196	-0.000007	0.000000	0.000000
995	0.000000	0.000000	-0.036554	-0.000000	0.000005	0.000000
996	0.000000	0.000000	-0.040708	-0.000008	0.000004	0.000000
997	0.000000	0.000000	-0.042405	-0.000000	0.000005	0.000000
998	0.000000	0.000000	-0.044111	-0.000000	0.000005	0.000000
999	0.000000	0.000000	-0.042026	0.000001	0.000000	0.000000
1000	0.000000	0.000000	-0.045449	0.000000	0.000005	0.000000
1001	0.000000	0.000000	-0.034878	0.000005	0.000000	0.000000
1002	0.000000	0.000000	-0.043895	0.000005	0.000000	0.000000
1003	0.000000	0.000000	-0.038005	0.000000	0.000001	0.000000
1004	0.000000	0.000000	-0.041670	0.000000	0.000001	0.000000
1005	0.000000	0.000000	-0.036227	0.000005	0.000001	0.000000
1006	0.000000	0.000000	-0.038297	0.000000	0.000004	0.000000
1007	0.000000	0.000000	-0.034347	0.000003	0.000001	0.000000
1008	0.000000	0.000000	-0.034193	0.000000	0.000000	0.000000
1009	0.000000	0.000000	-0.036420	0.000000	0.000000	0.000000
1010	0.000000	0.000000	-0.039795	0.000002	0.000004	0.000000
1011	0.000000	0.000000	-0.033586	0.000001	0.000000	0.000000
1012	0.000000	0.000000	-0.033381	0.000001	0.000000	0.000000
1013	0.000000	0.000000	-0.033586	0.000000	0.000004	0.000000
1014	0.000000	0.000000	-0.034584	0.000000	0.000000	0.000000
1015	0.000000	0.000000	-0.032590	0.000002	0.000000	0.000000
1016	0.000000	0.000000	-0.034732	0.000002	0.000000	0.000000
1017	0.000000	0.000000	-0.032586	0.000004	0.000000	0.000000
1018	0.000000	0.000000	-0.034194	0.000002	0.000000	0.000000
1019	0.000000	0.000000	-0.032590	0.000000	0.000000	0.000000
1020	0.000000	0.000000	-0.033553	0.000002	0.000004	0.000000
1021	0.000000	0.000000	-0.039795	0.000005	0.000000	0.000000
1022	0.000000	0.000000	-0.040866	0.000000	0.000000	0.000000
1023	0.000000	0.000000	-0.040469	0.000000	0.000004	0.000000
1024	0.000000	0.000000	-0.034163	0.000000	0.000000	0.000000
1025	0.000000	0.000000	-0.033808	0.000000	0.000000	0.000000

POSTAMENTO NODI

UNITA DI CARICO : 30 Nera Vertov

COMBINAZIONE

1	5	CONFEZIONAZIONE ANALISI STATICA																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
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339	-0.218003	-0.465367	-0.597343	0.003201	0.00108	-0.00311
	-0.166493	-0.445348	-0.488593	0.00099	0.00079	-0.00311
340	-0.024869	-0.450683	-0.110101	0.007676	0.00173	-0.00329
	0.004951	-0.112801	-0.122230	-0.003511	0.00178	-0.00511
341	0.004774	-0.226726	-0.114057	-0.003514	0.00176	-0.0047
	0.025039	-0.118146	-0.124005	-0.003601	0.00183	-0.00482
	0.019101	-0.428709	-0.389477	-0.003514	0.00176	-0.0047
	0.243169	-0.133085	-0.500780	0.003513	0.00119	-0.0049
346	-0.078322	-0.352371	-0.515150	0.00078	0.0008	-0.00367
	-0.163092	0.021434	-0.353548	-0.000201	-0.0001	-0.00367
347	-0.005160	-0.323492	-0.102628	-0.00202	-0.00010	-0.00050
	0.012786	-0.021466	-0.080446	0.00530	-0.00009	-0.00018
	-0.000132	-0.338136	-0.091301	-0.00014	-0.00004	-0.00034
	0.012139	0.033864	-0.083433	-0.00351	-0.00009	-0.00025

469	0.0401094	-0.335925	-0.123650	0.00414	0.00072	-0.00047	0.00000	0.00000	0.00000	-0.042183	-0.00012	0.00004	0.00000	1014	0.000000	0.000000	0.000000	-0.030018	0.00007	0.00003	0.00000	790	0.000000	0.000000	0.000000	-0.026170	0.00002	-0.00001	0.00000
470	0.041749	0.039398	-0.148579	-0.05661	0.00090	-0.00014	0.00000	0.00000	0.00000	-0.054178	0.00005	-0.00003	0.00000	1015	0.000000	0.000000	0.000000	-0.048349	-0.00006	0.00006	0.00000	791	0.000000	0.000000	0.000000	-0.026990	0.00000	-0.00001	0.00000
471	0.045221	0.040151	-0.041262	-0.044003	0.00000	-0.044003	0.00000	0.00000	0.00000	-0.043707	0.00000	-0.00000	0.00000	1016	0.000000	0.000000	0.000000	-0.043707	0.00000	0.00000	0.00000	792	0.000000	0.000000	0.000000	-0.026990	0.00000	-0.00001	0.00000
472	-0.040689	-0.130906	-0.113622	0.00741	0.01041	-0.00103	0.00000	0.00000	0.00000	-0.048942	0.00012	0.00000	0.00000	1017	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	793	0.000000	0.000000	0.000000	-0.026786	0.00000	-0.00001	0.00000
473	0.026028	0.000000	-0.040603	-0.040603	0.00000	-0.040603	0.00000	0.00000	0.00000	-0.040603	0.00000	0.00000	0.00000	1018	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	794	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
474	0.025793	-0.009714	-0.059002	0.00115	0.01214	-0.00103	0.00000	0.00000	0.00000	-0.047551	0.00002	0.00000	0.00000	1019	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	795	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
475	0.041206	0.040000	-0.040000	-0.040000	0.00000	-0.040000	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1020	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	796	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
476	0.041576	-0.079464	-0.400122	-0.00672	0.00006	-0.00047	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1021	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	797	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
477	0.277421	0.071762	-0.146627	-0.00007	0.00096	-0.00046	0.00000	0.00000	0.00000	-0.046627	0.00013	0.00002	0.00000	1022	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	798	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
478	0.277999	-0.450030	-0.046512	-0.00003	0.00000	-0.046512	0.00000	0.00000	0.00000	-0.046512	0.00000	0.00000	0.00000	1023	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	799	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
479	0.168452	-0.104857	-0.693546	0.00070	0.01144	-0.00132	0.00000	0.00000	0.00000	-0.046512	0.00000	0.00000	0.00000	1024	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	800	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
480	0.139131	-0.040000	-0.040000	-0.040000	0.00000	-0.040000	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1025	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	801	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
481	0.245170	-0.104765	-0.761935	-0.00021	0.01085	-0.00132	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1026	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	802	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
482	0.040000	-0.040000	-0.040000	-0.040000	0.00000	-0.040000	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1027	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	803	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
483	0.035955	-0.104839	-0.641056	-0.00039	0.01040	-0.00132	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1028	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	804	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
484	-0.025473	-0.671130	-0.649552	0.00000	0.00395	-0.00130	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1029	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	805	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
485	0.026079	-0.104835	-0.655773	0.00000	0.00395	-0.00130	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1030	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	806	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
486	0.215753	-0.292246	-0.903498	-0.00003	0.00079	-0.00135	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1031	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	807	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
487	0.277407	-0.175238	-0.660294	-0.00001	0.00006	-0.00187	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1032	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	808	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
488	0.025870	-0.282170	-0.330121	0.00073	0.00346	-0.00148	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1033	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	809	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
489	0.041723	-0.175399	-0.559576	-0.00004	0.00359	-0.00167	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1034	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	810	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
490	0.043750	-0.282130	-0.547115	-0.00096	0.00359	-0.00167	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1035	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	811	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
491	0.009016	-0.175307	-0.570402	0.00000	0.00354	-0.00154	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1036	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	812	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
492	0.145165	-0.282136	-0.527715	-0.00009	0.00086	-0.00104	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1037	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	813	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
493	-0.104081	-0.175289	-0.626217	-0.00007	0.00095	-0.00122	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1038	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	814	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
494	0.006490	0.008103	-0.092575	-0.00008	0.00007	-0.00023	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1039	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	815	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
495	0.006634	-0.261424	-0.065248	-0.00097	-0.00004	-0.00033	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1040	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	816	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
496	0.009048	0.008459	-0.093111	0.00004	0.00021	0.00023	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1041	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	817	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
497	0.062156	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1042	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	818	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
498	0.026282	0.084188	-0.049801	-0.00002	0.00038	-0.00017	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1043	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	819	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
499	0.026282	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1044	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	820	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
500	0.026282	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1045	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	821	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
501	0.026282	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1046	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000	822	0.000000	0.000000	0.000000	-0.027892	-0.00007	0.00001	0.00000
502	0.026282	-0.163817	-0.031188	0.00001	0.00035	-0.00034	0.00000	0.00000	0.00000	-0.040000	0.00000	0.00000	0.00000	1047	0.000000	0.000000	0.000000	-0.042914	-0.00005	0.00002	0.00000								

466	-0.043855	-0.099033	-0.267709	0.00089	0.00052	-0.00020	1011	0.000000	0.000000	-0.024663	0.00000	-0.00001	0.00000	739	0.048502	-0.000298	-0.035039	0.00033	-0.00006	-0.00015	959	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	959	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
467	-0.001017	-0.099012	-0.062134	0.00000	-0.00007	-0.00021	1012	0.000000	0.000000	-0.025274	0.00000	-0.00001	0.00000	740	0.037215	-0.127890	-0.029433	0.00055	-0.00010	-0.00007	960	0.000000	0.000000	-0.028919	-0.00001	0.00003	-0.00002	960	0.000000	0.000000	-0.028919	-0.00001	0.00003	-0.00002
468	-0.000779	-0.099013	-0.055600	0.00000	-0.00007	-0.00002	1013	0.000000	0.000000	-0.025987	0.00000	-0.00002	0.00000	741	0.001297	-0.000000	-0.025413	0.00000	-0.00000	0.00000	961	0.000000	0.000000	-0.029000	-0.00000	0.00002	-0.00003	961	0.000000	0.000000	-0.029000	-0.00000	0.00002	-0.00003
469	-0.023114	-0.099138	-0.085884	-0.00046	0.00049	-0.00018	1014	0.000000	0.000000	-0.027017	-0.00001	0.00002	0.00000	742	0.047983	-0.153828	-0.026278	0.00016	-0.00000	-0.00015	962	-0.010201	-0.151891	-0.080470	0.00046	-0.00007	-0.00000	962	-0.010201	-0.151891	-0.080470	0.00046	-0.00007	-0.00000
470	-0.002027	-0.025495	-0.349599	0.00019	0.00013	-0.00079	1015	0.000000	0.000000	-0.024703	0.00000	-0.00001	0.00000	743	0.002413	-0.024213	-0.020173	0.00000	-0.00000	0.00000	963	0.000000	0.000000	-0.027017	-0.00001	0.00003	-0.00002	963	0.000000	0.000000	-0.027017	-0.00001	0.00003	-0.00002
471	-0.000057	-0.049476	-0.067003	0.00000	-0.00000	-0.00000	1016	0.000000	0.000000	-0.025244	0.00000	-0.00002	0.00000	744	0.001960	-0.000728	-0.026118	0.00000	-0.00002	-0.00006	964	0.0007958	-0.151902	-0.073738	0.00000	-0.00006	-0.00001	964	0.0007958	-0.151902	-0.073738	0.00000	-0.00006	-0.00001
472	-0.019713	-0.063712	-0.067112	0.00014	0.00083	-0.00009	1017	0.000000	0.000000	-0.024618	0.00000	-0.00001	0.00000	745	0.001144	-0.004040	-0.025231	0.00000	-0.00000	0.00000	965	0.000000	0.000000	-0.025231	-0.00000	0.00004	-0.00000	965	0.000000	0.000000	-0.025231	-0.00000	0.00004	-0.00000
473	-0.129977	-0.000000	-0.000000	-0.00000	-0.00000	-0.00000	1018	0.000000	0.000000	-0.025015	0.00000	-0.00000	0.00000	746	0.001963	-0.001234	-0.030275	0.00001	-0.00002	-0.00012	966	0.012963	-0.152016	-0.265049	-0.00003	-0.00011	-0.00004	966	0.012963	-0.152016	-0.265049	-0.00003	-0.00011	-0.00004
474	-0.119772	-0.236260	-0.478813	0.00077	0.00101	-0.00098	1019	0.000000	0.000000	-0.024048	0.00000	-0.00001	0.00000	747	-0.063030	-0.087139	-0.188902	0.00110	-0.01350	-0.00017	967	-0.137719	-0.040340	-0.287330	-0.00217	-0.00026	-0.00007	967	-0.137719	-0.040340	-0.287330	-0.00217	-0.00026	-0.00007
475	-0.134406	-0.236011	-0.428132	0.00000	0.00106	-0.00008	1020	0.000000	0.000000	-0.024885	0.00001	0.00002	0.00000	748	0.001352	-0.000102	-0.031880	0.00000	-0.00000	0.00000	968	-0.124070	-0.000000	-0.000000	-0.00000	-0.00000	-0.00000	968	-0.124070	-0.000000	-0.000000	-0.00000	-0.00000	-0.00000
476	-0.010565	-0.000000	-0.000000	-0.00000	-0.00000	-0.00000	1021	0.000000	0.000000	-0.023788	0.00000	0.00000	0.00000	749	-0.003952	-0.087469	-0.046412	0.00050	-0.00004	-0.00018	969	-0.114601	-0.040163	-0.324019	0.00242	-0.00006	-0.00004	969	-0.114601	-0.040163	-0.324019	0.00242	-0.00006	-0.00004
477	-0.007701	-0.126202	-0.389948	0.00026	0.00048	-0.00000	1022	0.000000	0.000000	-0.023743	0.00000	0.00000	0.00000	750	0.000611	-0.006137	-0.023743	0.00000	-0.00000	0.00000	970	0.000000	0.000000	-0.023743	-0.00000	0.00000	-0.00000	970	0.000000	0.000000	-0.023743	-0.00000	0.00000	-0.00000
478	-0.130869	-0.000000	-0.000000	-0.00000	-0.00000	-0.00000	1023	0.000000	0.000000	-0.023672	0.00000	-0.00000	0.00000	751	-0.040875	-0.029257	-0.068513	0.00004	-0.00008	-0.00018	971	-0.027007	-0.103525	-0.065612	-0.00000	-0.00002	-0.00016	971	-0.027007	-0.103525	-0.065612	-0.00000	-0.00002	-0.00016
479	-0.013836	-0.140075	-0.340075	0.00014	0.00221	-0.00097	1024	0.000000	0.000000	-0.023552	0.00000	-0.00001	0.00000	752	-0.040875	-0.029257	-0.068513	0.00004	-0.00008	-0.00018	972	-0.003031	-0.236507	-0.048891	0.00017	0.00006	-0.00011	972	-0.003031	-0.236507	-0.048891	0.00017	0.00006	-0.00011
480	-0.005063	-0.440032	-0.346636	0.00000	-0.00000	-0.00000	1025	0.000000	0.000000	-0.023586	-0.00001	-0.00001	0.00000	753	0.006296	-0.000000	-0.023586	0.00000	-0.00000	0.00000	973	-0.000000	0.000000	-0.023586	-0.00000	0.00000	-0.00000	973	-0.000000	0.000000	-0.023586	-0.00000	0.00000	-0.00000
481	-0.029067	-0.140201	-0.452017	0.00074	0.00059	-0.00000	731	0.020282	-0.087575	-0.052797	-0.00011	0.00036	-0.00013	749	0.002822	-0.015907	-0.032719	0.00019	0.00022	0.00004	974	0.000000	0.000000	-0.028901	0.00000	-0.00001	0.00000	974	0.000000	0.000000	-0.028901	0.00000	-0.00001	0.00000
482	-0.002292	-0.001682	-0.031812	0.00007	0.00003	-0.00017	740	0.021250	-0.018415	-0.052622	-0.00007	0.00011	0.00015	750	0.002106	-0.007554	-0.023074	0.00000	0.00000	0.00000	975	-0.020278	-0.235486	-0.153662	0.00006	0.00002	-0.00013	975	-0.020278	-0.235486	-0.153662	0.00006	0.00002	-0.00013
483	-0.000628	-0.025202	-0.039648	0.00000	-0.00000	-0.00000	741	0.002106	-0.007554	-0.023074	0.00000	0.00000	0.00000	751	0.002106	-0.007554	-0.023074	0.00000	0.00000	0.00000	976	-0.016499	-0.103533	-0.133628	0.00000	0.00000	-0.00000	976	-0.016499	-0.103533	-0.133628	0.00000	0.00000	-0.00000
484	-0.035725	-0.025993	-0.038017	0.00028	0.00002	-0.00010	742	0.002694	-0.018800	-0.052648	-0.00143	0.00038	-0.00015	752	0.002694	-0.018800	-0.052648	-0.00143	0.00038	-0.00015	977	-0.002690	-0.235496	-0.049857	0.00043	-0.00008	-0.00015	977	-0.002690	-0.235496	-0.049857	0.00043	-0.00008	-0.00015
485	-0.046641	-0.167912	-0.031004	0.00009	-0.00008	-0.00000	743	0.000000	-0.000000	-0.023715	-0.00006	0.00006	0.00000	753	0.000000	-0.000000	-0.023715	-0.00006	0.00006	0.00000	978	-0.016517	-0.194557	-0.138654	0.00009	0.00001	-0.00014	978	-0.016517	-0.194557	-0.138654	0.00009	0.00001	-0.00014
486	-0.037291	-0.091051	-0.032244	0.00046	-0.00009	-0.00010	744	0.002921	-0.013058	-0.037214	-0.00049	0.00054	-0.00014	754	0.002921	-0.013058	-0.037214	-0.00049	0.00054	-0.00014	979	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	979	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
487	-0.043712	-0.101936	-0.033437	0.00021	0.00009	-0.00015	745	0.002921	-0.013058	-0.037214	-0.00049	0.00054	-0.00014	755	0.002921	-0.013058	-0.037214	-0.00049	0.00054	-0.00014	980	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	980	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
488	-0.011551	-0.001685	-0.026146	0.00002	0.00000	-0.00010	746	0.002154	-0.008083	-0.027764	0.00000	-0.00010	-0.00010	756	0.002154	-0.008083	-0.027764	0.00000	-0.00010	-0.00010	981	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	981	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
489	-0.012205	-0.025286	-0.135891	0.00000	-0.00137	-0.00016	747	0.002205	-0.025286	-0.135891	0.00000	-0.00137	-0.00016	757	0.002205	-0.025286	-0.135891	0.00000	-0.00137	-0.00016	982	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	982	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
490	-0.002282	-0.025219	-0.043888	0.00041	0.00035	-0.00016	748	0.002282	-0.025219	-0.043888	0.00041	0.00035	-0.00016	758	0.002282	-0.025219	-0.043888	0.00041	0.00035	-0.00016	983	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	983	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
491	-0.001028	-0.025219	-0.037883	0.00021	0.00024	-0.00017	749	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0.00017	759	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0.00017	984	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	984	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
492	-0.001028	-0.025219	-0.037883	0.00021	0.00024	-0.00017	750	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0.00017	760	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0.00017	985	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	985	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
493	-0.001028	-0.025219	-0.037883	0.00021	0.00024	-0.00017	751	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0.00017	761	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0.00017	986	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	986	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
494	-0.001028	-0.025219	-0.037883	0.00021	0.00024	-0.00017	752	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0.00017	762	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0.00017	987	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007	987	0.000000	0.000000	-0.024844	0.00002	0.00002	-0.00007
495	-0.001028	-0.025219	-0.037883	0.00021	0.00024	-0.00017	753	0.002282	-0.025219	-0.037883	0.00021	0.00024	-0																					

3 A*var_abitazione___ + 0.30

1) +1.00*c001 +1.00*c002 +0.30*c009

unità di misura: SX,SY,SZ [m]; RX,RY,RZ [rad]

Coefficiente moltiplicativo: 1.000000

Nodo SX SY SZ RX RY RZ

1	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
2	-0.076082	-0.008318	-0.271164	0.00215	0.00068	-0.00054
3	+0.022667	-0.069882	-0.209514	0.00241	-0.00041	-0.00028
4	+0.024724	-0.153106	-0.266570	0.00062	0.00000	-0.00011
11	+0.000920	-0.008350	-0.053227	0.00042	-0.00008	-0.00008
12	-0.001715	-0.069939	-0.049502	0.00007	0.00004	0.00004
14	-0.000682	-0.155223	-0.054580	0.00030	-0.00007	-0.00011
19	0.001365	-0.000400	-0.031554	0.00000	0.00005	0.00000
20	0.013904	-0.008346	-0.050638	-0.00014	0.00020	-0.00071
21	0.000779	-0.069938	-0.044378	0.00017	-0.00040	-0.00013
23	0.001531	-0.155236	-0.090114	0.00019	0.00001	-0.00011
28	0.001096	-0.000448	-0.022884	0.00000	0.00001	-0.00024
29	0.144657	-0.008257	-0.232557	-0.00078	0.00068	-0.00080
30	0.016744	-0.069929	-0.068717	-0.00007	0.00006	-0.00010
32	0.026244	-0.155279	-0.042386	0.00006	0.00006	-0.00011
37	0.001387	-0.000446	-0.072881	0.00000	0.00001	0.00000
38	0.000421	-0.069935	-0.043090	0.00034	-0.00001	-0.00013
39	0.000451	-0.155246	-0.090253	0.00004	0.00000	-0.00011
40	0.000000	0.000000	-0.037398	0.00000	0.00004	-0.00070
41	0.006812	-0.008352	-0.048384	0.00013	0.00003	-0.00070
42	0.000684	-0.072508	-0.057857	-0.00018	-0.00004	-0.00071
107	0.000000	0.000000	-0.039863	0.00000	0.00003	0.00000
109	0.000000	0.000000	-0.032544	-0.00007	0.00004	0.00000
168	0.000000	0.000000	-0.033827	0.00006	0.00004	0.00000
210	-0.043499	-0.157813	-0.126593	0.00073	0.00032	-0.00012
211	-0.001026	-0.155648	-0.054641	0.00078	-0.00008	-0.00012
212	0.001613	-0.155640	-0.049180	0.00000	-0.00052	-0.00011
213	0.016529	-0.156678	-0.042421	0.00000	-0.00064	-0.00012
339	-0.093625	-0.082711	-0.262786	0.00139	0.00048	-0.00062
340	-0.096659	-0.074739	-0.062123	0.00000	-0.00000	-0.00000
341	0.007586	-0.072110	-0.059562	-0.00000	0.00090	-0.00069
342	0.104123	-0.068388	-0.217753	-0.00216	0.00052	-0.00074
466	-0.024714	-0.076029	-0.209582	0.00069	0.00000	0.00015
467	0.000115	-0.075993	-0.049634	0.00077	-0.00007	-0.00016
468	0.001325	-0.069115	-0.044647	0.00007	0.00013	0.00000
469	0.017053	-0.069081	-0.068782	-0.00036	0.00037	-0.00014
470	-0.027674	-0.039060	-0.271254	0.00012	-0.00012	0.00000
471	-0.002507	-0.094063	-0.053520	0.00133	0.00074	-0.00062
472	0.0214967	-0.007333	-0.050750	-0.00090	0.00066	-0.00062
473	0.117858	0.000666	-0.233541	0.00113	0.00104	0.00071
726	-0.093629	-0.178862	-0.178011	0.00060	0.00081	-0.00065
727	-0.104123	-0.178967	-0.180905	0.00000	0.00000	-0.00007
728	-0.007489	-0.178950	-0.313242	0.00008	0.00136	-0.00072
729	-0.006759	-0.178964	-0.310622	0.00020	0.00196	-0.00071
730	-0.117852	-0.110336	-0.290413	-0.00025	0.00050	-0.00078
731	-0.015040	-0.110335	-0.271795	0.00011	0.00175	-0.00077
732	-0.000106	-0.110303	-0.275127	0.00000	0.00022	-0.00000
733	-0.072697	-0.110295	-0.335911	0.00057	0.00049	-0.00054
734	0.001380	-0.000923	-0.026913	0.00001	0.00002	-0.00013
745	-0.001194	-0.040463	-0.033279	-0.00024	-0.00001	-0.00013
737	0.026595	-0.040514	-0.027267	0.00022	0.00016	-0.00007
738	0.032254	-0.139358	-0.029143	0.00000	0.00031	-0.00000
739	0.027808	-0.069798	-0.027286	0.00036	-0.00008	-0.00007
740	0.021540	-0.155581	-0.028275	0.00016	0.00006	-0.00011
741	0.000817	-0.000625	-0.023618	0.00001	0.00001	-0.00007
742	0.000820	-0.000447	-0.023637	0.00001	0.00001	-0.00007
745	-0.018521	-0.040109	-0.127760	0.00078	-0.00286	-0.00012
746	-0.002466	-0.040461	-0.036671	0.00032	0.00027	-0.00013
747	0.000081	-0.040461	-0.031938	0.00016	-0.00019	-0.00013
748	0.015578	-0.040518	-0.044395	-0.00008	0.00018	-0.00010
749	0.016494	-0.040158	-0.044416	-0.00036	0.00028	-0.00012
750	-0.000895	-0.041283	-0.033864	-0.00021	0.00042	-0.00011
751	-0.000981	-0.042060	-0.036696	0.00077	0.00042	-0.00014
752	-0.033362	-0.040451	-0.127783	0.00049	0.00067	-0.00013
753	0.027423	-0.041615	-0.027307	0.00022	0.00017	-0.00010
754	0.027396	-0.071555	-0.027319	0.00035	-0.00009	-0.00009
760	0.016488	-0.129402	-0.054833	0.00001	0.00053	-0.00012
761	0.000000	0.000000	-0.028804	-0.00007	0.00005	0.00000
762	0.000000	0.000000	-0.038814	-0.00007	0.00005	0.00000
763	0.000000	0.000000	-0.034165	-0.00007	0.00004	0.00000
764	0.000000	0.000000	-0.032300	-0.00007	0.00005	0.00000
765	0.000000	0.000000	-0.035818	-0.00007	0.00004	0.00000
766	0.000000	0.000000	-0.037158	-0.00005	0.00004	0.00000
767	0.000000	0.000000	-0.035111	-0.00006	0.00005	0.00000
768	0.000000	0.000000	-0.038586	-0.00005	0.00004	0.00000
769	0.000000	0.000000	-0.038641	-0.00005	0.00004	0.00000
770	0.000000	0.000000	-0.037564	0.00004	0.00004	0.00000
771	0.000000	0.000000	-0.039598	0.00005	0.00005	0.00000
772	0.000000	0.000000	-0.038958	0.00004	0.00004	0.00000
773	0.000000	0.000000	-0.039041	0.00006	0.00004	0.00000
774	0.000000	0.000000	-0.032773	0.00006	0.00005	0.00000
775	0.000000	0.000000	-0.036618	0.00006	0.00004	0.00000
776	0.000000	0.000000	-0.032022	0.00006	0.00004	0.00000
777	0.000000	0.000000	-0.039458	0.00006	0.00005	0.00000
778	0.000000	0.000000	-0.020659	-0.00005	-0.00002	0.00000
779	0.000000	0.000000	-0.030462	-0.00005	-0.00002	0.00000
780	0.000000	0.000000	-0.022993	-0.00005	-0.00002	0.00000
781	0.000000	0.000000	-0.023205	-0.00005	-0.00002	0.00000
782	0.000000	0.000000	-0.025264	-0.00004	-0.00002	0.00000
783	0.000000	0.000000	-0.025485	-0.00004	-0.00002	0.00000
784	0.000000	0.000000	-0.026467	0.00000	-0.00001	0.00000
785	0.000000	0.000000	-0.025370	0.00003	-0.00002	0.00000
786	0.000000	0.000000	-0.025545	0.00003	-0.00002	0.00000
787	0.000000	0.000000	-0.023779	0.00003	-0.00001	0.00000
788	0.000000	0.000000	-0.023622	0.00003	-0.00001	0.00000
789	0.000000	0.000000	-0.022615	0.00002	-0.00001	0.00000
790	0.000000	0.000000	-0.022737	0.00002	-0.00001	0.00000
791	0.000000	0.000000	-0.023176	0.00000	-0.00001	0.00000
795	0.000000	0.000000	-0.023176	0.00000	-0.00001	0.00000
797	0.000000	0.000000	-0.023252	0.00000	-0.00001	0.00000
798	0.000000	0.000000	-0.019549	-0.00006	0.00000	0.00000
799	0.000000	0.000000	-0.023136	-0.00006	0.00000	0.00000
800	0.000000	0.000000	-0.022225	-0.00006	0.00001	0.00000
801	0.000000	0.000000	-0.034897	-0.00005	0.00000	0.00000
802	0.000000	0.000000	-0.024885	-0.00005	0.00001	0.00000
803	0.000000	0.000000	-0.026960	-0.00001	-0.00001	0.00000
804	0.000000	0.000000	-0.025599	-0.00003	0.00000	0.00000
805	0.000000	0.000000	-0.025521	0.00003	0.00001	0.00000
806	0.000000	0.000000	-0.024003	0.00003	0.00000	0.00000
807	0.000000	0.000000	-0.023918	0.00003	0.00001	0.00000
808	0.000000	0.000000	-0.022568	0.00002	0.00000	0.00000
813	0.000000	0.000000	-0.023703	-0.00001	0.00001	0.00000
814	0.000000	0.000000	-0.023716	0.00000	0.00002	0.00000
909	0.000000	0.000000	-0.023269	0.00000	0.00002	0.00000
924	0.000000	0.000000	-0.023224	0.00000	-0.00001	0.00000
943	0.000000	0.000000	-0.023159	0.00000	-0.00001	0.00000
951	0.000399	-0.130367	-0.036578	0.00022	0.00001	-0.00011
953	0.021863	-0.155746	-0.028322	-0.00073	-0.00059	-0.00010
954	0.000000	0.000000	-0.026534	0.00000	0.00001	0.00000
957	0.000000	0.000000	-0.022797	0.00001	0.00001	-0.00024
958	0.000000	0.000000	-0.026130	0.00000	-0.00001	-0.00013
959	0.000000	0.000000	-0.023271	0.00000	0.00001	-0.00007
960	0.000000	0.000000	-0.023271	0.00000	-0.00001	-0.00007
961	-0.006365	-0.077536	-0.063101	0.00044	0.00006	-0.00070
962	-0.007784	-0.027513	-0.059456	-0.00008	-0.00004	-0.00071
963	-0.103398	-0.025738	-0.115722	-0.00164	0.00014	-0.00075
964	-0.094350	-0.077481	-0.262708	0.00035	0.00014	-0.00066
965	0.000000	0.000000	-0.023198	0.00000	0.00002	0.00000
966	0.000000	0.000000	-0.023107	0.00000	-0.00001	0.00000
967	-0.014440	-0.130358	-0.116973	0.00071	0.00003	-0.00010
968	-0.000744	-0.133367	-0.038672	0.00029	-0.00003	-0.00011

969	0.001543	-0.130367	-0.035659	0.00013	0.00001	-0.00011
970	0.016514	-0.130367	-0.054801	-0.00009	-0.00001	-0.00011
972	-0.000028	-0.131812	-0.039684	0.00078	0.00004	-0.00010
973	0.001603	-0.131026	-0.035691	0.00000	0.00004	-0.00011
975	0.013911	-0.131916	-0.029175	-0.00073	0.00008	-0.00010
976	-0.014395	-0.133886	-0.116993	0.00073	0.00021	-0.00010
978	0.001396	0.000162	-0.038664	0.00000	0.00000	-0.00070
979	0.000000	0.000000	-0.020449	-0.00006	0.00002	0.00000
980	0.000000	0.000000	-0.023024	-0.00005	0.00002	0.00000
981	0.000000	0.000000	-0.025886	-0.00006	0.00002	0.00000
982	0.000000	0.000000	-0.026854	-0.00006	0.00002	0.00000
983	0.000000	0.000000	-0.025106	-0.00003	0.00002	0.00000
984	0.000000	0.000000	-0.025066	-0.00004	0.00007	0.00000
985	0.000000	0.000000	-0.026151	-0.00001	0.00002	0.00000
986	0.000000	0.000000	-0.024932	-0.00001	0.00007	0.00000
987	0.000000	0.000000	-0.025873	0.00002	0.00000	0.00000
988	0.000000	0.000000	-0.026887	0.00003	0.00007	0.00000
989	0.000000	0.000000	-0.024696	0.00003	0.00002	0.00000
990	0.000000	0.000000	-0.028154	0.00004	0.00006	0.00000
991	0.000000	0.000000	-0.023180	-0.00003	-0.00001	0.00000
992	0.000000	0.000000	-0.026022	0.00005	0.00005	0.00000
993	0.000000	0.000000	-0.019149	-0.00005	-0.00001	0.00000
994	0.000000	0.000000	-0.021257	-0.00005	-0.00001	0.00000
995	0.000000	0.000000	-0.018984	-0.00005	-0.00001	0.00000
996	0.000000	0.000000	-0.021430	-0.00005	0.00002	0.00000
997	0.000000	0.000000	-0.023484	-0.00003	-0.00002	0.00000
998	0.000000	0.000000	-0.023536	-0.00004	0.00001	0.00000
999	0.000000	0.000000	-0.024371	0.00000	-0.00001	0.00000
1000	0.000000	0.000000	-0.024540	-0.00001	0.00002	0.00000
1001	0.000000	0.000000	-0.023809	0.00002	-0.00001	0.00000
1002	0.000000	0.000000	-0.024098	0.00002	-0.00001	0.00000
1003	0.000000	0.000000	-0.022746	0.00002	-0.00001	0.00000
1004	0.000000	0.000000	-0.022914	0.00003	0.00001	0.00000
1005	0.000000	0.000000	-0.022743	0.00002	-0.00001	0.00000
1006	0.000000	0.000000	-0.021881	0.00002	0.00001	0.00000
1007	0.000000	0.000000	-0.021151	0.00000	-0.00001	0.00000
1008	0.000000	0.000000	-0.022313	0.00000	-0.00001	0.00000
1009	0.000000	0.000000	-0.021415	0.00000	0.00001	0.00000
1010	0.000000	0.000000	-0.022448	0.00000	0.00001	0.00000
1011	0.000000	0.000000	-0.021475	-0.00001	-0.00001	0.00000
1012	0.000000	0.000000	-0.022782	-0.00002	-0.00001	0.00000
1013	0.000000	0.000000	-0.021478	0.00000	0.00000	0.00000
1014	0.000000	0.000000	-0.022727	-0.00001	0.00001	0.00000
1015	0.000000	0.000000	-0.021727	-0.00003	0.00000	0.00000
1016	0.000000	0.000000	-0.021701	0.00000	0.00001	0.00000
1017	0.000000	0.000000	-0.021885	0.00000	-0.00001	0.00000
1018	0.000000	0.000000	-0.021768	0.00000	0.00000	0.00000
1019	0.000000	0.000000	-0.021788	0.00000	-0.00001	0.00000
1020	0.000000	0.000000	-0.021764	0.00000	0.00000	0.00000
1021	0.000000	0.000000	-0.021762	0.00000	0.00002	0.00000
1022	0.000000	0.000000	-0.021737	0.00001	0.00001	0.00000
1023	0.000000	0.000000	-0.021173	-0.00001	0.00000	0.00000
1024	0.000000	0.000000	-0.022442	0.00000	-0.00001	0.00000
1025	0.000000	0.000000	-0.020929	-0.00001	-0.00001	0.00000

REAZIONI VINCOLARI:

REAZIONI VINCOLARI									
CONDIZIONE : 1 Peso proprio									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	321.4	-68.7	0.0	0.0	0.0	0.0			
954	54.7	-48.5	0.0	0.0	0.0	0.0			
957	18.8	-29.8	0.0	0.0	0.0	0.0			
958	-284.8	-48.2	0.0	0.0	0.0	0.0			
959	126.9	111.0	0.0	0.0	0.0	0.0			
960	-237.0	84.2	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 2 Permanente									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	372.1	56.5	0.0	0.0	0.0	0.0			
954	-53.5	58.8	0.0	0.0	0.0	0.0			
957	-22.0	-149.5	0.0	0.0	0.0	0.0			
958	-274.6	75.9	0.0	0.0	0.0	0.0			
959	124.7	-77.3	0.0	0.0	0.0	0.0			
960	-146.7	35.6	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 3 A:var_abitazione									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	651.2	98.9	0.0	0.0	0.0	0.0			
954	-93.6	102.9	0.0	0.0	0.0	0.0			
957	-38.5	-261.7	0.0	0.0	0.0	0.0			
958	-480.6	132.8	0.0	0.0	0.0	0.0			
959	218.2	-135.3	0.0	0.0	0.0	0.0			
960	-256.8	62.3	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 4 Neve (<1000m_slm)									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	177.8	57.2	0.0	0.0	0.0	0.0			
954	-59.4	49.4	0.0	0.0	0.0	0.0			
957	-24.3	-79.4	0.0	0.0	0.0	0.0			
958	-151.1	36.7	0.0	0.0	0.0	0.0			
959	87.7	-44.8	0.0	0.0	0.0	0.0			
960	-30.7	-19.2	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 5 Vento_Y									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	16.1	308.2	0.0	0.0	0.0	0.0			
954	-0.1	380.8	0.0	0.0	0.0	0.0			
957	12.6	708.7	0.0	0.0	0.0	0.0			
958	-40.3	274.7	0.0	0.0	0.0	0.0			
959	-80.6	-142.3	0.0	0.0	0.0	0.0			
960	112.3	-47.2	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 6 Sisma_X									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	-162.0	-168.9	0.0	0.0	0.0	0.0			
954	-696.9	-114.5	0.0	0.0	0.0	0.0			
957	-539.4	264.4	0.0	0.0	0.0	0.0			
958	-558.2	-82.3	0.0	0.0	0.0	0.0			
959	-96.9	131.1	0.0	0.0	0.0	0.0			
960	-53.2	-29.7	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 7 Sisma_Y									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	13.1	-512.3	0.0	0.0	0.0	0.0			
954	-22.0	-560.5	0.0	0.0	0.0	0.0			
957	3.1	-1028.8	1.0	0.0	0.0	0.0			
958	-47.5	-365.2	0.0	0.0	0.0	0.0			
959	138.3	239.5	0.0	0.0	0.0	0.0			
960	-180.1	120.6	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 8 Torcente_add_X									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	-31.2	52.1	0.0	0.0	0.0	0.0			
954	21.0	0.0	0.0	0.0	0.0	0.0			
957	-22.3	11.0	0.0	0.0	0.0	0.0			
958	-42.3	-49.5	0.0	0.0	0.0	0.0			
959	-12.2	16.5	0.0	0.0	0.0	0.0			
960	2.3	-36.1	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CONDIZIONE : 9 Torcente_add_Y									
Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	14.9	-29.4	0.0	0.0	0.0	0.0			
954	-13.2	1.2	0.0	0.0	0.0	0.0			
957	31.2	-6.0	0.0	0.0	0.0	0.0			
958	-23.4	23.3	0.0	0.0	0.0	0.0			
959	8.6	-8.0	0.0	0.0	0.0	0.0			
960	0.9	18.9	0.0	0.0	0.0	0.0			

REAZIONI VINCOLARI									
CASO DI CARICO : 1 SLU									
COMBINAZIONE									
N. 4 CONDIZIONE ANALISI STATICA									
1) 1.00*0000 + 1.30									
2) 1.00*0000 + 1.50									
3) 1.00*0000 + 1.50									
4) 1.00*0000 + 1.50									

Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]									
Coefficiente moltiplicativo: 1.000000									
Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	2219.4	229.7	0.0	0.0	0.0	0.0			
954	Sx	Sy	Sz	Rx	Ry	Rz			

Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
957	-102.9	-774.7	0.0	0.0	0.0	0.0			
958	-1729.6	305.4	0.0	0.0	0.0	0.0			
959	-811.0	-241.8	0.0	0.0	0.0	0.0			
960	-959.5	227.6	0.0	0.0	0.0	0.0			

CASO DI CARICO : 2 SLU VENTOX

COMBINAZIONE

N. 4 CONDIZIONE ANALISI STATICA									
1) 1.00*0000 + 1.30									
2) 1.00*0000 + 1.50									
3) 1.00*0000 + 1.50									
4) 1.00*0000 + 1.50									

Unità di misura: Sx,Sy,Sz [daN];Rx,Ry,Rz [daNcm]

Coefficiente moltiplicativo: 1.000000

Nodo	Sx	Sy	Sz	Rx	Ry	Rz			
40	2219.4	229.7	0.0	0.0	0.0	0.0			
954	Sx	Sy	Sz	Rx	Ry	Rz			
957	-238.5	253.7	0.0	0.0	0.0	0.0			
958	-102.9	-774.7	0.0	0.0	0.0	0.0			
959	-1729.6	305.4	0.0	0.0	0.0	0.0			
960	-811.0	-241.8	0.0	0.0	0.0	0.0			
960	-959.5	227.6	0.0	0.0	0.0	0.0			

CASO DI CARICO : 3 SLU VENTOX

COMBINAZIONE

N. 5 CONDIZIONE ANALISI STATICA			
1	Pesq_proprio_____ +	1.30	
2	Permanente_____ +	1.50	
3	A:var_abitazione_____ +	1.50	
4	Neve (<1000m_slm)_____ +	1.50	

Nodo	959	SX	SY	SZ	RX	RY	RZ
		378.3	-42.9	0.0	0.0	0.0	0.0
Nodo	960	SX	SY	SZ	RX	RY	RZ
		-518.3	147.1	0.0	0.0	0.0	0.0

REAZIONI VINCOLARI

CASO DI CARICO : 13 Frequente Vento

COMBINAZIONE

N. 5 CONDIZIONI ANALISI STATICA

- 1 Peso_proprio_____+ 1.00
- 2 Permanente_____+ 1.00
- 3 A'Var_abitazione_____+ 0.50
- 4 NiveL_c(1000n_sln)_____+ 0.20
- 5 Vento_y_____+ 0.20

- 1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004 +0.20*c005
- 2) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004 -0.20*c005

Unità di misura: SX,SY,SZ [dm];RX,RY,RZ [dm/cm]

Coefficiente moltiplicativo:		1.000000					
Nodo	40	SX	SY	SZ	RX	RY	RZ
		1057.9	110.4	0.0	0.0	0.0	0.0
		1051.4	-12.9	0.0	0.0	0.0	0.0
Nodo	954	SX	SY	SZ	RX	RY	RZ
		-57.4	148.2	0.0	0.0	0.0	0.0
		-57.4	-4.9	0.0	0.0	0.0	0.0
Nodo	957	SX	SY	SZ	RX	RY	RZ
		-24.9	-184.3	0.0	0.0	0.0	0.0
		-29.9	-467.8	0.0	0.0	0.0	0.0
Nodo	958	SX	SY	SZ	RX	RY	RZ
		-842.0	156.3	0.0	0.0	0.0	0.0
		-817.8	46.5	0.0	0.0	0.0	0.0
Nodo	959	SX	SY	SZ	RX	RY	RZ
		362.2	-71.4	0.0	0.0	0.0	0.0
		394.4	-14.5	0.0	0.0	0.0	0.0
Nodo	960	SX	SY	SZ	RX	RY	RZ
		-495.8	137.7	0.0	0.0	0.0	0.0
		-540.7	156.6	0.0	0.0	0.0	0.0

REAZIONI VINCOLARI

CASO DI CARICO : 14 Quasi Perm

COMBINAZIONE

N. 3 CONDIZIONI ANALISI STATICA

- 1 Peso_proprio_____+ 1.00
- 2 Permanente_____+ 1.00
- 3 A'Var_abitazione_____+ 0.30

- 1) +1.00*c001 +1.00*c002 +0.30*c003

Unità di misura: SX,SY,SZ [dm];RX,RY,RZ [dm/cm]

Coefficiente moltiplicativo:		1.000000					
Nodo	40	SX	SY	SZ	RX	RY	RZ
		888.8	17.5	0.0	0.0	0.0	0.0
		-26.8	41.2	0.0	0.0	0.0	0.0
Nodo	954	SX	SY	SZ	RX	RY	RZ
		-14.8	-257.8	0.0	0.0	0.0	0.0
		-703.6	67.5	0.0	0.0	0.0	0.0
Nodo	958	SX	SY	SZ	RX	RY	RZ
		317.1	-6.9	0.0	0.0	0.0	0.0
		-460.8	138.5	0.0	0.0	0.0	0.0

66.	-76.0	0.0	0.0	0.0	0.0	0.0	4.	-3901.7	-18.5	-4.8	0.0	-3.0	11.6	18.	329.8	-619.6	28.1	84.0	2758.0	10524.0	173.	-347.6	828.5	-0.5	0.0	94.8	-10852.1							
99.	-76.0	0.0	0.0	0.0	0.0	0.0	5.	-3901.5	-18.5	-4.8	0.0	0.0	0.0	35.	329.8	-805.2	28.1	84.0	2765.5	9395.4	201.	-347.6	1125.7	-0.5	0.0	110.6	17240.2							
132.	-76.0	0.0	0.0	0.0	0.0	0.0	PROGR.	3901.0	0.0	0.0	0.0	0.0	0.0	PROGR.	329.8	-961.0	28.1	84.0	2772.0	7541.2	202.	-347.6	1242.9	-0.5	0.0	126.4	15875.6							
165.	-76.0	0.0	0.0	0.0	0.0	0.0	NORM	3901.0	0.0	0.0	0.0	0.0	0.0	NORM	329.8	-1176.4	28.1	84.0	2780.5	58378.6	ASTA	136	749	469	0.0	0.0	0.0	0.0						
198.	-76.0	0.0	0.0	0.0	0.0	0.0	1.	-2997.2	22.3	-187.7	0.0	-936.5	-111.6	88.	329.8	-1261.9	28.1	84.0	2788.0	36398.4	PROGR.	NORM	TY	TZ	TORS	MY	NZZ							
231.	-76.0	0.0	0.0	0.0	0.0	0.0	2.	-2997.0	22.3	-187.7	0.0	-936.5	-111.6	123.	329.8	-1261.9	28.1	84.0	2795.5	10717.2	115.	-441.7	761.2	0.6	0.0	147.7	0.0							
264.	-76.0	0.0	0.0	0.0	0.0	0.0	3.	-2996.8	22.3	-187.3	0.0	-936.5	-111.6	140.	329.8	-1261.9	28.1	84.0	2803.0	17391.5	29.	-441.7	467.1	0.6	0.0	-17.9	17700.3							
PROGR.	3901.0	0.0	0.0	0.0	0.0	0.0	4.	-2996.7	22.3	-187.3	0.0	-936.5	-111.6	152.	329.8	-1261.9	28.1	84.0	2810.5	2699.9	86.	-441.7	467.1	0.6	0.0	-35.5	26857.4							
0.	757.7	0.0	0.0	0.0	0.0	0.0	1.	-2996.5	22.3	-187.3	0.0	-936.5	-111.6	165.	329.8	-1261.9	28.1	84.0	2818.0	17391.5	66.	-441.7	-127.2	0.6	0.0	-53.8	27471.4							
33.	757.7	0.0	0.0	0.0	0.0	0.0	2.	-2996.3	22.3	-187.3	0.0	-936.5	-111.6	178.	329.8	-1261.9	28.1	84.0	2825.5	17391.5	115.	-441.7	-424.4	0.6	0.0	-71.8	19542.3							
66.	757.7	0.0	0.0	0.0	0.0	0.0	3.	-2996.1	22.3	-187.3	0.0	-936.5	-111.6	191.	329.8	-1261.9	28.1	84.0	2833.0	17391.5	123.	-441.7	-724.5	0.6	0.0	-89.7	3070.0							
99.	757.7	0.0	0.0	0.0	0.0	0.0	4.	-2995.9	22.3	-187.3	0.0	-936.5	-111.6	204.	329.8	-1261.9	28.1	84.0	2840.5	17391.5	136.	-441.7	-1018.7	0.6	0.0	-107.6	21945.4							
132.	757.7	0.0	0.0	0.0	0.0	0.0	5.	-2995.8	22.3	-187.3	0.0	-936.5	-111.6	217.	329.8	-1261.9	28.1	84.0	2848.0	17391.5	149.	-441.7	-1313.8	0.6	0.0	-125.0	33504.0							
165.	757.7	0.0	0.0	0.0	0.0	0.0	ASTA	104	nodi	72	466	MY	NZZ	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	230.	-441.7	-1613.0	0.6	0.0	-143.5	37905.6							
198.	757.7	0.0	0.0	0.0	0.0	0.0	1.	-2516.1	-95.1	5374.0	0.0	26870.2	475.6	81.	-708.2	-926.8	2.4	-2026.1	-1357.2	153.1	115.	-441.7	-1760.8	0.6	0.0	-153.1	41511.1							
231.	757.7	0.0	0.0	0.0	0.0	0.0	2.	-2515.9	-95.1	5374.0	0.0	26870.2	475.6	98.	-708.2	-935.8	2.4	-2026.1	-1357.2	166.6	115.	-441.7	-1760.8	0.6	0.0	-166.6	44511.1							
264.	757.7	0.0	0.0	0.0	0.0	0.0	3.	-2515.7	-95.1	5374.0	0.0	26870.2	475.6	114.	-708.2	-944.8	2.4	-2026.1	-1357.2	180.1	115.	-441.7	-1760.8	0.6	0.0	-180.1	47511.1							
ASTA	83	nodi	467	470	0.0	0.0	4.	-2515.5	-95.1	5374.0	0.0	16793.9	297.3	130.	-708.2	-953.8	2.4	-2026.1	-1357.2	193.6	115.	-441.7	-1760.8	0.6	0.0	-193.6	50511.1							
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	1.	-2515.3	-95.1	5374.0	0.0	13455.1	237.8	ASTA	121	nodi	747	748	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	20.	-15.8	821.6	0.6	0.0	-15.8	821.6		
0.	943.4	0.0	0.0	0.0	0.0	0.0	2.	-2515.2	-95.1	5374.0	0.0	10076.3	178.4	1.	-169.1	1135.0	-23.8	-237.7	-283.2	-10186.0	58.	-15.8	524.4	-5.9	-15.5	-335.4	19764.2							
45.	943.4	0.0	0.0	0.0	0.0	0.0	3.	-2515.0	-95.1	5374.0	0.0	6717.6	118.9	16.	-169.1	1126.0	-23.8	-237.7	-302.9	-10941.8	144.	-15.8	367.0	-5.9	-15.5	-308.9	2611.7							
90.	943.4	0.0	0.0	0.0	0.0	0.0	4.	-2514.8	-95.1	5374.0	0.0	3358.8	59.5	33.	-169.1	1117.0	-23.8	-237.7	-322.6	-11200.2	173.	-15.8	204.2	-5.9	-15.5	-1177.0	0.0							
134.	943.4	0.0	0.0	0.0	0.0	0.0	5.	-2514.6	-95.1	5374.0	0.0	0.0	0.0	65.	-169.1	1099.0	-23.8	-237.7	-342.1	-11470.2	201.	-15.8	96.1	-5.9	-15.5	208.9	-11640.2							
179.	943.4	0.0	0.0	0.0	0.0	0.0	PROGR.	428.4	720.0	-1842.7	0.0	-90713.7	-3600.0	98.	-169.1	1080.0	-23.8	-237.7	-361.6	-11740.2	230.	-15.8	-1258.5	-5.9	-15.5	677.8	-4550.5							
224.	943.4	0.0	0.0	0.0	0.0	0.0	1.	-4128.0	720.0	-1842.7	0.0	-68035.3	-2700.0	114.	-169.1	1072.0	-23.8	-237.7	-381.1	-12010.2	ASTA	138	nodi	975	953	0.0	0.0	0.0	0.0					
269.	943.4	0.0	0.0	0.0	0.0	0.0	2.	-4127.9	720.0	-1842.7	0.0	-66066.1	-2550.0	130.	-169.1	1063.0	-23.8	-237.7	-400.6	-12260.2	0.	-54.4	891.1	0.0	0.0	-0.1	29900.7							
313.	943.4	0.0	0.0	0.0	0.0	0.0	3.	-4127.7	720.0	-1842.7	0.0	-64017.6	-2350.0	146.	-169.1	1054.0	-23.8	-237.7	-420.1	-12510.2	29.	-54.4	291.0	0.0	0.0	-0.4	64072.6							
358.	943.4	0.0	0.0	0.0	0.0	0.0	4.	-4127.3	720.0	-1842.7	0.0	-62067.4	-2150.0	162.	-169.1	1045.0	-23.8	-237.7	-439.6	-12760.2	86.	-54.4	89.1	0.0	0.0	-0.5	65349.8							
ASTA	86	nodi	19	473	0.0	0.0	5.	-4127.0	720.0	-1842.7	0.0	-60117.9	-1950.0	178.	-169.1	1036.0	-23.8	-237.7	-459.1	-13010.2	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	270.	-54.4	891.1	0.0	0.0	-0.1	29900.7
0.	72.8	0.0	0.0	0.0	0.0	0.0	1.	-4126.8	720.0	-1842.7	0.0	-58168.4	-1750.0	194.	-169.1	1027.0	-23.8	-237.7	-478.6	-13260.2	86.	-54.4	291.0	0.0	0.0	-0.4	64072.6							
45.	72.8	0.0	0.0	0.0	0.0	0.0	2.	-4126.6	720.0	-1842.7	0.0	-56218.9	-1550.0	210.	-169.1	1018.0	-23.8	-237.7	-498.1	-13510.2	270.	-54.4	891.1	0.0	0.0	-0.1	29900.7							
90.	72.8	0.0	0.0	0.0	0.0	0.0	3.	-4126.4	720.0	-1842.7	0.0	-54269.4	-1350.0	226.	-169.1	1009.0	-23.8	-237.7	-517.6	-13760.2	86.	-54.4	291.0	0.0	0.0	-0.4	64072.6							
134.	72.8	0.0	0.0	0.0	0.0	0.0	4.	-4126.2	720.0	-1842.7	0.0	-52319.9	-1150.0	242.	-169.1	1000.0	-23.8	-237.7	-537.1	-14010.2	270.	-54.4	891.1	0.0	0.0	-0.1	29900.7							
179.	72.8	0.0	0.0	0.0	0.0	0.0	5.	-4126.0	720.0	-1842.7	0.0	-50370.4	-950.0	258.	-169.1	991.0	-23.8	-237.7	-556.6	-14260.2	86.	-54.4	291.0	0.0	0.0	-0.4	64072.6							
224.	72.8	0.0	0.0	0.0	0.0	0.0	ASTA	106	nodi	21	468	MY	NZZ	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	270.	-54.4	891.1	0.0	0.0	-0.1	29900.7							
269.	72.8	0.0	0.0	0.0	0.0	0.0	0.	-9774.0	-675.0	9248.5	0.0	46242.4	3375.2	15.	-8.3	297.3	24.9	5.7	2805.3	40205.3	270.	-54.4	891.1	0.0	0.0	-0.1	29900.7							
313.	72.8	0.0	0.0	0.0	0.0	0.0	1.	-9773.8	-675.0	9248.5	0.0	40662.1	2953.3	35.	-8.3	143.3	24.9	5.7	2368.9	40205.3	174.	-54.4	-594.3	0.0	0.0	-0.7	51256.9							
358.	72.8	0.0	0.0	0.0	0.0	0.0	2.	-9773.6	-675.0	9248.5	0.0	34082.8	2507.3	53.	-8.3	103.8	24.9	5.7	1951.5	40205.3	174.	-54.4	-594.3	0.0	0.0	-0.7	51256.9							
ASTA	88	nodi	468	442	0.0	0.0	3.	-9773.4	-675.0	9248.5	0.0	28001.5	2059.5	71.	-8.3	164.9	24.9	5.7	1496.1	40205.3	230.	-54.4	-1188.6	0.0	0.0	-0.9	-2.6							
0.	210.1	0.0	0.0	0.0	0.0	0.0	4.	-9773.2	-675.0	9248.5	0.0	21913.2	1511.6	88.	-8.3	219.0	24.9	5.7	1036.6	40205.3	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	270.	-54.4	891.1	0.0	0.0	-0.1	29900.7
45.	210.1	0.0	0.0	0.0	0.0	0.0	5.	-9773.0	-675.0	9248.5	0.0	15860.6	941.8	105.	-8.3	274.1	24.9	5.7	581.1	40205.3	0.	-768.9	798.5	1.6	-5.8	234.1	-9338.1							
90.	210.1	0.0	0.0	0.0	0.0	0.0	PROGR.	977.2	-675.0	9248.5	0.0	9980.2	371.0	123.	-8.3	329.2	24.9	5.7	123.5	40205.3	10.	-768.9	619.2	1.6	-5.8	407.0	6031.3							
134.	210.1	0.0	0.0	0.0	0.0	0.0	1.	-9772.8	-675.0	9248.5	0.0	9370.7	321.0	140.	-8.3	383.3	24.9	5.7	685.9	40205.3	35.	-768.9	427.1	1.6	-5.8	179.1	12112.7							
179.	210.1	0.0	0.0	0.0	0.0	0.0	2.	-9772.6	-675.0	9248.5	0.0	8760.2	271.0	157.	-8.3	437.5	24.9	5.7	231.7	40205.3	105.	-768.9	241.7	1.6	-5.8	-35.1	17969.6							
224.	210.1	0.0	0.0	0.0	0.0	0.0	3.	-9772.4	-675.0	9248.5	0.0	8149.7	221.0	174.	-8.3	491.7	24.9	5.7	78.1	40205.3	270.	-768.9	56.2	1.6	-5.8	123.3	20573.5							
269.	210.1	0.0	0.0	0.0	0.0	0.0	4.	-9772.2	-675.0	9248.5	0.0	7529.2	171.0	191.	-8.3	545.9	24.9	5.7	26.6	40205.3	105.	-768.9	241.7	1.6	-5.8	67.5	16044.2							
313.	210.1	0.0	0.0	0.0	0.0	0.0	5.	-9772.0	-675.0	9248.5	0.0	6918.7	121.0	208.	-8.3	599.9	24.9	5.7	26.6	40205.3	123.	-768.9	-500.6	1.6	-5.8	39.6	8908.3							
358.	210.1	0.0	0.0	0.0	0.0	0.0	ASTA	107	nodi	30	470	MY	NZZ	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	270.	-768.9	146.8	1.6	-5.8	107.6								

1979.6	782.2	-0.7	-55.8	278.8	-16540.2
1980.6	1156.9	-0.7	-55.8	308.9	25796.6
1981.6	-200.0	0.0	-55.8	339.6	79016.6
sta	4	nodi	230		
1982.6	1174.4	-1567.1	-0.8	-58.9	100.4
1983.6	954.5	-1182.4	-0.8	-58.9	132.1
1984.6	73.8	-84.0	-0.8	-58.9	195.7
1985.6	116.5	-443.1	-0.8	-58.9	193.3
1986.6	206.6	-106.6	-0.8	-58.9	284.3
1987.6	230.0	76.2	-0.8	-58.9	258.6
1988.6	-143.7	105.6	-0.8	-58.9	290.9
1989.6	-363.1	306.3	-0.8	-58.9	320.7
1990.6	-582.7	1430.3	-0.8	-58.9	353.5
sta	8	nodi	470		
1991.6	-3.7	-122.7	-1.2	-60.7	-103.6
1992.6	-3.7	-1081.9	2.4	-128.0	289.4
1993.6	-3.7	-688.2	2.4	-128.0	346.7
1994.6	-3.7	-688.2	2.4	-128.0	346.7
1995.6	-3.7	-500.6	2.4	-128.0	353.5
1996.6	-3.7	-500.6	2.4	-128.0	353.5
1997.6	-3.7	-113.0	2.4	-128.0	367.2
1998.6	-3.7	-113.0	2.4	-128.0	367.2
1999.6	-3.7	274.6	2.4	-128.0	367.2
sta	10	nodi	467		
2000.6	-27.4	-1306.4	9.3	-119.1	322.2
2001.6	-27.4	-918.8	9.3	-119.1	322.2
2002.6	-27.4	-918.8	9.3	-119.1	322.2
2003.6	-27.4	-512.1	9.3	-119.1	322.2
2004.6	-27.4	-337.4	9.3	-119.1	322.2
2005.6	-27.4	-337.4	9.3	-119.1	322.2
2006.6	-27.4	-50.2	9.3	-119.1	322.2
2007.6	-27.4	-50.2	9.3	-119.1	322.2
2008.6	-27.4	-50.2	9.3	-119.1	322.2
2009.6	-27.4	-50.2	9.3	-119.1	322.2
2010.6	-27.4	-50.2	9.3	-119.1	322.2
2011.6	-27.4	-50.2	9.3	-119.1	322.2
2012.6	-27.4	-50.2	9.3	-119.1	322.2
2013.6	-27.4	-50.2	9.3	-119.1	322.2
2014.6	-27.4	-50.2	9.3	-119.1	322.2
2015.6	-27.4	-50.2	9.3	-119.1	322.2
2016.6	-27.4	-50.2	9.3	-119.1	322.2
2017.6	-27.4	-50.2	9.3	-119.1	322.2
2018.6	-27.4	-50.2	9.3	-119.1	322.2
2019.6	-27.4	-50.2	9.3	-119.1	322.2
2020.6	-27.4	-50.2	9.3	-119.1	322.2
2021.6	-27.4	-50.2	9.3	-119.1	322.2
2022.6	-27.4	-50.2	9.3	-119.1	322.2
2023.6	-27.4	-50.2	9.3	-119.1	322.2
2024.6	-27.4	-50.2	9.3	-119.1	322.2
2025.6	-27.4	-50.2	9.3	-119.1	322.2
2026.6	-27.4	-50.2	9.3	-119.1	322.2
2027.6	-27.4	-50.2	9.3	-119.1	322.2
2028.6	-27.4	-50.2	9.3	-119.1	322.2
2029.6	-27.4	-50.2	9.3	-119.1	322.2
2030.6	-27.4	-50.2	9.3	-119.1	322.2
2031.6	-27.4	-50.2	9.3	-119.1	322.2
2032.6	-27.4	-50.2	9.3	-119.1	322.2
2033.6	-27.4	-50.2	9.3	-119.1	322.2
2034.6	-27.4	-50.2	9.3	-119.1	322.2
2035.6	-27.4	-50.2	9.3	-119.1	322.2
2036.6	-27.4	-50.2	9.3	-119.1	322.2
2037.6	-27.4	-50.2	9.3	-119.1	322.2
2038.6	-27.4	-50.2	9.3	-119.1	322.2
2039.6	-27.4	-50.2	9.3	-119.1	322.2
2040.6	-27.4	-50.2	9.3	-119.1	322.2
2041.6	-27.4	-50.2	9.3	-119.1	322.2
2042.6	-27.4	-50.2	9.3		

[illegible]

32.5	1386.	-2.8	10.4	-94.3	-71105.1	0.0
32.5	1377.8	-2.8	10.4	-48.3	-48843.3	0.0
32.5	1358.8	-2.8	10.4	-21.2	-2523.8	0.0
32.5	1359.8	-2.8	10.4	43.8	-415.6	0.0
32.5	1359.8	-2.8	10.4	89.9	-798.3	0.0
32.5	1341.7	-2.8	10.4	136.0	39470.9	0.0
32.5	1332.7	-2.8	10.4	182.0	61471.1	0.0
150	node1	968	TORS	MY	MZZ	0.0
150	NORM	TY	T22	TORS	MY	MZZ
0.	-762.9	8.5	20.9	0.0	104.5	-42.5
1.	-762.9	8.5	20.9	0.0	138.0	-12365.6
2.	-762.9	8.5	20.9	0.0	170.0	-278.0
3.	-762.9	8.5	20.9	0.0	214.0	-37744.8
4.	-762.9	8.5	20.9	0.0	252.0	-5963.9
5.	-762.9	8.5	20.9	0.0	290.0	-690.0
6.	-762.9	8.5	20.9	0.0	328.0	-7691.0
7.	-762.9	8.5	20.9	0.0	366.0	-9593.1
8.	-762.9	8.5	20.9	0.0	404.0	-10737.4
9.	-762.9	8.5	20.9	0.0	442.0	0.0
10.	-762.9	8.5	20.9	0.0	480.0	0.0
11.	-762.9	8.5	20.9	0.0	518.0	0.0
12.	-762.9	8.5	20.9	0.0	556.0	0.0
13.	-762.9	8.5	20.9	0.0	594.0	0.0
14.	-762.9	8.5	20.9	0.0	632.0	0.0
15.	-762.9	8.5	20.9	0.0	670.0	0.0
16.	-762.9	8.5	20.9	0.0	708.0	-31.8
17.	-762.9	8.5	20.9	0.0	746.0	-10.4
18.	-762.9	8.5	20.9	0.0	784.0	-21.2
19.	-762.9	8.5	20.9	0.0	822.0	-31.8
20.	-762.9	8.5	20.9	0.0	860.0	-42.5
21.	-762.9	8.5	20.9	0.0	898.0	-53.2
22.	-762.9	8.5	20.9	0.0	936.0	-63.9
23.	-762.9	8.5	20.9	0.0	974.0	-74.6
24.	-762.9	8.5	20.9	0.0	1012.0	-85.3
25.	-762.9	8.5	20.9	0.0	1050.0	-96.0
26.	-762.9	8.5	20.9	0.0	1088.0	-106.7
27.	-762.9	8.5	20.9	0.0	1126.0	-117.4
28.	-762.9	8.5	20.9	0.0	1164.0	-128.1
29.	-762.9	8.5	20.9	0.0	1202.0	-138.8
30.	-762.9	8.5	20.9	0.0	1240.0	-149.5
31.	-762.9	8.5	20.9	0.0	1278.0	-160.2
32.	-762.9	8.5	20.9	0.0	1316.0	-170.9
33.	-762.9	8.5	20.9	0.0	1354.0	-181.6
34.	-762.9	8.5	20.9	0.0	1392.0	-192.3
35.	-762.9	8.5	20.9	0.0	1430.0	-203.0
36.	-762.9	8.5	20.9	0.0	1468.0	-213.7
37.	-762.9	8.5	20.9	0.0	1506.0	-224.4
38.	-762.9	8.5	20.9	0.0	1544.0	-235.1
39.	-762.9	8.5	20.9	0.0	1582.0	-245.8
40.	-762.9	8.5	20.9	0.0	1620.0	-256.5
41.	-762.9	8.5	20.9	0.0	1658.0	-267.2
42.	-762.9	8.5	20.9	0.0	1696.0	-277.9
43.	-762.9	8.5	20.9	0.0	1734.0	-288.6
44.	-762.9	8.5	20.9	0.0	1772.0	-299.3
45.	-762.9	8.5	20.9	0.0	1810.0	-310.0
46.	-762.9	8.5	20.9	0.0	1848.0	-320.7
47.	-762.9	8.5	20.9	0.0	1886.0	-331.4
48.	-762.9	8.5	20.9	0.0	1924.0	-342.1
49.	-762.9	8.5	20.9	0.0	1962.0	-352.8
50.	-762.9	8.5	20.9	0.0	2000.0	-363.5
51.	-762.9	8.5	20.9	0.0	2038.0	-374.2
52.	-762.9	8.5	20.9	0.0	2076.0	-384.9
53.	-762.9	8.5	20.9	0.0	2114.0	-395.6
54.	-762.9	8.5	20.9	0.0	2152.0	-406.3
55.	-762.9	8.5	20.9	0.0	2190.0	-417.0
56.	-762.9	8.5	20.9	0.0	2228.0	-427.7
57.	-762.9	8.5	20.9	0.0	2266.0	-438.4
58.	-762.9	8.5	20.9	0.0	2304.0	-449.1
59.	-762.9	8.5	20.9	0.0	2342.0	-459.8
60.	-762.9	8.5	20.9	0.0	2380.0	-470.5
61.	-762.9	8.5	20.9	0.0	2418.0	-481.2
62.	-762.9	8.5	20.9	0.0	2456.0	-491.9
63.	-762.9	8.5	20.9	0.0	2494.0	-502.6
64.	-762.9	8.5	20.9	0.0	2532.0	-513.3
65.	-762.9	8.5	20.9	0.0	2570.0	-524.0
66.	-762.9	8.5	20.9	0.0	2608.0	-534.7
67.	-762.9	8.5	20.9	0.0	2646.0	-545.4
68.	-762.9	8.5	20.9	0.0	2684.0	-556.1
69.	-762.9	8.5	20.9	0.0	2722.0	-566.8
70.	-762.9	8.5	20.9	0.0	2760.0	-577.5
71.	-762.9	8.5	20.9	0.0	2798.0	-588.2
72.	-762.9	8.5	20.9	0.0	2836.0	-598.9
73.	-762.9	8.5	20.9	0.0	2874.0	-609.6
74.	-762.9	8.5	20.9	0.0	2912.0	-620.3
75.	-762.9	8.5	20.9	0.0	2950.0	-631.0
76.	-762.9	8.5	20.9	0.0	2988.0	-641.7
77.	-762.9	8.5	20.9	0.0	3026.0	-652.4
78.	-762.9	8.5	20.9	0.0	3064.0	-663.1
79.	-762.9	8.5	20.9	0.0	3102.0	-673.8
80.	-762.9	8.5	20.9	0.0	3140.0	-684.5
81.	-762.9	8.5	20.9	0.0	3178.0	-695.2
82.	-762.9	8.5	20.9	0.0	3216.0	-705.9
83.	-762.9	8.5	20.9	0.0	3254.0	-716.6
84.	-762.9	8.5	20.9	0.0	3292.0	-727.3
85.	-762.9	8.5	20.9	0.0	3330.0	-738.0
86.	-762.9	8.5	20.9	0.0	3368.0	-748.7
87.	-762.9	8.5	20.9	0.0	3406.0	-759.4
88.	-762.9	8.5	20.9	0.0	3444.0	-770.1
89.	-762.9	8.5	20.9	0.0	3482.0	-780.8
90.	-762.9	8.5	20.9	0.0	3520.0	-791.5
91.	-762.9	8.5	20.9	0.0	3558.0	-802.2
92.	-762.9	8.5	20.9	0.0	3596.0	-812.9
93.	-762.9	8.5	20.9	0.0	3634.0	-823.6
94.	-762.9	8.5	20.9	0.0	3672.0	-834.3
95.	-762.9	8.5	20.9	0.0	3710.0	-845.0
96.	-762.9	8.5	20.9	0.0	3748.0	-855.7
97.	-762.9	8.5	20.9	0.0	3786.0	-866.4
98.	-762.9	8.5	20.9	0.0	3824.0	-877.1
99.	-762.9	8.5	20.9	0.0	3862.0	-887.8
100.	-762.9	8.5	20.9	0.0	3900.0	-898.5
101.	-762.9	8.5	20.9	0.0	3938.0	-909.2
102.	-762.9	8.5	20.9	0.0	3976.0	-919.9
103.	-762.9	8.5	20.9	0.0	4014.0	-930.6
104.	-762.9	8.5	20.9	0.0	4052.0	-941.3
105.	-762.9	8.5	20.9	0.0	4090.0	-952.0
106.	-762.9	8.5	20.9	0.0	4128.0	-962.7
107.	-762.9	8.5	20.9	0.0	4166.0	-973.4
108.	-762.9	8.5	20.9	0.0	4204.0	-984.1
109.	-762.9	8.5	20.9	0.0	4242.0	-994.8
110.	-762.9	8.5	20.9	0.0	4280.0	-1005.5
111.	-762.9	8.5	20.9	0.0	4318.0	-1016.2
112.	-762.9	8.5	20.9	0.0	4356.0	-1026.9
113.	-762.9	8.5	20.9	0.0	4394.0	-1037.6
114.	-762.9	8.5	20.9	0.0	4432.0	-1048.3
115.	-762.9	8.5	20.9	0.0	4470.0	-1059.0
116.	-762.9	8.5	20.9	0.0	4508.0	-1069.7
117.	-762.9	8.5	20.9	0.0	4546.0	-1080.4
118.	-762.9	8.5	20.9	0.0	4584.0	-1091.1
119.	-762.9	8.5	20.9	0.0	4622.0	-1101.8
120.	-762.9	8.5	20.9	0.0	4660.0	-1112.5
121.	-762.9	8.5	20.9	0.0	4698.0	-1123.2
122.	-762.9	8.5	20.9	0.0	4736.0	-1133.9
123.	-762.9	8.5	20.9	0.0	4774.0	-1144.6
124.	-762.9	8.5	20.9	0.0	4812.0	-1155.3
125.	-762.9	8.5	20.9	0.0	4850.0	-1166.0
126.	-762.9	8.5	20.9	0.0	4888.0	-1176.7
127.	-762.9	8.5	20.9	0.0	4926.0	-1187.4
128.	-762.9	8.5	20.9	0.0	4964.0	-1198.1
129.	-762.9	8.5	20.9	0.0	5002.0	-1208.8
130.	-762.9	8.5	20.9	0.0	5040.0	-1219.5
131.	-762.9	8.5	20.9	0.0	5078.0	-1230.2
132.	-762.9	8.5	20.9	0.0	5116.0	-1240.9
133.	-762.9	8.5	20.9	0.0	5154.0	-1251.6
134.	-762.9	8.5	20.9	0.0	5192.0	-1262.3
135.	-762.9	8.5	20.9	0.0	5230.0	-1273.0
136.	-762.9	8.5	20.9	0.0	5268.0	-1283.7
137.	-762.9	8.5	20.9	0.0	5306.0	-1294.4
138.	-762.9	8.5	20.9	0.0	5344.0	-1305.1
139.	-762.9	8.5	20.9	0.0	5382.0	-1315.8
140.	-762.9	8.5	20.9	0.0	5420.0	-1326.5
141.	-762.9	8.5	20.9	0.0	5458.0	-1337.2
142.	-762.9	8.5	20.9	0.0	5496.0	-1347.9
143.	-762.9	8.5	20.9	0.0	5534.0	-1358.6
144.	-762.9	8.5	20.9	0.0	5572.0	-1369.3
145.	-762.9	8.5	20.9	0.0	5610.0	-1379.9
146.	-762.9	8.5	20.9	0.0	5648.0	-1390.6
147.	-762.9	8.5	20.9	0.0	5686.0	-1401.3
148.	-762.9	8.5	20.9	0.0	5724.0	-1412.0
149.	-762.9	8.5	20.9	0.0	5762.0	-1422.7
150.	-762.9	8.5	20.9	0.0	5800.0	-1433.4
151.	-762.9	8.5	20.9	0.0	5838.0	-1444.1
152.	-762.9	8.5	20.9	0.0	5876.0	-1454.8
153.	-762.9	8.5	20.9	0.0	5914.0	-1465.5
154.	-762.9	8.5	20.9	0.0	5952.0	-1476.2
155.	-762.9	8.5	20.9	0.0	5990.0	-1486.9
156.	-762.9	8.5	20.9	0.0	6028.0	-1497.6
157.	-762.9	8.5	20.9	0.0	6066.0	-1508.3
158.	-762.9	8.5	20.9	0.0	6104.0	-1519.0
159.	-762.9	8.5	20.9	0.0	6142.0	-1529.7
160.	-762.9	8.5	20.9	0.0	6180.0	-1540.4
161.	-762.9	8.5	20.9	0.0	6218.0	-1551.1
162.	-762.9	8.5	20.9	0.0	6256.0	-1561.8
163.	-762.9	8.5	20.9	0.0	6294.0	-1572.5
164.	-762.9	8.5	20.9	0.0	6332.0	-1583.2
165.	-762.9	8.5	20.9	0.0	6370.0	-1593.9
166.	-762.9	8.5	20.9	0.0	6408.0	-1604.6
167.	-762.9	8.5	20.9	0.0	6446.0	-1615.3
168.	-762.9	8.5	20.9	0.0	6484.0	-1626.0
169.	-762.9	8.5	20.9	0.0	6522.0	-1636.7
170.	-762.9	8.5	20.9	0.0	6560.0	-1647.4
171.	-762.9	8.5	20.9	0.0	6598.0	-1658.1
172.	-762.9	8.5	20.9	0.0	6636.0	-1668.8
173.	-762.9	8.5	20.9	0.0	6674.0	-1679.5
174.	-762.9	8.5	20.9	0.0	67	

SOLLECITAZIONE ASSE		3 SUI SUDVY		COMBINAZIONE		
N. 5 CONDIZIONI ANALISI STATISTICA						
1	Peso, proprio	1	1,30			
2	Permanente	1	1,30			
3	A variabile	1	1,50			
4	Neve (<100mm_sla)	1	1,50			
5	Vento_U	1	1,50			
1	+1.50C001	+1.50C002	+1.50C003	+1.50C004	+1.50C005	
2	+1.50C001	+1.50C003	+1.50C003	+1.50C004	+1.50C005	
Unità di misura: peso e freeze [mm]NORM,TZZ,TZZ [dsk]						
MEZZ.MYRI [Sons]						
MEZZ.	NORM	TZZ	466	404	MEZZ	
PROG.	TZZ	TZZ	TZZ	TZZ	MEZZ	
0.	-223.4	-1081.0	-0.7	-44.8	78.7	66678.2
125.	-790.9	-1474.6	-0.7	-44.8	117.6	71167.6
42.	-636.4	-1458.4	-0.7	-44.8	109.0	13764.7
125.	-790.9	-1332.0	-0.7	-44.8	117.6	71167.6
42.	-648.9	-706.7	-0.7	-44.8	139.4	-2352.5
125.	-1204.1	-726.2	-0.7	-66.9	177.2	-2072.0
167.	-1070.1	-311.6	-0.7	-66.9	200.1	-5128.0
167.	-1070.1	72.6	-0.7	-66.9	200.1	-5128.0
125.	-1204.1	72.6	-0.7	-66.9	237.0	-5005.6
167.	-1204.1	311.6	-0.7	-66.9	237.0	-5005.6
125.	-1843.6	392.0	-0.7	-66.9	266.9	-41274.9
125.	-1501.5	787.8	-0.7	-66.9	266.9	-41274.9
125.	-1501.5	-777.4	-0.7	-66.9	266.9	-41274.9
252.	-1715.6	1166.7	-0.7	-44.8	291.1	2943.5
252.	-1715.6	-1166.7	-0.7	-44.8	291.1	2943.5
324.	-1928.8	1521.8	-0.7	-44.8	321.5	8006.4
324.	-1928.8	-1521.8	-0.7	-44.8	321.5	8006.4
ASTA	4	1579	220	339	78012	
PROG.	TZZ	TZZ	TZZ	TZZ		
125.	1464.6	-1579.5	-0.9	-61.9	105.5	10233.6
42.	884.2	-1350.4	-0.9	-55.9	95.5	94135.4
42.	1245.0	-1350.4	-0.9	-61.9	105.5	10233.6
84.	1005.6	-1184.0	-0.9	-55.9	132.0	36702.2
84.	1005.6	-830.2	-0.9	-61.9	158.8	1079.5
125.	889.9	-805.3	-0.9	-55.9	168.8	-5007.6
125.	889.9	-450.6	-0.9	-55.9	168.8	-5007.6
125.	225.3	-450.6	-0.9	-55.9	205.2	-30974.0

[illegible]

[illegible]

[illegible][illegible]

[illegible]

[illegible]

[illegible]

3.	-33.2	-856.5	-917.0	-4199.2	6679.4	7097.3	0.0	15.8	-26.3	-91.6	-505.6	81.9	-42.0	4.	34.8	627.7	-566.6	2365.4	-3713.9	-3865.2	16.1	-320.7	57.9	23	1677.8	1111.1	-952.0
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-5305.9	-4510.9	-15.8	-26.3	-91.6	-505.6	-196.4	-4.0	-34.8	-663.2	-526.4	-2658.1	-2703.7	-2918.0	0.0	32	north	39	73			
	-33.2	-856.5	-917.0	-4199.2	-6500.7	-530																					

[illegible]

PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										
																										ASTA	PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
																																																					ASTA	PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																				
																																																																																ASTA	PROGR.	0.	NORM	TYV	TZ2	TORS	MYV	MZZ	-336.2	334.5	0.3	0.0	0.5	-627.2	-443.3	532.7	-15.0	0.0	-65.6	-2330.7	24.0	-9.6	-0.1	0.0	-0.1	6.0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																									
45.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0

3.	50.3	-60.4	-8.6	0.0	-26.7	188.7	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5	
3.	-62.7	60.5	-12.0	0.0	-37.4	-189.1	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0	
3.	-50.3	60.4	8.6	0.0	21.4	-150.9	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	-1.9	-26.7	1.6	-323.5	3.9	20.0	-14.5	176.7	-443.9	1200.6	
3.	50.3	-60.5	-8.6	0.0	-21.4	150.9	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0	
3.	-62.7	60.5	-12.0	0.0	22.5	113.4	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0	
3.	-50.3	60.4	8.6	0.0	16.0	113.3	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	-1.9	-26.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
4.	-62.7	60.5	-12.0	0.0	-22.5	-113.4	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0	
4.	-62.7	60.5	-12.0	0.0	10.7	-75.5	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	-1.9	-26.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
4.	-50.3	60.4	8.6	0.0	-10.8	75.5	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	-1.9	-26.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
4.	-62.7	60.5	-12.0	0.0	-13.0	-75.5	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0	
5.	-50.3	60.4	8.6	0.0	0.0	0.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	-1.9	-26.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
5.	-62.7	60.5	-12.0	0.0	0.0	0.0	0.0	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0	
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	19.7	-5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-24.6	-29.6	-3.7	35.8	102.5	-1155.1	3.1	-11.7	3.0	-18.0	-244.9	189.0
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-19.7	5.1	1.9	-26.7	32.3	413.0	6.2	-11.7	-3.0	-18.0	241.2	-178.5
Asta	PROGR.	0.	109	nord	11	471	785	0.	93.8	24.8	-26.4	0.0	-6509.4	-5138.3	-2											

5.	Asta PROGR. 0.	8.1	41.9	0.0	0.0	0.0	-26.2	76.5	8.0	0.0	0.0	3.0	686.5	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	41.5	-19.0	0.0	-35.6	-77.7		
		-6.6	-6.3	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-4.0	-915.4	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	19.0	0.0	23.7	-91.8		
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.1	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	19.0	0.0	-7.6	-44.3		
		-8.1	-41.9	0.0	0.0	0.0	0.0	-35.1	-9.1	0.1	0.0	-7.7	-1044.7	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-35.4	6.1	0.0	7.6	-44.3	
		-8.0	-41.9	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8	
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8	
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8	
		-8.1	-41.9	0.0	0.0	0.0	0.0	-35.1	-9.1	0.1	0.0	-7.7	-1044.7	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-35.4	6.1	0.0	7.6	-44.3	
		-8.0	-41.9	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	0.0	-915.4	0	-107.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
		-6.0	0.0	0.0	0.0	0.0	0.0	-76.5	-8.0	0.0	0.0	-7.0	-1044.7	0	-70.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-41.5	-19.0	0.0	-23.7	-91.8
1.	Asta PROGR. 0.	127	746	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777		
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
2.	Asta PROGR. 0.	127	746	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777		
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	
		norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	norm	

	317.9	12.7	-23.4	81.6	7868.8	-1623.3		3.9	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5415.8	70.1		-3.9	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	-61.4	-5415.7	70.1		0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.	-317.9	-12.7	-23.4	-81.6	-7868.8	1623.3		-4.8	0.0	0.0	0.0	0.0	0.0	0.0
	-317.9	-12.7	-23.4	-81.6	-7883.4	-1615.4		3.9	0.0	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5426.3	-71.6		0.0	0.0	0.0	0.0	0.0	0.0	0.0
	234.3	1.6	-17.5	61.4	5426.7	-71.2		0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.	-317.9	-12.7	-23.4	-81.6	-7883.4	-1615.4		3.9	0.0	0.0	0.0	0.0	0.0	0.0
	-317.9	-12.7	-23.4	-81.6	-7898.1	-1607.4		0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5437.6	-72.2		245.6	8.1	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5437.6	-72.2		-245.6	-8.1	0.0	0.0	0.0	0.0	0.0
3.	-317.9	-12.7	-23.4	-81.6	-7898.1	-1607.4		-245.6	-8.1	0.0	0.0	-0.6	-202.8	-0.0
	-317.9	-12.7	-23.4	-81.6	-7912.4	-1599.5		0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5448.6	-73.2		-245.6	-8.1	0.0	0.0	-1.1	-232.5	-0.0
	-234.3	1.6	-17.5	-61.4	-5448.6	-73.2		245.6	8.1	0.0	0.0	0.0	0.0	0.0
4.	-317.9	-12.7	-23.4	-81.6	-7912.7	-1599.5		-245.6	-8.1	0.0	0.0	-1.2	-385.7	-0.0
	-317.9	-12.7	-23.4	-81.6	-7927.3	-1591.5		0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5459.5	-74.3		-245.6	-8.1	0.0	0.0	2.2	-465.0	-0.0
	-234.3	1.6	-17.5	-61.4	-5459.5	-74.3		245.6	8.1	0.0	0.0	0.0	0.0	0.0
4.	-317.9	-12.7	-23.4	-81.6	-7927.3	-1591.5		-245.6	-8.1	0.0	0.0	1.2	-385.7	-0.0
	-317.9	-12.7	-23.4	-81.6	-7942.0	-1583.5		0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5470.4	-75.3		-245.6	-8.1	0.0	0.0	1.8	-578.5	-0.0
	-234.3	1.6	-17.5	-61.4	-5470.4	-75.3		245.6	8.1	0.0	0.0	0.0	0.0	0.0
5.	-317.9	-12.7	-23.4	-81.6	-7942.0	-1583.5		-245.6	-8.1	0.0	0.0	-2.4	-771.4	-0.0
	-317.9	-12.7	-23.4	-81.6	-7956.6	-1575.6		0.0	0.0	0.0	0.0	0.0	0.0	0.0
	-234.3	1.6	-17.5	-61.4	-5481.4	-76.3		-245.6	-8.1	0.0	0.0	-4.4	-930.1	-0.0
	-234.3	1.6	-17.5	-61.4	-5481.4	-76.3		245.6	8.1	0.0	0.0	0.0	0.0	0.0
	-317.9	-12.7	-23.4	-81.6	-7956.6	-1575.6		-245.6	-8.1	0.0	0.0	-3.0	-964.2	-0.0
ASTA	149	notH						245.6	8.1	0.0	0.0	0.0	0.0	0.0
PROD.	NORM	TYV	TZZ	TORS	MMY	MZZ		-245.6	-8.1	0.0	0.0	-3.5	-116.6	-0.0
	-21.4	13.4	-3.7	4.4	-885.7	-1576.0		245.6	8.1	0.0	0.0	3.0	964.2	-0.0
	-2.6	1.0	-2.5	-9.8	-588.5	-74.8		-245.6	-8.1	0.0	0.0	0.0	0.0	0.0
	-2.6	1.0	-2.5	-9.8	-588.4	-74.8		245.6	8.1	0.0	0.0	6.6	1395.1	-0.0
42.	-21.4	13.4	-3.7	4.4	-885.7	-1576.0		-4.4	-245.6	-8.1	0.0	-6.6	-1395.1	-0.0
	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		245.6	8.1	0.0	0.0	3.6	1157.0	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	7.7	1627.6	-0.0
84.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
126.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
168.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
209.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
251.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
293.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
335.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
ASTA	150	notH						245.6	8.1	0.0	0.0	0.0	0.0	0.0
PROD.	NORM	TYV	TZZ	TORS	MMY	MZZ		-245.6	-8.1	0.0	0.0	-3.5	-116.6	-0.0
	-21.4	13.4	-3.7	4.4	-885.7	-1576.0		245.6	8.1	0.0	0.0	3.0	964.2	-0.0
	-2.6	1.0	-2.5	-9.8	-588.5	-74.8		-245.6	-8.1	0.0	0.0	0.0	0.0	0.0
	-2.6	1.0	-2.5	-9.8	-588.4	-74.8		245.6	8.1	0.0	0.0	6.6	1395.1	-0.0
10.	-21.4	13.4	-3.7	4.4	-885.7	-1576.0		-4.4	-245.6	-8.1	0.0	-6.6	-1395.1	-0.0
	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		245.6	8.1	0.0	0.0	3.6	1157.0	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	7.7	1627.6	-0.0
34.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
67.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
101.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
135.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
168.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
202.	-21.4	13.4	-3.7	4.4	-730.8	-1013.0		-4.4	-245.6	-8.1	0.0	-7.7	-1627.6	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	4.7	1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		-245.6	-8.1	0.0	0.0	-4.4	-1349.9	-0.0
	-2.6	1.0	-2.5	9.8	-484.0	-116.5		245.6	8.1	0.0	0.0	-4.4	-1349.9	-0.0
236.	-21.4	13.4</												

[illegible]

236.	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	33.1	0.0	0.0	0.0	-124.1	99.8	515.9	125.7	0.0	5138.3	-6509.4	-95.5	-517.2	253.4	0.0	15203.4	31029.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-33.1	0.0	0.0	0.0	-37.2	-600.9	-38.8	0.0	2200.9	6999.8	95.5	517.2	-253.4	0.0	-12023.4	-31029.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	37.2	600.9	38.8	0.0	-2200.9	-6999.8	-95.5	517.2	-253.4	0.0	12023.4	31029.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-93.8	-515.9	-125.7	0.0	-5138.3	6509.4	95.5	-517.2	253.4	0.0	-12023.4	-31029.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	175	norm	960	741	norm	MY	NZZ	75.	-36.1	561.7	-273.3	0.0	-12306.7	-25276.9
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	norm	MY	722	norm	MY	NZZ	75.	-36.1	561.7	-273.3	0.0	-12306.7	-25276.9	
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	652.7	50.9	65.8	0.0	13052.6	-47148.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
269.	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	2708.6	17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	-31.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.8	0.0	-2708.6	-17418.6	95.5	-517.2	253.4	0.0	12306.7	25276.9		
	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.6	65.8	65.											

131.	-8.6	-4.4	3.0	23.8	-302.3	176.2	38.	210.7	-0.9	0.2	20.6	-32.0	111.5	336.	-377.9	7.5	0.0	3.2	14.3	872.7	168.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	8.9	3.1	-3.1	-27.9	306.0	-127.2		-220.2	-0.1	-0.4	-24.8	43.1	5.4		377.9	-7.5	0.0	-3.2	-15.6	-1188.5		812.5	-4.0	0.0	1.4	-5.1	1125.7	
	-8.9	-3.1	-3.1	-27.9	306.0	-127.2		-220.2	0.1	0.4	-24.8	43.1	5.4		-377.9	7.5	0.0	-3.2	-15.6	-1188.5		812.5	-4.0	0.0	1.4	-5.1	1125.7	
	8.6	4.4	-3.0	-23.8	-302.3	-176.2		-210.7	-0.9	0.2	-20.6	32.0	-111.5		274.4	-6.2	0.0	-1.3	-5.4	-938.7		-869.6	-2.9	0.0	3.8	-13.3	1143.6	
150.	-8.6	-4.4	3.0	23.8	-357.9	193.7	56.	210.7	-0.9	0.2	-20.6	-36.5	94.7	Asta PROGR. 0.	304.2	-8.0	-2.5	5.1	126.6	872.7	210.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	8.9	3.1	-3.1	-27.9	361.4	-109.7		-220.2	0.1	0.4	-24.8	-49.8	-2.7		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-5.1	1125.7	
	-8.9	-3.1	-3.1	-27.9	361.4	-109.7		-220.2	0.1	0.4	-24.8	-49.8	-2.7		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-869.6	-2.9	0.0	3.8	-13.3	1143.6	
	8.6	4.4	-3.0	-23.8	-357.9	-193.7		-210.7	-0.9	0.2	-20.6	-40.7	78.0		240.9	6.3	-2.4	1.6	-39.8	-812.5		812.5	-4.0	0.0	1.4	-5.1	1125.7	
Asta PROGR. 0.	-8.6	-4.4	3.0	23.8	-413.5	111.2	75.	210.7	-0.9	0.2	-20.6	-41.0	78.0	19.	304.2	-8.0	-2.5	5.1	126.6	872.7	252.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	8.9	3.1	-3.1	-27.9	420.7	-12.2		-220.2	0.1	0.4	-24.8	56.5	0.1		240.9	6.3	-2.4	1.6	-39.8	-812.5		812.5	-4.0	0.0	1.4	-5.1	1125.7	
	-8.9	-3.1	-3.1	-27.9	420.7	-12.2		-220.2	0.1	0.4	-24.8	56.5	0.1		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-869.6	-2.9	0.0	3.8	-13.3	1143.6	
	8.6	4.4	-3.0	-23.8	-413.5	-111.2		-210.7	-0.9	0.2	-20.6	-41.0	78.0		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-5.1	1125.7	
19.	-3.0	-1.8	-0.1	-7.6	928.9	-0.6	94.	210.7	-0.9	0.2	-20.6	-45.5	61.2	113.	304.2	-8.0	-2.5	5.1	126.6	872.7	294.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	3.4	-7.1	-1.8	-0.1	-25.8	1061.8		-220.2	0.1	-0.4	-24.8	63.3	-2.6		240.9	6.3	-2.4	1.6	-39.8	-812.5		812.5	-4.0	0.0	1.4	-7.1	623.1	
	-3.4	7.1	1.8	0.1	25.8	-1061.8		-220.2	0.1	-0.4	-24.8	63.3	-2.6		-240.9	6.3	2.4	-1.6	39.8	-812.5		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	25.8	-1061.8		-210.7	-0.9	0.2	-20.6	-41.0	78.0		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.1	623.1	
38.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	113.	210.7	-0.9	0.2	-20.6	-45.5	61.2	56.	304.2	-8.0	-2.5	5.1	126.6	872.7	336.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	70.0	-5.2		240.9	6.3	-2.4	1.6	85.1	-701.1		812.5	-4.0	0.0	1.4	-7.8	455.6	
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-220.2	0.1	-0.4	-24.8	70.0	-5.2		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	-7.6	-928.9		-210.7	-0.9	0.2	-20.6	-45.5	61.2		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.8	455.6	
75.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	131.	210.7	-0.9	0.2	-20.6	-54.5	27.7	75.	304.2	-8.0	-2.5	5.1	126.6	872.7	Asta PROGR. 0.	31	noft	342	727	noft	MY	NZZ
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	76.7	-7.9		240.9	6.3	-2.4	1.6	-130.2	582.4		812.5	-4.0	0.0	1.4	-7.8	455.6	
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-220.2	0.1	-0.4	-24.8	76.7	-7.9		-304.2	8.0	2.5	-5.1	-126.6	-872.7		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	-7.6	-928.9		-210.7	-0.9	0.2	-20.6	-54.5	27.7		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.8	455.6	
94.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	150.	210.7	-0.9	0.2	-20.6	-59.0	10.9	94.	304.2	-8.0	-2.5	5.1	126.6	872.7	113.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		240.9	6.3	-2.4	1.6	-175.4	-463.6		812.5	-4.0	0.0	1.4	-7.8	455.6	
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		-304.2	8.0	2.5	-5.1	-175.4	-463.6		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	-7.6	-928.9		-210.7	-0.9	0.2	-20.6	-59.0	10.9		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.8	455.6	
113.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	Asta PROGR. 0.	210.7	-0.9	0.2	-20.6	-59.0	-10.9	131.	304.2	-8.0	-2.5	5.1	126.6	872.7	150.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		240.9	6.3	-2.4	1.6	-175.4	-463.6		812.5	-4.0	0.0	1.4	-7.8	455.6	
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		-304.2	8.0	2.5	-5.1	-175.4	-463.6		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	-7.6	-928.9		-210.7	-0.9	0.2	-20.6	-59.0	-10.9		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.8	455.6	
131.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	56.	210.7	-0.9	0.2	-20.6	-63.7	16	94.	304.2	-8.0	-2.5	5.1	126.6	872.7	113.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		240.9	6.3	-2.4	1.6	-175.4	-463.6		812.5	-4.0	0.0	1.4	-7.8	455.6	
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		-304.2	8.0	2.5	-5.1	-175.4	-463.6		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	-7.6	-928.9		-210.7	-0.9	0.2	-20.6	-63.7	16		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.8	455.6	
150.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	75.	210.7	-0.9	0.2	-20.6	-63.7	16	Asta PROGR. 0.	304.2	-8.0	-2.5	5.1	126.6	872.7	150.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		240.9	6.3	-2.4	1.6	-175.4	-463.6		812.5	-4.0	0.0	1.4	-7.8	455.6	
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		-304.2	8.0	2.5	-5.1	-175.4	-463.6		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	-7.6	-928.9		-210.7	-0.9	0.2	-20.6	-63.7	16		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.8	455.6	
Asta PROGR. 0.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	94.	210.7	-0.9	0.2	-20.6	-63.7	16	113.	304.2	-8.0	-2.5	5.1	126.6	872.7	19.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		240.9	6.3	-2.4	1.6	-175.4	-463.6		812.5	-4.0	0.0	1.4	-7.8	455.6	
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		-304.2	8.0	2.5	-5.1	-175.4	-463.6		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	-7.6	-928.9		-210.7	-0.9	0.2	-20.6	-63.7	16		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.8	455.6	
42.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	113.	210.7	-0.9	0.2	-20.6	-63.7	16	131.	304.2	-8.0	-2.5	5.1	126.6	872.7	150.	-869.6	2.9	0.0	-3.8	13.3	-1143.6	
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		240.9	6.3	-2.4	1.6	-175.4	-463.6		812.5	-4.0	0.0	1.4	-7.8	455.6	
	-3.4	7.1	1.8	0.1	-7.6	-928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		-304.2	8.0	2.5	-5.1	-175.4	-463.6		-869.6	-2.9	0.0	3.8	-18.3	782.7	
	3.0	-6.8	1.8	0.1	-7.6	-928.9		-210.7	-0.9	0.2	-20.6	-63.7	16		304.2	-8.0	-2.5	5.1	126.6	872.7		812.5	-4.0	0.0	1.4	-7.8	455.6	
83.	-3.0	6.8	1.8	-2.2	-9.3	-893.0	131.	210.7	-0.9	0.2	-20.6	-63.7	16	150.	304.2	-8.0	-2.5	5.1	126.6	872.7	Asta PROGR. 0.	32	noft	473	730	noft	MY	NZZ
	3.4	-7.1	-1.8	-0.1	-7.6	928.9		-220.2	0.1	-0.4	-24.8	83.5	-10.5		240.9	6.3	-2.4	1.6	-175.4	-463.6		812.5	-4.0	0.0	1.4	-7.8	45	

43.	426.6	-205.3	-4.4	-15.8	728.0	20973.9	98.	53.2	-83.0	16.5	82.3	-1604.7	-6861.7	-7.1	-107.0	19.8	98.9	-643.0	-2087.3	130.	19.3	-117.9	37.9	56.8	-2931.1	18567.3
	426.6	-205.3	-4.4	-15.8	728.0	20973.9	98.	-45.9	-76.0	-15.6	-82.3	-1523.7	-7943.1	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	728.0	20973.9	98.	-45.9	-76.0	-15.6	-82.3	-1523.7	-7943.1	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
85.	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	-53.2	-83.0	-16.5	-82.3	-1604.7	-6861.7	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	-53.2	-83.0	-16.5	-82.3	-1604.7	-6861.7	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	579.1	11248.6	114.	-53.2	-83.0	-16.5	-82.3	-1604.7	-6861.7	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
128.	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	542.5	11248.6	114.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
170.	454.9	-199.8	-4.6	-8.6	384.7	2650.4	130.	-53.2	-83.0	-16.5	-82.3	-1872.2	9710.0	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	384.7	2650.4	130.	-53.2	-83.0	-16.5	-82.3	-1872.2	9710.0	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	384.7	2650.4	130.	-53.2	-83.0	-16.5	-82.3	-1872.2	9710.0	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
213.	426.6	-205.3	-4.4	-15.8	171.6	5201.9	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	171.6	5201.9	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	171.6	5201.9	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
255.	454.9	-199.8	-4.6	-8.6	384.7	2650.4	130.	-53.2	-83.0	-16.5	-82.3	-1872.2	9710.0	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	384.7	2650.4	130.	-53.2	-83.0	-16.5	-82.3	-1872.2	9710.0	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	384.7	2650.4	130.	-53.2	-83.0	-16.5	-82.3	-1872.2	9710.0	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
298.	426.6	-205.3	-4.4	-15.8	384.8	31377.6	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	384.8	31377.6	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	384.8	31377.6	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
340.	454.9	-199.8	-4.6	-8.6	586.9	30797.2	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	586.9	30797.2	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	586.9	30797.2	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
382.	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
424.	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
466.	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
508.	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
550.	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
592.	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
634.	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	426.6	-205.3	-4.4	-15.8	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
676.	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
	454.9	-199.8	-4.6	-8.6	781.3	48828.1	130.	-45.9	-76.0	-15.6	-78.1	-1777.1	8871.6	-7.1	-107.0	-19.8	-98.9	-643.0	-2087.3	130.	-19.3	-123.7	-37.9	-56.8	-2931.1	-17665.6
718.	426.6	-205.3	-4.4	-15.8																						

61.	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	151.4	4.4	29.0	101.3	-1677.9	-10.6	6.4	-11.4	-5.8	355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	-75.6	-1693.4	-6.3	6.7	-9.1	-5.6	290.1	-109.3	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	111.5	-1448.9	-10.6	-6.4	11.4	5.8	-355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	111.5	-1448.9	-10.6	-6.4	11.4	5.8	-355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
98.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
114.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
130.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
144.	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	180.6	-208.4	-29.9	-149.4	-1456.7	9367.7	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
	177.2	-52.2	126.0	1638.5	10821.0	-30.5	-151.4	-4.4	-29.0	30.1	19326.9	-6.3	-6.7	9.1	5.6	-142.4	218.7	-259.3	0.0	0.0	0.0	0.0	0.0
	142.7	-177.2	-25.2	126.0	-1228.9	7941.0	-30.5	-151.4	-4.4	29.0	177.5	1434.9	-10.6	-6.7	9.1	5.8	-437.7	-101.8	0.0	0.0	0.0	0.0	0.0
ASTA PRGR.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NORM	TYT	TZZ	TORS	MYT	MZZ																	
	-6.7	68.7	0.1	65.6	0.0	-752.0	-30.5	-151.4	-4.4	-29.0	386.2	6931.8	-10.6	-6.4	11.4	5.8	-355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	-6.7	68.7	0.1	65.6	0.0	-752.0	-30.5	-151.4	-4.4	-29.0	386.2	6931.8	-10.6	-6.4	11.4	5.8	-355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	-7.3	61.2	0.2	70.8	0.0	-633.5	-30.5	-151.4	-4.4	-29.0	386.2	6931.8	-10.6	-6.4	11.4	5.8	-355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	7.3	-61.2	-0.2	-70.8	0.0	363.2	-30.5	-151.4	-4.4	-29.0	386.2	6931.8	-10.6	-6.4	11.4	5.8	-355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	6.7	-68.7	-0.1	-65.6	-0.4	-363.7	-30.5	-151.4	-4.4	-29.0	386.2	6931.8	-10.6	-6.4	11.4	5.8	-355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	-7.3	-61.2	-0.2	-70.8	0.0	-633.5	-30.5	-151.4	-4.4	-29.0	386.2	6931.8	-10.6	-6.4	11.4	5.8	-355.0	-101.8	0.0	0.0	0.0	0.0	0.0
	7.3	-61.2	-0.2	-70.8	0.0	-633.5	-30.5	-151.4	-4														

[illegible]

[illegible]

[illegible]

126.	-283.6	195.9	-6.7	-3.1	-1449.6	-1244.5
	-297.0	-203.6	7.2	-2.6	1353.3	1002.9
	-297.0	-203.6	7.2	2.6	1187.7	1002.9
	283.6	-195.9	6.7	3.1	1449.6	1244.5
168.	-283.6	195.9	-6.7	-3.1	-1449.6	-1244.5
	-297.0	-203.6	7.2	-2.6	1353.3	1002.9
	-297.0	-203.6	7.2	2.6	1225.2	7499.8
	283.6	-195.9	6.7	3.1	1449.6	1244.5
209.	-283.6	195.9	-6.7	-3.1	-884.6	15163.9
	-297.0	-203.6	7.2	-2.6	1353.3	1002.9
	-297.0	-203.6	7.2	2.6	-935.3	16025.5
	283.6	-195.9	6.7	3.1	884.6	-15163.9
251.	-283.6	195.9	-6.7	-3.1	-602.1	23368.1
	-297.0	-203.6	7.2	-2.6	635.4	-24551.2
	-297.0	-203.6	7.2	2.6	-635.4	24551.2
	283.6	-195.9	6.7	3.1	602.1	-23368.1
293.	-283.6	195.9	-6.7	-3.1	-337.1	3157.3
	-297.0	-203.6	7.2	-2.6	335.4	-3307.9
	-297.0	-203.6	7.2	2.6	-335.4	3307.9
	283.6	-195.9	6.7	3.1	337.1	-3157.3
335.	-283.6	195.9	-6.7	-3.1	-37.0	39776.6
	-297.0	-203.6	7.2	-2.6	35.4	-4168.6
	-297.0	-203.6	7.2	2.6	-35.4	4168.6
	283.6	-195.9	6.7	3.1	37.0	-39776.6
Asta	150	noth	760	963	37.0	
PROG.	NOB	TYT	TZZ	TORS	MYV	MZZ
	-40.8	0.0	0.0	0.0	0.7	0.0
	73.2	0.0	0.0	0.0	-1.0	0.0
	-73.2	0.0	0.0	0.0	1.0	0.0
34.	-40.8	0.0	0.0	0.0	-0.7	0.0
	73.2	0.0	0.0	0.0	0.5	0.0
	73.2	0.0	0.0	0.0	-0.7	0.0
	-73.2	0.0	0.0	0.0	0.7	0.0
67.	-40.8	0.0	0.0	0.0	-0.5	0.0
	-40.8	0.0	0.0	0.0	0.2	0.0
	73.2	0.0	0.0	0.0	-0.4	0.0
	-73.2	0.0	0.0	0.0	0.4	0.0
101.	-40.8	0.0	0.0	0.0	-0.2	0.0
	-40.8	0.0	0.0	0.0	0.8	0.0
	73.2	0.0	0.0	0.0	-0.1	0.0
	-73.2	0.0	0.0	0.0	0.1	0.0
135.	-40.8	0.0	0.0	0.0	0.0	0.0
	-40.8	0.0	0.0	0.0	-0.2	0.0
	73.2	0.0	0.0	0.0	0.2	0.0
	-73.2	0.0	0.0	0.0	-0.2	0.0
168.	-40.8	0.0	0.0	0.0	-0.4	0.0
	73.2	0.0	0.0	0.0	0.5	0.0
	-73.2	0.0	0.0	0.0	-0.5	0.0
	-40.8	0.0	0.0	0.0	0.4	0.0
202.	-40.8	0.0	0.0	0.0	-0.6	0.0
	73.2	0.0	0.0	0.0	0.8	0.0
	-73.2	0.0	0.0	0.0	-0.8	0.0
	-40.8	0.0	0.0	0.0	0.6	0.0
236.	-40.8	0.0	0.0	0.0	-0.8	0.0
	73.2	0.0	0.0	0.0	1.0	0.0
	-73.2	0.0	0.0	0.0	-1.1	0.0
	-40.8	0.0	0.0	0.0	0.8	0.0
269.	-40.8	0.0	0.0	0.0	-1.0	0.0
	73.2	0.0	0.0	0.0	1.4	0.0
	-73.2	0.0	0.0	0.0	-1.4	0.0
	-40.8	0.0	0.0	0.0	1.0	0.0
Asta	154	noth	973	1103	37.0	
PROG.	NOB	TYT	TZZ	TORS	MYV	MZZ
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
29.	-3.9	0.0	0.0	0.0	0.0	0.0
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
58.	-3.9	0.0	0.0	0.0	0.0	0.0
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
86.	-3.9	0.0	0.0	0.0	0.0	0.0
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
115.	-3.9	0.0	0.0	0.0	0.0	0.0
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
144.	-3.9	0.0	0.0	0.0	0.0	0.0
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
173.	-3.9	0.0	0.0	0.0	0.0	0.0
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
201.	-3.9	0.0	0.0	0.0	0.0	0.0
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
230.	-3.9	0.0	0.0	0.0	0.0	0.0
	3.9	0.0	0.0	0.0	0.0	0.0
	-4.0	0.0	0.0	0.0	0.0	0.0
	4.0	0.0	0.0	0.0	0.0	0.0
Asta	-3.9	noth	972	1101	37.0	
	NOB	TYT	TZZ	TORS	MYV	MZZ
	105.6	-0.3	-0.1	0.0	0.0	0.0
	-101.7	-0.4	0.1	0.0	0.0	0.0
29.	101.7	0.4	-0.1	0.0	0.0	0.0
	-105.6	0.3	0.1	0.0	0.0	0.0
	105.6	-0.3	-0.1	0.0	1.5	-9.7
	-101.7	-0.4	0.1	0.0	-1.6	-11.0
58.	101.7	0.4	-0.1	0.0	1.6	11.0
	-105.6	0.3	0.1	0.0	-1.5	9.7
	105.6	-0.3	-0.1	0.0	3.0	-29.4
	-101.7	-0.4	0.1	0.0	-3.2	-22.0
86.	101.7	0.4	-0.1	0.0	7.9	44.9
	-105.6	0.3	0.1	0.0	-3.0	19.4
	105.6	-0.3	-0.1	0.0	4.5	-4.1
	-101.7	-0.4	0.1	0.0	-4.7	-33.0
115.	101.7	0.4	-0.1	0.0	4.7	33.0
	-105.6	0.3	0.1	0.0	-4.6	-38.8
	105.6	-0.3	-0.1	0.0	6.1	-38.8
	-101.7	-0.4	0.1	0.0	-6.3	-44.0
144.	101.7	0.4	-0.1	0.0	6.3	44.0
	-105.6	0.3	0.1	0.0	-7.6	-38.8
	105.6	-0.3	-0.1	0.0	7.6	-46.5
	-101.7	-0.4	0.1	0.0	-7.9	-55.5
173.	101.7	0.4	-0.1	0.0	7.9	55.5
	-105.6	0.3	0.1	0.0	-7.6	48.0
	105.6	-0.3	-0.1	0.0	9.1	-40.2
	-101.7	-0.4	0.1	0.0	-9.5	-66.0
201.	101.7	0.4	-0.1	0.0	9.5	66.0
	-105.6	0.3	0.1	0.0	-9.1	48.2
	105.6	-0.3	-0.1	0.0	10.6	-67.9
	-101.7	-0.4	0.1	0.0	-10.6	-77.0
230.	101.7	0.4	-0.1	0.0	11.1	77.0
	-105.6	0.3	0.1	0.0	-11.1	67.9
	105.6	-0.3	-0.1	0.0	12.2	-77.7
	-101.7	-0.4	0.1	0.0	-12.2	-88.0
86.	101.7	0.4	-0.1	0.0	12.2	88.0

0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2	359	46.7	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
4.0	4.0	51.9	0.0	100.0	-7.4		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-13.9	-21.9	0.0	0.0	-1.2	-630.2	410.	-46.7	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9	0.0	0.0	-2.3	-1204.6		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	3.9	41.9	0.0	78.5	-7.3		13.9	21.9	0.0	0.0	1.2	630.2		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-4.0	-53.9	0.0	-100.0	7.4		-13.9	-21.9	0.0	0.0	-1.2	-630.2		-100.6	0.0	0.0	0.0	0.0	0.0	-64.1	1.7	482.9	0.0	-114012.2	-3188.4
0.0	4.0	53.9	0.0	66.6	-4.9		16.7	20.9	0.0	0.0	2.3	1204.6		100.6	0.0	0.0	0.0	0.0	0.0	64.1	-1.7	-482.9	0.0	-114012.2	3188.4
0.0	-3.9	-41.9	0.0	-78.5	7.3		-16.7	-20.9																	

Asta	PROGR.	176	NORM	TYV	959	742	TORS	MYV	MZZ	-133.7	-462.6	-0.1	-8.9	15.6	23240.1	-56.4	-43.8	9.2	59.8	-874.2	-592.0	-535.1	444.6	-24.3	71.7	735.5	-29279.9
15.	0.	-1089.3	129.6	247.5	0.0	-66396.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
30.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
45.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
60.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
75.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
90.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
105.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
120.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
135.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
150.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
165.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
180.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
195.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
210.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
225.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
240.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
255.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
270.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
285.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
300.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
315.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
330.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
345.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
360.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
375.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
390.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
405.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
420.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
435.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
450.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
465.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
480.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3	-30.3	53.3	21363.3	38.2	-57.5	-3.0	18.7	393.5	-89.4	840.8	462.3	22.7	43.6	-954.8	-31262.1
495.	0.	-1089.3	129.6	247.5	0.0	-63245.0	-1330.9	-273.9	64.2	3976.7	-29.2	-0.3</															

58/136

0.7	9.4	1.5	-70.4	137.6	2214.3
-13.2	28.2	-0.1	115.2	-13.5	2393.2
-13.2	-27.5	-1.1	-98.2	137.5	2393.2
-1.3	-56.7	-0.5	92.2	-45.1	2148.7
-0.7	-51.4	-1.5	94.4	151.2	2746.9
-13.2	-27.7	-0.1	115.2	-13.5	2393.2
-1.3	-116.3	1.1	-98.3	99.5	1908.3
-13.2	-91.5	-0.5	92.2	-45.1	2148.7
-13.2	-132.2	-1.1	-98.3	124.8	2031.9
-13.7	-91.5	-0.1	115.2	-13.5	2393.2
-13.7	-149.1	-1.1	-98.3	130.0	2119.4
-1.3	-178.4	-0.5	92.2	-45.0	2173.2
-0.7	-177.1	-1.5	94.4	151.2	2746.9
-13.2	-154.0	-0.1	115.2	-8.6	1902.7
-13.2	-239.0	-1.1	-98.3	62.2	1216.6
-1.3	-239.2	-0.5	92.2	-46.4	1371.2
-0.7	-238.9	-1.5	70.4	17.1	1425.7
-13.7	-300.0	-1.1	-98.3	-6.9	913.6
-13.7	-294.7	-1.5	-70.4	45.5	9631.3
-13.2	-279.0	-0.1	115.2	-13.5	2393.2
-13.7	-279.6	-1.1	-98.3	25.4	1025.6
-1.3	-360.9	-0.5	92.2	-45.7	2173.2
-0.7	-360.9	-1.5	70.4	17.1	1425.7
-13.2	-360.9	-0.1	115.2	-3.6	612.8
-13.2	-440.5	-1.1	-98.3	18.4	1314.3
-1.3	-421.7	-0.5	92.2	12.2	-363.2
-0.7	-421.4	-1.5	70.4	17.1	-363.2
-13.2	-397.7	-0.1	115.2	-1.9	-294.0
145	noth	760	760	MY	MZZ
-377.1	-40.0	19.2	0.0	96.2	199.9
-377.1	-33.9	6.3	0.0	29.6	161.1
-377.1	-33.9	6.3	0.0	31.5	169.7
-377.1	-42.9	-18.7	0.0	-93.7	-74.4
-377.0	-40.0	19.2	0.0	94.4	174.9
-377.0	36.9	-5.8	0.0	-25.4	-161.5
-377.0	36.9	-5.8	0.0	27.2	161.5
-377.0	-42.9	-18.7	0.0	-82.0	-187.9
-376.9	-40.0	19.2	0.0	94.4	174.9
-376.9	36.9	-5.8	0.0	-23.6	-127.3
-376.9	36.9	-5.8	0.0	25.4	127.3
-376.7	-40.0	19.2	0.0	60.1	124.9
-376.7	-40.0	19.2	0.0	60.1	124.9
-376.7	-33.9	6.3	0.0	29.6	161.1
-376.7	-33.9	6.3	0.0	31.5	169.7
-376.7	42.9	-18.7	0.0	-58.6	-146.2
-376.6	36.9	-5.8	0.0	-48.6	-9.9
-376.6	36.9	-5.8	0.0	-45.5	-92.3
-376.6	-42.9	-18.7	0.0	-36.4	-135.7
-376.6	-42.9	-18.7	0.0	-46.9	-107.4
-376.4	-40.0	19.2	0.0	94.4	174.9
-376.4	36.9	-5.8	0.0	-10.9	-69.2
-376.4	-33.9	6.3	0.0	11.8	63.6
-376.4	-33.9	6.3	0.0	13.7	63.6
-376.3	-40.0	19.2	0.0	24.0	50.0
-376.3	-40.0	19.2	0.0	24.0	50.0
-376.3	-33.9	6.3	0.0	29.6	161.1
-376.3	-33.9	6.3	0.0	31.5	169.7
-376.2	-40.0	19.2	0.0	12.0	42.4
-376.2	-40.0	19.2	0.0	12.0	42.4
-376.2	36.9	-5.8	0.0	-3.6	-23.1
-376.2	36.9	-5.8	0.0	-3.7	-23.1
-376.2	-42.9	-18.7	0.0	-11.7	-26.8
-376.0	-40.0	19.2	0.0	94.4	174.9
-376.0	36.9	-5.8	0.0	0.0	0.0
-376.0	36.9	-5.8	0.0	0.0	0.0
-376.0	-42.9	-18.7	0.0	0.0	0.0
145	noth	760	213	MY	MZZ
125.2	-376.0	0.0	0.0	-0.4	0.8
125.2	-376.0	0.0	0.0	-0.5	0.8
-99.1	-376.0	0.0	0.0	-0.2	0.8
146.1	-376.0	0.0	0.0	0.5	0.8
125.2	-376.0	0.0	0.0	-0.1	-948.7
119.9	-282.0	0.0	0.0	0.2	-948.7
119.9	-282.0	0.0	0.0	0.2	-948.7
146.1	-282.0	0.0	0.0	0.4	-948.7
125.2	-188.0	0.0	0.0	-0.3	-1621.6
119.9	-188.0	0.0	0.0	-0.3	-1621.6
-99.1	-188.0	0.0	0.0	-0.1	-1621.6
146.1	-188.0	0.0	0.0	-0.1	-1621.6
125.2	-94.0	0.0	0.0	-0.2	-2069.7
119.9	-94.0	0.0	0.0	-0.2	-2069.7
-99.1	-94.0	0.0	0.0	-0.1	-2069.7
146.1	-94.0	0.0	0.0	0.3	-2069.7
119.9	0.0	0.0	0.0	0.3	-2162.1
-99.1	0.0	0.0	0.0	0.3	-2162.1
146.1	0.0	0.0	0.0	0.2	-2162.1
125.2	94.0	0.0	0.0	-0.1	-2069.9
119.9	94.0	0.0	0.0	-0.1	-2069.9
-99.1	94.0	0.0	0.0	-0.1	-2069.9
146.1	94.0	0.0	0.0	-0.1	-2069.9
125.2	-188.0	0.0	0.0	-0.1	-1621.6
119.9	-188.0	0.0	0.0	-0.1	-1621.6
-99.1	-188.0	0.0	0.0	-0.0	-1621.6
146.1	-188.0	0.0	0.0	0.1	-1621.6
125.2	-94.0	0.0	0.0	-0.1	-1621.6
119.9	-94.0	0.0	0.0	-0.1	-1621.6
-99.1	-94.0	0.0	0.0	0.0	-949.3
146.1	-94.0	0.0	0.0	0.1	-949.3
125.2	-376.0	0.0	0.0	0.0	0.0
119.9	-376.0	0.0	0.0	0.0	0.0
-99.1	-376.0	0.0	0.0	0.0	0.0
146.1	-376.0	0.0	0.0	0.0	0.0
145	noth	773	754	MY	MZZ
-1768.5	88.6	-66.9	317.6	17700.4	-8530.4
-613.3	56.4	-27.2	155.2	4670.6	-8767.5
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-413.5	62.1	-22.6	131.5	4258.3	-8762.2
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-612.9	56.4	-27.2	155.2	4687.6	-8767.5
-1588.7	88.6	-66.9	317.6	17700.4	-8530.4
-413.1	62.1	-22.6	131.5	2277.4	-8728.4
-1767.7	88.6	-66.9	317.6	17784.1	-8416.6
-612.5	56.4	-27.2	155.2	4687.6	-8767.5
-1587.9	88.6	-66.9	317.6	17784.1	-8416.6
-1767.3	88.6	-66.9	317.6	17825.9	-8364.7
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-412.4	62.1	-22.6	131.5	2300.7	-8650.7
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-611.8	56.4	-27.2	155.2	4738.5	-8722.4
-1587.5	88.6	-66.9	317.6	17825.9	-8364.7
-412.0	62.1	-22.6	131.5	2314.8	-8611.9
-1766.5	88.6	-66.9	317.6	17909.5	-8253.5
-611.4	56.4	-27.2	155.2	4738.5	-8722.4
-1586.8	88.6	-66.9	317.6	17948.0	-8039.5
-1586.8	88.6	-66.9	317.6	17948.0	-8039.5
-1766.2	88.6	-66.9	317.6	17961.3	-8128.1
-1586.8	88.6	-66.9	317.6	17961.3	-8128.1
-1586.4	94.3	-62.2	293.9	15522.0	-7983.2
-411.2	62.1	-22.6	131.5	2343.1	-8534.3
-1586.2	88.6	-66.9	317.6	17961.3	-8128.1

		-610.6	56.4	-27.2	155.2	4789.5	-7721.6
		-1566.0	64.3	-62.4	239.9	13560.9	-8921.6
		-410.8	62.4	-31.5	76.6	2400.5	-8495.5
		-1765.4	88.6	-66.9	137.6	1803.0	-8087.4
		-610.2	56.4	-27.2	155.2	4789.5	-7721.6
		-1566.0	64.3	-62.4	239.9	13560.9	-8921.6
		-410.5	62.1	-32.6	131.5	2371.4	-8456.7
ASTR.	147						
PGC	NORM	TY	TZ	TORS	MY	MZ	
	-398.4	7.5	-5.5	11.0	-3343.0	-7675.3	
	-742.5	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-386.0	7.5	-5.5	11.0	-3343.0	-7675.3	
	-779.2	4.2	-15.1	7.6	-4132.4	-7907.6	
	-327.7	7.5	-5.5	11.0	-3343.0	-7675.3	
	-716.8	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-310.3	11.9	-7.2	-3.4	-5234.3	-7955.1	
	-753.3	4.2	-15.1	7.6	-4132.4	-7907.6	
	-347.1	7.5	-5.5	11.0	-3343.0	-7675.3	
	-691.1	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-284.6	11.9	-7.2	-3.4	-5234.3	-7955.1	
	-327.7	7.5	-5.5	11.0	-3343.0	-7675.3	
	-341.4	7.5	-5.5	11.0	-3343.0	-7675.3	
	-465.5	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-259.0	11.9	-7.2	-3.4	-5234.3	-7955.1	
	-702.2	4.2	-15.1	7.6	-4132.4	-7907.6	
	-75.7	7.5	-5.5	11.0	-3343.0	-7675.3	
	-639.8	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-233.3	11.9	-7.2	-3.4	-5234.3	-7955.1	
	-495.3	4.2	-15.1	7.6	-4132.4	-7907.6	
	-270.0	7.5	-5.5	11.0	-3343.0	-7675.3	
	-614.1	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-207.6	11.9	-7.2	-3.4	-5234.3	-7955.1	
	-650.8	4.2	-15.1	7.6	-4132.4	-7907.6	
	-244.4	7.5	-5.5	11.0	-3343.0	-7675.3	
	-588.4	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-182.0	11.9	-7.2	-3.4	-5234.3	-7955.1	
	-625.2	4.2	-15.1	7.6	-4132.4	-7907.6	
	-218.7	7.5	-5.5	11.0	-3343.0	-7675.3	
	-562.8	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-456.3	11.9	-7.2	-3.4	-5234.3	-7955.1	
	-509.5	4.2	-15.1	7.6	-4132.4	-7907.6	
	-193.0	7.5	-5.5	11.0	-3343.0	-7675.3	
	-557.1	8.6	-13.8	-6.8	-4440.6	-8859.6	
	-130.6	11.9	-7.2	-3.4	-5234.3	-7955.1	
ASTR.	148						
PGC	NORM	TY	TZ	TORS	MY	MZ	
	-3302.8	11.1	-10.6	304.1	1530.2	3227.9	
	-1575.0	0.0	30.3	161.0	-8013.2	3241.9	
	-1106.3	-3.3	-4.7	283.8	1684.6	3078.7	
	-1658.5	-14.4	36.2	140.8	-10684.7	4768.0	
	-1022.4	11.1	-10.6	304.1	1536.8	3154.4	
	-1574.6	0.0	30.3	161.0	-8013.2	3241.9	
	-1105.9	-3.3	-4.7	283.8	1687.5	3076.6	
	-1658.1	-14.4	36.2	140.8	-10571.5	4777.0	
	-1022.0	11.1	-10.6	304.1	1545.4	3211.4	
	-1574.2	0.0	30.3	161.0	-8411.1	3207.5	
	-1105.5	-3.3	-4.7	283.8	1687.5	3076.6	
	-1657.8	-14.4	36.2	140.8	-10594.1	4768.0	
	-1021.6	11.1	-10.6	304.1	1553.8	3233.3	
	-1573.9	0.0	30.3	161.0	-8160.1	3214.8	
	-1105.2	-3.3	-4.7	283.8	1693.3	3075.5	
	-1657.4	-14.4	36.2	140.8	-10617.0	4773.0	
	-1021.3	11.1	-10.6	304.1	1516.7	3153.2	
	-1573.5	0.0	30.3	161.0	-8145.4	3214.8	
	-1104.8	-3.3	-4.7	283.8	1696.3	3070.4	
	-1657.0	-14.4	36.2	140.8	-10639.4	4750.0	
	-1020.9	11.1	-10.6	304.1	1545.1	3211.4	
	-1573.1	0.0	30.3	161.0	-8198.0	3214.8	
	-1105.5	-3.3	-4.7	283.8	1696.3	3076.6	
	-1656.6	-14.4	36.2	140.8	-10662.1	4741.0	
	-1020.5	11.1	-10.6	304.1	1545.0	3211.4	
	-1572.7	0.0	30.3	161.0	-8216.9	3214.8	
	-1104.0	-3.3	-4.7	283.8	1702.1	3066.3	
	-1656.2	-14.4	36.2	140.8	-10684.7	4732.0	
	-1020.1	11.1	-10.6	304.1	1576.6	3156.0	
	-1572.3	0.0	30.3	161.0	-8216.9	3214.8	
	-1103.6	-3.3	-4.7	283.8	1705.1	3064.2	
	-1655.8	-14.4	36.2	140.8	-10707.4	4723.0	
	-1019.7	11.1	-10.6	304.1	1585.9	3214.8	
	-1571.9	0.0	30.3	161.0	-8254.8	3214.8	
	-1103.2	-3.3	-4.7	283.8	1708.0	3062.2	
	-1655.5	-14.4	36.2	140.8	-10730.0	4714.1	
ASTR.	149						
PGC	NORM	TY	TZ	TORS	MY	MZ	
	-1023.0	13.7	13.1	6.9	898.7	1557.8	
	-1004.2	1.3	12.2	-1.9	630.8	3089.7	
	-998.9	-0.7	14.1	-7.3	6126.1	3079.9	
	-1013.2	-1.3	14.1	-7.3	6600.7	4709.0	
	-997.3	13.7	13.1	6.9	4727.8	2131.9	
	-978.6	0.7	19.3	12.2	5493.6	3261.4	
	-971.3	-0.7	14.1	-7.3	6126.1	3079.9	
	-954.5	-13.2	20.5	-1.9	5740.4	4157.9	
	-971.6	1.3	14.1	6.9	4727.8	2131.9	
	-952.9	1.3	19.3	12.2	4684.3	3314.1	
	-957.6	1.3	14.1	-7.3	6126.1	3079.9	
	-908.8	-13.2	20.5	-1.9	4880.6	3605.9	
	-946.0	13.7	13.1	6.9	3179.0	2820.0	
	-927.2	1.3	12.2	-1.9	630.8	3089.7	
	-921.9	-0.7	14.1	-7.3	6324.7	2967.2	
	-935.2	-1.3	14.1	-7.3	6030.8	3089.7	
	-903.3	13.7	13.1	6.9	2629.1	3854.1	
	-901.3	-0.7	19.3	12.2	5365.9	3419.5	
	-896.2	-0.7	14.1	-7.3	6324.7	2967.2	
	-877.5	-13.2	20.5	-1.9	3161.0	2502.0	
	-873.7	13.7	13.1	6.9	3924.6	3868.8	
	-875.9	1.3	19.3	12.2	2556.6	3472.1	
	-870.6	-0.7	14.1	-7.3	6324.7	2967.2	
	-851.8	-13.2	20.5	-1.9	2301.2	1950.0	
	-860.9	13.7	13.1	6.9	1529.2	5002.2	
	-849.2	1.3	19.3	12.2	4447.4	3800.0	
	-844.9	-0.7	14.1	-7.3	6253.3	2873.4	
	-845.1	-0.7	14.1	-7.3	6441.8	3800.0	
	-843.3	13.7	13.1	6.9	979.3	5576.3	
	-834.5	1.3	19.3	12.2	3825.2	3847.8	
	-819.2	-0.7	14.1	-7.3	927.8	2844.8	
	-800.5	-13.2	20.5	-1.9	181.6	846.0	
	-817.6	13.7	13.1	6.9	429.4	6302.4	
	-798.8	1.3	19.3	12.2	12.1	3630.2	
	-793.5	-0.7	14.1	-7.3	322.4	24.4	
	-774.8	-13.2	20.5	-1.9	-278.1	294.0	
ASTR.	150						
PGC	NORM	TY	TZ	TORS	MY	MZ	
	38.3	0.0	0.0	0.4	-0.4	0.7	
	18.2	0.0	0.0	0.4	-0.4	0.7	
	18.2	0.0	0.0	0.4	-0.4	0.7	
	38.3	0.0	0.0	0.4	-0.4	0.7	
	-27.8	0.0	0.0	0.4	0.3	0.7	
	38.3	0.0	0.0	0.4	-0.4	0.7	
	-47.9	0.0	0.0	0.4	0.4	0.7	
	38.3	0.0	0.0	0.4	-0.4	0.7	
	-47.9	0.0	0.0	0.4	0.3	0.7	
	38.3	0.0	0.0	0.4	0.4	0.7	
	-47.9	0.0	0.0	0.4	0.3	0.7	
	38.3	0.0	0.0	0.4	0.4	0.7	
	-47.9	0.0	0.0	0.4	0.3	0.7	
	38.3	0.0	0.0	0.4	0.4	0.7	

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Asta	PROGR.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	12.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.	26.	27.	28.	29.	30.	31.	32.	33.	34.	35.	36.	37.	38.	39.	40.	41.	42.	43.	44.	45.	46.	47.	48.	49.	50.	51.	52.	53.	54.	55.	56.	57.	58.	59.	60.	61.	62.	63.	64.	65.	66.	67.	68.	69.	70.	71.	72.	73.	74.	75.	76.	77.	78.	79.	80.	81.	82.	83.	84.	85.	86.	87.	88.	89.	90.	91.	92.	93.	94.	95.	96.	97.	98.	99.	100.	101.	102.	103.	104.	105.	106.	107.	108.	109.	110.	111.	112.	113.	114.	115.	116.	117.	118.	119.	120.	121.	122.	123.	124.	125.	126.	127.	128.	129.	130.	131.	132.	133.	134.	135.	136.	137.	138.	139.	140.	141.	142.	143.	144.	145.	146.	147.	148.	149.	150.	151.	152.	153.	154.	155.	156.	157.	158.	159.	160.	161.	162.	163.	164.	165.	166.	167.	168.	169.	170.	171.	172.	173.	174.	175.	176.	177.	178.	179.	180.	181.	182.	183.	184.	185.	186.	187.	188.	189.	190.	191.	192.	193.	194.	195.	196.	197.	198.	199.	200.	201.	202.	203.	204.	205.	206.	207.	208.	209.	210.	211.	212.	213.	214.	215.	216.	217.	218.	219.	220.	221.	222.	223.	224.	225.	226.	227.	228.	229.	230.
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PROGR.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.	12.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.	26.	27.	28.	29.	30.	31.	32.	33.	34.	35.	36.	37.	38.	39.	40.	41.	42.	43.	44.	45.	46.	47.	48.	49.	50.	51.	52.	53.	54.	55.	56.	57.	58.	59.	60.	61.	62.	63.	64.	65.	66.	67.	68.	69.	70.	71.	72.	73.	74.	75.	76.	77.	78.	79.	80.	81.	82.	83.	84.	85.	86.	87.	88.	89.	90.	91.	92.	93.	94.	95.	96.	97.	98.	99.	100.	101.	102.	103.	104.	105.	106.	107.	108.	109.	110.	111.	112.	113.	114.	115.	116.	117.	118.	119.	120.	121.	122.	123.	124.	125.	126.	127.	128.	129.	130.	131.	132.	133.	134.	135.	136.	137.	138.	139.	140.	141.	142.	143.	144.	145.	146.	147.	148.	149.	150.	151.	152.	153.	154.	155.	156.	157.	158.	159.	160.	161.	162.	163.	164.	165.	166.	167.	168.	169.	170.	171.	172.	173.	174.	175.	176.	177.	178.	179.	180.	181.	182.	183.	184.	185.	186.	187.	188.	189.	190.	191.	192.	193.	194.	195.	196.	197.	198.	199.	200.	201.	202.	203.	204.	205.	206.	207.	208.	209.	210.	211.	212.	213.	214.	215.	216.	217.	218.	219.	220.	221.	222.	223.	224.	225.	226.	227.	228.	229.	230.	231.	232.	233.	234.	235.	236.	237.	238.	239.	240.	241.	242.	243.	244.	245.	246.	247.	248.	249.	250.	251.	252.	253.	254.	255.	256.	257.	258.	259.	260.	261.	262.	263.	264.	265.	266.	267.	268.	269.	270.	271.	272.	273.	274.	275.	276.	277.	278.	279.	280.	281.	282.	283.	284.	285.	286.	287.	288.	289.	290.	291.	292.	293.	294.	295.	296.	297.	298.	299.	300.	301.	302.	303.	304.	305.	306.	307.	308.	309.	310.	311.	312.	313.	314.	315.	316.	317.	318.	319.	320.	321.	322.	323.	324.	325.	326.	327.	328.	329.	330.	331.	332.	333.	334.	335.	336.	337.	338.	339.	340.	341.	342.	343.	344.	345.	346.	347.	348.	349.	350.	351.	352.	353.	354.	355.	356.	357.	358.	359.	360.	361.	362.	363.	364.	365.	366.	367.	368.	369.	370.	371.	372.	373.	374.	375.	376.	377.	378.	379.	380.	381.	382.	383.	384.	385.	386.	387.	388.	389.	390.	391.	392.	393.	394.	395.	396.	397.	398.	399.	400.	401.	402.	403.	404.	405.	406.	407.	408.	409.	410.	411.	412.	413.	414.	415.	416.	417.	418.	419.	420.	421.	422.	423.	424.	425.	426.	427.	428.	429.	430.	431.	432.	433.	434.	435.	436.	437.	438.	439.	440.	441.	442.	443.	444.	445.	446.	447.	448.	449.	450.	451.	452.	453.	454.	455.	456.	457.	458.	459.	460.	461.	462.	463.	464.	465.	466.	467.	468.	469.	470.	471.	472.	473.	474.	475.	476.	477.	478.	479.	480.	481.	482.	483.	484.	485.	486.	487.	488.	489.	490.	491.	492.	493.	494.	495.	496.	497.	498.	499.	500.	501.	502.	503.	504.	505.	506.	507.	508.	509.	510.	511.	512.	513.	514.	515.	516.	517.	518.	519.	520.	521.	522.	523.	524.	525.	526.	527.	528.	529.	530.	531.	532.	533.	534.	535.	536.	537.	538.	539.	540.	541.	542.	543.	544.	545.	546.	547.	548.	549.	550.	551.	552.	553.	554.	555.	556.	557.	558.	559.	560.	561.	562.	563.	564.	565.	566.	567.	568.	569.	570.	571.	572.	573.	574.	575.	576.	577.	578.	579.	580.	581.	582.	583.	584.	585.	586.	587.	588.	589.	590.	591.	592.	593.	594.	595.	596.	597.	598.	599.	600.	601.	602.	603.	604.	605.	606.	607.	608.	609.	610.	611.	612.	613.	614.	615.	616.	617.	618.	619.	620.	621.	622.	623.	624.	625.	626.	627.	628.	629.	630.	631.	632.	633.	634.	635.	636.	637.	638.	639.	640.	641.	642.	643.	644.	645.	646.	647.	648.	649.	650.	651.	652.	653.	654.	655.	656.	657.	658.	659.	660.	661.	662.	663.	664.	665.	666.	667.	668.	669.	670.	671.	672.	673.	674.	675.	676.	677.	678.	679.	680.	681.	682.	683.	684.	685.	686.	687.	688.	689.	690.	691.	692.	693.	694.	695.	696.	697.	698.	699.	700.	701.	702.	703.	704.	705.	706.	707.	708.	709.	710.	711.	712.	713.	714.	715.	716.	717.	718.	719.	720.	721.	722.	723.	724.	725.	726.	727.	728.	729.	730.	731.	732.	733.	734.	735.	736.	737.	738.	739.	740.	741.	742.	743.	744.	745.	746.	747.	748.	749.	750.	751.	752.	753.	754.	755.	756.	757.	758.	759.	760.	761.	762.	763.	764.	765.	766.	767.	768.	769.	770.	771.	772.	773.	774.	775.	776.	777.	778.	779.	780.	781.	782.	783.	784.	785.	786.	787.	788.	789.	790.	791.	792.	793.	794.	795.	796.	797.	798.	799.	800.	801.	802.	803.	804.	805.	806.	807.	808.	809.	810.	811.	812.	813.	814.	815.	816.	817.	818.	819.	820.	821.	822.	823.	824.	825.	826.	827.	828.	829.	830.	831.	832.	833.	834.	835.	836.	837.	838.	839.	840.	841.	842.	843.	844.	845.	846.	847.	848.	849.	850.	851.	852.	853.	854.	855.	856.	857.	858.	859.	860.	861.	862.	863.	864.	865.	866.	867.	868.	869.	870.	871.	872.	873.	874.	875.	876.	877.	878.	879.	880.	881.	882.	883.	884.	885.	886.	887.	888.	889.	890.	891.	892.	893.	894.	895.	896.	897.	898.	899.	900.	901.	902.	903.	904.	905.	906.	907.	908.	909.	910.	911.	912.	913.	914.	915.	916.	917.	918.	919.	920.	921.	922.	923.	924.	925.	926.	927.	928.	929.	930.	931.	932.	933.	934.	935.	936.	937.	938.	939.	940.	941.	942.	943.	944.	945.	946.	947.	948.	949.	950.	951.	952.	953.	954.	955.	956.	957.	958.	959.	960.	961.	962.	963.	964.	965.	966.	967.	968.	969.	970.	971.	972.	973.	974.	975.	976.	977.	978.	979.	980.	981.	982.	983.	984.	985.	986.	987.	988.	989.	990.	991.	992.	993.	994.	995.	996.	997.	998.	999.	1000.
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69/136

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25.	122.8	0.0	0.0	0.0	0.0	4.	-869.9	3.5	-4148.2	0.0	-5185.2	-4.4	0.	-6083.5	20.1	14.9	0.0	3316.4	13564.5	3.	-595.5	-272.0	290.5	0.0	469.6	510.0					
50.	122.8	0.0	0.0	0.0	0.0	4.	-869.7	3.5	-4148.2	0.0	-2592.6	-2.2	41.	-6082.2	20.1	14.9	0.0	2700.3	14391.8	4.	-595.3	-272.0	290.5	0.0	313.1	340.0					
74.	122.8	0.0	0.0	0.0	0.0	5.	-869.6	3.5	-4148.2	0.0	-6032.9	0.0	85.	-6032.9	20.1	14.9	0.0	2064.2	15202.0	5.	-595.2	-272.0	290.5	0.0	156.5	170.0					
99.	122.8	0.0	0.0	0.0	0.0	Asta	99	ndi	964	339	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	5.	-595.1	-272.0	290.5	0.0	0.0	0.0	0.0						
124.	122.8	0.0	0.0	0.0	0.0	PROGR.	124	ndi	964	339	105.	-5982.3	20.1	14.9	0.0	852.1	16073.8	Asta	130	ndi	752	468	MY	NZZ							
149.	122.8	0.0	0.0	0.0	0.0	PROGR.	149	ndi	964	339	206.	-5957.0	20.1	14.9	0.0	2700.1	15202.0	PROGR.	130	ndi	752	468	MY	NZZ							
174.	122.8	0.0	0.0	0.0	0.0	1.	-1923.1	16.2	45.7	0.0	200.1	-70.9	248.	-5931.7	20.1	14.9	0.0	-380.1	18528.4	0.	-714.5	-595.1	-0.3	0.0	0.0						
198.	122.8	0.0	0.0	0.0	0.0	2.	-1923.0	16.2	45.7	0.0	171.5	-60.7	289.	-5906.4	20.1	14.9	0.0	-296.2	19155.7	0.	-714.5	-595.1	-0.3	0.0	0.0						
Asta	75	ndi	760	212	MY	2.	-1922.8	16.2	45.7	0.0	140.9	-50.6	330.	-5881.2	20.1	14.9	0.0	-1612.2	20183.1	0.	-714.5	-595.1	-0.3	0.0	0.0						
PROGR.	75	ndi	760	212	MY	3.	-1922.7	16.2	45.7	0.0	118.4	-40.5	Asta	116	ndi	741	737	86.	-714.5	-187.2	-0.3	0.0	19.0	-2277.2							
33.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.6	16.2	45.7	0.0	85.7	-30.4	PROGR.	116	ndi	741	737	86.	-714.5	-187.2	-0.3	0.0	28.5	-2586.4							
66.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.4	16.2	45.7	0.0	57.2	-20.2	0.	-3793.3	-15.6	11.9	0.0	-2215.2	17264.7	0.	-714.5	-595.1	-0.3	0.0	0.0						
99.	-13.8	0.0	0.0	0.0	0.0	4.	-1922.3	16.2	45.7	0.0	30.0	-10.1	4.	-3792.8	-15.6	11.9	0.0	-2094.1	16622.4	0.	-714.5	-595.1	-0.3	0.0	0.0						
131.	-13.8	0.0	0.0	0.0	0.0	5.	-1922.1	16.2	45.7	0.0	0.0	0.0	14.	-3791.9	-15.6	11.9	0.0	-1393.0	19869.8	0.	-714.5	-595.1	-0.3	0.0	0.0						
165.	-13.8	0.0	0.0	0.0	0.0	Asta	100	ndi	760	212	124.	-6007.6	20.1	14.9	0.0	1468.2	16046.5	201.	-232.8	753.4	-0.4	0.0	66.4	20373.6							
198.	-13.8	0.0	0.0	0.0	0.0	PROGR.	100	ndi	760	212	165.	-3192.1	-15.6	11.9	0.0	-4170.8	14697.0	PROGR.	132	ndi	751	467	MY	NZZ							
264.	-13.8	0.0	0.0	0.0	0.0	0.	-2707.3	-29.4	-3.3	0.0	-16.4	146.8	206.	-3166.8	-15.6	11.9	0.0	-4659.7	14055.1	0.	-714.5	-595.1	-0.3	0.0	0.0						
PROGR.	78	ndi	976	471	MY	1.	-2707.2	-29.4	-3.3	0.0	-14.4	128.5	289.	-3166.8	-15.6	11.9	0.0	-4659.7	14055.1	0.	-714.5	-595.1	-0.3	0.0	0.0						
33.	-13.8	0.0	0.0	0.0	0.0	2.	-2706.9	-29.4	-3.3	0.0	-12.3	110.1	289.	-3166.8	-15.6	11.9	0.0	-4659.7	14055.1	0.	-714.5	-595.1	-0.3	0.0	0.0						
66.	-13.8	0.0	0.0	0.0	0.0	3.	-2706.7	-29.4	-3.3	0.0	-8.0	31.0	330.	-3192.1	-15.6	11.9	0.0	-4170.8	14697.0	0.	-714.5	-595.1	-0.3	0.0	0.0						
99.	-13.8	0.0	0.0	0.0	0.0	4.	-2706.6	-29.4	-3.3	0.0	-6.2	55.1	Asta	117	ndi	742	739	86.	-714.5	-187.2	-0.3	0.0	28.5	-2586.4							
131.	-13.8	0.0	0.0	0.0	0.0	4.	-2706.5	-29.4	-3.3	0.0	-4.1	38.7	PROGR.	117	ndi	742	739	86.	-714.5	-187.2	-0.3	0.0	28.5	-2586.4							
165.	-13.8	0.0	0.0	0.0	0.0	5.	-2706.3	-29.4	-3.3	0.0	-2.1	18.4	0.	-3516.2	-45.9	11.4	0.0	-1613.7	21067.7	0.	-714.5	-595.1	-0.3	0.0	0.0						
198.	-13.8	0.0	0.0	0.0	0.0	Asta	101	ndi	962	341	124.	-3440.4	-65.9	-111.4	0.0	2353.9	2898.8	115.	-581.0	-157.8	0.3	0.0	-34.9	2706.9							
264.	-13.8	0.0	0.0	0.0	0.0	PROGR.	101	ndi	962	341	165.	-3415.1	-65.9	-111.4	0.0	2353.9	2898.8	144.	-581.0	-157.8	0.3	0.0	-34.9	2706.9							
PROGR.	79	ndi	749	468	MY	0.	-2617.0	-12.4	-3.2	0.0	-15.9	61.9	206.	-3389.8	-65.9	-111.4	0.0	6834.9	2947.9	173.	-581.0	-157.8	0.3	0.0	-34.9	2706.9					
33.	-50.7	0.0	0.0	0.0	0.0	1.	-2616.8	-12.4	-3.2	0.0	-13.9	54.2	248.	-3364.5	-65.9	-111.4	0.0	11429.3	2075.0	29.	-232.8	-241.3	-0.4	0.0	21.2	-25316.0					
66.	-50.7	0.0	0.0	0.0	0.0	2.	-2616.6	-12.4	-3.2	0.0	-9.9	38.7	289.	-3339.2	-65.9	-111.4	0.0	16023.7	1837.1	58.	-232.8	-241.3	-0.4	0.0	21.2	-25316.0					
99.	-50.7	0.0	0.0	0.0	0.0	3.	-2616.4	-12.4	-3.2	0.0	-6.0	23.2	330.	-3319.1	-65.9	-111.4	0.0	20618.1	15131.9	86.	-232.8	-241.3	-0.4	0.0	21.2	-25316.0					
131.	-50.7	0.0	0.0	0.0	0.0	4.	-2616.3	-12.4	-3.2	0.0	-4.0	15.5	PROGR.	102	ndi	962	341	165.	-3415.1	-65.9	-111.4	0.0	2353.9	2898.8							
165.	-50.7	0.0	0.0	0.0	0.0	4.	-2616.1	-12.4	-3.2	0.0	-2.0	7.7	0.	-221.3	-290.0	18.9	56.0	2181.5	7093.6	144.	-232.8	-241.3	-0.4	0.0	21.2	-25316.0					
198.	-50.7	0.0	0.0	0.0	0.0	5.	-2615.9	-12.4	-3.2	0.0	0.0	0.0	35.	-221.3	-339.4	18.9	56.0	1520.4	62416.5	173.	-232.8	-241.3	-0.4	0.0	21.2	-25316.0					
264.	-50.7	0.0	0.0	0.0	0.0	Asta	102	ndi	962	341	165.	-3415.1	-65.9	-111.4	0.0	2353.9	2898.8	201.	-232.8	-241.3	-0.4	0.0	21.2	-25316.0							
PROGR.	79	ndi	749	468	MY	PROGR.	102	ndi	962	341	165.	-3415.1	-65.9	-111.4	0.0	2353.9	2898.8	221.	-232.8	-241.3	-0.4	0.0	21.2	-25316.0							
33.	-50.7	0.0	0.0	0.0	0.0	0.	-2008.2	15.0	-125.1	0.0	-425.4	-75.2	70.	-221.3	-339.4	18.9	56.0	859.2	30171.8	Asta	136	ndi	749	469	MY	NZZ					
66.	-50.7	0.0	0.0	0.0	0.0	1.	-2008.0	15.0	-125.1	0.0	-347.3	-65.8	88.	-221.3	-339.4	18.9	56.0	528.6	24275.8	PROGR.	136	ndi	749	469	MY	NZZ					
99.	-50.7	0.0	0.0	0.0	0.0	1.	-2007.9	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-1163.0	18.9	56.0	132.5	12063.5	PROGR.	136	ndi	749	469	MY	NZZ					
131.	-50.7	0.0	0.0	0.0	0.0	2.	-2007.7	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-1163.0	18.9	56.0	132.5	12063.5	PROGR.	136	ndi	749	469	MY	NZZ					
165.	-50.7	0.0	0.0	0.0	0.0	3.	-2007.5	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-1163.0	18.9	56.0	132.5	12063.5	PROGR.	136	ndi	749	469	MY	NZZ					
198.	-50.7	0.0	0.0	0.0	0.0	4.	-2007.3	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-1163.0	18.9	56.0	132.5	12063.5	PROGR.	136	ndi	749	469	MY	NZZ					
264.	-50.7	0.0	0.0	0.0	0.0	5.	-2007.1	15.0	-125.1	0.0	-469.0	-56.0	123.	-221.3	-1163.0	18.9	56.0	132.5	12063.5	PROGR.	136	ndi	749	469	MY	NZZ					
Asta	82	ndi	967	467	MY	Asta	104	ndi	967	467	466	MY	NZZ	PROGR.	104	ndi	967	467	466	MY	NZZ	PROGR.	104	ndi	967	467	MY	NZZ			
PROGR.	82	ndi	967	467	MY	PROGR.	104	ndi	967	467	466	MY	NZZ	PROGR.	104	ndi	967	467	466	MY	NZZ	PROGR.	104	ndi	967	467	MY	NZZ			
33.	-508.4	0.0	0.0	0.0	0.0	0.	-1683.4	-61.8	3997.8	0.0	17988.8	319.1	16.	-475.2	-590.2	1.7	-1359.9	-0.0	1252.4	86.	-236.4	-85.3	0.4	0.0	-36.1	18384.2					
66.	-508.4	0.0	0.0	0.0	0.0	1.	-1683.2	-61.8	3997.8	0.0	15740.2	279.2	16.	-475.2	-590.2	1.7	-1359.9	-0.0	1252.4	86.	-236.4	-85.3	0.4	0.0	-36.1	18384.2					
99.	-508.4	0.0	0.0	0.0	0.0	2.	-1683.1	-61.8	3997.8	0.0	14801.6	239.3	16.	-475.2	-590.2	1.7	-1359.9	-0.0	1252.4	86.	-236.4	-85.3	0.4	0.0	-36.1	18384.2					
131.	-508.4	0.0	0.0	0.0	0.0	3.	-1682.9	-61.8	3997.8	0.0	11243.0	199.4	16.	-475.2	-590.2	1.7	-1359.9	-0.0	1252.4	86.	-236.4	-85.3	0.4	0.0	-36.1	18384.2					
165.	-508.4	0.0	0.0	0.0	0.0	4.	-1682.8	-61.8	3997.8	0.0	6745.8	119.7	16.	-475.2	-590.2	1.7	-1359.9	-0.0	1252.4	86.	-236.4	-85.3	0.4	0.0	-36.1	18384.2					
198.	-508.4	0.0	0.0	0.0	0.0	5.	-1682.5	-61.8	3997.8	0.0	4497.2	79.8	16.	-475.2	-590.2	1.7	-1359.9	-0.0	1252.4	86.	-236.4	-85.3	0.4	0.0	-36.1	18384.2					
264.	-508.4	0.0	0.0	0.0	0.0	Asta	83	ndi	467	470	466	MY	NZZ	PROGR.	83	ndi	467	470	466	MY	NZZ	PROGR.	83	ndi	467	470	466	MY	NZZ		
Asta	83	ndi	467	470	466	MY	PROGR.	83	ndi	467	470	466	MY	NZZ	PROGR.	83	ndi	467	470	466	MY	NZZ	PROGR.	83	ndi	467	470	466	MY	NZZ	
PROGR.	83	ndi	467	470	466	MY	PROGR.	83	ndi	467	470	466	MY	NZZ	PROGR.	83	ndi	467	470	466	MY	NZZ	PROGR.	83	ndi	467	470	466	MY	NZZ	
33.	-632.7	0.0	0.0	0.0	0.0	0.	-1682.5	-61.8	3997.8	0.0	4497.2	79.8	16.	-475.2	-590.2	1.7	-1359.9	-0.0	1252.4	86											

[illegible]

-118.0	MMY	MZZ
-118.0	286.1	10806.0
-118.0	239.5	8635.8
-118.0	192.8	66832.0
-118.0	146.2	49931.1
-118.0	99.5	34796.8
-118.0	52.2	24413.6
-118.0	6.2	12472.6
-118.0	-40.4	4964.6
-118.0	-67.1	-131.7
731		
-109.7	MMY	MZZ
-109.7	292.5	110748.9
-109.7	333.3	88572.9
-109.7	374.8	67017.9
-109.7	414.8	50919.1
-109.7	455.6	35841.3
-109.7	496.4	23136.3
-109.7	537.1	12363.9
-109.7	577.7	3204.1
-109.7	618.7	-142.5
473		
TORS	MMY	MZZ
0.0	0.0	0.0
0.0	-23.5	30264.5
0.0	-46.9	49988.8
0.0	-70.4	59172.9
0.0	-93.8	57816.7
0.0	-117.3	45503.2
0.0	-140.7	23483.5
0.0	-164.2	-9893.4
0.0	-187.7	-53010.6
342		
TORS	MMY	MZZ
48.7	-83.0	45568.3
48.7	-105.6	28631.5
48.7	-128.2	15638.1
48.7	-150.8	19271.4
48.7	-173.4	29211.9
48.7	-196.0	22913.3
48.7	-218.6	8948.9
48.7	-241.2	-15555.8
48.7	-263.8	-50060.7
727		
TORS	MMY	MZZ
-91.4	-252.2	-50067.7
-91.4	-205.7	-33774.6
-91.4	-159.3	-23142.4
-91.4	-112.8	-13420.8
-91.4	-66.4	-5802.9
-91.4	-19.9	-97.0
-91.4	26.5	1864.5
-91.4	73.0	2094.1
-91.4	119.4	-109.0
730		
TORS	MMY	MZZ
-94.9	-161.9	-53010.6
-94.9	-128.7	-37087.1
-94.9	-195.5	-25192.4
-94.9	-112.4	-14692.4
-94.9	-229.2	-7305.1
-94.9	-246.0	-1710.6
-94.9	-262.8	-178.5
-94.9	-279.7	1780.2
-94.9	-296.5	1381.5
38		
TORS	MMY	MZZ
43.6	2464.8	38665.6
43.6	2029.6	35132.8
43.6	1594.1	31542.8
43.6	1159.1	28607.3
43.6	723.8	2354.5
43.6	288.5	2190.8
43.6	-146.5	18549.0
43.6	-582.0	15196.2
43.6	-1017.3	11843.5
39		
TORS	MMY	MZZ
-2.4	-1016.9	-25583.2
-2.4	-842.6	-21070.7
-2.4	-668.3	-16558.2
-2.4	-494.1	-12045.8
-2.4	-319.8	-7533.3
-2.4	-145.6	-3020.9
-2.4	28.7	1491.6
-2.4	202.9	604.1
-2.4	377.4	10016.5
41		
TORS	MMY	MZZ
0.0	-5064.5	19900.6
0.0	-4822.6	13529.7
0.0	-2960.6	5050.8
0.0	-1958.7	17607.9
0.0	-896.8	2047.1
0.0	145.2	22686.2
0.0	167.1	2523.3
0.0	2229.1	27764.4
0.0	-1324.2	46896.9
0.0	-3003.5	25306.8
42		
TORS	MMY	MZZ
6.3	3576.2	55882.1
6.3	3135.7	14594.2
6.3	2695.3	11001.3
6.3	2254.8	7408.4
6.3	1814.4	3815.5
6.3	1373.9	222.6
6.3	93.5	-3370.3
6.3	693.0	-6963.2
6.3	52.6	-10556.1
314.5		
TORS	MMY	MZZ
314.5	0.0	314.7
314.5	-102.2	35627.8
314.5	-204.4	-71882.8
314.5	-306.6	-107050.4
314.5	-408.8	-144130.6
314.5	-510.4	-189257.3
314.5	-613.2	-217038.8
314.5	-715.6	-253646.4
314.5	-817.6	-290508.8
29		
TORS	MMY	MZZ
-203.7	-5296.7	-274910.1
-203.7	-4634.6	-240343.2
-203.7	-3972.2	-206017.7
-203.7	-3310.4	-17124

[illegible]

67.	-4.7	0.0	0.0	0.9	0.1	1.5	
68.	-4.7	0.0	0.0	0.9	0.2	1.5	
101.	-4.7	0.0	0.0	0.9	0.3	1.5	
125.	-4.7	0.0	0.0	0.9	0.4	1.5	
168.	-4.7	0.0	0.0	0.9	0.5	1.5	
202.	-4.7	0.0	0.0	0.9	0.5	1.5	
236.	-4.7	0.0	0.0	0.9	0.6	1.5	
269.	-4.7	0.0	0.0	0.9	0.6	1.5	
Asta	154	nodi	973	712			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	6.2	-795.8	0.0	0.0	0.0	0.0	
29.	6.2	-596.8	0.0	0.0	0.0	-2010.8	
38.	6.2	-397.9	0.0	0.0	0.0	-3437.9	
62.	6.2	-198.9	0.0	0.0	0.0	-4289.4	
85.	6.2	0.0	0.0	0.0	0.0	-4787.2	
144.	6.2	-198.9	0.0	0.0	0.0	-4289.4	
164.	6.2	-397.9	0.0	0.0	0.0	-3437.9	
201.	6.2	-596.8	0.0	0.0	0.0	-2010.8	
230.	6.2	-795.8	0.0	0.0	0.0	0.0	
Asta	156	nodi	972	711			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-58.6	6.4	0.4	0.0	62.0	0.0	
29.	-58.6	445.7	0.4	0.0	-10.1	15673.0	
38.	-58.6	246.7	0.4	0.0	-20.0	25606.4	
62.	-58.6	67.8	0.4	0.0	-30.3	39860.2	
115.	-58.6	-151.2	0.4	0.0	-40.4	26374.3	
144.	-58.6	-350.1	0.4	0.0	-50.7	21687.9	
173.	-58.6	-549.0	0.4	0.0	-60.5	8243.5	
201.	-58.6	-748.0	0.4	0.0	-70.4	-3014.4	
230.	-58.6	-946.9	0.4	0.0	-80.7	-34765.9	
Asta	157	nodi	969	970			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	21.3	948.6	0.0	7.0	-124.5	-78409.6	
16.	21.3	941.7	0.0	7.0	-61.9	-620.8	
31.	21.3	934.8	-1.9	7.0	-62.5	-47804.6	
43.	21.3	927.8	-1.9	7.0	-62.5	-47804.6	
65.	21.3	920.9	-1.9	7.0	-0.4	-1968.9	
81.	21.3	914.0	-1.9	7.0	30.6	-2741.3	
114.	21.3	907.1	-1.9	7.0	61.2	-2741.3	
114.	21.3	900.1	-1.9	7.0	92.6	26738.1	
201.	21.3	893.2	-1.9	7.0	123.6	41308.9	
Asta	158	nodi	967	968			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-14.2	-510.6	5.7	28.3	0.0	0.0	
16.	-14.2	-517.5	5.7	28.3	-92.0	-82.0	
31.	-14.2	-524.4	5.7	28.3	-183.1	-82.0	
49.	-14.2	-531.3	5.7	28.3	-275.9	-25356.8	
61.	-14.2	-538.2	5.7	28.3	-367.8	-45388.3	
81.	-14.2	-545.2	5.7	28.3	-459.8	-45271.7	
98.	-14.2	-552.2	5.7	28.3	-551.8	-45867.9	
114.	-14.2	-559.1	5.7	28.3	-643.7	-60667.7	
130.	-14.2	-566.0	5.7	28.3	-735.7	-69098.1	
Asta	159	nodi	966	967			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-510.6	5.7	14.2	0.0	71.2	-28.3	
1.	-510.5	5.7	14.2	0.0	62.3	62.8	
2.	-510.2	5.7	14.2	0.0	53.4	-17.7	
3.	-510.0	5.7	14.2	0.0	35.5	-14.1	
4.	-509.9	5.7	14.2	0.0	26.6	-10.6	
4.	-509.8	5.7	14.2	0.0	17.8	-7.1	
4.	-509.6	5.7	14.2	0.0	8.9	-3.5	
5.	-509.5	5.7	14.2	0.0	0.0	0.0	
Asta	160	nodi	969	973			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-796.9	6.2	0.0	0.0	0.0	-31.1	
1.	-796.7	6.2	0.0	0.0	0.0	-27.2	
2.	-796.6	6.2	0.0	0.0	0.0	-23.3	
12.	-796.5	6.2	0.0	0.0	0.0	-19.4	
13.	-796.4	6.2	0.0	0.0	0.0	-15.5	
23.	-796.2	6.2	0.0	0.0	0.0	-11.6	
4.	-796.1	6.2	0.0	0.0	0.0	-7.7	
4.	-795.9	6.2	0.0	0.0	0.0	-3.9	
5.	-795.8	6.2	0.0	0.0	0.0	0.0	
Asta	161	nodi	968	972			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-645.7	-58.6	0.4	0.0	0.0	292.8	
1.	-645.6	-58.6	0.4	0.0	1.3	236.2	
2.	-645.4	-58.6	0.4	0.0	1.3	219.6	
3.	-645.3	-58.6	0.4	0.0	1.3	183.0	
3.	-645.2	-58.6	0.4	0.0	0.9	146.4	
4.	-645.0	-58.6	0.4	0.0	0.9	119.8	
4.	-644.9	-58.6	0.4	0.0	0.4	73.2	
4.	-644.8	-58.6	0.4	0.0	0.0	36.6	
5.	-644.6	-58.6	0.4	0.0	0.0	0.0	
Asta	162	nodi	968	951			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-14.6	-1211.7	-52.9	-264.5	-735.7	-69906.3	
1.	-14.6	-1212.3	-52.9	-264.5	-669.7	-69906.3	
3.	-14.6	-1212.8	-52.9	-264.5	-603.4	-74933.0	
4.	-14.6	-1213.3	-52.9	-264.5	-537.3	-79571.3	
5.	-14.6	-1213.9	-52.9	-264.5	-471.9	-84209.6	
6.	-14.6	-1214.4	-52.9	-264.5	-405.0	-77488.0	
12.	-14.6	-1214.9	-52.9	-264.5	-339.4	-70766.3	
9.	-14.6	-1215.5	-52.9	-264.5	-272.8	-65025.3	
10.	-14.6	-1216.0	-52.9	-264.5	-206.6	-60084.9	
Asta	163	nodi	951	969			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	21.3	1748.8	-8.1	-24.0	-80.7	-8204.9	
1.	21.3	1748.2	-8.1	-24.0	-195.5	-93639.0	
3.	21.3	1748.7	-8.1	-24.0	-185.9	-93639.0	
4.	21.3	1748.8	-8.1	-24.0	-175.2	-89327.3	
5.	21.3	1747.6	-8.1	-24.0	-165.1	-87142.4	
17.	21.3	1747.1	-8.1	-24.0	-154.9	-84957.4	
8.	21.3	1746.6	-8.1	-24.0	-144.8	-82774.7	
10.	21.3	1746.0	-8.1	-24.0	-134.7	-80591.9	
10.	21.3	1745.5	-8.1	-24.0	-124.5	-78409.6	
Asta	165	nodi	970	714			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-18.9	-590.5	-0.3	0.0	0.0	0.0	
29.	-18.9	-310.6	-0.3	0.0	9.8	-11789.2	
58.	-18.9	-111.6	-0.3	0.0	19.6	-1876.8	
87.	-18.9	17.3	-0.3	0.0	29.1	-1805.7	
114.	-18.9	286.3	-0.3	0.0	39.1	-1285.0	
144.	-18.9	485.2	-0.3	0.0	48.9	-174.6	
173.	-18.9	684.2	-0.3	0.0	58.7	-8965.2	
201.	-18.9	883.3	-0.3	0.0	68.5	37395.1	
230.	-18.9	1082.1	-0.3	0.0	78.0	61600.4	
Asta	166	nodi	735	951			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-3171.4	-73.2	-3.9	-0.9	-1071.7	11031.0	
43.	-3145.3	-73.2	-3.9	-0.9	-907.7	9321.0	
72.	-3119.3	-73.2	-3.9	-0.9	-743.6	8831.0	
128.	-3093.2	-73.2	-3.9	-0.9	-579.6	1704.0	
173.	-3067.1	-73.2	-3.9	-0.9	-415.5	-1405.0	
213.	-3041.1	-73.2	-3.9	-0.9	-251.6	-4514.0	
255.	-3015.0	-73.2	-3.9	-0.9	-87.6	-7623.0	
282.	-2989.0	-73.2	-3.9	-0.9	78.0	-13841.0	
Asta	167	nodi	749	754			
PROGR.	NORM	TY	TZ	TORS	M1Y	M2Z	
0.	-257.0	0.0	0.0	0.0	0.0	0.0	
34.	-257.0	0.0	0.0	0.0	0.0	0.0	
67.	-257.0	0.0	0.0	0.0	0.0	0.0	
102.	-257.0	0.0	0.0	0.0	0.0	0.0	
135.	-257.0	0.0	0.0	0.0	0.0	0.0	
168.	-257.0	0.0	0.0	0.0	0.0	0.0	

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33.	10.6	857.5	-14.3	-119.7	-55.0	-4002.8	114.	-1.0	-129.2	1.7	-69.7	-171.8	-13529.9	45.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.3	-286.4	3806.6	0.0	4758.3	358.0	
49.	10.6	850.6	-14.3	-119.7	178.0	-2614.2	130.	-1.0	-132.3	1.7	-69.7	-138.9	-15654.2	90.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.2	-286.4	3806.6	0.0	2379.1	179.0	
81.	10.6	843.7	-14.3	-119.7	41.1	-13796.0	Asta	82	10.6	843.7	-14.3	-119.7	41.1	-13796.0	729.	85.1	0.0	0.0	0.0	0.0	0.0	4.	-4010.0	-286.4	3806.6	0.0	729.0	0.0
89.	10.6	836.8	-14.3	-119.7	644.0	1277.5	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	180.	85.1	0.0	0.0	0.0	0.0	0.0	Asta	107	nodi	30	469	MY	NZZ	
98.	10.6	829.8	-14.3	-119.7	877.0	14815.5	0.	45.0	3.7	-1.1	-0.3	-164.3	-15737.8	225.	85.1	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	
114	110.6	822.9	-14.3	-119.7	110.6	822.9	1	45.0	3.7	-1.1	-0.3	-164.3	-15737.8	270.	85.1	0.0	0.0	0.0	0.0	0.0	1.	-990.5	30.7	1121.6	0.0	5608.0	-133.4	
130.	10.6	816.0	-14.3	-119.7	1343.0	41562.8	5.	45.0	2.8	-1.1	-0.9	-158.7	-15721.5	315.	85.1	0.0	0.0	0.0	0.0	0.0	1.	-990.5	30.7	1121.6	0.0	4907.0	-134.3	
Asta	46	nodi	964	8	6.0	2.3	360.	85.0	0.0	0.0	0.0	-157.0	-15701.3	360.	85.0	0.0	0.0	0.0	0.0	0.0	2.	-990.5	30.7	1121.6	0.0	1121.6	-115.1	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	10.	45.0	1.9	-1.1	-0.9	-153.1	-15709.9	Asta	89	nodi	211	339	MY	NZZ	2.	-990.2	30.7	1121.6	0.0	3305.0	-95.9	
0.	-27.8	-1176.2	10.3	51.5	0.0	130.1	13.	45.0	1.4	-1.1	-0.3	-150.3	-15705.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	3.	-990.1	30.7	1121.6	0.0	2804.0	-76.7	
16.	-27.8	-1183.1	10.3	51.5	0.0	130.2	16.	45.0	1.9	-1.1	-0.3	-147.5	-15703.0	1.	-990.6	30.7	1121.6	0.0	0.0	0.0	1.	-990.6	30.7	1121.6	0.0	2184.9	-57.7	
33.	-27.8	-1190.0	10.3	51.5	-334.5	-3831.2	18.	45.0	0.4	-1.1	-0.9	-144.7	-15701.3	45.	-51.0	0.0	0.0	0.0	0.0	0.0	4.	-989.8	30.7	1121.6	0.0	1402.0	-38.4	
49.	-27.8	-1197.0	10.3	51.5	-634.5	-4370.5	20.	45.0	0.0	-1.1	-0.9	-141.9	-15700.8	90.	-51.0	0.0	0.0	0.0	0.0	0.0	5.	-989.5	30.7	1121.6	0.0	701.6	-10.2	
65.	-27.8	-1203.9	10.3	51.5	-669.0	-4772.3	Asta	59	nodi	728	727	MY	NZZ	135.	-51.0	0.0	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	
81.	-27.8	-1210.8	10.3	51.5	-678.8	-4858.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	135.	-51.0	0.0	0.0	0.0	0.0	0.0	1.	-1350.7	39.1	37.2	0.0	185.9	-195.5	
98.	-27.8	-1217.7	10.3	51.5	-1003.5	-116565.1	0.	1.5	132.0	-0.2	67.3	-82.7	-15628.3	225.	-51.0	0.0	0.0	0.0	0.0	0.0	1.	-1350.6	39.1	37.2	0.0	139.4	-146.6	
114.	-27.8	-1224.7	10.3	51.5	-1170.8	-136498.9	16.	1.5	129.0	-0.2	67.3	-89.9	-13507.7	270.	-51.0	0.0	0.0	0.0	0.0	0.0	2.	-1350.5	39.1	37.2	0.0	92.9	-97.7	
130.	-27.8	-1231.6	10.3	51.5	-1338.0	-156387.0	13.	1.5	125.9	-0.2	67.3	-87.1	-11486.8	360.	-51.0	0.0	0.0	0.0	0.0	0.0	3.	-1350.2	39.1	37.2	0.0	69.7	-73.3	
Asta	67	nodi	961	42	82	2	45.	1.5	122.8	-0.2	67.3	-84.3	-9415.7	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	4.	-1349.9	39.1	37.2	0.0	23.2	-24.4	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	65.	1.5	119.8	-0.2	67.3	-81.5	-7444.4	0.	91	nodi	5	210	MY	NZZ	1.	-1405.8	-110.4	-0.1	0.0	-0.4	276.0	
0.	-25.8	-2888.1	-9.0	-45.1	-1338.0	-156377.0	81.	1.5	116.7	-0.2	67.3	-78.7	-5527.7	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	3.	-1330.3	39.1	37.2	0.0	92.9	-97.7	
1.	-25.8	-2888.6	-9.0	-45.1	-1326.8	-159987.5	96.	1.5	113.7	-0.2	67.3	-75.8	-3650.9	1.	-361.7	7.6	1068.2	0.0	5341.2	-37.9	1.	-1350.2	39.1	37.2	0.0	69.7	-73.3	
3.	-25.8	-2889.1	-9.0	-45.1	-1315.5	-163396.5	114.	1.5	110.6	-0.2	67.3	-72.0	-1828.8	3.	-361.0	7.6	1068.2	0.0	4673.5	-39.2	3.	-1350.0	39.1	37.2	0.0	46.7	-48.9	
4.	-25.8	-2889.7	-9.0	-45.1	-1304.2	-167210.3	130.	1.5	107.5	-0.2	67.3	-70.2	-56.4	1.	-361.3	7.6	1068.2	0.0	4005.9	-28.5	4.	-1349.8	39.1	37.2	0.0	23.2	-24.4	
5.	-25.8	-2890.2	-9.0	-45.1	-1293.0	-170922.7	Asta	67	nodi	473	731	MY	NZZ	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	1.	-1405.8	-110.4	-0.1	0.0	-0.4	276.0	
6.	-25.8	-2890.7	-9.0	-45.1	-1281.7	-174455.8	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	3.	-361.2	7.6	1068.2	0.0	2670.6	-19.0	Asta	109	nodi	11	471	MY	NZZ	
7.	-25.8	-2891.3	-9.0	-45.1	-1270.4	-178049.5	25.	-154.5	0.0	0.0	0.0	0.0	0.0	4.	-360.9	7.6	1068.2	0.0	1335.3	-9.5	0.	-1406.4	-110.4	-0.1	0.0	-0.7	552.1	
9.	-25.8	-2891.8	-9.0	-45.1	-1259.2	-181663.9	50.	-154.5	0.0	0.0	0.0	0.0	0.0	4.	-360.8	7.6	1068.2	0.0	667.6	-4.7	1.	-1406.2	-110.4	-0.1	0.0	-0.6	483.1	
10.	-25.8	-2892.3	-9.0	-45.1	-1247.9	-185279.0	99.	-154.5	0.0	0.0	0.0	0.0	0.0	4.	-360.6	7.6	1068.2	0.0	338.2	-23.7	2.	-1405.9	-110.4	-0.1	0.0	-0.4	345.1	
Asta	48	nodi	42	82	2	2	45.	1.5	119.8	-0.2	67.3	-81.5	-7444.4	Asta	92	nodi	14	211	MY	NZZ	3.	-1405.8	-110.4	-0.1	0.0	-0.4	276.0	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	124.	-125.5	-19142.2	0.0	0.0	0.0	0.0	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	1.	-1406.2	-110.4	-0.1	0.0	-0.6	483.1	
0.	-76.5	2889.1	-2.3	-11.5	-1247.6	-187810.1	149.	-154.5	0.0	0.0	0.0	0.0	0.0	1.	-922.1	-56.7	2454.4	0.0	1227.2	283.3	2.	-1405.9	-110.4	-0.1	0.0	-0.4	345.1	
1.	-76.5	2888.6	-2.3	-11.5	-1247.6	-187810.1	174.	-154.5	0.0	0.0	0.0	0.0	0.0	1.	-921.9	-56.7	2454.4	0.0	1078.2	247.9	4.	-1405.5	-110.4	-0.1	0.0	-0.3	207.0	
3.	-76.5	2888.1	-2.3	-11.5	-1247.6	-187810.1	198.	-154.5	0.0	0.0	0.0	0.0	0.0	2.	-921.8	-56.7	2454.4	0.0	928.2	212.5	Asta	107	nodi	30	469	MY	NZZ	
5.	-76.5	2887.0	-2.3	-11.5	-1239.0	-176980.8	Asta	70	nodi	470	732	MY	NZZ	3.	-921.7	-56.7	2454.4	0.0	7670.1	177.1	1.	-1405.3	-110.4	-0.1	0.0	-0.3	207.0	
7.	-76.5	2886.5	-2.3	-11.5	-1231.7	-173274.2	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	4.	-921.5	-56.7	2454.4	0.0	6136.7	147.7	2.	-1405.2	-110.4	-0.1	0.0	-0.3	207.0	
8.	-76.5	2885.9	-2.3	-11.5	-1233.3	-169764.7	0.	-152.0	0.0	0.0	0.0	0.0	0.0	3.	-921.4	-56.7	2454.4	0.0	4602.1	106.2	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	
9.	-76.5	2885.4	-2.3	-11.5	-1230.4	-166517.6	25.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-921.3	-56.7	2454.4	0.0	3068.0	70.8	1.	-1405.8	87.7	0.8	0.0	3.8	-438.4	
10.	-76.5	2884.9	-2.3	-11.5	-1227.0	-162623.2	74.	-152.0	0.0	0.0	0.0	0.0	0.0	5.	-921.2	-56.7	2454.4	0.0	1534.0	35.4	0.	-1405.6	87.7	0.8	0.0	3.8	-389.6	
Asta	69	nodi	962	965	14	34	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	Asta	92	nodi	14	211	MY	NZZ	1.	-1405.6	87.7	0.8	0.0	3.8	-389.6	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	99.	-152.0	0.0	0.0	0.0	0.0	0.0	1.	-995.9	3.2	1264.7	0.0	1304.7	0.0	2.	-1405.6	87.7	0.8	0.0	3.8	-389.6	
0.	-74.5	1281.0	-9.4	-47.2	-1227.5	-162590.8	124.	-152.0	0.0	0.0	0.0	0.0	0.0	3.	-995.6	3.2	1264.7	0.0	474.7	-11.8	3.	-1405.6	87.7	0.8	0.0	3.8	-389.6	
1.	-74.5	1280.5	-9.4	-47.2	-1227.5	-162590.8	149.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-995.5	3.2	1264.7	0.0	324.7	-3.9	Asta	111	nodi	29	473	MY	NZZ	
3.	-74.5	1276.2	-9.4	-47.2	-1215.2	-161152.1	174.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-995.4	3.2	1264.7	0.0	790.4	-2.0	1.	-1270.5	24.9	89.3	0.0	446.6	-124.6	
4.	-74.5	1260.3	-9.4	-47.2	-1215.2	-161152.1	198.	-152.0	0.0	0.0	0.0	0.0	0.0	4.	-995.3	3.2	1264.7	0.0	1580.9	-1.9	2.	-1270.4	24.9	89.3	0.0	390.8	-109.0	
5.	-74.5	1260.3	-9.4	-47.2	-1215.2	-161152.1	Asta	71	nodi	342	733	MY	NZZ	Asta	94	nodi	32	213	MY	NZZ	3.	-1270.3	24.9	89.3	0.0	390.8	-109.0	
7.	-74.5	1256.4	-9.4	-47.2	-1215.2	-161152.1	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	1.	-995.9	3.2	1264.7	0.0	1304.7	0.0	4.	-1270.3	24.9	89.3	0.0	390.8	-109.0	
8.	-74.5	1256.4	-9.4	-47.2	-1215.2	-161152.1	198.	-152.0	0.0	0.0	0.0	0.0	0.0	3.	-995.6	3.2	1264.7	0.0	474.7	-11.8	1.	-1270.3	24.9	89.3	0.0	390.8	-109.0	
9.	-74.5	1256.4	-9.4	-47.2	-1215.2	-161152.1	Asta	71	nodi	342	733	MY	NZZ	1.	-995.9	3.2	1264.7	0.0	1304.7	0.0	2.	-1270.3	24.9	89.3	0.0	390.8	-109.0	
10.	-74.5	1256.4	-9.4	-47.2	-1215.2	-161152.1	PROGR.	NORM	TY	TZ	TORS	MY	NZZ	3.	-995.6	3.2	1264.7	0.0	474.7	-11.8	4.	-1270.3	24.9	89.3	0.0	390.8	-109.0	
Asta	71	nodi	342	733	MY	NZZ	25.	64.2	0.0	0.0	0.0	0.0	0.0	4.	-995.5	3.2	1264.7	0.0	1580.9	-1.9	Asta	111	nodi	29	473	MY	NZZ	
PROGR.	NORM	TY	TZ	TORS	MY	NZZ	74.	64.2	0.0																			

0.	-30.4	-803.9	-8.1	990	-159.0	-49431.4	88.	-315.0	-53.2	0.7	-1.3	42.4	8306.4
1.	-30.4	-804.5	-8.1	940.1	-148.9	-50436.7	100.	-315.0	-130.5	0.7	-1.3	29.4	6699.7
2.	-30.4	-804.5	-8.1	940.1	-148.9	-50436.7	120.	-315.0	-207.0	0.7	-1.3	29.4	6699.7
3.	-30.4	-804.5	-8.1	940.1	-128.6	-52449.1	140.	-315.0	-285.0	0.7	-1.3	3.5	-571.2
4.	-30.4	-806.1	-8.1	940.1	-118.5	-5346.4	Asta	142	nodi	970	738		
5.	-30.4	-806.6	-8.1	940.1	-108.6	-5446.2	PROGR.	NORM	TY	TYZ	TORS	MY	NZZ
6.	-30.4	-807.1	-8.1	940.1	-98.3	-5547.8	0.	3.2	77.4	0.6	13.5	84.3	26673.3
7.	-30.4	-807.6	-8.1	940.1	-88.3	-5648.4	1.	3.2	77.4	0.6	13.5	84.3	26673.3
8.	-30.4	-808.1	-8.1	940.1	-78.0	-5749.0	2.	3.2	77.4	0.6	13.5	84.3	26673.3
9.	-30.4	-808.2	-8.1	940.1	-68.0	-5849.6	3.	3.2	77.4	0.6	13.5	84.3	26673.3
10.	-30.4	-808.2	-8.1	940.1	-58.0	-5950.2	4.	3.2	77.4	0.6	13.5	84.3	26673.3
11.	-30.4	-808.2	-8.1	940.1	-48.0	-6050.8	5.	3.2	77.4	0.6	13.5	84.3	26673.3
12.	-30.4	-808.2	-8.1	940.1	-38.0	-6151.4	6.	3.2	77.4	0.6	13.5	84.3	26673.3
13.	-30.4	-808.2	-8.1	940.1	-28.0	-6252.0	7.	3.2	77.4	0.6	13.5	84.3	26673.3
14.	-30.4	-808.2	-8.1	940.1	-18.0	-6352.6	8.	3.2	77.4	0.6	13.5	84.3	26673.3
15.	-30.4	-808.2	-8.1	940.1	-8.0	-6453.2	9.	3.2	77.4	0.6	13.5	84.3	26673.3
16.	-30.4	-808.2	-8.1	940.1	2.0	-6553.8	10.	3.2	77.4	0.6	13.5	84.3	26673.3
17.	-30.4	-808.2	-8.1	940.1	12.0	-6654.4	11.	3.2	77.4	0.6	13.5	84.3	26673.3
18.	-30.4	-808.2	-8.1	940.1	22.0	-6755.0	12.	3.2	77.4	0.6	13.5	84.3	26673.3
19.	-30.4	-808.2	-8.1	940.1	32.0	-6855.6	13.	3.2	77.4	0.6	13.5	84.3	26673.3
20.	-30.4	-808.2	-8.1	940.1	42.0	-6956.2	14.	3.2	77.4	0.6	13.5	84.3	26673.3
21.	-30.4	-808.2	-8.1	940.1	52.0	-7056.8	15.	3.2	77.4	0.6	13.5	84.3	26673.3
22.	-30.4	-808.2	-8.1	940.1	62.0	-7157.4	16.	3.2	77.4	0.6	13.5	84.3	26673.3
23.	-30.4	-808.2	-8.1	940.1	72.0	-7258.0	17.	3.2	77.4	0.6	13.5	84.3	26673.3
24.	-30.4	-808.2	-8.1	940.1	82.0	-7358.6	18.	3.2	77.4	0.6	13.5	84.3	26673.3
25.	-30.4	-808.2	-8.1	940.1	92.0	-7459.2	19.	3.2	77.4	0.6	13.5	84.3	26673.3
26.	-30.4	-808.2	-8.1	940.1	102.0	-7559.8	20.	3.2	77.4	0.6	13.5	84.3	26673.3
27.	-30.4	-808.2	-8.1	940.1	112.0	-7660.4	21.	3.2	77.4	0.6	13.5	84.3	26673.3
28.	-30.4	-808.2	-8.1	940.1	122.0	-7761.0	22.	3.2	77.4	0.6	13.5	84.3	26673.3
29.	-30.4	-808.2	-8.1	940.1	132.0	-7861.6	23.	3.2	77.4	0.6	13.5	84.3	26673.3
30.	-30.4	-808.2	-8.1	940.1	142.0	-7962.2	24.	3.2	77.4	0.6	13.5	84.3	26673.3
31.	-30.4	-808.2	-8.1	940.1	152.0	-8062.8	25.	3.2	77.4	0.6	13.5	84.3	26673.3
32.	-30.4	-808.2	-8.1	940.1	162.0	-8163.4	26.	3.2	77.4	0.6	13.5	84.3	26673.3
33.	-30.4	-808.2	-8.1	940.1	172.0	-8264.0	27.	3.2	77.4	0.6	13.5	84.3	26673.3
34.	-30.4	-808.2	-8.1	940.1	182.0	-8364.6	28.	3.2	77.4	0.6	13.5	84.3	26673.3
35.	-30.4	-808.2	-8.1	940.1	192.0	-8465.2	29.	3.2	77.4	0.6	13.5	84.3	26673.3
36.	-30.4	-808.2	-8.1	940.1	202.0	-8565.8	30.	3.2	77.4	0.6	13.5	84.3	26673.3
37.	-30.4	-808.2	-8.1	940.1	212.0	-8666.4	31.	3.2	77.4	0.6	13.5	84.3	26673.3
38.	-30.4	-808.2	-8.1	940.1	222.0	-8767.0	32.	3.2	77.4	0.6	13.5	84.3	26673.3
39.	-30.4	-808.2	-8.1	940.1	232.0	-8867.6	33.	3.2	77.4	0.6	13.5	84.3	26673.3
40.	-30.4	-808.2	-8.1	940.1	242.0	-8968.2	34.	3.2	77.4	0.6	13.5	84.3	26673.3
41.	-30.4	-808.2	-8.1	940.1	252.0	-9068.8	35.	3.2	77.4	0.6	13.5	84.3	26673.3
42.	-30.4	-808.2	-8.1	940.1	262.0	-9169.4	36.	3.2	77.4	0.6	13.5	84.3	26673.3
43.	-30.4	-808.2	-8.1	940.1	272.0	-9270.0	37.	3.2	77.4	0.6	13.5	84.3	26673.3
44.	-30.4	-808.2	-8.1	940.1	282.0	-9370.6	38.	3.2	77.4	0.6	13.5	84.3	26673.3
45.	-30.4	-808.2	-8.1	940.1	292.0	-9471.2	39.	3.2	77.4	0.6	13.5	84.3	26673.3
46.	-30.4	-808.2	-8.1	940.1	302.0	-9571.8	40.	3.2	77.4	0.6	13.5	84.3	26673.3
47.	-30.4	-808.2	-8.1	940.1	312.0	-9672.4	41.	3.2	77.4	0.6	13.5	84.3	26673.3
48.	-30.4	-808.2	-8.1	940.1	322.0	-9773.0	42.	3.2	77.4	0.6	13.5	84.3	26673.3
49.	-30.4	-808.2	-8.1	940.1	332.0	-9873.6	43.	3.2	77.4	0.6	13.5	84.3	26673.3
50.	-30.4	-808.2	-8.1	940.1	342.0	-9974.2	44.	3.2	77.4	0.6	13.5	84.3	26673.3
51.	-30.4	-808.2	-8.1	940.1	352.0	-10074.8	45.	3.2	77.4	0.6	13.5	84.3	26673.3
52.	-30.4	-808.2	-8.1	940.1	362.0	-10175.4	46.	3.2	77.4	0.6	13.5	84.3	26673.3
53.	-30.4	-808.2	-8.1	940.1	372.0	-10276.0	47.	3.2	77.4	0.6	13.5	84.3	26673.3
54.	-30.4	-808.2	-8.1	940.1	382.0	-10376.6	48.	3.2	77.4	0.6	13.5	84.3	26673.3
55.	-30.4	-808.2	-8.1	940.1	392.0	-10477.2	49.	3.2	77.4	0.6	13.5	84.3	26673.3
56.	-30.4	-808.2	-8.1	940.1	402.0	-10577.8	50.	3.2	77.4	0.6	13.5	84.3	26673.3
57.	-30.4	-808.2	-8.1	940.1	412.0	-10678.4	51.	3.2	77.4	0.6	13.5	84.3	26673.3
58.	-30.4	-808.2	-8.1	940.1	422.0	-10779.0	52.	3.2	77.4	0.6	13.5	84.3	26673.3
59.	-30.4	-808.2	-8.1	940.1	432.0	-10879.6	53.	3.2	77.4	0.6	13.5	84.3	26673.3
60.	-30.4	-808.2	-8.1	940.1	442.0	-10980.2	54.	3.2	77.4	0.6	13.5	84.3	26673.3
61.	-30.4	-808.2	-8.1	940.1	452.0	-11080.8	55.	3.2	77.4	0.6	13.5	84.3	26673.3
62.	-30.4	-808.2	-8.1	940.1	462.0	-11181.4	56.	3.2	77.4	0.6	13.5	84.3	26673.3
63.	-30.4	-808.2	-8.1	940.1	472.0	-11282.0	57.	3.2	77.4	0.6	13.5	84.3	26673.3
64.	-30.4	-808.2	-8.1	940.1	482.0	-11382.6	58.	3.2	77.4	0.6	13.5	84.3	26673.3
65.	-30.4	-808.2	-8.1	940.1	492.0	-11483.2	59.	3.2	77.4	0.6	13.5	84.3	26673.3
66.	-30.4	-808.2	-8.1	940.1	502.0	-11583.8	60.	3.2	77.4	0.6	13.5	84.3	26673.3
67.	-30.4	-808.2	-8.1	940.1	512.0	-11684.4	61.	3.2	77.4	0.6	13.5	84.3	26673.3
68.	-30.4	-808.2	-8.1	940.1	522.0	-11785.0	62.	3.2	77.4	0.6	13.5	84.3	26673.3
69.	-30.4	-808.2	-8.1	940.1	532.0	-11885.6	63.	3.2	77.4	0.6	13.5	84.3	26673.3
70.	-30.4	-808.2	-8.1	940.1	542.0	-11986.2	64.	3.2	77.4	0.6	13.5	84.3	26673.3
71.	-30.4	-808.2	-8.1	940.1	552.0	-12086.8	65.	3.2	77.4	0.6	13.5	84.3	26673.3
72.	-30.4	-808.2	-8.1	940.1	562.0	-12187.4	66.	3.2	77.4	0.6	13.5	84.3	26673.3
73.	-30.4	-808.2	-8.1	940.1	572.0	-12288.0	67.	3.2	77.4	0.6	13.5	84.3	26673.3
74.	-30.4	-808.2	-8.1	940.1	582.0	-12388.6	68.	3.2	77.4	0.6	13.5	84.3	26673.3
75.	-30.4	-808.2	-8.1	940.1	592.0	-12489.2	69.	3.2	77.4	0.6	13.5	84.3	26673.3
76.	-30.4	-808.2	-8.1	940.1	602.0	-12589.8	70.	3.2	77.4	0.6	13.5	84.3	26673.3
77.	-30.4	-808.2	-8.1	940.1	612.0	-12690.4	71.	3.2	77.4	0.6	13.5	84.3	26673.3
78.	-30.4	-808.2	-8.1	940.1	622.0	-12791.0	72.	3.2	77.4	0.6	13.5	84.3	26673.3
79.	-30.4	-808.2	-8.1	940.1	632.0	-12891.6	73.	3.2	77.4	0.6	13.5	84.3	26673.3
80.	-30.4	-808.2	-8.1	940.1	642.0	-12992.2	74.	3.2	77.4	0.6	13.5	84.3	26673.3
81.	-30.4	-808.2	-8.1	940.1	652.0	-13092.8	75.	3.2	77.4	0.6	13.5	84.3	26673.3
82.	-30.4	-808.2	-8.1	940.1	662.0	-13193.4	76.	3.2	77.4	0.6	13.5	84.3	26673.3
83.	-30.4	-808.2	-8.1	940.1	672.0	-13294.0	77.	3.2	77.4	0.6	13.5	84.3	26673.3
84.	-30.4	-808.2	-8.1	940.1	682.0	-13394.6	78.	3.2	77.4	0.6	13.5	84.3	26673.3
85.	-30.4	-808.2	-8.1	940.1	692.0	-13495.2	79.	3.2	77.4	0.6	13.5	84.3	26673.3
86.	-30.4	-808.2	-8.1	940.1	702.0	-13595.8	80.	3.2	77.4	0.6	13.5	84.3	26673.3
87.	-30.4	-808.2	-8.1	940.1	712.0	-13696.4	81.	3.2	77.4	0.6	13.5	84.3	26673.3
88.	-30.4	-808.2	-8.1	940.1	722.0	-13797.0	82.	3.2	77.4	0.6	13.5	84.3	26673.3
89.	-30.4	-808.2	-8.1	940.1	732.0	-13897.6	83.	3.2	77.4	0.6	13.5	84.3	26673.3
90.	-30.4	-808.2	-8.1	940.1	742.0	-13998.2	84.	3.2	77.4	0.6	13.5	84.3	26673.3
91.	-30.4	-808.2	-8.1	940.1	752.0	-14098.8	85.	3.2	77.4	0.6	13.5	84.3	26673.3
92.	-30.4	-808.2	-8.1	940.1	762.0	-14199.4	86.	3.2	77.4	0.6	13.5	84.3	26673.3
93.	-30.4	-808.2	-8.1	940.1	772.0	-14299.9	87.	3.2	77.4	0.6	13.5		

200	198.2	-276.0	0.5	-21.4	-131.7	109.5	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	5.	-25.8	-2890.2	-9.0	-45.1	-1289.0	-17082.7	0.0	Asta	67	north	473	731	MY	MZZ		
201	-118.2	-428.6	0.5	-21.4	-150.5	-14583.7	0.0	0.	-4488.8	62.9	-2.4	-2.6	-593.3	-15216.1	6.	-25.8	-2890.7	-9.0	-45.1	-1291.7	-17445.8	0.0	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	
202	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	0.	-4462.2	62.9	-2.4	-2.6	-593.3	-15216.1	6.	-25.8	-2891.3	-9.0	-45.1	-1290.4	-17459.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
334	-62.4	-733.8	0.5	-21.4	-188.1	-63064.3	0.0	85.	-4436.2	62.9	-2.4	-2.6	-390.8	-9668.2	9.	-25.8	-2891.8	-9.0	-45.1	-1259.2	-18166.9	0.0	25.	-154.5	0.0	0.0	0.0	0.0	0.0	
335	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	138.	-4401.1	62.9	-2.4	-2.6	-390.8	-9668.2	9.	-25.8	-2892.3	-9.0	-45.1	-1267.9	-18379.0	0.0	74.	-154.5	0.0	0.0	0.0	0.0	0.0	
336	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	180.	-4384.1	62.9	-2.4	-2.6	-188.3	-4620.2	48	-76.5	2889.2	-2.3	-11.5	-1250.5	-19142.2	0.0	74.	-154.5	0.0	0.0	0.0	0.0	0.0	
0.	238.3	471.4	0.5	-25.3	-43.2	-20972.2	0.0	213.	-4380.0	62.9	-2.4	-2.6	-47.0	-1962.2	48	-76.5	2889.2	-2.3	-11.5	-1250.5	-19142.2	0.0	124.	-154.5	0.0	0.0	0.0	0.0	0.0	
148	148.9	218.8	0.5	-25.3	-43.2	-20972.2	0.0	252.	-4319.9	62.9	-2.4	-2.6	-14.3	-727.7	1.	-76.5	2888.6	-2.3	-11.5	-1247.6	-18780.1	0.0	124.	-154.5	0.0	0.0	0.0	0.0	0.0	
84.	59.4	166.2	0.5	-25.3	-84.6	-5822.3	0.0	288.	-4305.9	62.9	-2.4	-2.6	-116.5	-3401.7	1.	-76.5	2888.6	-2.3	-11.5	-1244.9	-18419.7	0.0	149.	-154.5	0.0	0.0	0.0	0.0	0.0	
126	126.0	126.0	0.5	-25.3	-84.6	-5822.3	0.0	340.	-4279.8	62.9	-2.4	-2.6	-216.6	-6709.7	4.	-76.5	2887.5	-2.3	-11.5	-1241.9	-18058.9	0.0	179.	-154.5	0.0	0.0	0.0	0.0	0.0	
168	-119.5	-139.0	0.5	-25.3	-127.9	-6967.6	0.0	Asta	35	north	978	41	0.0	2078.1	18633.1	4.	-76.5	2887.5	-2.3	-11.5	-1241.9	-18058.9	0.0	198.	-154.5	0.0	0.0	0.0	0.0	0.0
200	200.0	200.0	0.5	-25.3	-127.9	-6967.6	0.0	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	6.	-25.8	-2887.5	-2.3	-11.5	-1238.1	-17337.4	0.0	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	
252	-298.4	-444.2	0.5	-25.3	-167.3	-17376.7	0.0	0.	-1192.0	76.5	-34.6	0.0	-3625.6	6017.9	6.	-76.5	2886.5	-2.3	-11.5	-1238.1	-17337.4	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
294	-387.9	-596.8	0.5	-25.3	-188.0	-29407.7	0.0	21.	-1190.3	76.5	-34.6	0.0	-2912.6	7594.8	8.	-76.5	2885.9	-2.3	-11.5	-1233.3	-16094.7	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
336	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	41.	-1189.6	76.5	-34.6	0.0	-1189.6	7594.8	10.	-76.5	2884.9	-2.3	-11.5	-1227.7	-15653.2	0.0	50.	-152.0	0.0	0.0	0.0	0.0	0.0	
Asta	35	north	978	41	0.0	2078.1	18633.1	61.	-1188.0	76.5	-34.6	0.0	-1188.0	7594.8	10.	-76.5	2884.9	-2.3	-11.5	-1227.7	-15653.2	0.0	50.	-152.0	0.0	0.0	0.0	0.0	0.0	
0.	-52.1	76.7	-1.5	83.7	-192.8	-67690.4	0.0	103.	-1185.7	76.5	-34.6	0.0	-60.8	1300.2	4.	-74.5	1281.0	-9.4	-47.2	-1227.5	-16250.8	0.0	99.	-152.0	0.0	0.0	0.0	0.0	0.0	
19	-0.2	680.5	-1.5	83.7	-164.4	-54940.8	0.0	124.	-1184.1	76.5	-34.6	0.0	0.	552.2	1540.9	4.	-74.5	1274.1	-9.4	-47.2	-1074.7	-14180.1	0.0	124.	-152.0	0.0	0.0	0.0	0.0	0.0
38	-0.1	609.6	-1.5	83.7	-148.0	-41870.5	0.0	149.	-1183.4	76.5	-34.6	0.0	0.	1705.2	1705.2	16.	-74.5	1274.1	-9.4	-47.2	-1074.7	-14180.1	0.0	149.	-152.0	0.0	0.0	0.0	0.0	0.0
56	-52.1	53.0	-1.5	83.7	-107.5	-31180.6	0.0	174.	-1182.7	76.5	-34.6	0.0	0.	1705.2	1705.2	35.	-74.5	1267.2	-9.4	-47.2	-920.6	-12115.1	0.0	174.	-152.0	0.0	0.0	0.0	0.0	0.0
94	-52.1	327.8	-1.5	83.7	-50.7	-12420.8	0.0	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	65.	-74.5	1263.3	-9.4	-47.2	-613.8	-8018.6	0.0	Asta	71	north	342	728	MY	MZZ	
131	-52.1	294.9	-1.5	83.7	-26.7	-2210.0	0.0	0.	-598.8	-50.7	6.7	2.6	2246.5	1046.5	65.	-74.5	1263.3	-9.4	-47.2	-613.8	-8018.6	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
150	-52.1	214.9	-1.5	83.7	-6.7	-3221.0	0.0	42.	-596.2	-50.7	6.7	2.6	2003.2	8706.3	65.	-74.5	1263.3	-9.4	-47.2	-613.8	-8018.6	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	64.	-593.5	-50.7	6.7	2.6	1721.8	6385.1	114.	-74.5	1262.6	-9.4	-47.2	-153.4	-1800.0	0.0	25.	-64.2	0.0	0.0	0.0	0.0	0.0	0.0	
19	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	146.	-590.8	-50.7	6.7	2.6	1490.8	6107.7	130.	-74.5	1262.6	-9.4	-47.2	-153.4	-1800.0	0.0	74.	-64.2	0.0	0.0	0.0	0.0	0.0	
39	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	180.	-588.4	-50.7	6.7	2.6	1159.1	2342.7	130.	-74.5	1262.6	-9.4	-47.2	-153.4	-1800.0	0.0	74.	-64.2	0.0	0.0	0.0	0.0	0.0	
56	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	251.	-583.8	-50.7	6.7	2.6	596.3	-1899.7	130.	-74.5	1262.6	-9.4	-47.2	-153.4	-1800.0	0.0	74.	-64.2	0.0	0.0	0.0	0.0	0.0	
75	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	293.	-580.7	-50.7	6.7	2.6	580.7	-1899.7	130.	-74.5	1262.6	-9.4	-47.2	-153.4	-1800.0	0.0	74.	-64.2	0.0	0.0	0.0	0.0	0.0	
94	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	335.	-578.1	-50.7	6.7	2.6	33.6	-644.2	130.	-74.5	1262.6	-9.4	-47.2	-153.4	-1800.0	0.0	74.	-64.2	0.0	0.0	0.0	0.0	0.0	
113	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	49.	-29.8	-337.1	1.3	37.9	-61.5	-1058.1	0.0	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	
131	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	0.	-37.2	-130.9	39.1	195.5	0.0	185.9	0.	-29.8	-337.1	1.3	37.9	-61.5	-1058.1	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
150	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	16.	-37.2	-130.9	39.1	195.5	0.0	185.9	0.	0.	-37.2	-130.9	39.1	195.5	0.0	25.	-72.7	0.0	0.0	0.0	0.0	0.0	0.0	
Asta	37	north	472	731	MY	MZZ	33.	-37.2	-136.4	39.1	195.5	-1270.5	-4394.5	114.	-29.8	-364.8	1.3	37.9	-148.1	-3398.4	0.0	25.	-72.7	0.0	0.0	0.0	0.0	0.0	0.0	
0.	-287.7	-412.6	-0.7	32.8	-39.3	1852.1	0.0	49.	-37.2	-137.1	39.1	195.5	-1905.8	-6617.5	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
19	-198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	81.	-37.2	-138.5	39.1	195.5	-3176.4	-11079.3	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
38	-198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	130.	-37.2	-139.4	39.1	195.5	-4446.9	-15023.4	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
56	-198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	114.	-37.2	-139.4	39.1	195.5	-5082.2	-17569.9	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
75	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	Asta	39	north	472	731	MY	MZZ	1.	-250.0	-2226.4	-2.3	-245.4	-166.3	-3989.3	0.0	149.	-72.7	0.0	0.0	0.0	0.0	0.0	
94	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	0.	-37.2	-139.4	39.1	195.5	-5082.2	-17569.9	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
113	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	3.	-250.0	-2226.4	-2.3	-245.4	-166.3	-3989.3	0.0	149.	-72.7	0.0	0.0	0.0	0.0	0.0	
131	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	0.	-37.2	-139.4	39.1	195.5	-5082.2	-17569.9	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
150	198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	16.	-37.2	-139.4	39.1	195.5	-5082.2	-17569.9	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
Asta	39	north	472	731	MY	MZZ	16.	-37.2	-139.4	39.1	195.5	-5082.2	-17569.9	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.	-287.7	-412.6	-0.7	32.8	-39.3	1852.1	0.0	PROGR.	NORM	TTY	TZZ	TORS	MY	MZZ	1.	-250.0	-2226.4	-2.3	-245.4	-166.3	-3989.3	0.0	149.	-72.7	0.0	0.0	0.0	0.0	0.0	
19	-198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	0.	-37.2	-139.4	39.1	195.5	-5082.2	-17569.9	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
38	-198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	16.	-37.2	-139.4	39.1	195.5	-5082.2	-17569.9	130.	-29.8	-371.7	1.3	37.9	-169.3	-3998.8	0.0	0.	-152.0	0.0	0.0	0.0	0.0	0.0	
56	-198.2	-276.0	0.5	-21.4	-131.7	109.5	0.0	114.	-37.2	-139.4	39.1	195.5	-5082.2																	

2.	-361.3	7.6	1068.2	0.0	3388.2	-23.7	5.	-1349.8	39.1	37.2	0.0	0.0	0.0	1.	-311.3	-168.0	-68.0	0.0	-255.2	-75.2	4.	-484.3	1.8	1.2	0.0	0.8	-1.1
3.	-361.2	7.6	1068.2	0.0	2670.6	-19.0	6.	-1029.1	21.5	11	471			2.	-311.2	20.0	-68.0	0.0	-212.7	-62.7	5.	-484.1	1.8	1.2	0.0	0.0	0.0
4.	-361.0	7.6	1068.2	0.0	3021.9	-24.2	7.	-1029.1	21.5	12	471			3.	-311.1	20.0	-68.0	0.0	-170.1	-145.1	6.	-1029.1	21.5	1.2	0.0	0.0	0.0
5.	-360.9	7.6	1068.2	0.0	1335.3	-9.5	8.	-1406.4	-110.4	-0.1	0.0	MY	MZZ	4.	-310.9	20.0	-68.0	0.0	-127.6	-37.6	7.	-1029.1	21.5	1.2	0.0	0.0	0.0
6.	-360.8	7.6	1068.2	0.0	667.6	-0.0	9.	-1405.2	-110.4	-0.1	0.0	-0.6	483.1	0.	-310.8	20.0	-68.0	0.0	-85.1	-25.1	8.	-1405.2	21.5	1.2	0.0	0.0	0.0
7.	-360.6	7.6	1068.2	0.0	0.0	0.0	10.	-1405.1	-110.4	-0.1	0.0	-0.4	345.1	0.	-310.7	20.0	-68.0	0.0	-42.1	-12.1	9.	-1405.1	21.5	1.2	0.0	0.0	0.0
8.	-360.4	7.6	1068.2	0.0	0.0	0.0	11.	-1405.0	-110.4	-0.1	0.0	-0.4	345.1	0.	-310.6	20.0	-68.0	0.0	-42.1	-12.1	10.	-1405.0	21.5	1.2	0.0	0.0	0.0
9.	-360.2	7.6	1068.2	0.0	0.0	0.0	12.	-1404.9	-110.4	-0.1	0.0	-0.4	345.1	0.	-310.5	20.0	-68.0	0.0	-42.1	-12.1	11.	-1404.9	21.5	1.2	0.0	0.0	0.0
10.	-360.0	7.6	1068.2	0.0	0.0	0.0	13.	-1404.8	-110.4	-0.1	0.0	-0.4	345.1	0.	-310.4	20.0	-68.0	0.0	-42.1	-12.1	12.	-1404.8	21.5	1.2	0.0	0.0	0.0
11.	-359.8	7.6	1068.2	0.0	0.0	0.0	14.	-1404.7	-110.4	-0.1	0.0	-0.4	345.1	0.	-310.3	20.0	-68.0	0.0	-42.1	-12.1	13.	-1404.7	21.5	1.2	0.0	0.0	0.0
12.	-359.6	7.6	1068.2	0.0	0.0	0.0	15.	-1404.6	-110.4	-0.1	0.0	-0.4	345.1	0.	-310.2	20.0	-68.0	0.0	-42.1	-12.1	14.	-1404.6	21.5	1.2	0.0	0.0	0.0
13.	-359.4	7.6	1068.2	0.0	0.0	0.0	16.	-1404.5	-110.4	-0.1	0.0	-0.4	345.1	0.	-310.1	20.0	-68.0	0.0	-42.1	-12.1	15.	-1404.5	21.5	1.2	0.0	0.0	0.0
14.	-359.2	7.6	1068.2	0.0	0.0	0.0	17.	-1404.4	-110.4	-0.1	0.0	-0.4	345.1	0.	-310.0	20.0	-68.0	0.0	-42.1	-12.1	16.	-1404.4	21.5	1.2	0.0	0.0	0.0
15.	-359.0	7.6	1068.2	0.0	0.0	0.0	18.	-1404.3	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.9	20.0	-68.0	0.0	-42.1	-12.1	17.	-1404.3	21.5	1.2	0.0	0.0	0.0
16.	-358.8	7.6	1068.2	0.0	0.0	0.0	19.	-1404.2	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.8	20.0	-68.0	0.0	-42.1	-12.1	18.	-1404.2	21.5	1.2	0.0	0.0	0.0
17.	-358.6	7.6	1068.2	0.0	0.0	0.0	20.	-1404.1	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.7	20.0	-68.0	0.0	-42.1	-12.1	19.	-1404.1	21.5	1.2	0.0	0.0	0.0
18.	-358.4	7.6	1068.2	0.0	0.0	0.0	21.	-1404.0	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.6	20.0	-68.0	0.0	-42.1	-12.1	20.	-1404.0	21.5	1.2	0.0	0.0	0.0
19.	-358.2	7.6	1068.2	0.0	0.0	0.0	22.	-1403.9	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.5	20.0	-68.0	0.0	-42.1	-12.1	21.	-1403.9	21.5	1.2	0.0	0.0	0.0
20.	-358.0	7.6	1068.2	0.0	0.0	0.0	23.	-1403.8	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.4	20.0	-68.0	0.0	-42.1	-12.1	22.	-1403.8	21.5	1.2	0.0	0.0	0.0
21.	-357.8	7.6	1068.2	0.0	0.0	0.0	24.	-1403.7	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.3	20.0	-68.0	0.0	-42.1	-12.1	23.	-1403.7	21.5	1.2	0.0	0.0	0.0
22.	-357.6	7.6	1068.2	0.0	0.0	0.0	25.	-1403.6	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.2	20.0	-68.0	0.0	-42.1	-12.1	24.	-1403.6	21.5	1.2	0.0	0.0	0.0
23.	-357.4	7.6	1068.2	0.0	0.0	0.0	26.	-1403.5	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.1	20.0	-68.0	0.0	-42.1	-12.1	25.	-1403.5	21.5	1.2	0.0	0.0	0.0
24.	-357.2	7.6	1068.2	0.0	0.0	0.0	27.	-1403.4	-110.4	-0.1	0.0	-0.4	345.1	0.	-309.0	20.0	-68.0	0.0	-42.1	-12.1	26.	-1403.4	21.5	1.2	0.0	0.0	0.0
25.	-357.0	7.6	1068.2	0.0	0.0	0.0	28.	-1403.3	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.9	20.0	-68.0	0.0	-42.1	-12.1	27.	-1403.3	21.5	1.2	0.0	0.0	0.0
26.	-356.8	7.6	1068.2	0.0	0.0	0.0	29.	-1403.2	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.8	20.0	-68.0	0.0	-42.1	-12.1	28.	-1403.2	21.5	1.2	0.0	0.0	0.0
27.	-356.6	7.6	1068.2	0.0	0.0	0.0	30.	-1403.1	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.7	20.0	-68.0	0.0	-42.1	-12.1	29.	-1403.1	21.5	1.2	0.0	0.0	0.0
28.	-356.4	7.6	1068.2	0.0	0.0	0.0	31.	-1403.0	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.6	20.0	-68.0	0.0	-42.1	-12.1	30.	-1403.0	21.5	1.2	0.0	0.0	0.0
29.	-356.2	7.6	1068.2	0.0	0.0	0.0	32.	-1402.9	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.5	20.0	-68.0	0.0	-42.1	-12.1	31.	-1402.9	21.5	1.2	0.0	0.0	0.0
30.	-356.0	7.6	1068.2	0.0	0.0	0.0	33.	-1402.8	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.4	20.0	-68.0	0.0	-42.1	-12.1	32.	-1402.8	21.5	1.2	0.0	0.0	0.0
31.	-355.8	7.6	1068.2	0.0	0.0	0.0	34.	-1402.7	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.3	20.0	-68.0	0.0	-42.1	-12.1	33.	-1402.7	21.5	1.2	0.0	0.0	0.0
32.	-355.6	7.6	1068.2	0.0	0.0	0.0	35.	-1402.6	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.2	20.0	-68.0	0.0	-42.1	-12.1	34.	-1402.6	21.5	1.2	0.0	0.0	0.0
33.	-355.4	7.6	1068.2	0.0	0.0	0.0	36.	-1402.5	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.1	20.0	-68.0	0.0	-42.1	-12.1	35.	-1402.5	21.5	1.2	0.0	0.0	0.0
34.	-355.2	7.6	1068.2	0.0	0.0	0.0	37.	-1402.4	-110.4	-0.1	0.0	-0.4	345.1	0.	-308.0	20.0	-68.0	0.0	-42.1	-12.1	36.	-1402.4	21.5	1.2	0.0	0.0	0.0
35.	-355.0	7.6	1068.2	0.0	0.0	0.0	38.	-1402.3	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.9	20.0	-68.0	0.0	-42.1	-12.1	37.	-1402.3	21.5	1.2	0.0	0.0	0.0
36.	-354.8	7.6	1068.2	0.0	0.0	0.0	39.	-1402.2	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.8	20.0	-68.0	0.0	-42.1	-12.1	38.	-1402.2	21.5	1.2	0.0	0.0	0.0
37.	-354.6	7.6	1068.2	0.0	0.0	0.0	40.	-1402.1	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.7	20.0	-68.0	0.0	-42.1	-12.1	39.	-1402.1	21.5	1.2	0.0	0.0	0.0
38.	-354.4	7.6	1068.2	0.0	0.0	0.0	41.	-1402.0	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.6	20.0	-68.0	0.0	-42.1	-12.1	40.	-1402.0	21.5	1.2	0.0	0.0	0.0
39.	-354.2	7.6	1068.2	0.0	0.0	0.0	42.	-1401.9	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.5	20.0	-68.0	0.0	-42.1	-12.1	41.	-1401.9	21.5	1.2	0.0	0.0	0.0
40.	-354.0	7.6	1068.2	0.0	0.0	0.0	43.	-1401.8	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.4	20.0	-68.0	0.0	-42.1	-12.1	42.	-1401.8	21.5	1.2	0.0	0.0	0.0
41.	-353.8	7.6	1068.2	0.0	0.0	0.0	44.	-1401.7	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.3	20.0	-68.0	0.0	-42.1	-12.1	43.	-1401.7	21.5	1.2	0.0	0.0	0.0
42.	-353.6	7.6	1068.2	0.0	0.0	0.0	45.	-1401.6	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.2	20.0	-68.0	0.0	-42.1	-12.1	44.	-1401.6	21.5	1.2	0.0	0.0	0.0
43.	-353.4	7.6	1068.2	0.0	0.0	0.0	46.	-1401.5	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.1	20.0	-68.0	0.0	-42.1	-12.1	45.	-1401.5	21.5	1.2	0.0	0.0	0.0
44.	-353.2	7.6	1068.2	0.0	0.0	0.0	47.	-1401.4	-110.4	-0.1	0.0	-0.4	345.1	0.	-307.0	20.0	-68.0	0.0	-42.1	-12.1	46.	-1401.4	21.5	1.2	0.0	0.0	0.0
45.	-353.0	7.6	1068.2	0.0	0.0	0.0	48.	-1401.3	-110.4	-0.1	0.0	-0.4	345.1	0.	-306.9	20.0	-68.0	0.0	-42.1	-12.1	47.	-1401.3	21.5	1.2	0.0	0.0	0.0
46.	-352.8	7.6	1068.2	0.0	0.0	0.0	49.	-1401.2	-110.4	-0.1	0.0	-0.4	345.1	0.	-306.8	20.0	-68.0	0.0	-42.1	-12.1	48.	-1401.2	21.5	1.2	0.0	0.0	0.0
47.	-352.6	7.6	1068.2	0.0	0.0	0.0	50.	-1401.1	-110.4	-0.1	0.0	-0.4	345.1	0.	-306.7	20.0	-68.0	0.0	-42.1	-12.1	49.	-1401.1	21.5	1.2	0.0	0.0	0.0
48.	-352.4	7.6	1068.2	0.0	0.0	0.0	51.	-1401.0	-110.4	-0.1	0.0	-0.4	345.1	0.	-306.6	20.0	-68.0	0.0	-42.1	-12.1	50.	-1401.0	21.5	1.2	0.0	0.0	0.0
49.	-352.2	7.6	1068.2	0.0	0.0	0.0	52.	-1400.9	-110.4	-0.1	0.0	-0.4	345.1	0.	-306.5	20.0	-68.0	0.0	-42.1	-12.1	51.	-1400.9	21.5	1.2	0.0	0.0	0.0
50.	-352.0	7.6	1068.2	0.0	0.0	0.0	53.	-1400.8	-110.4	-0.1	0.0	-0.4	345.1	0.	-306.4	20.0	-68.0	0.0	-42.1	-12.1	52.	-1400.8	21.5	1.2	0.0	0.0	0.0
51.	-351.8	7.6	1068.2	0.0	0.0	0.0	54.	-1400.7	-110.4	-0.1	0.0	-0.4	345.1	0.	-306.3	20.0	-68.0	0.0	-42.1	-12.1	53.	-1400.7	21.5	1.2	0.0	0.0	0.0
52.	-351.6	7.6	1068.2	0.0	0.0	0.0	55.	-1400.6	-110.4</																		

34/136

128.	-4385.2	86.5	-1.8	-0.3	-347.3	-10222.8	16.	-61.2	-843.1	-36.9	-184.7	600.4	-2540.6	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ		20.	-89.9	-18.6	-73.9	-11.6	239.0	-14348.6	
	-4461.1	39.3	-3.0	-4.8	-306.9	-8042.6		-59.3	-817.4	-41.6	-208.1	676.5	-2483.3		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2		-116.4	-18.1	-69.7	-11.0	95.1	-14495.2	
	-4559.1	86.5	-1.8	-0.0	-259.2	-8501.8	33.	-59.3	-850.8	-36.9	-184.7	600.4	-2540.6		0.	-100.0	1298.4	-6.7	-33.7	-876.7	-164686.2	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ
170.	-4435.0	39.3	-3.0	-4.8	-179.6	-6371.7		-59.3	-824.3	-41.6	-208.1	1353.0	-15797.4	16.	-100.0	1294.6	-6.7	-33.7	-767.2	-143644.0		0.	-6.2	121.3	-3.1	76.7	-183.4	-14028.3	
213.	-4333.1	86.5	-1.8	-0.0	-196.9	-2863.8		-61.2	-857.0	-36.9	-184.7	1801.2	-30367.6	33.	-100.0	1256.8	-12.1	-60.7	-1381.0	-159956.3		16.	-6.2	121.3	-3.1	76.7	-183.4	-14028.3	
255.	-4382.9	39.3	-3.0	-4.8	-81.3	-3814.3	65.	-61.2	-851.3	-41.6	-208.1	1353.0	-15797.4	33.	-100.0	1256.8	-12.1	-60.7	-1381.0	-159956.3		16.	-6.2	121.3	-3.1	76.7	-183.4	-14028.3	
	-4307.0	86.5	-1.8	-0.3	-121.7	-808.3		-61.2	-863.9	-36.9	-184.7	2401.2	-44150.0	49.	-100.0	1249.9	-12.1	-60.7	-1181.7	-115958.8		16.	-6.2	121.3	-3.1	76.7	-183.4	-14028.3	
298.	-4356.9	39.3	-3.0	-4.8	-254.9	-8485.3	81.	-61.2	-870.8	-36.9	-184.7	3002.0	-58245.0	49.	-100.0	1249.9	-12.1	-60.7	-1181.7	-115958.8		33.	-6.2	115.1	-3.1	76.7	-183.4	-14028.3	
340.	-4330.8	39.3	-3.0	-4.8	-329.6	-8127.1	98.	-59.3	-845.1	-41.6	-208.1	3382.4	-64990.2	65.	-100.0	1270.7	-6.7	-33.7	-438.4	-93335.9		49.	-6.2	117.0	-3.2	75.4	-171.4	-10322.6	
	-4028.9	86.5	-1.8	-0.0	-100.0	-1183.9	114.	-59.3	-852.0	-41.6	-208.1	4075.9	-70279.6	81.	-100.0	1263.7	-6.7	-33.7	-328.8	-60010.5		33.	-6.2	114.0	-3.2	75.4	-171.4	-10322.6	
ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	130.	-59.3	-851.6	-41.6	-208.1	4735.3	-84181.5	98.	-100.0	1256.8	-6.7	-33.7	-219.2	-40812.0		65.	-6.2	109.0	-3.2	75.4	-171.4	-10322.6
0.	-1121.1	22.8	-32.2	0.0	-3314.7	16129.2		-59.3	-865.9	-41.6	-208.1	5411.8	-98396.0	114.	-100.0	1249.9	-6.7	-33.7	-109.6	-1079.1		81.	-6.2	101.7	-3.2	75.4	-171.4	-10322.6	
21.	-11082.8	130.1	-36.9	0.0	-3996.5	-4029.3	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		98.	-6.2	102.9	-3.1	75.4	-171.4	-10322.6
41.	-11895.9	130.1	-36.9	0.0	-1985.0	17071.2		0.	-2569.0	247.8	1258.1	4803.1	-138932.2	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		114.	-6.2	99.8	-3.1	75.4	-171.4	-10322.6	
	-11897.5	130.1	-36.9	0.0	-2414.3	1272.2		1.1	-2569.5	247.8	1258.1	4493.4	-142143.8	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
62.	-11883.2	22.8	-32.2	0.0	-1520.1	17542.3		0.6	-2564.0	328.0	1210.7	5091.9	-175990.8	0.	-30.7	-309.1	1.3	47.5	0.0	5267.2		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
83.	-11884.8	130.1	-36.9	0.0	-1653.3	3954.9	3.	0.6	-2561.0	328.0	1210.7	4591.9	-141393.7	16.	-30.7	-316.0	1.3	47.5	-21.6	188.0		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
	-11870.6	22.8	-32.2	0.0	-655.2	18013.3		4.1	-2570.6	247.8	1258.1	4803.1	-138932.2	33.	-30.7	-323.0	1.3	47.5	-43.2	-5003.8		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
103.	-11857.9	22.8	-32.2	0.0	9.6	8484.4	5.	0.6	-2561.5	328.0	1210.7	4181.9	-144393.2	49.	-30.7	-329.9	1.3	47.5	-64.8	-10308.1		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
124.	-11845.3	22.8	-32.2	0.0	674.5	18955.4	6.	0.6	-2562.0	328.0	1210.7	3772.0	-147595.4	65.	-28.9	-344.3	1.3	47.5	-62.1	-10864.2		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
	-11846.9	130.1	-36.9	0.0	629.9	12003.3	8.	1.1	-2571.6	247.8	1258.1	3254.3	-154996.6	81.	-28.9	-351.3	1.3	47.5	-62.1	-10864.2		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
144.	-11832.6	22.8	-32.2	0.0	1333.4	19405.4	9.	1.1	-2572.2	247.8	1258.1	2944.6	-158211.5	98.	-30.7	-343.7	1.3	47.5	-68.4	-11573.0		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
	-11834.2	130.1	-36.9	0.0	1391.0	14685.9	11.	1.1	-2572.7	247.8	1258.1	2634.8	-161427.0	114.	-30.7	-343.7	1.3	47.5	-68.4	-11573.0		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
165.	-11820.0	22.8	-32.2	0.0	2004.2	19897.4	12.	0.6	-2562.6	328.0	1210.7	2542.1	-157025.9	130.	-30.7	-357.6	1.3	47.5	-151.2	-13651.0		130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
	-11821.6	130.1	-36.9	0.0	2152.0	17388.7	13.	0.6	-2564.2	328.0	1210.7	2132.2	-160104.8	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
0.	-5996.5	-76.3	6.5	6.0	2197.7	15102.9	ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
42.	-5977.2	-25.0	7.0	6.0	1927.0	11097.3	1.	-54.7	5807.8	289.8	1394.4	2232.8	-153167.3	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
84.	-5951.6	-25.0	7.0	6.0	1807.3	5505.4	3.	-54.7	5807.2	289.8	1394.4	1936.6	-144537.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
126.	-5949.4	-25.0	7.0	6.0	1787.3	4458.6	1.	-54.7	5807.2	289.8	1394.4	1936.6	-144537.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
	-5900.2	-25.0	7.0	6.0	1495.2	3411.8	3.	-54.7	5806.7	289.8	1394.4	1568.3	-137099.2	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
209.	-5848.9	-25.0	7.0	6.0	844.3	-875.4	5.	-54.7	5806.2	289.8	1394.4	1153.3	-110725.2	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
251.	-5842.4	-25.0	7.0	6.0	573.7	-407.0	6.	-54.7	5806.2	289.8	1394.4	835.4	-104762.6	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
293.	-5816.8	-25.0	7.0	6.0	303.0	-726.7	8.	-54.7	5806.2	289.8	1394.4	519.1	-100701.1	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
335.	-5791.1	-25.0	7.0	6.0	-326.9	-775.2	10.	-54.7	5806.2	289.8	1394.4	19.1	-100701.1	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
0.	-45.1	-1342.9	37.4	186.8	0.0	225.3	1.	-54.7	5805.5	289.8	1394.4	-436.4	-80736.7	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
16.	-45.1	-1349.8	37.4	186.8	-607.0	-2162.6	16.	-54.7	5805.5	289.8	1394.4	-436.4	-80736.7	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
49.	-45.1	-1356.7	37.4	186.8	-1214.1	-14363.0	13.1	-54.7	5805.5	289.8	1394.4	-436.4	-80736.7	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
65.	-45.1	-1372.7	37.4	186.8	-1807.5	-26605.1	13.1	-54.7	5805.5	289.8	1394.4	-436.4	-80736.7	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
81.	-45.1	-1386.6	37.4	186.8	-2404.0	-39808.8	13.1	-54.7	5805.5	289.8	1394.4	-436.4	-80736.7	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
98.	-45.1	-1393.5	37.4	186.8	-3011.5	-53097.9	13.1	-54.7	5805.5	289.8	1394.4	-436.4	-80736.7	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
114.	-45.1	-1404.4	37.4	186.8	-3618.2	-67370.4	13.1	-54.7	5805.5	289.8	1394.4	-436.4	-80736.7	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
130.	-45.1	-1414.3	37.4	186.8	-4224.9	-81723.1	13.1	-54.7	5805.5	289.8	1394.4	-436.4	-80736.7	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
ASTA	PROGR.	NORM	TYT	TZZ	TORS	MYT	MZZ	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	
0.	-67.7	1309.8	-27.9	-139.4	-3624.6	-167226.8	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9	130.	-100.0	1245.0	-6.7	-33.7	-197.3	-19465.9		
16.	-67.7	1309.8	-27.9	-1																									

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126.	-44.5	-11.7	-0.3	20.5	77.1	-7099.9	130.	69.8	989.4	-19.4	-97.2	0.0	-349.2	3.	-180.2	1072.2	-3.5	-21.3	-101.1	-31368.5	231.	-5.6	0.0	0.0	0.0	0.0
168.	253.0	106.9	-0.3	20.5	91.1	-5100.4	131.	69.8	989.4	-19.4	-97.2	0.0	-349.2	4.	-180.2	1071.7	-3.5	-21.3	-96.7	-3003.6	264.	-5.6	0.0	0.0	0.0	0.0
210.	94.4	137.1	-0.3	20.5	101.1	-5100.4	132.	69.8	989.4	-19.4	-97.2	0.0	-349.2	5.	-180.2	1071.2	-3.5	-21.3	-91.2	-3003.6	298.	-5.6	0.0	0.0	0.0	0.0
252.	163.9	343.9	-0.3	20.5	119.2	-13840.3	133.	69.8	989.4	-19.4	-97.2	0.0	-349.2	6.	-180.2	1070.6	-3.5	-21.3	-87.9	-2730.7	331.	-5.6	0.0	0.0	0.0	0.0
294.	233.4	462.4	-0.3	20.5	133.2	-20781.5	134.	69.8	989.4	-19.4	-97.2	0.0	-349.2	7.	-180.2	1070.1	-3.5	-21.3	-83.5	-2602.7	365.	-5.6	0.0	0.0	0.0	0.0
336.	301.9	581.0	-0.3	20.5	147.2	-27617.7	135.	69.8	989.4	-19.4	-97.2	0.0	-349.2	8.	-180.2	1069.6	-3.5	-21.3	-79.0	-2467.5	399.	-5.6	0.0	0.0	0.0	0.0
378.	370.4	700.5	-0.3	20.5	161.3	-34523.9	136.	69.8	989.4	-19.4	-97.2	0.0	-349.2	9.	-180.2	1069.1	-3.5	-21.3	-74.5	-2338.9	433.	-5.6	0.0	0.0	0.0	0.0
420.	439.9	819.0	-0.3	20.5	175.4	-41430.1	137.	69.8	989.4	-19.4	-97.2	0.0	-349.2	10.	-180.2	1068.6	-3.5	-21.3	-69.5	-2210.3	467.	-5.6	0.0	0.0	0.0	0.0
462.	509.4	938.0	-0.3	20.5	189.5	-48336.3	138.	69.8	989.4	-19.4	-97.2	0.0	-349.2	11.	-180.2	1068.1	-3.5	-21.3	-64.5	-2081.7	501.	-5.6	0.0	0.0	0.0	0.0
504.	579.9	1057.0	-0.3	20.5	203.6	-55242.5	139.	69.8	989.4	-19.4	-97.2	0.0	-349.2	12.	-180.2	1067.6	-3.5	-21.3	-59.5	-1953.1	535.	-5.6	0.0	0.0	0.0	0.0
546.	649.4	1176.0	-0.3	20.5	217.7	-62148.7	140.	69.8	989.4	-19.4	-97.2	0.0	-349.2	13.	-180.2	1067.1	-3.5	-21.3	-54.5	-1824.5	569.	-5.6	0.0	0.0	0.0	0.0
588.	719.9	1295.0	-0.3	20.5	231.8	-69054.9	141.	69.8	989.4	-19.4	-97.2	0.0	-349.2	14.	-180.2	1066.6	-3.5	-21.3	-49.5	-1695.9	603.	-5.6	0.0	0.0	0.0	0.0
630.	789.4	1414.0	-0.3	20.5	245.9	-75961.1	142.	69.8	989.4	-19.4	-97.2	0.0	-349.2	15.	-180.2	1066.1	-3.5	-21.3	-44.5	-1567.3	637.	-5.6	0.0	0.0	0.0	0.0
672.	859.9	1533.0	-0.3	20.5	260.0	-82867.3	143.	69.8	989.4	-19.4	-97.2	0.0	-349.2	16.	-180.2	1065.6	-3.5	-21.3	-39.5	-1438.7	671.	-5.6	0.0	0.0	0.0	0.0
714.	929.4	1652.0	-0.3	20.5	274.1	-89773.5	144.	69.8	989.4	-19.4	-97.2	0.0	-349.2	17.	-180.2	1065.1	-3.5	-21.3	-34.5	-1310.1	705.	-5.6	0.0	0.0	0.0	0.0
756.	999.9	1771.0	-0.3	20.5	288.2	-96679.7	145.	69.8	989.4	-19.4	-97.2	0.0	-349.2	18.	-180.2	1064.6	-3.5	-21.3	-29.5	-1181.5	739.	-5.6	0.0	0.0	0.0	0.0
798.	1069.4	1890.0	-0.3	20.5	302.3	-103585.9	146.	69.8	989.4	-19.4	-97.2	0.0	-349.2	19.	-180.2	1064.1	-3.5	-21.3	-24.5	-1052.9	773.	-5.6	0.0	0.0	0.0	0.0
840.	1139.9	2009.0	-0.3	20.5	316.4	-110492.1	147.	69.8	989.4	-19.4	-97.2	0.0	-349.2	20.	-180.2	1063.6	-3.5	-21.3	-19.5	-924.3	807.	-5.6	0.0	0.0	0.0	0.0
882.	1209.4	2128.0	-0.3	20.5	330.5	-117398.3	148.	69.8	989.4	-19.4	-97.2	0.0	-349.2	21.	-180.2	1063.1	-3.5	-21.3	-14.5	-795.7	841.	-5.6	0.0	0.0	0.0	0.0
924.	1279.9	2247.0	-0.3	20.5	344.6	-124304.5	149.	69.8	989.4	-19.4	-97.2	0.0	-349.2	22.	-180.2	1062.6	-3.5	-21.3	-9.5	-667.1	875.	-5.6	0.0	0.0	0.0	0.0
966.	1349.4	2366.0	-0.3	20.5	358.7	-131210.7	150.	69.8	989.4	-19.4	-97.2	0.0	-349.2	23.	-180.2	1062.1	-3.5	-21.3	-4.5	-538.5	909.	-5.6	0.0	0.0	0.0	0.0
1008.	1419.9	2485.0	-0.3	20.5	372.8	-138116.9	151.	69.8	989.4	-19.4	-97.2	0.0	-349.2	24.	-180.2	1061.6	-3.5	-21.3	0.5	-409.9	943.	-5.6	0.0	0.0	0.0	0.0
1050.	1489.4	2604.0	-0.3	20.5	386.9	-145023.1	152.	69.8	989.4	-19.4	-97.2	0.0	-349.2	25.	-180.2	1061.1	-3.5	-21.3	5.5	-281.3	977.	-5.6	0.0	0.0	0.0	0.0
1092.	1559.9	2723.0	-0.3	20.5	401.0	-151929.3	153.	69.8	989.4	-19.4	-97.2	0.0	-349.2	26.	-180.2	1060.6	-3.5	-21.3	10.5	-152.7	1011.	-5.6	0.0	0.0	0.0	0.0
1134.	1629.4	2842.0	-0.3	20.5	415.1	-158835.5	154.	69.8	989.4	-19.4	-97.2	0.0	-349.2	27.	-180.2	1060.1	-3.5	-21.3	15.5	-24.1	1045.	-5.6	0.0	0.0	0.0	0.0
1176.	1699.9	2961.0	-0.3	20.5	429.2	-165741.7	155.	69.8	989.4	-19.4	-97.2	0.0	-349.2	28.	-180.2	1059.6	-3.5	-21.3	20.5	7.5	1079.	-5.6	0.0	0.0	0.0	0.0
1218.	1769.4	3080.0	-0.3	20.5	443.3	-172647.9	156.	69.8	989.4	-19.4	-97.2	0.0	-349.2	29.	-180.2	1059.1	-3.5	-21.3	25.5	15.5	1113.	-5.6	0.0	0.0	0.0	0.0
1260.	1839.9	3199.0	-0.3	20.5	457.4	-179554.1	157.	69.8	989.4	-19.4	-97.2	0.0	-349.2	30.	-180.2	1058.6	-3.5	-21.3	30.5	23.5	1147.	-5.6	0.0	0.0	0.0	0.0
1302.	1909.4	3318.0	-0.3	20.5	471.5	-186460.3	158.	69.8	989.4	-19.4	-97.2	0.0	-349.2	31.	-180.2	1058.1	-3.5	-21.3	35.5	31.5	1181.	-5.6	0.0	0.0	0.0	0.0
1344.	1979.9	3437.0	-0.3	20.5	485.6	-193366.5	159.	69.8	989.4	-19.4	-97.2	0.0	-349.2	32.	-180.2	1057.6	-3.5	-21.3	40.5	39.5	1215.	-5.6	0.0	0.0	0.0	0.0
1386.	2049.4	3556.0	-0.3	20.5	499.7	-200272.7	160.	69.8	989.4	-19.4	-97.2	0.0	-349.2	33.	-180.2	1057.1	-3.5	-21.3	45.5	47.5	1249.	-5.6	0.0	0.0	0.0	0.0
1428.	2119.9	3675.0	-0.3	20.5	513.8	-207178.9	161.	69.8	989.4	-19.4	-97.2	0.0	-349.2	34.	-180.2	1056.6	-3.5	-21.3	50.5	55.5	1283.	-5.6	0.0	0.0	0.0	0.0
1470.	2189.4	3794.0	-0.3	20.5	527.9	-214085.1	162.	69.8	989.4	-19.4	-97.2	0.0	-349.2	35.	-180.2	1056.1	-3.5	-21.3	55.5	63.5	1317.	-5.6	0.0	0.0	0.0	0.0
1512.	2259.9	3913.0	-0.3	20.5	542.0	-221000.3	163.	69.8	989.4	-19.4	-97.2	0.0	-349.2	36.	-180.2	1055.6	-3.5	-21.3	60.5	71.5	1351.	-5.6	0.0	0.0	0.0	0.0
1554.	2329.4	4032.0	-0.3	20.5	556.1	-227906.5	164.	69.8	989.4	-19.4	-97.2	0.0	-349.2	37.	-180.2	1055.1	-3.5	-21.3	65.5	79.5	1385.	-5.6	0.0	0.0	0.0	0.0
1596.	2399.9	4151.0	-0.3	20.5	570.2	-234812.7	165.	69.8	989.4	-19.4	-97.2	0.0	-349.2	38.	-180.2	1054.6	-3.5	-21.3	70.5	87.5	1419.	-5.6	0.0	0.0	0.0	0.0
1638.	2469.4	4270.0	-0.3	20.5	584.3	-241718.9	166.	69.8	989.4	-19.4	-97.2	0.0	-349.2	39.	-180.2	1054.1	-3.5	-21.3	75.5	95.5	1453.	-5.6	0.0	0.0	0.0	0.0
1680.	2539.9	4389.0	-0.3	20.5	598.4	-248625.1	167.	69.8	989.4	-19.4	-97.2	0.0	-349.2	40.	-180.2	1053.6	-3.5	-21.3	80.5	103.5	1487.	-5.6	0.0	0.0	0.0	0.0
1722.	2609.4	4508.0	-0.3	20.5	612.5	-255531.3	168.	69.8	989.4	-19.4	-97.2	0.0	-349.2	41.	-180.2	1053.1	-3.5	-21.3	85.5	111.5	1521.	-5.6	0.0	0.0	0.0	0.0
1764.	2679.9	4627.0	-0.3	20.5	626.6	-262437.5	169.	69.8	989.4	-19.4	-97.2	0.0	-349.2	42.	-180.2	1052.6	-3.5	-21.3	90.5	119.5	1555.	-5.6	0.0	0.0	0.0	0.0
1806.	2749.4	4746.0	-0.3	20.5	640.7	-269343.7	170.	69.8	989.4	-19.4	-97.2	0.0	-349.2	43.	-180.2	1052.1	-3.5	-21.3	95.5	127.5	1589.	-5.6	0.0	0.0	0.0	0.0
1848.	2819.9	4865.0	-0.3	20.5	654.8	-276249.9	171.	69.8	989.4	-19.4	-97.2	0.0	-349.2	44.	-180.2	1051.6	-3.5	-21.3	100.5	135.5	1623.	-5.6	0.0	0.0	0.0	0.0
1890.	2889.4	4984.0	-0.3	20.5	668.9	-283156.1	172.	69.8	989.4	-19.4	-97.2	0.0	-349.2	45.	-180.2	1051.1	-3.5	-21.3	105.5	143.5	1657.	-5.6	0.0	0.0	0.0	0.0
1932.	2959.9	5103.0	-0.3	20.5	683.0	-290062.3	173.	69.8	989.4	-19.4	-97.2	0.0	-349.2	46.	-180.2	1050.6	-3.5	-21.3	110.5	151.5	1691.	-5.6	0.0	0.0	0.0	0.0
1974.	3029.4	5222.0	-0.3	20.5	697.1	-296968.5	174.	69.8	989.4	-19.4	-97.2	0.0	-349.2	47.	-180.2	1050.1	-3.5	-21.3	115.5	159.5	1725.	-5.6	0.0	0.0	0.0	0.0
2016.	3099.9	5341.0	-0.3	20.5	711.2	-303874.7	175.	69.8	989.4	-19.4	-97.2	0.0	-349.2	48.	-180.2	1049.6	-3.5	-21.3	120.5	167.5	1759.	-5.6	0.0	0.0	0.0	0.0
2058.	3169.4	5460.0	-0.3	20.5	725.3	-310780.9	176.	69.8	989.4	-19.4	-97.2	0.0	-349.2	49.	-180.2	1049.1	-3.5	-21.3	125.5	175.5	1793.	-5.6	0.0	0.0	0.0	0.0
2100.	3239.9	5579.0	-0.3	20.5	739.4	-317687.1	177.	69.8	989.4	-19.4	-97.2	0.0	-349.2	50.	-180.2	1048.6	-3.5	-21.3	130.5	183.5	1827.	-5.6	0.0	0.0	0.0	0.0
2142.	3309.4	5698.0	-0.3	20.5	753.5	-324593.3	178.	69.8	989.4	-19.4	-97.2	0.0	-349.2	51.	-180.2	1048.1	-3.5	-21.3	135.5	191.5	1861.	-5.6	0.0	0.0	0.0	0.0
2184.	3379.9	5817.0	-0.3	20.5	767.6	-331499.5	179.	69.8	989.4																	

1.	-1292.0	-15.7	-1.6	0.0	-6.9	68.8	248.	-1762.5	-5.1	4.7	0.0	-2322.4	7084.3	0.	280.2	302.6	0.1	0.0	0.0	209.	-873.2	0.3	16.8	2.5	2390.2	3189.1					
1.	-1291.9	-15.7	-1.6	0.0	-5.9	58.9	289.	-1737.3	-5.1	4.7	0.0	-2317.5	6875.1	29.	280.2	208.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1				
2.	-1291.7	-15.7	-1.6	0.0	-5.9	58.9	330.	-1721.0	-5.1	4.7	0.0	-2317.0	6875.0	58.	280.2	208.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1				
3.	-1291.6	-15.7	-1.6	0.0	-3.9	39.3	Asta	117	742	739	MY	NZZ	739	86.	280.2	20.6	0.1	0.0	-4.3	7347.7	251.	-847.5	0.3	16.8	2.5	1485.3	3200.1				
3.	-1291.5	-15.7	-1.6	0.0	-2.9	29.5	PROGR.	117	742	739	MY	NZZ	739	115.	280.2	-73.5	0.1	0.0	-17.0	13147.7	Asta	150	780	953	MY	NZZ	780				
3.	-1291.4	-15.7	-1.6	0.0	-1.9	19.5	0.	-1304.6	-31.4	-53.9	0.0	-7828.6	17780.5	144.	280.2	-107.5	0.1	0.0	-21.3	9717.7	PROGR.	150	780	953	MY	NZZ	780				
4.	-1291.2	-15.7	-1.6	0.0	-1.0	9.8	41.	-1889.3	-31.4	-53.9	0.0	-9605.9	16485.6	173.	280.2	-261.5	0.1	0.0	-25.6	3546.0	0.	-4.8	0.0	0.0	0.4	0.0	0.4				
5.	-1291.0	-15.7	-1.6	0.0	-0.9	3.4	13.	-1864.0	-31.4	-53.9	0.0	-7702.7	15393.2	201.	280.2	-355.5	0.1	0.0	-29.8	1327.5	135.	-4.8	0.0	0.0	0.4	0.0	0.4				
Asta	101	742	739	MY	NZZ	739	124.	-1838.7	-31.4	-53.9	0.0	-1160.4	13895.8	230.	280.2	-449.5	0.1	0.0	-34.1	-16893.6	307.	-4.8	0.0	0.0	0.4	0.1	0.7				
PROGR.	101	742	739	MY	NZZ	739	365.	-1813.4	-31.4	-53.9	0.0	-1062.4	12600.9	Asta	134	750	468	MY	NZZ	468	601.	-4.8	0.0	0.0	0.4	0.1	0.7				
1.	-1252.4	-5.4	-1.5	0.0	-7.5	27.0	178.	-1781.1	-31.4	-53.9	0.0	-303.5	2878.6	PROGR.	134	750	468	MY	NZZ	468	135.	-4.8	0.0	0.0	0.4	0.1	0.7				
1.	-1252.3	-5.4	-1.5	0.0	-6.5	23.6	248.	-1762.5	-31.4	-53.9	0.0	-9507.9	10011.1	0.	-110.0	-305.0	-0.2	0.0	0.0	0.0	368.	-4.8	0.0	0.0	0.4	0.2	0.7				
1.	-1252.2	-5.4	-1.5	0.0	-5.5	20.2	289.	-1737.3	-31.4	-53.9	0.0	-7702.7	15393.2	0.	-110.0	-305.0	-0.2	0.0	0.0	0.0	202.	-4.8	0.0	0.0	0.4	0.2	0.7				
2.	-1252.0	-5.4	-1.5	0.0	-4.7	16.9	330.	-1762.5	-31.4	-53.9	0.0	-9953.4	7421.3	58.	-110.0	-313.0	-0.2	0.0	10.2	-12039.9	368.	-4.8	0.0	0.0	0.4	0.3	0.7				
2.	-1251.9	-5.4	-1.5	0.0	-3.7	12.5	Asta	119	742	739	MY	NZZ	739	Asta	119	742	739	MY	NZZ	739	289.	-4.8	0.0	0.0	0.4	0.3	0.7				
3.	-1251.7	-5.4	-1.5	0.0	-2.8	10.1	PROGR.	119	742	739	MY	NZZ	739	115.	-110.0	73.0	-0.2	0.0	20.3	-13229.0	Asta	154	780	973	212	MY	NZZ	780			
4.	-1251.6	-5.4	-1.5	0.0	-1.9	6.7	0.	106.7	-134.6	9.1	26.0	1052.1	36841.0	144.	-110.0	367.0	-0.2	0.0	25.4	-9779.5	PROGR.	154	780	973	212	MY	NZZ	780			
4.	-1251.5	-5.4	-1.5	0.0	-0.9	3.4	18.	106.7	-134.6	9.1	26.0	1052.1	36841.0	201.	-110.0	367.0	-0.2	0.0	30.5	-3827.4	PROGR.	154	780	973	212	MY	NZZ	780			
5.	-1251.3	-5.4	-1.5	0.0	0.0	0.0	35.	106.7	-256.3	9.1	26.0	733.0	30000.8	230.	-110.0	355.0	-0.2	0.0	35.6	5277.5	58.	-2.6	-188.0	0.0	0.0	-949.4	0.0				
Asta	102	742	739	MY	NZZ	739	52.	106.7	-317.1	9.1	26.0	574.4	24893.9	0.	-110.0	449.0	-0.2	0.0	40.6	16785.0	29.	2.6	-282.0	0.0	0.0	0.0	0.0				
PROGR.	102	742	739	MY	NZZ	739	70.	106.7	-387.9	9.1	26.0	413.8	18802.3	Asta	136	749	469	MY	NZZ	469	86.	2.6	-94.0	0.0	0.0	0.0	-2027.0	0.0			
0.	-954.3	7.5	-57.1	0.0	-283.6	-37.5	88.	106.7	-438.8	9.1	26.0	254.2	11736.1	PROGR.	136	749	469	MY	NZZ	469	115.	2.6	0.0	0.0	0.0	0.0	-2162.6	0.0			
1.	-954.2	7.5	-57.1	0.0	-249.9	-32.8	105.	106.7	-499.6	9.1	26.0	34.6	3545.3	0.	-142.9	240.9	0.0	0.0	-5.8	5573.8	144.	2.6	94.0	0.0	0.0	0.0	-2027.0	0.0			
1.	-954.1	7.5	-57.1	0.0	-214.2	-28.1	123.	106.7	-560.4	9.1	26.0	-65.0	-5730.1	29.	142.9	146.9	0.0	0.0	-11.5	8444.8	173.	2.6	188.0	0.0	0.0	0.0	-2162.6	0.0			
2.	-953.9	7.5	-57.1	0.0	-178.5	-23.4	140.	106.7	-631.3	9.1	26.0	-224.6	-16007.1	58.	142.9	52.9	0.0	0.0	-11.5	8444.8	201.	2.6	282.0	0.0	0.0	0.0	0.0	-949.4	0.0		
3.	-953.8	7.5	-57.1	0.0	-142.8	-18.7	Asta	120	745	746	MY	NZZ	746	86.	142.9	-41.1	0.2	0.0	-17.3	8613.2	PROGR.	120	745	746	MY	NZZ	746	0.0	0.0	0.0	0.0
4.	-953.5	7.5	-57.1	0.0	-71.4	-9.4	0.	-229.4	-278.1	1.1	-659.0	0.0	604.7	144.	142.9	-229.2	0.2	0.0	-28.8	841.8	PROGR.	120	745	746	MY	NZZ	746	0.0	0.0	0.0	0.0
4.	-953.4	7.5	-57.1	0.0	-35.7	-4.7	16.	-229.4	-285.0	1.1	-659.0	-17.2	-3971.0	173.	142.9	-323.2	0.2	0.0	-34.6	-7029.9	0.	-25.2	305.7	0.2	0.0	0.0	0.0	0.0	0.0		
5.	-953.2	7.5	-57.1	0.0	0.0	0.0	33.	-229.4	-292.0	1.1	-659.0	-34.5	-8659.3	201.	142.9	-417.2	0.2	0.0	-40.3	-17449.3	58.	-25.2	117.6	0.2	0.0	0.0	-14.8	14200.9	0.0		
Asta	104	746	747	MY	NZZ	747	49.	-229.4	-298.9	1.1	-659.0	-51.7	-13460.2	230.	142.9	-511.2	0.2	0.0	-46.1	-13085.4	58.	-25.2	117.6	0.2	0.0	0.0	-9.9	12170.0	0.0		
PROGR.	104	746	747	MY	NZZ	747	65.	-229.4	-305.8	1.1	-659.0	-83.2	-23399.5	0.	-6.8	352.1	-1.9	-4.6	-220.0	-8487.8	115.	-25.2	-70.4	0.2	0.0	0.0	-19.7	13529.2	0.0		
0.	-790.0	-30.8	1698.2	0.0	8490.9	153.8	98.	-229.4	-319.7	1.1	-659.0	-106.4	-28338.1	PROGR.	104	746	747	MY	NZZ	747	144.	-25.2	-164.4	0.2	0.0	0.0	-24.7	10354.7	0.0		
1.	-790.0	-30.8	1698.2	0.0	7429.5	134.6	115.	-229.4	-335.6	1.1	-659.0	-137.9	-39152.8	0.	-6.8	352.1	-1.9	-4.6	-220.0	-8487.8	173.	-25.2	-164.4	0.2	0.0	0.0	-24.7	10354.7	0.0		
2.	-789.9	-30.8	1698.2	0.0	6380.4	115.4	130.	-229.4	-335.5	1.1	-659.0	-137.9	-39152.8	PROGR.	104	746	747	MY	NZZ	747	201.	-25.2	-164.4	0.2	0.0	0.0	-24.7	10354.7	0.0		
3.	-789.8	-30.8	1698.2	0.0	5306.8	96.1	Asta	121	747	748	MY	NZZ	748	58.	-6.8	164.1	-1.9	-4.6	-109.4	6315.6	201.	-25.2	-164.4	0.2	0.0	0.0	-24.7	10354.7	0.0		
3.	-789.7	-30.8	1698.2	0.0	4291.6	76.9	PROGR.	121	747	748	MY	NZZ	748	115.	-6.8	-23.9	-1.9	-4.6	-1.2	10380.2	201.	-25.2	-164.4	0.2	0.0	0.0	-24.7	10354.7	0.0		
3.	-789.5	-30.8	1698.2	0.0	3184.1	57.7	0.	-90.6	412.8	-7.6	-75.0	-97.9	-3539.9	115.	-6.8	-23.9	-1.9	-4.6	-1.2	10380.2	201.	-25.2	-164.4	0.2	0.0	0.0	-24.7	10354.7	0.0		
4.	-789.3	-30.8	1698.2	0.0	2122.7	38.5	0.	-90.6	412.8	-7.6	-75.0	-97.9	-3539.9	115.	-6.8	-23.9	-1.9	-4.6	-1.2	10380.2	201.	-25.2	-164.4	0.2	0.0	0.0	-24.7	10354.7	0.0		
4.	-789.2	-30.8	1698.2	0.0	1061.4	19.3	33.	-90.6	398.9	-7.6	-75.0	167.1	-22200.0	173.	-6.8	-23.9	-1.9	-4.6	-1.2	10380.2	201.	-25.2	-164.4	0.2	0.0	0.0	-24.7	10354.7	0.0		
5.	-789.1	-30.8	1698.2	0.0	0.0	0.0	49.	-90.6	398.9	-7.6	-75.0	167.1	-22200.0	201.	-6.8	-306.0	-1.9	-4.6	-167.1	-3847.1	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	0.0			
Asta	106	748	749	MY	NZZ	749	65.	-90.6	385.0	-7.6	-75.0	167.1	-22200.0	201.	-6.8	-306.0	-1.9	-4.6	-167.1	-3847.1	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	0.0			
PROGR.	106	748	749	MY	NZZ	749	81.	-90.6	378.1	-7.6	-75.0	167.1	-22200.0	201.	-6.8	-306.0	-1.9	-4.6	-167.1	-3847.1	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	0.0			
0.	-1311.1	218.9	-5793.2	0.0	-2896.8	-109.7	88.	-90.6	378.1	-7.6	-75.0	167.1	-22200.0	201.	-6.8	-306.0	-1.9	-4.6	-167.1	-3847.1	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	0.0			
1.	-1311.0	218.9	-5793.2	0.0	-2534.1	-97.9	PROGR.	106	748	749	MY	NZZ	749	115.	-6.8	-306.0	-1.9	-4.6	-167.1	-3847.1	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	0.0			
1.	-1310.8	218.9	-5793.2	0.0	-2174.4	-82.0	114.	-90.6	364.3	-7.6	-75.0	167.1	-22200.0	201.	-6.8	-306.0	-1.9	-4.6	-167.1	-3847.1	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	0.0			
2.	-1310.7	218.9	-5793.2	0.0	-1869.2	-66.2	130.	-90.6	351.3	-7.6	-75.0	167.1	-22200.0	201.	-6.8	-306.0	-1.9	-4.6	-167.1	-3847.1	16.	0.0	500.2	-1.0	3.5	-44.5	-31867.8	0.0			
3.	-1310.5	218.9	-5793.2	0.0	-1448.9	-54.7	Asta	122	748	749	MY	NZZ	749	29.	-17.3	282.0	0.0	0.0	0.0	9459.3	130.	0.0	458.6	-1.0	3.5	37.2	6699.7	0.0			
3.	-1310.4	218.9	-5793.2	0.0	-1103.2	-43.0	PROGR.	122	748	749	MY	NZZ	749	86.	-17.3	94.0	0.0	0.0	-0.1	10209.9	130.	0.0	458.6	-1.0	3.5	37.2	6699.7	0.0			
4.	-1310.3	218.9	-5793.2	0.0	-734.5	-27.7	0.	-17.3	94.0	0.0	0.0	-0.1	10																		

PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-125.8	0.0	0.0	0.0	0.0	0.0
34.	-125.8	0.0	0.0	0.0	0.0	0.0
67.	-125.8	0.0	0.0	0.0	0.0	0.0
101.	-125.8	0.0	0.0	0.0	0.0	0.0
135.	-125.8	0.0	0.0	0.0	0.0	0.0
168.	-125.8	0.0	0.0	0.0	0.0	0.0
202.	-125.8	0.0	0.0	0.0	0.0	0.0
236.	-125.8	0.0	0.0	0.0	0.0	0.0
269.	-125.8	0.0	0.0	0.0	0.0	0.0
Asta	168	noth	753	953		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	19.4	0.0	0.0	0.0	0.0	0.0
51.	19.4	0.0	0.0	0.0	0.0	0.0
103.	19.4	0.0	0.0	0.0	0.0	0.0
154.	19.4	0.0	0.0	0.0	0.0	0.0
205.	19.4	0.0	0.0	0.0	0.0	0.0
257.	19.4	0.0	0.0	0.0	0.0	0.0
308.	19.4	0.0	0.0	0.0	0.0	0.0
359.	19.4	0.0	0.0	0.0	0.0	0.0
410.	19.4	0.0	0.0	0.0	0.0	0.0
Asta	169	noth	741	754		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	142.5	0.0	0.0	0.0	0.0	0.0
51.	142.5	0.0	0.0	0.0	0.0	0.0
102.	142.5	0.0	0.0	0.0	0.0	0.0
152.	142.5	0.0	0.0	0.0	0.0	0.0
203.	142.5	0.0	0.0	0.0	0.0	0.0
254.	142.5	0.0	0.0	0.0	0.0	0.0
305.	142.5	0.0	0.0	0.0	0.0	0.0
356.	142.5	0.0	0.0	0.0	0.0	0.0
406.	142.5	0.0	0.0	0.0	0.0	0.0
Asta	170	noth	740	953		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-553.3	10.5	1202.5	0.0	6012.6	-52.7
1.	-553.2	10.5	1202.5	0.0	5261.0	-46.1
2.	-553.1	10.5	1202.5	0.0	4509.4	-39.6
3.	-552.9	10.5	1202.5	0.0	3757.9	-33.0
4.	-552.8	10.5	1202.5	0.0	3006.3	-26.4
5.	-552.7	10.5	1202.5	0.0	2254.7	-19.8
6.	-552.5	10.5	1202.5	0.0	1503.1	-13.2
7.	-552.4	10.5	1202.5	0.0	751.6	-6.6
8.	-552.2	10.5	1202.5	0.0	0.0	0.0
Asta	171	noth	738	975		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-377.1	-17.3	0.0	0.0	0.0	86.6
1.	-377.0	-17.3	0.0	0.0	0.0	75.7
2.	-376.8	-17.3	0.0	0.0	0.0	64.9
3.	-376.7	-17.3	0.0	0.0	0.0	54.1
4.	-376.6	-17.3	0.0	0.0	0.0	43.3
5.	-376.4	-17.3	0.0	0.0	0.0	32.5
6.	-376.3	-17.3	0.0	0.0	0.0	21.6
7.	-376.2	-17.3	0.0	0.0	0.0	10.8
8.	-376.0	-17.3	0.0	0.0	0.0	0.0
Asta	172	noth	40	978		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-10163.7	-888.8	-17.5	0.0	-6752.6	103550.9
15.	-10070.0	-888.8	-17.5	0.0	-6489.1	90218.3
30.	-9976.2	-888.8	-17.5	0.0	-6226.3	76885.8
45.	-9882.5	-888.8	-17.5	0.0	-5963.4	63553.2
60.	-9788.7	-888.8	-17.5	0.0	-5700.6	50220.7
75.	-9695.0	-888.8	-17.5	0.0	-5437.7	36888.1
90.	-9601.2	-888.8	-17.5	0.0	-5174.9	23555.6
105.	-9507.5	-888.8	-17.5	0.0	-4912.0	10223.0
120.	-9413.7	-888.8	-17.5	0.0	-4649.1	-3109.5
Asta	173	noth	954	37		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-8791.4	26.8	-41.2	0.0	-13995.1	-375.7
15.	-8697.6	26.8	-41.2	0.0	-13352.9	-339.8
30.	-8603.9	26.8	-41.2	0.0	-12710.6	-299.9
45.	-8510.1	26.8	-41.2	0.0	-12068.3	-259.0
60.	-8416.4	26.8	-41.2	0.0	-11426.0	-218.0
75.	-8322.6	26.8	-41.2	0.0	-10783.8	-178.1
90.	-8228.9	26.8	-41.2	0.0	-10141.5	-138.2
105.	-8135.1	26.8	-41.2	0.0	-9499.2	-98.3
120.	-8041.4	26.8	-41.2	0.0	-8856.9	-58.4
Asta	174	noth	958	734		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-4015.0	703.6	-67.5	0.0	-15330.2	-8302.4
15.	-3921.2	703.6	-67.5	0.0	-14317.6	-7247.9
30.	-3827.5	703.6	-67.5	0.0	-13305.1	-6193.4
45.	-3733.7	703.6	-67.5	0.0	-12292.5	-5137.9
60.	-3640.0	703.6	-67.5	0.0	-11279.9	-4083.4
75.	-3546.2	703.6	-67.5	0.0	-10267.4	-3028.9
90.	-3452.5	703.6	-67.5	0.0	-9254.8	-1971.4
105.	-3358.7	703.6	-67.5	0.0	-8242.2	-917.9
120.	-3265.0	703.6	-67.5	0.0	-7229.7	1395.5
Asta	175	noth	960	741		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-2546.8	460.8	-138.5	0.0	-24959.2	-5642.5
15.	-2453.0	460.8	-138.5	0.0	-22881.7	-4953.1
30.	-2359.3	460.8	-138.5	0.0	-20804.2	-4263.7
45.	-2265.5	460.8	-138.5	0.0	-18726.7	-3573.3
60.	-2171.8	460.8	-138.5	0.0	-16649.2	-2876.9
75.	-2078.0	460.8	-138.5	0.0	-14571.7	-2180.5
90.	-1984.3	460.8	-138.5	0.0	-12494.3	-1484.1
105.	-1890.5	460.8	-138.5	0.0	-10416.8	-802.7
120.	-1796.8	460.8	-138.5	0.0	-8339.3	-111.3
Asta	176	noth	959	742		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-2664.6	-317.1	6.9	0.0	-16951.0	3023.6
15.	-2570.8	-317.1	6.9	0.0	-17054.7	2546.0
30.	-2477.1	-317.1	6.9	0.0	-17158.4	2070.5
45.	-2383.3	-317.1	6.9	0.0	-17262.1	1594.0
60.	-2289.6	-317.1	6.9	0.0	-17365.8	1117.5
75.	-2195.8	-317.1	6.9	0.0	-17469.4	641.0
90.	-2102.1	-317.1	6.9	0.0	-17573.1	168.4
105.	-2008.3	-317.1	6.9	0.0	-17676.8	-307.1
120.	-1914.6	-317.1	6.9	0.0	-17780.5	-782.6
Asta	178	noth	37	19		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	0.0	380.1	0.6	-1421.6	20.0	-3827.8
1.	0.0	380.6	0.6	-1421.6	19.2	-3351.7
3.	0.0	380.1	0.6	-1421.6	18.5	-2876.6
4.	0.0	379.5	0.6	-1421.6	17.7	-2401.6
5.	0.0	379.0	0.6	-1421.6	16.9	-1927.5
6.	0.0	378.5	0.6	-1421.6	16.2	-1454.4
7.	0.0	377.9	0.6	-1421.6	15.4	-981.4
8.	0.0	377.4	0.6	-1421.6	14.6	-509.3
9.	0.0	376.9	0.6	-1421.6	13.8	-37.9
10.	0.0	376.4	0.6	-1421.6	13.0	114.1
Asta	181	noth	957	28		
PROGR.	NORM	TYV	TZZ	TORS	MYV	KZZ
0.	-540.5	14.8	257.8	0.0	30940.0	-1778.1
15.	-540.5	14.8	257.8	0.0	2707.5	-155.8
30.	-540.5	14.8	257.8	0.0	2320.0	-133.5
45.	-540.5	14.8	257.8	0.0	1932.5	-111.1
60.	-540.5	14.8	257.8	0.0	1545.0	-88.9
75.	-540.5	14.8	257.8	0.0	1157.5	-66.6
90.	-540.5	14.8	257.8	0.0	770.0	-44.4
105.	-540.5	14.8	257.8	0.0	382.5	-22.2
120.	-540.5	14.8	257.8	0.0	0.0	0.0

COLLEZIONE GASZ RETTANGOLARE					
CONFEZIONE : 80x170x35 mm - 80 Tonnelle, Adatt. X					
Unità di misura: cm, S.S. [decimetro]					
GASCO	415	SS =	0.	Sf =	0.
GASCO	416	SS =	0.	Sf =	0.
GASCO	417	SS =	0.	Sf =	0.
GASCO	418	SS =	0.	Sf =	0.
GASCO	419	SS =	0.	Sf =	0.
GASCO	420	SS =	0.	Sf =	0.
GASCO	421	SS =	0.	Sf =	0.
GASCO	422	SS =	0.	Sf =	0.
GASCO	423	SS =	0.	Sf =	0.
GASCO	424	SS =	0.	Sf =	0.
GASCO	425	SS =	0.	Sf =	0.
GASCO	426	SS =	0.	Sf =	0.
GASCO	427	SS =	0.	Sf =	0.
GASCO	428	SS =	0.	Sf =	0.
GASCO	429	SS =	0.	Sf =	0.
GASCO	430	SS =	0.	Sf =	0.
GASCO	431	SS =	0.	Sf =	0.
GASCO	432	SS =	0.	Sf =	0.
GASCO	433	SS =	0.	Sf =	0.
GASCO	434	SS =	0.	Sf =	0.
GASCO	435	SS =	0.	Sf =	0.
GASCO	436	SS =	0.	Sf =	0.
GASCO	437	SS =	0.	Sf =	0.
GASCO	438	SS =	0.	Sf =	0.
GASCO	439	SS =	0.	Sf =	0.
GASCO	440	SS =	0.	Sf =	0.
GASCO	441	SS =	0.	Sf =	0.
GASCO	442	SS =	0.	Sf =	0.
GASCO	443	SS =	0.	Sf =	0.
GASCO	444	SS =	0.	Sf =	0.
GASCO	445	SS =	0.	Sf =	0.
GASCO	446	SS =	0.	Sf =	0.
GASCO	447	SS =	0.	Sf =	0.
GASCO	448	SS =	0.	Sf =	0.
GASCO	449	SS =	0.	Sf =	0.
GASCO	450	SS =	0.	Sf =	0.
GASCO	451	SS =	0.	Sf =	0.
GASCO	452	SS =	0.	Sf =	0.
GASCO	453	SS =	0.	Sf =	0.
GASCO	454	SS =	0.	Sf =	0.
GASCO	455	SS =	0.	Sf =	0.

COLLETTAZIONE		COSTI RETTANGOLARI		CONFEZIONE			
misura		9 Torcette_add_Y		9 Torcette_add_Y			
misura		9 Torcette_add_Y		9 Torcette_add_Y			
GC810	415	55	=	0.	51	=	0.
GC811	416	55	=	0.	51	=	0.
GC812	417	55	=	0.	51	=	0.
GC813	418	55	=	0.	51	=	0.
GC814	419	55	=	0.	51	=	0.
GC815	420	55	=	0.	51	=	0.
GC816	421	55	=	0.	51	=	0.
GC817	422	55	=	0.	51	=	0.
GC818	423	55	=	0.	51	=	0.
GC819	424	55	=	0.	51	=	0.
GC820	425	55	=	0.	51	=	0.
GC821	426	55	=	0.	51	=	0.
GC822	427	55	=	0.	51	=	0.
GC823	428	55	=	0.	51	=	0.
GC824	429	55	=	0.	51	=	0.
GC825	430	55	=	0.	51	=	0.
GC826	431	55	=	0.	51	=	0.
GC827	432	55	=	0.	51	=	0.
GC828	433	55	=	0.	51	=	0.
GC829	434	55	=	0.	51	=	0.
GC830	435	55	=	0.	51	=	0.
GC831	436	55	=	0.	51	=	0.
GC832	437	55	=	0.	51	=	0.
GC833	438	55	=	0.	51	=	0.
GC834	439	55	=	0.	51	=	0.
GC835	440	55	=	0.	51	=	0.
GC836	441	55	=	0.	51	=	0.
GC837	442	55	=	0.	51	=	0.
GC838	443	55	=	0.	51	=	0.
GC839	444	55	=	0.	51	=	0.
GC840	445	55	=	0.	51	=	0.
GC841	446	55	=	0.	51	=	0.
GC842	447	55	=	0.	51	=	0.
GC843	448	55	=	0.	51	=	0.
GC844	449	55	=	0.	51	=	0.
GC845	450	55	=	0.	51	=	0.
GC846	451	55	=	0.	51	=	0.
GC847	452	55	=	0.	51	=	0.
GC848	453	55	=	0.	51	=	0.
GC849	454	55	=	0.	51	=	0.
GC850	455	55	=	0.	51	=	0.

COMBINAZIONE

GUSCIO	454	SS =	11.1	SI =	11.1
GUSCIO	455	SS =	10.9	SI =	10.9
GUSCIO	456	SS =	12.8	SI =	12.8
GUSCIO	457	SS =	4.6	SI =	4.6
GUSCIO	458	SS =	5.8	SI =	5.8
GUSCIO	459	SS =	5.4	SI =	5.4
GUSCIO	460	SS =	4.1	SI =	4.1
GUSCIO	461	SS =	3.1	SI =	3.1
GUSCIO	462	SS =	6.5	SI =	6.5
GUSCIO	463	SS =	5.1	SI =	5.1
GUSCIO	464	SS =	3.8	SI =	3.8
GUSCIO	465	SS =	4.2	SI =	4.2
GUSCIO	466	SS =	3.7	SI =	3.7
GUSCIO	467	SS =	3.5	SI =	3.5
GUSCIO	468	SS =	4.5	SI =	4.5
GUSCIO	469	SS =	4.0	SI =	4.0
GUSCIO	470	SS =	4.1	SI =	4.1
GUSCIO	471	SS =	3.5	SI =	3.5
GUSCIO	472	SS =	4.4	SI =	4.4
GUSCIO	473	SS =	4.3	SI =	4.3
GUSCIO	474	SS =	4.2	SI =	4.2
GUSCIO	475	SS =	2.8	SI =	2.8
GUSCIO	476	SS =	4.1	SI =	4.1
GUSCIO	477	SS =	3.1	SI =	3.1
GUSCIO	478	SS =	2.9	SI =	2.9
GUSCIO	479	SS =	1.2	SI =	1.2
GUSCIO	480	SS =	2.9	SI =	2.9
GUSCIO	481	SS =	1.2	SI =	1.2
GUSCIO	482	SS =	5.7	SI =	5.7
GUSCIO	483	SS =	4.7	SI =	4.7
GUSCIO	484	SS =	3.7	SI =	3.7
GUSCIO	485	SS =	4.9	SI =	4.9
GUSCIO	486	SS =	4.3	SI =	4.3
GUSCIO	487	SS =	6.2	SI =	6.2
GUSCIO	488	SS =	2.2	SI =	2.2
GUSCIO	489	SS =	6.8	SI =	6.8
GUSCIO	490	SS =	21.7	SI =	21.7
GUSCIO	491	SS =	19.4	SI =	19.4
GUSCIO	492	SS =	6.0	SI =	6.0
GUSCIO	493	SS =	7.3	SI =	7.3
GUSCIO	494	SS =	1.4	SI =	1.4
GUSCIO	495	SS =	6.0	SI =	6.0
GUSCIO	496	SS =	17.3	SI =	17.3
GUSCIO	497	SS =	11.3	SI =	11.3
GUSCIO	498	SS =	2.5	SI =	2.5
GUSCIO	499	SS =	4.8	SI =	4.8
tensione max =		21.7	guscio =	490	

SOLLECITAZIONE GUSCI RETTANGOLARE
CASO DI CARICO : 3 SLU VENTIV

N. 5 CONDIZIONI ANALISI STATICA
1 peso proprio + 1.30
2 permanenti + 1.50
3 A'var. abitazione + 1.50
4 neve (-1000h/m) + 1.50
5 vento + 1.50

1) +1.30*c001 +1.50*c002 +1.50*c003 +1.50*c004 +1.50*c005
2) +1.30*c001 +1.50*c002 +1.50*c003 +1.50*c004 -1.50*c005
Unità di misura: SI,SS [daN/cm2]

GUSCIO	415	SS =	3.5	SI =	3.5
		SS =	2.9	SI =	2.9
GUSCIO	416	SS =	2.6	SI =	2.6
		SS =	1.9	SI =	1.9
GUSCIO	417	SS =	9.5	SI =	9.5
		SS =	7.6	SI =	7.6
GUSCIO	418	SS =	9.6	SI =	9.6
		SS =	8.0	SI =	8.0
GUSCIO	419	SS =	24.2	SI =	24.2
		SS =	19.0	SI =	19.0
GUSCIO	420	SS =	17.6	SI =	17.6
		SS =	16.6	SI =	16.6
GUSCIO	421	SS =	18.2	SI =	18.2
		SS =	22.2	SI =	22.2
GUSCIO	422	SS =	16.6	SI =	16.6

COMBINAZIONE

		SS =	17.1	SI =	17.1
GUSCIO	423	SS =	6.9	SI =	6.9
		SS =	8.4	SI =	8.4
GUSCIO	424	SS =	7.5	SI =	7.5
		SS =	8.7	SI =	8.7
GUSCIO	425	SS =	2.4	SI =	2.4
		SS =	3.1	SI =	3.1
GUSCIO	426	SS =	1.6	SI =	1.6
		SS =	2.0	SI =	2.0
GUSCIO	427	SS =	6.6	SI =	6.6
		SS =	5.7	SI =	5.7
GUSCIO	428	SS =	8.1	SI =	8.1
		SS =	7.1	SI =	7.1
GUSCIO	429	SS =	4.7	SI =	4.7
		SS =	4.4	SI =	4.4
GUSCIO	430	SS =	10.9	SI =	10.9
		SS =	9.3	SI =	9.3
GUSCIO	431	SS =	11.8	SI =	11.8
		SS =	10.2	SI =	10.2
GUSCIO	432	SS =	9.9	SI =	9.9
		SS =	9.0	SI =	9.0
GUSCIO	433	SS =	15.5	SI =	15.5
		SS =	13.5	SI =	13.5
GUSCIO	434	SS =	15.1	SI =	15.1
		SS =	13.7	SI =	13.7
GUSCIO	435	SS =	22.4	SI =	22.4
		SS =	17.6	SI =	17.6
GUSCIO	436	SS =	14.3	SI =	14.3
		SS =	13.2	SI =	13.2
GUSCIO	437	SS =	14.6	SI =	14.6
		SS =	13.6	SI =	13.6
GUSCIO	438	SS =	17.6	SI =	17.6
		SS =	20.6	SI =	20.6
GUSCIO	439	SS =	8.8	SI =	8.8
		SS =	8.2	SI =	8.2
GUSCIO	440	SS =	10.4	SI =	10.4
		SS =	10.5	SI =	10.5
GUSCIO	441	SS =	9.2	SI =	9.2
		SS =	9.8	SI =	9.8
GUSCIO	442	SS =	5.4	SI =	5.4
		SS =	6.8	SI =	6.8
GUSCIO	443	SS =	7.3	SI =	7.3
		SS =	7.9	SI =	7.9
GUSCIO	444	SS =	4.6	SI =	4.6
		SS =	5.3	SI =	5.3
GUSCIO	445	SS =	3.7	SI =	3.7
		SS =	2.2	SI =	2.2
GUSCIO	446	SS =	5.3	SI =	5.3
		SS =	3.4	SI =	3.4
GUSCIO	447	SS =	4.0	SI =	4.0
		SS =	3.0	SI =	3.0
GUSCIO	448	SS =	7.9	SI =	7.9
		SS =	5.1	SI =	5.1
GUSCIO	449	SS =	9.3	SI =	9.3
		SS =	6.4	SI =	6.4
GUSCIO	450	SS =	9.0	SI =	9.0
		SS =	6.6	SI =	6.6
GUSCIO	451	SS =	17.1	SI =	17.1
		SS =	10.5	SI =	10.5
GUSCIO	452	SS =	12.8	SI =	12.8
		SS =	10.3	SI =	10.3
GUSCIO	453	SS =	19.6	SI =	19.6
		SS =	11.9	SI =	11.9
GUSCIO	454	SS =	11.4	SI =	11.4
		SS =	12.1	SI =	12.1
GUSCIO	455	SS =	11.8	SI =	11.8
		SS =	10.0	SI =	10.0
GUSCIO	456	SS =	12.2	SI =	12.2

		SS =	13.9	SI =	13.9
GUSCIO	457	SS =	4.2	SI =	4.2
		SS =	5.0	SI =	5.0
GUSCIO	458	SS =	5.7	SI =	5.7
		SS =	5.9	SI =	5.9
GUSCIO	459	SS =	5.4	SI =	5.4
		SS =	5.4	SI =	5.4
GUSCIO	460	SS =	3.7	SI =	3.7
		SS =	4.5	SI =	4.5
GUSCIO	461	SS =	3.0	SI =	3.0
		SS =	3.5	SI =	3.5
GUSCIO	462	SS =	3.8	SI =	3.8
		SS =	9.5	SI =	9.5
GUSCIO	463	SS =	4.1	SI =	4.1
		SS =	6.2	SI =	6.2
GUSCIO	464	SS =	3.3	SI =	3.3
		SS =	4.5	SI =	4.5
GUSCIO	465	SS =	5.4	SI =	5.4
		SS =	3.9	SI =	3.9
GUSCIO	466	SS =	2.7	SI =	2.7
		SS =	5.6	SI =	5.6
GUSCIO	467	SS =	3.1	SI =	3.1
		SS =	4.3	SI =	4.3
GUSCIO	468	SS =	3.3	SI =	3.3
		SS =	5.7	SI =	5.7
GUSCIO	469	SS =	6.3	SI =	6.3
		SS =	4.2	SI =	4.2
GUSCIO	470	SS =	3.5	SI =	3.5
		SS =	4.8	SI =	4.8
GUSCIO	471	SS =	4.1	SI =	4.1
		SS =	3.8	SI =	3.8
GUSCIO	472	SS =	3.6	SI =	3.6
		SS =	5.5	SI =	5.5
GUSCIO	473	SS =	3.6	SI =	3.6
		SS =	5.2	SI =	5.2
GUSCIO	474	SS =	3.4	SI =	3.4
		SS =	5.1	SI =	5.1
GUSCIO	475	SS =	1.9	SI =	1.9
		SS =	3.9	SI =	3.9
GUSCIO	476	SS =	2.9	SI =	2.9
		SS =	5.4	SI =	5.4
GUSCIO	477	SS =	2.1	SI =	2.1
		SS =	4.1	SI =	4.1
GUSCIO	478	SS =	1.9	SI =	1.9
		SS =	4.8	SI =	4.8
GUSCIO	479	SS =	0.4	SI =	0.4
		SS =	2.1	SI =	2.1
GUSCIO	480	SS =	2.1	SI =	2.1
		SS =	5.8	SI =	5.8
GUSCIO	481	SS =	1.2	SI =	1.2
		SS =	1.9	SI =	1.9
GUSCIO	482	SS =	6.4	SI =	6.4
		SS =	6.9	SI =	6.9
GUSCIO	483	SS =	4.0	SI =	4.0
		SS =	5.4	SI =	5.4
GUSCIO	484	SS =	5.7	SI =	5.7
		SS =	3.0	SI =	3.0
GUSCIO	485	SS =	4.2	SI =	4.2
		SS =	6.2	SI =	6.2
GUSCIO	486	SS =	2.9	SI =	2.9
		SS =	5.8	SI =	5.8
GUSCIO	487	SS =	10.3	SI =	10.3
		SS =	2.7	SI =	2.7
GUSCIO	488	SS =	2.9	SI =	2.9
		SS =	1.4	SI =	1.4
GUSCIO	489	SS =	8.2	SI =	8.2
		SS =	5.4	SI =	5.4
GUSCIO	490	SS =	26.0	SI =	26.0
		SS =	17.8	SI =	17.8

GUSCIO	491	SS =	19.3	SI =	19.3
		SS =	20.3	SI =	20.3
GUSCIO	492	SS =	6.1	SI =	6.1
		SS =	5.8	SI =	5.8
GUSCIO	493	SS =	3.8	SI =	3.8
		SS =	11.6	SI =	11.6
GUSCIO	494	SS =	1.9	SI =	1.9
		SS =	1.0	SI =	1.0
GUSCIO	495	SS =	8.3	SI =	8.3
		SS =	3.6	SI =	3.6
GUSCIO	496	SS =	24.7	SI =	24.7
		SS =	9.9	SI =	9.9
GUSCIO	497	SS =	6.1	SI =	6.1
		SS =	16.7	SI =	16.7
GUSCIO	498	SS =	2.6	SI =	2.6
		SS =	4.2	SI =	4.2
GUSCIO	499	SS =	4.2	SI =	4.2
		SS =	5.5	SI =	5.5
tensione max =		26.0	guscio =	490	

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 4 SISMAX SLU

N. 2 CONDIZIONI ANALISI STATICA
6 SISMAX + 1.00
8 Torcente_add_X + 1.00
1) +1.00*c006 +1.00*c008
2) -1.00*c006 +1.00*c008
3) +1.00*c006 -1.00*c008
4) -1.00*c006 -1.00*c008
Unità di misura: SI,SS [daN/cm2]

GUSCIO	415	SS =	0.4	SI =	0.4
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
GUSCIO	416	SS =	0.4	SI =	0.4
		SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
GUSCIO	417	SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
GUSCIO	418	SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
		SS =	0.5	SI =	0.5
GUSCIO	419	SS =	0.5	SI =	0.5
		SS =	0.6	SI =	0.6
		SS =	2.5	SI =	2.5
GUSCIO	420	SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.5	SI =	2.5
GUSCIO	421	SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
GUSCIO	422	SS =	1.8	SI =	1.8
		SS =	2.7	SI =	2.7
		SS =	3.1	SI =	3.1
GUSCIO	423	SS =	3.1	SI =	3.1
		SS =	2.7	SI =	2.7
		SS =	1.9	SI =	1.9
GUSCIO	424	SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	1.9	SI =	1.9
GUSCIO	425	SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
GUSCIO	426	SS =	0.8	SI =	0.8
		SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
GUSCIO	427	SS =	0.8	SI =	0.8
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6

QJSCIO 426 SS = 0.6 SI = 0.6
SS = 0.3 SI = 0.3
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.3 SI = 0.3
QJSCIO 427 SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
QJSCIO 428 SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
QJSCIO 429 SS = 0.7 SI = 0.7
SS = 0.8 SI = 0.8
SS = 0.8 SI = 0.8
SS = 0.7 SI = 0.7
QJSCIO 430 SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
QJSCIO 431 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 432 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 433 SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.1 SI = 1.1
QJSCIO 434 SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
QJSCIO 435 SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
QJSCIO 436 SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
QJSCIO 437 SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
QJSCIO 438 SS = 2.0 SI = 2.0
SS = 2.3 SI = 2.3
SS = 2.3 SI = 2.3
SS = 2.0 SI = 2.0
QJSCIO 439 SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.2 SI = 1.2
QJSCIO 440 SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
QJSCIO 441 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
QJSCIO 442 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2

QJSCIO 443 SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
QJSCIO 444 SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
QJSCIO 445 SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
QJSCIO 446 SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
QJSCIO 447 SS = 1.4 SI = 1.4
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.4 SI = 1.4
QJSCIO 448 SS = 1.4 SI = 1.4
SS = 1.5 SI = 1.5
SS = 1.5 SI = 1.5
SS = 1.4 SI = 1.4
QJSCIO 449 SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
QJSCIO 450 SS = 1.7 SI = 1.7
SS = 2.0 SI = 2.0
SS = 2.0 SI = 2.0
SS = 1.7 SI = 1.7
QJSCIO 451 SS = 3.4 SI = 3.4
SS = 3.7 SI = 3.7
SS = 3.7 SI = 3.7
SS = 3.4 SI = 3.4
QJSCIO 452 SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
QJSCIO 453 SS = 3.5 SI = 3.5
SS = 3.8 SI = 3.8
SS = 3.8 SI = 3.8
SS = 3.5 SI = 3.5
QJSCIO 454 SS = 2.7 SI = 2.7
SS = 3.2 SI = 3.2
SS = 3.2 SI = 3.2
SS = 2.7 SI = 2.7
QJSCIO 455 SS = 1.2 SI = 1.2
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.2 SI = 1.2
QJSCIO 456 SS = 3.1 SI = 3.1
SS = 3.5 SI = 3.5
SS = 3.5 SI = 3.5
SS = 3.1 SI = 3.1
QJSCIO 457 SS = 1.1 SI = 1.1
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.1 SI = 1.1
QJSCIO 458 SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
QJSCIO 459 SS = 1.7 SI = 1.7
SS = 1.9 SI = 1.9
SS = 1.9 SI = 1.9
SS = 1.7 SI = 1.7

QJSCIO 460 SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
QJSCIO 461 SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
QJSCIO 462 SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
SS = 2.4 SI = 2.4
QJSCIO 463 SS = 1.3 SI = 1.3
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.3 SI = 1.3
QJSCIO 464 SS = 1.4 SI = 1.4
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.4 SI = 1.4
QJSCIO 465 SS = 1.7 SI = 1.7
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.7 SI = 1.7
QJSCIO 466 SS = 1.5 SI = 1.5
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.5 SI = 1.5
QJSCIO 467 SS = 1.3 SI = 1.3
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
QJSCIO 468 SS = 1.4 SI = 1.4
SS = 1.2 SI = 1.2
SS = 1.2 SI = 1.2
SS = 1.4 SI = 1.4
QJSCIO 469 SS = 2.1 SI = 2.1
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 2.1 SI = 2.1
QJSCIO 470 SS = 1.0 SI = 1.0
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.0 SI = 1.0
QJSCIO 471 SS = 1.9 SI = 1.9
SS = 1.5 SI = 1.5
SS = 1.5 SI = 1.5
SS = 1.9 SI = 1.9
QJSCIO 472 SS = 1.0 SI = 1.0
SS = 1.1 SI = 1.1
SS = 1.1 SI = 1.1
SS = 1.0 SI = 1.0
QJSCIO 473 SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
QJSCIO 474 SS = 0.9 SI = 0.9
SS = 0.8 SI = 0.8
SS = 0.8 SI = 0.8
SS = 0.9 SI = 0.9
QJSCIO 475 SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
SS = 0.6 SI = 0.6
QJSCIO 476 SS = 0.4 SI = 0.4
SS = 0.5 SI = 0.5
SS = 0.5 SI = 0.5
SS = 0.4 SI = 0.4

QJSCIO 477 SS = 0.6 SI = 0.6
SS = 0.5 SI = 0.5
SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
QJSCIO 478 SS = 1.3 SI = 1.3
SS = 0.9 SI = 0.9
SS = 0.9 SI = 0.9
SS = 1.3 SI = 1.3
QJSCIO 479 SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
SS = 0.2 SI = 0.2
QJSCIO 480 SS = 1.4 SI = 1.4
SS = 1.6 SI = 1.6
SS = 1.6 SI = 1.6
SS = 1.4 SI = 1.4
QJSCIO 481 SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
SS = 0.5 SI = 0.5
SS = 0.6 SI = 0.6
QJSCIO 482 SS = 2.8 SI = 2.8
SS = 2.0 SI = 2.0
SS = 2.0 SI = 2.0
SS = 2.8 SI = 2.8
QJSCIO 483 SS = 1.0 SI = 1.0
SS = 0.7 SI = 0.7
SS = 0.7 SI = 0.7
SS = 1.0 SI = 1.0
QJSCIO 484 SS = 2.0 SI = 2.0
SS = 1.4 SI = 1.4
SS = 1.4 SI = 1.4
SS = 2.0 SI = 2.0
QJSCIO 485 SS = 1.3 SI = 1.3
SS = 1.0 SI = 1.0
SS = 1.0 SI = 1.0
SS = 1.3 SI = 1.3
QJSCIO 486 SS = 1.7 SI = 1.7
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 1.7 SI = 1.7
QJSCIO 487 SS = 2.5 SI = 2.5
SS = 1.7 SI = 1.7
SS = 1.7 SI = 1.7
SS = 2.5 SI = 2.5
QJSCIO 488 SS = 1.5 SI = 1.5
SS = 1.8 SI = 1.8
SS = 1.8 SI = 1.8
SS = 1.5 SI = 1.5
QJSCIO 489 SS = 1.9 SI = 1.9
SS = 2.1 SI = 2.1
SS = 2.1 SI = 2.1
SS = 1.9 SI = 1.9
QJSCIO 490 SS = 2.5 SI = 2.5
SS = 2.6 SI = 2.6
SS = 2.6 SI = 2.6
SS = 2.5 SI = 2.5
QJSCIO 491 SS = 1.8 SI = 1.8
SS = 1.9 SI = 1.9
SS = 1.9 SI = 1.9
SS = 1.8 SI = 1.8
QJSCIO 492 SS = 0.9 SI = 0.9
SS = 1.3 SI = 1.3
SS = 1.3 SI = 1.3
SS = 0.9 SI = 0.9
QJSCIO 493 SS = 2.4 SI = 2.4
SS = 1.8 SI = 1.8
SS = 1.8 SI = 1.8
SS = 2.4 SI = 2.4
QJSCIO 494 SS = 0.9 SI = 0.9

		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
QUSC10	495	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.2	SI =	2.2
QUSC10	496	SS =	3.5	SI =	3.5
		SS =	4.0	SI =	4.0
		SS =	4.0	SI =	4.0
		SS =	3.5	SI =	3.5
QUSC10	497	SS =	2.8	SI =	2.8
		SS =	3.2	SI =	3.2
		SS =	3.2	SI =	3.2
		SS =	2.8	SI =	2.8
QUSC10	498	SS =	1.4	SI =	1.4
		SS =	1.9	SI =	1.9
		SS =	1.9	SI =	1.9
		SS =	1.4	SI =	1.4
QUSC10	499	SS =	0.9	SI =	0.9
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
tensione max =		SS =	0.9	SI =	0.9
		4.0	guscio =	496	

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 5 S15WY SU
N. 2 CONDIZIONI ANALISI STATICA
7 S15WY +- 1.00
9 Torcente_add_Y +- 1.00
1) +1.00e+007 +1.00e+009
2) -1.00e+007 +1.00e+009
3) +1.00e+007 -1.00e+009
4) -1.00e+007 -1.00e+009
Unità di misura: SI,SS [daN/cm2]

COMBINAZIONE

		SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
QUSC10	425	SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
QUSC10	426	SS =	0.3	SI =	0.3
		SS =	0.2	SI =	0.2
		SS =	0.2	SI =	0.2
		SS =	0.3	SI =	0.3
QUSC10	427	SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
QUSC10	428	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	429	SS =	0.5	SI =	0.5
		SS =	0.4	SI =	0.4
		SS =	0.4	SI =	0.4
		SS =	0.5	SI =	0.5
QUSC10	430	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	431	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	432	SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
QUSC10	433	SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
QUSC10	434	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
QUSC10	435	SS =	3.1	SI =	3.1
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	3.1	SI =	3.1
QUSC10	436	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSC10	437	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	438	SS =	3.0	SI =	3.0
		SS =	2.7	SI =	2.7
		SS =	2.7	SI =	2.7
		SS =	3.0	SI =	3.0
QUSC10	439	SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
QUSC10	440	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
QUSC10	441	SS =	0.8	SI =	0.8
		SS =	0.7	SI =	0.7

		SS =	0.7	SI =	0.7
		SS =	0.8	SI =	0.8
QUSC10	442	SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
		SS =	2.2	SI =	2.2
		SS =	2.0	SI =	2.0
QUSC10	443	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
QUSC10	444	SS =	0.6	SI =	0.6
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.6	SI =	0.6
QUSC10	445	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
QUSC10	446	SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
QUSC10	447	SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
QUSC10	448	SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.5	SI =	1.5
QUSC10	449	SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
QUSC10	450	SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.4	SI =	1.4
QUSC10	451	SS =	4.5	SI =	4.5
		SS =	4.8	SI =	4.8
		SS =	4.8	SI =	4.8
		SS =	4.5	SI =	4.5
QUSC10	452	SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
QUSC10	453	SS =	4.2	SI =	4.2
		SS =	4.1	SI =	4.1
		SS =	4.1	SI =	4.1
		SS =	4.2	SI =	4.2
QUSC10	454	SS =	3.1	SI =	3.1
		SS =	3.4	SI =	3.4
		SS =	3.4	SI =	3.4
		SS =	3.1	SI =	3.1
QUSC10	455	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSC10	456	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
QUSC10	457	SS =	0.6	SI =	0.6
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.6	SI =	0.6
QUSC10	458	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5

		SS =	0.5	SI =	0.5
QUSC10	459	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
QUSC10	460	SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
		SS =	0.6	SI =	0.6
QUSC10	461	SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
QUSC10	462	SS =	3.1	SI =	3.1
		SS =	3.2	SI =	3.2
		SS =	3.2	SI =	3.2
		SS =	3.1	SI =	3.1
QUSC10	463	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSC10	464	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSC10	465	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
QUSC10	466	SS =	1.7	SI =	1.7
		SS =	1.8	SI =	1.8
		SS =	1.8	SI =	1.8
		SS =	1.7	SI =	1.7
QUSC10	467	SS =	1.0	SI =	1.0
		SS =	1.1	SI =	1.1
		SS =	1.1	SI =	1.1
		SS =	1.0	SI =	1.0
QUSC10	468	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
QUSC10	469	SS =	2.6	SI =	2.6
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	2.6	SI =	2.6
QUSC10	470	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
QUSC10	471	SS =	2.4	SI =	2.4
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.4	SI =	2.4
QUSC10	472	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.1	SI =	2.1
QUSC10	473	SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
QUSC10	474	SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
QUSC10	475	SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2

		SS =	1.2	SI =	1.2
GUSCIO	476	SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
GUSCIO	477	SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1
		SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
GUSCIO	478	SS =	2.2	SI =	2.2
		SS =	2.1	SI =	2.1
		SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	479	SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
GUSCIO	480	SS =	2.9	SI =	2.9
		SS =	3.0	SI =	3.0
		SS =	3.0	SI =	3.0
		SS =	2.9	SI =	2.9
GUSCIO	481	SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
		SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
GUSCIO	482	SS =	2.4	SI =	2.4
		SS =	2.5	SI =	2.5
		SS =	2.5	SI =	2.5
		SS =	2.4	SI =	2.4
GUSCIO	483	SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
GUSCIO	484	SS =	2.2	SI =	2.2
		SS =	2.0	SI =	2.0
		SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
GUSCIO	485	SS =	1.3	SI =	1.3
		SS =	1.4	SI =	1.4
		SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
GUSCIO	486	SS =	1.9	SI =	1.9
		SS =	2.2	SI =	2.2
		SS =	2.2	SI =	2.2
		SS =	1.9	SI =	1.9
GUSCIO	487	SS =	2.9	SI =	2.9
		SS =	3.6	SI =	3.6
		SS =	3.6	SI =	3.6
		SS =	2.9	SI =	2.9
GUSCIO	488	SS =	1.0	SI =	1.0
		SS =	0.9	SI =	0.9
		SS =	0.9	SI =	0.9
		SS =	1.0	SI =	1.0
GUSCIO	489	SS =	1.6	SI =	1.6
		SS =	1.5	SI =	1.5
		SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
GUSCIO	490	SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
		SS =	5.2	SI =	5.2
GUSCIO	491	SS =	3.8	SI =	3.8
		SS =	3.7	SI =	3.7
		SS =	3.7	SI =	3.7
		SS =	3.8	SI =	3.8
GUSCIO	492	SS =	1.1	SI =	1.1
		SS =	1.2	SI =	1.2
		SS =	1.2	SI =	1.2
		SS =	1.1	SI =	1.1

GUSCIO	493	SS =	4.2	SI =	4.2
		SS =	4.3	SI =	4.3
		SS =	4.3	SI =	4.3
		SS =	4.2	SI =	4.2
GUSCIO	494	SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
		SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3
GUSCIO	496	SS =	6.9	SI =	6.9
		SS =	7.3	SI =	7.3
		SS =	7.3	SI =	7.3
		SS =	6.9	SI =	6.9
GUSCIO	497	SS =	4.3	SI =	4.3
		SS =	5.0	SI =	5.0
		SS =	5.0	SI =	5.0
		SS =	4.3	SI =	4.3
GUSCIO	498	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
		SS =	1.6	SI =	1.6
		SS =	1.3	SI =	1.3
GUSCIO	499	SS =	0.7	SI =	0.7
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
		SS =	0.7	SI =	0.7
tensione max = 7,3 guscio = 496					
SOLLECITAZIONE GUSCI RETTANGOLARI					
CASO DI CARICO : 6 SLU con SISMAS					
N. 3 CONDIZIONI ANALISI STATICA					
1 Peso proprio + 1.00					
2 Permanente + 1.00					
3 Avar. abilitazione + 0.30					
N. 1 CASI DI CARICO					
4 SISMAS SLU 1.00					
1) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.001					
2) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.002					
3) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.003					
4) +1.00*c001 +1.00*c002 +0.30*c003 +1.00*c004.004					
Unità di misura: SI,SS (kN/cm2)					
GUSCIO	415	SS =	1.3	SI =	1.3
		SS =	1.2	SI =	1.2
		SS =	1.3	SI =	1.3
		SS =	1.1	SI =	1.1
GUSCIO	416	SS =	0.8	SI =	0.8
		SS =	0.9	SI =	0.9
		SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
GUSCIO	417	SS =	3.5	SI =	3.5
		SS =	2.6	SI =	2.6
		SS =	3.4	SI =	3.4
		SS =	2.5	SI =	2.5
GUSCIO	418	SS =	3.6	SI =	3.6
		SS =	2.5	SI =	2.5
		SS =	3.5	SI =	3.5
		SS =	2.4	SI =	2.4
GUSCIO	419	SS =	9.2	SI =	9.2
		SS =	5.8	SI =	5.8
		SS =	9.0	SI =	9.0
		SS =	5.5	SI =	5.5
GUSCIO	420	SS =	7.5	SI =	7.5
		SS =	4.1	SI =	4.1
		SS =	7.6	SI =	7.6
		SS =	4.0	SI =	4.0
GUSCIO	421	SS =	9.5	SI =	9.5
		SS =	4.2	SI =	4.2
		SS =	9.9	SI =	9.9
		SS =	4.8	SI =	4.8
GUSCIO	422	SS =	7.6	SI =	7.6
		SS =	3.7	SI =	3.7
		SS =	7.7	SI =	7.7

		SS =	3.9	SI =	3.9
GUSCIO	423	SS =	3.3	SI =	3.3
		SS =	2.1	SI =	2.1
		SS =	3.5	SI =	3.5
		SS =	2.3	SI =	2.3
GUSCIO	424	SS =	3.4	SI =	3.4
		SS =	2.0	SI =	2.0
		SS =	3.6	SI =	3.6
		SS =	2.2	SI =	2.2
GUSCIO	425	SS =	1.4	SI =	1.4
		SS =	0.9	SI =	0.9
		SS =	1.4	SI =	1.4
		SS =	1.0	SI =	1.0
GUSCIO	426	SS =	0.6	SI =	0.6
		SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
		SS =	0.7	SI =	0.7
GUSCIO	427	SS =	2.8	SI =	2.8
		SS =	1.9	SI =	1.9
		SS =	2.9	SI =	2.9
		SS =	1.9	SI =	1.9
GUSCIO	428	SS =	3.3	SI =	3.3
		SS =	2.1	SI =	2.1
		SS =	3.4	SI =	3.4
		SS =	2.1	SI =	2.1
GUSCIO	429	SS =	2.1	SI =	2.1
		SS =	1.4	SI =	1.4
		SS =	2.2	SI =	2.2
		SS =	1.4	SI =	1.4
GUSCIO	430	SS =	3.8	SI =	3.8
		SS =	3.4	SI =	3.4
		SS =	3.9	SI =	3.9
		SS =	3.4	SI =	3.4
GUSCIO	431	SS =	4.3	SI =	4.3
		SS =	3.4	SI =	3.4
		SS =	4.4	SI =	4.4
		SS =	3.4	SI =	3.4
GUSCIO	432	SS =	3.9	SI =	3.9
		SS =	2.5	SI =	2.5
		SS =	4.0	SI =	4.0
		SS =	2.6	SI =	2.6
GUSCIO	433	SS =	5.2	SI =	5.2
		SS =	5.5	SI =	5.5
		SS =	5.3	SI =	5.3
		SS =	5.5	SI =	5.5
GUSCIO	434	SS =	5.6	SI =	5.6
		SS =	4.7	SI =	4.7
		SS =	5.7	SI =	5.7
		SS =	4.8	SI =	4.8
GUSCIO	435	SS =	7.8	SI =	7.8
		SS =	6.3	SI =	6.3
		SS =	7.6	SI =	7.6
		SS =	6.2	SI =	6.2
GUSCIO	436	SS =	4.8	SI =	4.8
		SS =	5.0	SI =	5.0
		SS =	5.0	SI =	5.0
		SS =	5.1	SI =	5.1
GUSCIO	437	SS =	5.6	SI =	5.6
		SS =	4.5	SI =	4.5
		SS =	5.7	SI =	5.7
		SS =	4.7	SI =	4.7
GUSCIO	438	SS =	7.9	SI =	7.9
		SS =	5.2	SI =	5.2
		SS =	8.4	SI =	8.4
		SS =	5.7	SI =	5.7
GUSCIO	439	SS =	3.3	SI =	3.3
		SS =	2.8	SI =	2.8
		SS =	3.5	SI =	3.5
		SS =	3.1	SI =	3.1

GUSCIO	457	SS = 1.9	SI = 1.9
		SS = 2.4	SI = 2.4
		SS = 1.7	SI = 1.7
		SS = 2.2	SI = 2.2
GUSCIO	458	SS = 2.2	SI = 2.2
		SS = 2.9	SI = 2.9
		SS = 2.2	SI = 2.2
		SS = 2.8	SI = 2.8
GUSCIO	459	SS = 1.8	SI = 1.8
		SS = 3.4	SI = 3.4
		SS = 1.9	SI = 1.9
		SS = 3.3	SI = 3.3
GUSCIO	460	SS = 1.8	SI = 1.8
		SS = 2.1	SI = 2.1
		SS = 1.8	SI = 1.8
		SS = 2.2	SI = 2.2
GUSCIO	461	SS = 1.8	SI = 1.8
		SS = 1.8	SI = 1.8
		SS = 1.7	SI = 1.7
		SS = 1.9	SI = 1.9
GUSCIO	462	SS = 2.2	SI = 2.2
		SS = 4.4	SI = 4.4
		SS = 2.0	SI = 2.0
		SS = 4.3	SI = 4.3
GUSCIO	463	SS = 2.2	SI = 2.2
		SS = 2.7	SI = 2.7
		SS = 2.1	SI = 2.1
		SS = 2.8	SI = 2.8
GUSCIO	464	SS = 2.1	SI = 2.1
		SS = 2.2	SI = 2.2
		SS = 2.0	SI = 2.0
		SS = 2.3	SI = 2.3
GUSCIO	465	SS = 2.5	SI = 2.5
		SS = 2.8	SI = 2.8
		SS = 2.2	SI = 2.2
		SS = 2.6	SI = 2.6
GUSCIO	466	SS = 2.0	SI = 2.0
		SS = 2.4	SI = 2.4
		SS = 1.6	SI = 1.6
		SS = 2.4	SI = 2.4
GUSCIO	467	SS = 2.0	SI = 2.0
		SS = 2.2	SI = 2.2
		SS = 1.9	SI = 1.9
		SS = 2.4	SI = 2.4
GUSCIO	468	SS = 2.2	SI = 2.2
		SS = 2.2	SI = 2.2
		SS = 1.9	SI = 1.9
		SS = 2.2	SI = 2.2
GUSCIO	469	SS = 2.6	SI = 2.6
		SS = 2.6	SI = 2.6
		SS = 2.5	SI = 2.5
		SS = 2.9	SI = 2.9
GUSCIO	470	SS = 2.1	SI = 2.1
		SS = 2.2	SI = 2.2
		SS = 2.1	SI = 2.1
		SS = 2.3	SI = 2.3
GUSCIO	471	SS = 2.6	SI = 2.6
		SS = 1.9	SI = 1.9
		SS = 2.5	SI = 2.5
		SS = 2.2	SI = 2.2
GUSCIO	472	SS = 2.5	SI = 2.5
		SS = 2.6	SI = 2.6
		SS = 2.4	SI = 2.4
		SS = 2.6	SI = 2.6
GUSCIO	473	SS = 2.2	SI = 2.2
		SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.4	SI = 2.4
GUSCIO	474	SS = 2.4	SI = 2.4

GUSCIO	475	SS = 1.7	SI = 1.7
		SS = 2.4	SI = 2.4
		SS = 1.9	SI = 1.9
		SS = 1.5	SI = 1.5
GUSCIO	476	SS = 1.6	SI = 1.6
		SS = 1.4	SI = 1.4
		SS = 1.7	SI = 1.7
		SS = 1.9	SI = 1.9
GUSCIO	477	SS = 2.0	SI = 2.0
		SS = 1.8	SI = 1.8
		SS = 1.2	SI = 1.2
		SS = 1.7	SI = 1.7
GUSCIO	478	SS = 2.5	SI = 2.5
		SS = 0.9	SI = 0.9
		SS = 2.2	SI = 2.2
		SS = 1.0	SI = 1.0
GUSCIO	479	SS = 0.6	SI = 0.6
		SS = 0.4	SI = 0.4
		SS = 0.6	SI = 0.6
		SS = 0.5	SI = 0.5
GUSCIO	480	SS = 1.7	SI = 1.7
		SS = 2.2	SI = 2.2
		SS = 1.2	SI = 1.2
		SS = 2.0	SI = 2.0
GUSCIO	481	SS = 1.0	SI = 1.0
		SS = 0.7	SI = 0.7
		SS = 0.9	SI = 0.9
		SS = 0.6	SI = 0.6
GUSCIO	482	SS = 4.5	SI = 4.5
		SS = 2.1	SI = 2.1
		SS = 3.6	SI = 3.6
		SS = 2.3	SI = 2.3
GUSCIO	483	SS = 2.3	SI = 2.3
		SS = 2.0	SI = 2.0
		SS = 2.0	SI = 2.0
		SS = 1.8	SI = 1.8
GUSCIO	484	SS = 3.8	SI = 3.8
		SS = 0.8	SI = 0.8
		SS = 3.3	SI = 3.3
		SS = 1.2	SI = 1.2
GUSCIO	485	SS = 2.2	SI = 2.2
		SS = 2.8	SI = 2.8
		SS = 1.9	SI = 1.9
		SS = 2.8	SI = 2.8
GUSCIO	486	SS = 2.0	SI = 2.0
		SS = 2.6	SI = 2.6
		SS = 1.7	SI = 1.7
		SS = 2.6	SI = 2.6
GUSCIO	487	SS = 2.9	SI = 2.9
		SS = 4.1	SI = 4.1
		SS = 3.0	SI = 3.0
		SS = 5.3	SI = 5.3
GUSCIO	488	SS = 1.2	SI = 1.2
		SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
		SS = 2.1	SI = 2.1
GUSCIO	489	SS = 1.6	SI = 1.6
		SS = 4.0	SI = 4.0
		SS = 1.7	SI = 1.7
		SS = 3.8	SI = 3.8
GUSCIO	490	SS = 6.4	SI = 6.4
		SS = 8.4	SI = 8.4
		SS = 6.3	SI = 6.3
		SS = 8.3	SI = 8.3
GUSCIO	491	SS = 6.1	SI = 6.1

GUSCIO	492	SS = 7.5	SI = 7.5
		SS = 5.9	SI = 5.9
		SS = 7.3	SI = 7.3
		SS = 1.8	SI = 1.8
GUSCIO	493	SS = 3.1	SI = 3.1
		SS = 1.4	SI = 1.4
		SS = 2.8	SI = 2.8
		SS = 3.8	SI = 3.8
GUSCIO	494	SS = 3.4	SI = 3.4
		SS = 3.2	SI = 3.2
		SS = 3.4	SI = 3.4
		SS = 0.8	SI = 0.8
GUSCIO	495	SS = 1.3	SI = 1.3
		SS = 0.9	SI = 0.9
		SS = 1.2	SI = 1.2
		SS = 2.3	SI = 2.3
GUSCIO	496	SS = 3.7	SI = 3.7
		SS = 2.6	SI = 2.6
		SS = 3.7	SI = 3.7
		SS = 6.2	SI = 6.2
GUSCIO	497	SS = 8.6	SI = 8.6
		SS = 7.0	SI = 7.0
		SS = 9.1	SI = 9.1
		SS = 5.2	SI = 5.2
GUSCIO	498	SS = 6.8	SI = 6.8
		SS = 4.9	SI = 4.9
		SS = 5.5	SI = 5.5
		SS = 1.1	SI = 1.1
GUSCIO	499	SS = 2.6	SI = 2.6
		SS = 1.3	SI = 1.3
		SS = 2.0	SI = 2.0
		SS = 1.9	SI = 1.9
GUSCIO	499	SS = 2.7	SI = 2.7
		SS = 1.7	SI = 1.7
		SS = 2.7	SI = 2.7
		tensione max = 9.9	guscio = 421

SOLLECITAZIONE GUSCI RETTANGOLARI			
CASO DI CARICO : 7 SLU con SISNAV			
N. 3 CONDIZIONE ANALIST STATICA			
1	Peso proprio	+	1.00
2	Permanente	+	1.00
3	Accidentalizzazione	+	0.30
N. 1 CASO DI CARICO			
5	SISNAV SLU		1.00
1)	+1.00*c001	+1.00*c002	+0.30*c003
2)	+1.00*c001	+1.00*c002	+0.30*c003
3)	+1.00*c001	+1.00*c002	+0.30*c003
4)	+1.00*c001	+1.00*c002	+0.30*c003
Unità di misura: SI,SS [daN/cm2]			
GUSCIO	415	SS = 0.9	SI = 0.9
		SS = 1.5	SI = 1.5
		SS = 0.9	SI = 0.9
		SS = 1.5	SI = 1.5
GUSCIO	416	SS = 0.4	SI = 0.4
		SS = 1.2	SI = 1.2
		SS = 0.5	SI = 0.5
		SS = 1.2	SI = 1.2
GUSCIO	417	SS = 2.0	SI = 2.0
		SS = 3.9	SI = 3.9
		SS = 2.1	SI = 2.1
		SS = 4.0	SI = 4.0
GUSCIO	418	SS = 2.1	SI = 2.1
		SS = 3.9	SI = 3.9
		SS = 2.2	SI = 2.2
		SS = 3.9	SI = 3.9
GUSCIO	419	SS = 4.8	SI = 4.8
		SS = 10.0	SI = 10.0
		SS = 4.9	SI = 4.9
		SS = 10.2	SI = 10.2
GUSCIO	420	SS = 5.3	SI = 5.3
		SS = 6.4	SI = 6.4
		SS = 5.3	SI = 5.3
		SS = 6.5	SI = 6.5
GUSCIO	421	SS = 9.6	SI = 9.6

GUSCIO	422	SS = 5.3	SI = 5.3
		SS = 9.3	SI = 9.3
		SS = 5.1	SI = 5.1
		SS = 6.2	SI = 6.2
GUSCIO	423	SS = 5.5	SI = 5.5
		SS = 6.1	SI = 6.1
		SS = 5.4	SI = 5.4
		SS = 3.7	SI = 3.7
GUSCIO	424	SS = 1.9	SI = 1.9
		SS = 3.5	SI = 3.5
		SS = 1.8	SI = 1.8
		SS = 3.6	SI = 3.6
GUSCIO	425	SS = 2.2	SI = 2.2
		SS = 3.4	SI = 3.4
		SS = 2.1	SI = 2.1
		SS = 1.4	SI = 1.4
GUSCIO	426	SS = 0.7	SI = 0.7
		SS = 1.4	SI = 1.4
		SS = 0.6	SI = 0.6
		SS = 0.9	SI = 0.9
GUSCIO	427	SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
		SS = 2.7	SI = 2.7
		SS = 1.8	SI = 1.8
GUSCIO	428	SS = 2.7	SI = 2.7
		SS = 2.2	SI = 2.2
		SS = 3.2	SI = 3.2
		SS = 2.2	SI = 2.2
GUSCIO	429	SS = 3.1	SI = 3.1
		SS = 1.6	SI = 1.6
		SS = 1.8	SI = 1.8
		SS = 1.5	SI = 1.5
GUSCIO	430	SS = 1.8	SI = 1.8
		SS = 2.8	SI = 2.8
		SS = 4.4	SI = 4.4
		SS = 2.8	SI = 2.8
GUSCIO	431	SS = 4.4	SI = 4.4
		SS = 3.1	SI = 3.1
		SS = 4.6	SI = 4.6
		SS = 3.0	SI = 3.0
GUSCIO	432	SS = 4.6	SI = 4.6
		SS = 2.9	SI = 2.9
		SS = 3.7	SI = 3.7
		SS = 2.9	SI = 2.9
GUSCIO	433	SS = 3.7	SI = 3.7
		SS = 4.2	SI = 4.2
		SS = 6.5	SI = 6.5
		SS = 4.1	SI = 4.1
GUSCIO	434	SS = 6.5	SI = 6.5
		SS = 4.4	SI = 4.4
		SS = 5.8	SI = 5.8
		SS = 4.4	SI = 4.4
GUSCIO	435	SS = 5.7	SI = 5.7
		SS = 5.4	SI = 5.4
		SS = 9.4	SI = 9.4
		SS = 5.3	SI = 5.3
GUSCIO	436	SS = 9.5	SI = 9.5
		SS = 4.4	SI = 4.4
		SS = 5.4	SI = 5.4
		SS = 4.3	SI = 4.3
GUSCIO	437	SS = 5.3	SI = 5.3
		SS = 4.5	SI = 4.5
		SS = 4.4	SI = 4.4
		SS = 5.4	SI = 5.4
GUSCIO	438	SS = 4.4	SI = 4.4
		SS = 5.4	SI = 5.4
		SS = 9.3	SI = 9.3
		SS = 5.4	SI = 5.4

		SS = 6.1	SI = 6.1
		SS = 9.0	SI = 9.0
		SS = 6.0	SI = 6.0
QUSCIO	439	SS = 3.0	SI = 3.0
		SS = 3.3	SI = 3.3
		SS = 2.9	SI = 2.9
		SS = 3.2	SI = 3.2
QUSCIO	440	SS = 3.8	SI = 3.8
		SS = 3.6	SI = 3.6
		SS = 3.7	SI = 3.7
		SS = 3.6	SI = 3.6
QUSCIO	441	SS = 3.7	SI = 3.7
		SS = 3.0	SI = 3.0
		SS = 3.7	SI = 3.7
		SS = 3.0	SI = 3.0
QUSCIO	442	SS = 3.7	SI = 3.7
		SS = 1.9	SI = 1.9
		SS = 3.9	SI = 3.9
		SS = 1.8	SI = 1.8
QUSCIO	443	SS = 3.3	SI = 3.3
		SS = 2.4	SI = 2.4
		SS = 3.2	SI = 3.2
		SS = 2.4	SI = 2.4
QUSCIO	444	SS = 2.2	SI = 2.2
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.4	SI = 1.4
QUSCIO	445	SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
		SS = 0.4	SI = 0.4
		SS = 1.9	SI = 1.9
QUSCIO	446	SS = 0.8	SI = 0.8
		SS = 2.6	SI = 2.6
		SS = 0.8	SI = 0.8
		SS = 2.6	SI = 2.6
QUSCIO	447	SS = 0.8	SI = 0.8
		SS = 1.5	SI = 1.5
		SS = 0.7	SI = 0.7
		SS = 1.7	SI = 1.7
QUSCIO	448	SS = 1.2	SI = 1.2
		SS = 3.9	SI = 3.9
		SS = 1.2	SI = 1.2
		SS = 3.9	SI = 3.9
QUSCIO	449	SS = 1.5	SI = 1.5
		SS = 4.4	SI = 4.4
		SS = 1.5	SI = 1.5
		SS = 4.3	SI = 4.3
QUSCIO	450	SS = 1.5	SI = 1.5
		SS = 3.9	SI = 3.9
		SS = 1.5	SI = 1.5
		SS = 3.9	SI = 3.9
QUSCIO	451	SS = 3.3	SI = 3.3
		SS = 9.2	SI = 9.2
		SS = 3.4	SI = 3.4
		SS = 8.9	SI = 8.9
QUSCIO	452	SS = 3.2	SI = 3.2
		SS = 5.7	SI = 5.7
		SS = 3.2	SI = 3.2
		SS = 5.7	SI = 5.7
QUSCIO	453	SS = 3.3	SI = 3.3
		SS = 9.3	SI = 9.3
		SS = 3.3	SI = 3.3
		SS = 9.4	SI = 9.4
QUSCIO	454	SS = 6.1	SI = 6.1
		SS = 4.7	SI = 4.7
		SS = 6.4	SI = 6.4
		SS = 4.8	SI = 4.8
QUSCIO	455	SS = 3.2	SI = 3.2
		SS = 5.1	SI = 5.1

		SS = 3.2	SI = 3.2
		SS = 5.1	SI = 5.1
QUSCIO	456	SS = 5.8	SI = 5.8
		SS = 4.7	SI = 4.7
		SS = 5.9	SI = 5.9
		SS = 4.8	SI = 4.8
QUSCIO	457	SS = 1.9	SI = 1.9
		SS = 1.6	SI = 1.6
		SS = 2.1	SI = 2.1
		SS = 1.7	SI = 1.7
QUSCIO	458	SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.3	SI = 2.3
		SS = 2.3	SI = 2.3
QUSCIO	459	SS = 1.9	SI = 1.9
		SS = 1.9	SI = 1.9
		SS = 2.0	SI = 2.0
		SS = 1.9	SI = 1.9
QUSCIO	460	SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
		SS = 2.3	SI = 2.3
		SS = 1.5	SI = 1.5
QUSCIO	461	SS = 1.9	SI = 1.9
		SS = 1.4	SI = 1.4
		SS = 1.9	SI = 1.9
		SS = 1.3	SI = 1.3
QUSCIO	462	SS = 5.4	SI = 5.4
		SS = 1.9	SI = 1.9
		SS = 5.5	SI = 5.5
		SS = 1.9	SI = 1.9
QUSCIO	463	SS = 3.3	SI = 3.3
		SS = 1.3	SI = 1.3
		SS = 3.4	SI = 3.4
		SS = 1.3	SI = 1.3
QUSCIO	464	SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
		SS = 2.5	SI = 2.5
		SS = 1.2	SI = 1.2
QUSCIO	465	SS = 2.3	SI = 2.3
		SS = 3.2	SI = 3.2
		SS = 2.4	SI = 2.4
		SS = 3.4	SI = 3.4
QUSCIO	466	SS = 3.2	SI = 3.2
		SS = 1.3	SI = 1.3
		SS = 3.4	SI = 3.4
		SS = 1.0	SI = 1.0
QUSCIO	467	SS = 2.3	SI = 2.3
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.2	SI = 1.2
QUSCIO	468	SS = 2.8	SI = 2.8
		SS = 0.9	SI = 0.9
		SS = 2.9	SI = 2.9
		SS = 1.0	SI = 1.0
QUSCIO	469	SS = 2.4	SI = 2.4
		SS = 4.2	SI = 4.2
		SS = 2.7	SI = 2.7
		SS = 3.8	SI = 3.8
QUSCIO	470	SS = 2.7	SI = 2.7
		SS = 1.5	SI = 1.5
		SS = 2.6	SI = 2.6
		SS = 1.3	SI = 1.3
QUSCIO	471	SS = 2.6	SI = 2.6
		SS = 2.9	SI = 2.9
		SS = 2.5	SI = 2.5
		SS = 3.0	SI = 3.0
QUSCIO	472	SS = 3.2	SI = 3.2
		SS = 2.6	SI = 2.6

		SS = 3.4	SI = 3.4
		SS = 2.4	SI = 2.4
QUSCIO	473	SS = 3.0	SI = 3.0
		SS = 1.5	SI = 1.5
		SS = 3.0	SI = 3.0
		SS = 1.4	SI = 1.4
QUSCIO	474	SS = 3.0	SI = 3.0
		SS = 1.7	SI = 1.7
		SS = 2.9	SI = 2.9
		SS = 1.7	SI = 1.7
QUSCIO	475	SS = 2.4	SI = 2.4
		SS = 1.1	SI = 1.1
		SS = 2.4	SI = 2.4
		SS = 1.0	SI = 1.0
QUSCIO	476	SS = 3.2	SI = 3.2
		SS = 0.6	SI = 0.6
		SS = 3.2	SI = 3.2
		SS = 0.7	SI = 0.7
QUSCIO	477	SS = 2.4	SI = 2.4
		SS = 0.8	SI = 0.8
		SS = 2.4	SI = 2.4
		SS = 0.9	SI = 0.9
QUSCIO	478	SS = 3.2	SI = 3.2
		SS = 1.1	SI = 1.1
		SS = 3.2	SI = 3.2
		SS = 1.1	SI = 1.1
QUSCIO	479	SS = 1.3	SI = 1.3
		SS = 0.5	SI = 0.5
		SS = 1.3	SI = 1.3
		SS = 0.5	SI = 0.5
QUSCIO	480	SS = 3.8	SI = 3.8
		SS = 2.5	SI = 2.5
		SS = 4.1	SI = 4.1
		SS = 2.4	SI = 2.4
QUSCIO	481	SS = 1.3	SI = 1.3
		SS = 0.9	SI = 0.9
		SS = 1.4	SI = 1.4
		SS = 0.9	SI = 0.9
QUSCIO	482	SS = 3.3	SI = 3.3
		SS = 3.7	SI = 3.7
		SS = 3.6	SI = 3.6
		SS = 4.1	SI = 4.1
QUSCIO	483	SS = 2.5	SI = 2.5
		SS = 1.3	SI = 1.3
		SS = 2.7	SI = 2.7
		SS = 1.5	SI = 1.5
QUSCIO	484	SS = 1.8	SI = 1.8
		SS = 3.8	SI = 3.8
		SS = 1.9	SI = 1.9
		SS = 4.1	SI = 4.1
QUSCIO	485	SS = 3.4	SI = 3.4
		SS = 1.5	SI = 1.5
		SS = 3.5	SI = 3.5
		SS = 1.4	SI = 1.4
QUSCIO	486	SS = 3.3	SI = 3.3
		SS = 1.6	SI = 1.6
		SS = 3.4	SI = 3.4
		SS = 1.3	SI = 1.3
QUSCIO	487	SS = 1.7	SI = 1.7
		SS = 6.5	SI = 6.5
		SS = 1.9	SI = 1.9
		SS = 5.7	SI = 5.7
QUSCIO	488	SS = 0.7	SI = 0.7
		SS = 1.4	SI = 1.4
		SS = 0.5	SI = 0.5
		SS = 1.6	SI = 1.6
QUSCIO	489	SS = 0.7	SI = 0.7
		SS = 3.7	SI = 3.7
		SS = 0.8	SI = 0.8

		SS = 3.8	SI = 3.8
QUSCIO	490	SS = 4.1	SI = 4.1
		SS = 11.9	SI = 11.9
		SS = 4.2	SI = 4.2
		SS = 11.9	SI = 11.9
QUSCIO	491	SS = 8.0	SI = 8.0
		SS = 7.1	SI = 7.1
		SS = 8.1	SI = 8.1
		SS = 7.1	SI = 7.1
QUSCIO	492	SS = 2.3	SI = 2.3
		SS = 2.2	SI = 2.2
		SS = 2.5	SI = 2.5
		SS = 2.3	SI = 2.3
QUSCIO	493	SS = 6.8	SI = 6.8
		SS = 1.8	SI = 1.8
		SS = 6.9	SI = 6.9
		SS = 1.9	SI = 1.9
QUSCIO	494	SS = 0.1	SI = 0.1
		SS = 0.9	SI = 0.9
		SS = 0.1	SI = 0.1
		SS = 0.9	SI = 0.9
QUSCIO	495	SS = 0.4	SI = 0.4
		SS = 4.4	SI = 4.4
		SS = 0.4	SI = 0.4
		SS = 4.3	SI = 4.3
QUSCIO	496	SS = 1.0	SI = 1.0
		SS = 13.6	SI = 13.6
		SS = 1.0	SI = 1.0
		SS = 13.3	SI = 13.3
QUSCIO	497	SS = 8.9	SI = 8.9
		SS = 1.4	SI = 1.4
		SS = 9.6	SI = 9.6
		SS = 1.4	SI = 1.4
QUSCIO	498	SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	499	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	500	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	501	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	502	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	503	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	504	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	505	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	506	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6
		SS = 2.9	SI = 2.9
		SS = 1.5	SI = 1.5
		SS = 13.6	SI = 13.6
		SS = 4.96	SI = 4.96
		SS = 1.4	SI = 1.4
		SS = 2.1	SI = 2.1
		SS = 1.3	SI = 1.3
		SS = 2.4	SI = 2.4
		SS = 1.3	SI = 1.3
QUSCIO	507	SS = 2.8	SI = 2.8
		SS = 1.6	SI = 1.6

GUSCIO 435 SS = 13.5 SI = 13.5
GUSCIO 436 SS = 9.3 SI = 9.3
GUSCIO 437 SS = 9.5 SI = 9.5
GUSCIO 438 SS = 12.5 SI = 12.5
GUSCIO 439 SS = 5.8 SI = 5.8
GUSCIO 440 SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.4 SI = 6.4
GUSCIO 442 SS = 3.9 SI = 3.9
GUSCIO 443 SS = 5.2 SI = 5.2
GUSCIO 444 SS = 3.3 SI = 3.3
GUSCIO 445 SS = 2.0 SI = 2.0
GUSCIO 446 SS = 3.0 SI = 3.0
GUSCIO 447 SS = 2.3 SI = 2.3
GUSCIO 448 SS = 4.4 SI = 4.4
GUSCIO 449 SS = 5.3 SI = 5.3
GUSCIO 450 SS = 5.2 SI = 5.2
GUSCIO 451 SS = 8.8 SI = 8.8
GUSCIO 452 SS = 7.8 SI = 7.8
GUSCIO 453 SS = 10.6 SI = 10.6
GUSCIO 454 SS = 7.6 SI = 7.6
GUSCIO 455 SS = 7.4 SI = 7.4
GUSCIO 456 SS = 8.7 SI = 8.7
GUSCIO 457 SS = 3.1 SI = 3.1
GUSCIO 458 SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.8 SI = 2.8
GUSCIO 461 SS = 2.2 SI = 2.2
GUSCIO 462 SS = 4.4 SI = 4.4
GUSCIO 463 SS = 3.5 SI = 3.5
GUSCIO 464 SS = 2.6 SI = 2.6
GUSCIO 465 SS = 2.9 SI = 2.9
GUSCIO 466 SS = 2.6 SI = 2.6
GUSCIO 467 SS = 2.4 SI = 2.4
GUSCIO 468 SS = 3.1 SI = 3.1
GUSCIO 469 SS = 2.8 SI = 2.8
GUSCIO 470 SS = 2.9 SI = 2.9
GUSCIO 471 SS = 2.4 SI = 2.4
GUSCIO 472 SS = 3.1 SI = 3.1
GUSCIO 473 SS = 3.0 SI = 3.0
GUSCIO 474 SS = 2.9 SI = 2.9
GUSCIO 475 SS = 2.0 SI = 2.0
GUSCIO 476 SS = 2.9 SI = 2.9
GUSCIO 477 SS = 2.1 SI = 2.1
GUSCIO 478 SS = 2.0 SI = 2.0
GUSCIO 479 SS = 0.8 SI = 0.8
GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 9 Rara VentoX
N. 4 CONDIZIONI ANALISI STATICA
1 PnsL_proprio_____ + 1.00

COMBINAZIONE

2 Permanente_____ + 1.00
3 Avar_abitazione_____ + 1.00
4 Neve_(c<1000h_1m)_____ + 1.00
1) +1.00*c001 -1.00*c002 +1.00*c003 +1.00*c004
Unità di misura: SI,SS [daN/cm2]
GUSCIO 415 SS = 2.2 SI = 2.2
GUSCIO 416 SS = 1.5 SI = 1.5
GUSCIO 417 SS = 5.8 SI = 5.8
GUSCIO 418 SS = 5.9 SI = 5.9
GUSCIO 419 SS = 14.5 SI = 14.5
GUSCIO 420 SS = 11.5 SI = 11.5
GUSCIO 421 SS = 13.6 SI = 13.6
GUSCIO 422 SS = 11.3 SI = 11.3
GUSCIO 423 SS = 5.2 SI = 5.2
GUSCIO 424 SS = 5.5 SI = 5.5
GUSCIO 425 SS = 1.9 SI = 1.9
GUSCIO 426 SS = 1.2 SI = 1.2
GUSCIO 427 SS = 4.2 SI = 4.2
GUSCIO 428 SS = 5.1 SI = 5.1
GUSCIO 429 SS = 3.0 SI = 3.0
GUSCIO 430 SS = 6.8 SI = 6.8
GUSCIO 431 SS = 7.4 SI = 7.4
GUSCIO 432 SS = 6.3 SI = 6.3
GUSCIO 433 SS = 9.8 SI = 9.8
GUSCIO 434 SS = 9.8 SI = 9.8
GUSCIO 435 SS = 13.5 SI = 13.5
GUSCIO 436 SS = 9.3 SI = 9.3
GUSCIO 437 SS = 9.5 SI = 9.5
GUSCIO 438 SS = 12.5 SI = 12.5
GUSCIO 439 SS = 5.8 SI = 5.8
GUSCIO 440 SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.4 SI = 6.4
GUSCIO 442 SS = 3.9 SI = 3.9
GUSCIO 443 SS = 5.2 SI = 5.2
GUSCIO 444 SS = 3.3 SI = 3.3
GUSCIO 445 SS = 2.0 SI = 2.0
GUSCIO 446 SS = 3.0 SI = 3.0
GUSCIO 447 SS = 2.3 SI = 2.3
GUSCIO 448 SS = 4.4 SI = 4.4
GUSCIO 449 SS = 5.3 SI = 5.3
GUSCIO 450 SS = 5.2 SI = 5.2
GUSCIO 451 SS = 8.8 SI = 8.8
GUSCIO 452 SS = 7.8 SI = 7.8
GUSCIO 453 SS = 10.6 SI = 10.6
GUSCIO 454 SS = 7.6 SI = 7.6
GUSCIO 455 SS = 7.4 SI = 7.4
GUSCIO 456 SS = 8.7 SI = 8.7
GUSCIO 457 SS = 3.1 SI = 3.1
GUSCIO 458 SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.8 SI = 2.8
GUSCIO 461 SS = 2.2 SI = 2.2
GUSCIO 462 SS = 4.4 SI = 4.4
GUSCIO 463 SS = 3.5 SI = 3.5
GUSCIO 464 SS = 2.6 SI = 2.6
GUSCIO 465 SS = 2.9 SI = 2.9
GUSCIO 466 SS = 2.6 SI = 2.6
GUSCIO 467 SS = 2.4 SI = 2.4
GUSCIO 468 SS = 3.1 SI = 3.1
GUSCIO 469 SS = 2.8 SI = 2.8
GUSCIO 470 SS = 2.9 SI = 2.9
GUSCIO 471 SS = 2.4 SI = 2.4
GUSCIO 472 SS = 3.1 SI = 3.1
GUSCIO 473 SS = 3.0 SI = 3.0
GUSCIO 474 SS = 2.9 SI = 2.9
GUSCIO 475 SS = 2.0 SI = 2.0
GUSCIO 476 SS = 2.9 SI = 2.9
GUSCIO 477 SS = 2.1 SI = 2.1
GUSCIO 478 SS = 2.0 SI = 2.0
GUSCIO 479 SS = 0.8 SI = 0.8
GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

GUSCIO 480 SS = 2.0 SI = 2.0
GUSCIO 481 SS = 0.8 SI = 0.8
GUSCIO 482 SS = 4.0 SI = 4.0
GUSCIO 483 SS = 3.2 SI = 3.2
GUSCIO 484 SS = 2.6 SI = 2.6
GUSCIO 485 SS = 3.4 SI = 3.4
GUSCIO 486 SS = 3.0 SI = 3.0
GUSCIO 487 SS = 4.3 SI = 4.3
GUSCIO 488 SS = 1.4 SI = 1.4
GUSCIO 489 SS = 4.6 SI = 4.6
GUSCIO 490 SS = 14.6 SI = 14.6
GUSCIO 491 SS = 13.1 SI = 13.1
GUSCIO 492 SS = 4.0 SI = 4.0
GUSCIO 493 SS = 5.0 SI = 5.0
GUSCIO 494 SS = 1.0 SI = 1.0
GUSCIO 495 SS = 4.0 SI = 4.0
GUSCIO 496 SS = 11.8 SI = 11.8
GUSCIO 497 SS = 7.8 SI = 7.8
GUSCIO 498 SS = 1.8 SI = 1.8
GUSCIO 499 SS = 3.4 SI = 3.4
tensione max = 14,6 guscio = 490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 10 Rara VentoY

COMBINAZIONE

N. 5 CONDIZIONE ANALISI STATICA
1 PnsL_proprio_____ + 1.00
2 Permanente_____ + 1.00
3 Avar_abitazione_____ + 1.00
4 Neve_(c<1000h_1m)_____ + 1.00
5 Vento_Y_____ + 1.00
1) +1.00*c001 +1.00*c002 +1.00*c003 +1.00*c004 +1.00*c005
2) +1.00*c001 +1.00*c002 +1.00*c003 +1.00*c004 -1.00*c005
Unità di misura: SI,SS [daN/cm2]
GUSCIO 415 SS = 2.4 SI = 2.4
SS = 2.0 SI = 2.0
GUSCIO 416 SS = 1.8 SI = 1.8
SS = 1.3 SI = 1.3
GUSCIO 417 SS = 6.4 SI = 6.4
SS = 5.2 SI = 5.2
GUSCIO 418 SS = 6.5 SI = 6.5
SS = 5.4 SI = 5.4
GUSCIO 419 SS = 16.3 SI = 16.3
SS = 12.8 SI = 12.8
GUSCIO 420 SS = 11.8 SI = 11.8
SS = 11.2 SI = 11.2
GUSCIO 421 SS = 12.3 SI = 12.3
SS = 15.0 SI = 15.0
GUSCIO 422 SS = 11.2 SI = 11.2
SS = 11.5 SI = 11.5
GUSCIO 423 SS = 4.7 SI = 4.7
SS = 5.7 SI = 5.7
GUSCIO 424 SS = 5.1 SI = 5.1
SS = 5.8 SI = 5.8
GUSCIO 425 SS = 1.6 SI = 1.6
SS = 2.1 SI = 2.1
GUSCIO 426 SS = 1.1 SI = 1.1
SS = 1.3 SI = 1.3
GUSCIO 427 SS = 4.5 SI = 4.5
SS = 3.9 SI = 3.9
GUSCIO 428 SS = 5.5 SI = 5.5
SS = 4.8 SI = 4.8
GUSCIO 429 SS = 3.2 SI = 3.2
SS = 3.0 SI = 3.0
GUSCIO 430 SS = 7.4 SI = 7.4
SS = 6.3 SI = 6.3
GUSCIO 431 SS = 7.9 SI = 7.9
SS = 6.9 SI = 6.9
GUSCIO 432 SS = 6.7 SI = 6.7
SS = 6.1 SI = 6.1
GUSCIO 433 SS = 10.5 SI = 10.5
SS = 9.2 SI = 9.2
GUSCIO 434 SS = 10.2 SI = 10.2
SS = 9.3 SI = 9.3
GUSCIO 435 SS = 15.1 SI = 15.1

SS = 11.9 SI = 11.9
GUSCIO 436 SS = 9.7 SI = 9.7
SS = 8.9 SI = 8.9
GUSCIO 437 SS = 9.8 SI = 9.8
SS = 9.2 SI = 9.2
GUSCIO 438 SS = 11.9 SI = 11.9
SS = 14.0 SI = 14.0
GUSCIO 439 SS = 6.0 SI = 6.0
SS = 5.6 SI = 5.6
GUSCIO 440 SS = 7.1 SI = 7.1
SS = 7.1 SI = 7.1
GUSCIO 441 SS = 6.3 SI = 6.3
SS = 6.6 SI = 6.6
GUSCIO 442 SS = 3.7 SI = 3.7
SS = 4.6 SI = 4.6
GUSCIO 443 SS = 5.0 SI = 5.0
SS = 5.4 SI = 5.4
GUSCIO 444 SS = 3.1 SI = 3.1
SS = 3.6 SI = 3.6
GUSCIO 445 SS = 2.5 SI = 2.5
SS = 1.5 SI = 1.5
GUSCIO 446 SS = 3.6 SI = 3.6
SS = 2.3 SI = 2.3
GUSCIO 447 SS = 2.6 SI = 2.6
SS = 2.0 SI = 2.0
GUSCIO 448 SS = 5.4 SI = 5.4
SS = 3.5 SI = 3.5
GUSCIO 449 SS = 6.3 SI = 6.3
SS = 4.4 SI = 4.4
GUSCIO 450 SS = 6.0 SI = 6.0
SS = 4.5 SI = 4.5
GUSCIO 451 SS = 11.5 SI = 11.5
SS = 7.2 SI = 7.2
GUSCIO 452 SS = 8.7 SI = 8.7
SS = 7.0 SI = 7.0
GUSCIO 453 SS = 13.2 SI = 13.2
SS = 8.1 SI = 8.1
GUSCIO 454 SS = 7.8 SI = 7.8
SS = 8.3 SI = 8.3
GUSCIO 455 SS = 8.0 SI = 8.0
SS = 6.8 SI = 6.8
GUSCIO 456 SS = 8.3 SI = 8.3
SS = 9.4 SI = 9.4
GUSCIO 457 SS = 2.9 SI = 2.9
SS = 3.4 SI = 3.4
GUSCIO 458 SS = 3.9 SI = 3.9
SS = 4.0 SI = 4.0
GUSCIO 459 SS = 3.6 SI = 3.6
SS = 3.6 SI = 3.6
GUSCIO 460 SS = 2.6 SI = 2.6
SS = 3.1 SI = 3.1
GUSCIO 461 SS = 2.1 SI = 2.1
SS = 2.4 SI = 2.4
GUSCIO 462 SS = 2.6 SI = 2.6
SS = 6.5 SI = 6.5
GUSCIO 463 SS = 2.9 SI = 2.9
SS = 4.3 SI = 4.3
GUSCIO 464 SS = 2.3 SI = 2.3
SS = 3.1 SI = 3.1
GUSCIO 465 SS = 3.7 SI = 3.7
SS = 2.7 SI = 2.7
GUSCIO 466 SS = 1.9 SI = 1.9
SS = 3.8 SI = 3.8
GUSCIO 467 SS = 2.2 SI = 2.2
SS = 2.9 SI = 2.9
GUSCIO 468 SS = 2.3 SI = 2.3
SS = 3.9 SI = 3.9
GUSCIO 469 SS = 4.3 SI = 4.3

		SS =	2.9	SI =	2.9
GUSCIO	470	SS =	2.5	SI =	2.5
		SS =	3.3	SI =	3.3
GUSCIO	471	SS =	2.9	SI =	2.9
		SS =	2.6	SI =	2.6
GUSCIO	472	SS =	2.5	SI =	2.5
		SS =	3.8	SI =	3.8
GUSCIO	473	SS =	2.6	SI =	2.6
		SS =	3.6	SI =	3.6
GUSCIO	474	SS =	2.4	SI =	2.4
		SS =	3.5	SI =	3.5
GUSCIO	475	SS =	1.4	SI =	1.4
		SS =	2.7	SI =	2.7
GUSCIO	476	SS =	2.1	SI =	2.1
		SS =	3.7	SI =	3.7
GUSCIO	477	SS =	1.5	SI =	1.5
		SS =	2.8	SI =	2.8
GUSCIO	478	SS =	1.4	SI =	1.4
		SS =	3.3	SI =	3.3
GUSCIO	479	SS =	0.3	SI =	0.3
		SS =	1.4	SI =	1.4
GUSCIO	480	SS =	1.4	SI =	1.4
		SS =	4.0	SI =	4.0
GUSCIO	481	SS =	0.8	SI =	0.8
		SS =	1.3	SI =	1.3
GUSCIO	482	SS =	4.4	SI =	4.4
		SS =	4.7	SI =	4.7
GUSCIO	483	SS =	2.8	SI =	2.8
		SS =	3.7	SI =	3.7
GUSCIO	484	SS =	4.0	SI =	4.0
		SS =	2.0	SI =	2.0
GUSCIO	485	SS =	2.9	SI =	2.9
		SS =	4.3	SI =	4.3
GUSCIO	486	SS =	2.1	SI =	2.1
		SS =	4.0	SI =	4.0
GUSCIO	487	SS =	7.0	SI =	7.0
		SS =	2.0	SI =	2.0
GUSCIO	488	SS =	1.9	SI =	1.9
		SS =	0.9	SI =	0.9
GUSCIO	489	SS =	5.5	SI =	5.5
		SS =	3.6	SI =	3.6
GUSCIO	490	SS =	17.5	SI =	17.5
		SS =	12.0	SI =	12.0
GUSCIO	491	SS =	13.0	SI =	13.0
		SS =	13.7	SI =	13.7
GUSCIO	492	SS =	4.1	SI =	4.1
		SS =	3.9	SI =	3.9
GUSCIO	493	SS =	2.6	SI =	2.6
		SS =	7.8	SI =	7.8
GUSCIO	494	SS =	1.3	SI =	1.3
		SS =	0.7	SI =	0.7
GUSCIO	495	SS =	5.6	SI =	5.6
		SS =	2.5	SI =	2.5
GUSCIO	496	SS =	16.7	SI =	16.7
		SS =	6.8	SI =	6.8
GUSCIO	497	SS =	4.4	SI =	4.4
		SS =	11.4	SI =	11.4
GUSCIO	498	SS =	1.8	SI =	1.8
		SS =	2.8	SI =	2.8
GUSCIO	499	SS =	2.9	SI =	2.9
		SS =	3.8	SI =	3.8
		tensione max =	17.5	guscio =	490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 11 Frequente Ventox

N. 4 CONDIZIONI ANALISI STATICA

1	Peso_proprio	_____	+	1.00
2	Permanente	_____	+	1.00
3	A'Var_abbattazione	_____	+	0.50
4	Neve_(c<3000m_s1m)	_____	+	0.20

1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004
Unità di misura: SI,SS [daN/cm2]

GUSCIO 415 SS = 1.4 SI = 1.4

COMBINAZIONE

GUSCIO	416	SS =	1.0	SI =	1.0
GUSCIO	417	SS =	3.7	SI =	3.7
GUSCIO	418	SS =	3.8	SI =	3.8
GUSCIO	419	SS =	9.0	SI =	9.0
GUSCIO	420	SS =	7.2	SI =	7.2
GUSCIO	421	SS =	8.6	SI =	8.6
GUSCIO	422	SS =	7.2	SI =	7.2
GUSCIO	423	SS =	3.4	SI =	3.4
GUSCIO	424	SS =	3.5	SI =	3.5
GUSCIO	425	SS =	1.2	SI =	1.2
GUSCIO	426	SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
GUSCIO	429	SS =	2.0	SI =	2.0
GUSCIO	430	SS =	4.4	SI =	4.4
GUSCIO	431	SS =	4.7	SI =	4.7
GUSCIO	432	SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.3	SI =	6.3
GUSCIO	434	SS =	6.3	SI =	6.3
GUSCIO	435	SS =	8.6	SI =	8.6
GUSCIO	436	SS =	6.0	SI =	6.0
GUSCIO	437	SS =	6.1	SI =	6.1
GUSCIO	438	SS =	8.1	SI =	8.1
GUSCIO	439	SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
GUSCIO	442	SS =	2.6	SI =	2.6
GUSCIO	443	SS =	3.3	SI =	3.3
GUSCIO	444	SS =	2.1	SI =	2.1
GUSCIO	445	SS =	1.4	SI =	1.4
GUSCIO	446	SS =	2.0	SI =	2.0
GUSCIO	447	SS =	1.4	SI =	1.4
GUSCIO	448	SS =	3.0	SI =	3.0
GUSCIO	449	SS =	3.6	SI =	3.6
GUSCIO	450	SS =	3.3	SI =	3.3
GUSCIO	451	SS =	5.8	SI =	5.8
GUSCIO	452	SS =	5.2	SI =	5.2
GUSCIO	453	SS =	6.6	SI =	6.6
GUSCIO	454	SS =	5.1	SI =	5.1
GUSCIO	455	SS =	4.9	SI =	4.9
GUSCIO	456	SS =	5.7	SI =	5.7
GUSCIO	457	SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
GUSCIO	460	SS =	2.1	SI =	2.1
GUSCIO	461	SS =	1.6	SI =	1.6
GUSCIO	462	SS =	3.0	SI =	3.0
GUSCIO	463	SS =	2.6	SI =	2.6
GUSCIO	464	SS =	1.9	SI =	1.9
GUSCIO	465	SS =	2.1	SI =	2.1
GUSCIO	466	SS =	1.9	SI =	1.9
GUSCIO	467	SS =	1.8	SI =	1.8
GUSCIO	468	SS =	2.1	SI =	2.1
GUSCIO	469	SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.1	SI =	2.1
GUSCIO	471	SS =	1.8	SI =	1.8
GUSCIO	472	SS =	2.3	SI =	2.3
GUSCIO	473	SS =	2.2	SI =	2.2
GUSCIO	474	SS =	2.2	SI =	2.2
GUSCIO	475	SS =	1.4	SI =	1.4
GUSCIO	476	SS =	2.1	SI =	2.1
GUSCIO	477	SS =	1.6	SI =	1.6
GUSCIO	478	SS =	1.5	SI =	1.5
GUSCIO	479	SS =	0.6	SI =	0.6
GUSCIO	480	SS =	1.6	SI =	1.6
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.3	SI =	2.3

GUSCIO	484	SS =	2.1	SI =	2.1
GUSCIO	485	SS =	2.5	SI =	2.5
GUSCIO	486	SS =	2.2	SI =	2.2
GUSCIO	487	SS =	3.3	SI =	3.3
GUSCIO	488	SS =	0.8	SI =	0.8
GUSCIO	489	SS =	2.8	SI =	2.8
GUSCIO	490	SS =	9.1	SI =	9.1
GUSCIO	491	SS =	8.3	SI =	8.3
GUSCIO	492	SS =	2.4	SI =	2.4
GUSCIO	493	SS =	3.3	SI =	3.3
GUSCIO	494	SS =	0.6	SI =	0.6
GUSCIO	495	SS =	2.6	SI =	2.6
GUSCIO	496	SS =	7.7	SI =	7.7
GUSCIO	497	SS =	5.5	SI =	5.5
GUSCIO	498	SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.5	SI =	2.5
		tensione max =	9.1	guscio =	490

SOLLECITAZIONE GUSCI RETTANGOLARI
CASO DI CARICO : 12 Frequente Ventox

N. 4 CONDIZIONI ANALISI STATICA

1	Peso_proprio	_____	+	1.00
2	Permanente	_____	+	1.00
3	A'Var_abbattazione	_____	+	0.50
4	Neve_(c<3000m_s1m)	_____	+	0.20

1) +1.00*c001 +1.00*c002 +0.50*c003 +0.20*c004
Unità di misura: SI,SS [daN/cm2]

GUSCIO	415	SS =	1.4	SI =	1.4
GUSCIO	416	SS =	1.0	SI =	1.0
GUSCIO	417	SS =	3.7	SI =	3.7
GUSCIO	418	SS =	3.8	SI =	3.8
GUSCIO	419	SS =	9.0	SI =	9.0
GUSCIO	420	SS =	7.2	SI =	7.2
GUSCIO	421	SS =	8.6	SI =	8.6
GUSCIO	422	SS =	7.2	SI =	7.2
GUSCIO	423	SS =	3.4	SI =	3.4
GUSCIO	424	SS =	3.5	SI =	3.5
GUSCIO	425	SS =	1.2	SI =	1.2
GUSCIO	426	SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
GUSCIO	429	SS =	2.0	SI =	2.0
GUSCIO	430	SS =	4.4	SI =	4.4
GUSCIO	431	SS =	4.7	SI =	4.7
GUSCIO	432	SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.3	SI =	6.3
GUSCIO	434	SS =	6.3	SI =	6.3
GUSCIO	435	SS =	8.6	SI =	8.6
GUSCIO	436	SS =	6.0	SI =	6.0
GUSCIO	437	SS =	6.1	SI =	6.1
GUSCIO	438	SS =	8.1	SI =	8.1
GUSCIO	439	SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
GUSCIO	442	SS =	2.6	SI =	2.6
GUSCIO	443	SS =	3.3	SI =	3.3
GUSCIO	444	SS =	2.1	SI =	2.1
GUSCIO	445	SS =	1.4	SI =	1.4
GUSCIO	446	SS =	2.0	SI =	2.0
GUSCIO	447	SS =	1.4	SI =	1.4
GUSCIO	448	SS =	3.0	SI =	3.0
GUSCIO	449	SS =	3.6	SI =	3.6
GUSCIO	450	SS =	3.3	SI =	3.3
GUSCIO	451	SS =	5.8	SI =	5.8
GUSCIO	452	SS =	5.2	SI =	5.2
GUSCIO	453	SS =	6.6	SI =	6.6
GUSCIO	454	SS =	5.1	SI =	5.1
GUSCIO	455	SS =	4.9	SI =	4.9
GUSCIO	456	SS =	5.7	SI =	5.7
GUSCIO	457	SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
GUSCIO	460	SS =	2.1	SI =	2.1

COMBINAZIONE

GUSCIO	461	SS =	1.6	SI =	1.6
GUSCIO	462	SS =	3.0	SI =	3.0
GUSCIO	463	SS =	2.6	SI =	2.6
GUSCIO	464	SS =	1.9	SI =	1.9
GUSCIO	465	SS =	2.1	SI =	2.1
GUSCIO	466	SS =	1.9	SI =	1.9
GUSCIO	467	SS =	1.8	SI =	1.8
GUSCIO	468	SS =	2.1	SI =	2.1
GUSCIO	469	SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.1	SI =	2.1
GUSCIO	471	SS =	1.8	SI =	1.8
GUSCIO	472	SS =	2.3	SI =	2.3
GUSCIO	473	SS =	2.2	SI =	2.2
GUSCIO	474	SS =	2.2	SI =	2.2
GUSCIO	475	SS =	1.4	SI =	1.4
GUSCIO	476	SS =	2.1	SI =	2.1
GUSCIO	477	SS =	1.6	SI =	1.6
GUSCIO	478	SS =	1.5	SI =	1.5
GUSCIO	479	SS =	0.6	SI =	0.6
GUSCIO	480	SS =	1.6	SI =	1.6
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.3	SI =	2.3
GUSCIO	484	SS =	2.1	SI =	2.1
GUSCIO	485	SS =	2.5	SI =	2.5
GUSCIO	486	SS =	2.2	SI =	2.2
GUSCIO	487	SS =	3.3	SI =	3.3
GUSCIO	488	SS =	0.8	SI =	0.8
GUSCIO	489	SS =	2.8	SI =	2.8
GUSCIO	490	SS =	9.1	SI =	9.1
GUSCIO	491	SS =	8.3	SI =	8.3
GUSCIO	492	SS =	2.4	SI =	2.4
GUSCIO	493	SS =	3.3	SI =	3.3
GUSCIO	494	SS =	0.6	SI =	0.6
GUSCIO	495	SS =	2.6	SI =	2.6
GUSCIO	496	SS =	7.7	SI =	7.7
GUSCIO	497	SS =	5.5	SI =	5.5
GUSCIO	498	SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.5	SI =	2.5
		tensione max =	9.1	guscio =	490

		SS =	1.3	SI =	1.3
GUSCIO	426	SS =	0.8	SI =	0.8
		SS =	0.8	SI =	0.8
GUSCIO	427	SS =	2.8	SI =	2.8
		SS =	2.7	SI =	2.7
GUSCIO	428	SS =	3.3	SI =	3.3
		SS =	3.2	SI =	3.2
GUSCIO	429	SS =	2.0	SI =	2.0
		SS =	1.9	SI =	1.9
GUSCIO	430	SS =	4.5	SI =	4.5
		SS =	4.3	SI =	4.3
GUSCIO	431	SS =	4.8	SI =	4.8
		SS =	4.6	SI =	4.6
GUSCIO	432	SS =	4.1	SI =	4.1
		SS =	4.0	SI =	4.0
GUSCIO	433	SS =	6.4	SI =	6.4
		SS =	6.2	SI =	6.2
GUSCIO	434	SS =	6.4	SI =	6.4
		SS =	6.2	SI =	6.2
GUSCIO	435	SS =	8.9	SI =	8.9
		SS =	8.3	SI =	8.3
GUSCIO	436	SS =	6.1	SI =	6.1
		SS =	5.9	SI =	5.9
GUSCIO	437	SS =	6.1	SI =	6.1
		SS =	6.0	SI =	6.0
GUSCIO	438	SS =	7.9	SI =	7.9
		SS =	8.4	SI =	8.4
GUSCIO	439	SS =	3.8	SI =	3.8
		SS =	3.7	SI =	3.7
GUSCIO	440	SS =	4.5	SI =	4.5
		SS =	4.6	SI =	4.6
GUSCIO	441	SS =	4.1	SI =	4.1
		SS =	4.2	SI =	4.2
GUSCIO	442	SS =	2.6	SI =	2.6
		SS =	2.7	SI =	2.7
GUSCIO	443	SS =	3.3	SI =	3.3
		SS =	3.4	SI =	3.4
GUSCIO	444	SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	445	SS =	1.5	SI =	1.5
		SS =	1.3	SI =	1.3
GUSCIO	446	SS =	2.1	SI =	2.1
		SS =	1.9	SI =	1.9
GUSCIO	447	SS =	1.4	SI =	1.4
		SS =	1.3	SI =	1.3
GUSCIO	448	SS =	3.1	SI =	3.1
		SS =	2.8	SI =	2.8
GUSCIO	449	SS =	3.8	SI =	3.8
		SS =	3.4	SI =	3.4
GUSCIO	450	SS =	3.5	SI =	3.5
		SS =	3.1	SI =	3.1
GUSCIO	451	SS =	6.3	SI =	6.3
		SS =	5.4	SI =	5.4
GUSCIO	452	SS =	5.3	SI =	5.3
		SS =	5.0	SI =	5.0
GUSCIO	453	SS =	7.1	SI =	7.1
		SS =	6.1	SI =	6.1
GUSCIO	454	SS =	5.1	SI =	5.1
		SS =	5.1	SI =	5.1
GUSCIO	455	SS =	5.1	SI =	5.1
		SS =	4.8	SI =	4.8
GUSCIO	456	SS =	5.5	SI =	5.5
		SS =	5.8	SI =	5.8
GUSCIO	457	SS =	2.0	SI =	2.0
		SS =	2.1	SI =	2.1
GUSCIO	458	SS =	2.7	SI =	2.7
		SS =	2.7	SI =	2.7
GUSCIO	459	SS =	2.3	SI =	2.3
		SS =	2.3	SI =	2.3

GUSCIO	460	SS =	2.1	SI =	2.1
		SS =	2.2	SI =	2.2
GUSCIO	461	SS =	1.5	SI =	1.5
		SS =	1.6	SI =	1.6
GUSCIO	462	SS =	2.6	SI =	2.6
		SS =	3.4	SI =	3.4
GUSCIO	463	SS =	2.4	SI =	2.4
		SS =	2.7	SI =	2.7
GUSCIO	464	SS =	1.8	SI =	1.8
		SS =	2.0	SI =	2.0
GUSCIO	465	SS =	2.3	SI =	2.3
		SS =	2.0	SI =	2.0
GUSCIO	466	SS =	1.7	SI =	1.7
		SS =	2.1	SI =	2.1
GUSCIO	467	SS =	1.7	SI =	1.7
		SS =	1.9	SI =	1.9
GUSCIO	468	SS =	1.9	SI =	1.9
		SS =	2.3	SI =	2.3
GUSCIO	469	SS =	2.4	SI =	2.4
		SS =	2.1	SI =	2.1
GUSCIO	470	SS =	2.0	SI =	2.0
		SS =	2.2	SI =	2.2
GUSCIO	471	SS =	1.8	SI =	1.8
		SS =	1.9	SI =	1.9
GUSCIO	472	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
GUSCIO	473	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
GUSCIO	474	SS =	2.1	SI =	2.1
		SS =	2.3	SI =	2.3
GUSCIO	475	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
GUSCIO	476	SS =	2.0	SI =	2.0
		SS =	2.3	SI =	2.3
GUSCIO	477	SS =	1.5	SI =	1.5
		SS =	1.7	SI =	1.7
GUSCIO	478	SS =	1.3	SI =	1.3
		SS =	1.6	SI =	1.6
GUSCIO	479	SS =	0.4	SI =	0.4
		SS =	0.7	SI =	0.7
GUSCIO	480	SS =	1.2	SI =	1.2
		SS =	1.9	SI =	1.9
GUSCIO	481	SS =	0.6	SI =	0.6
		SS =	0.7	SI =	0.7
GUSCIO	482	SS =	2.7	SI =	2.7
		SS =	2.8	SI =	2.8
GUSCIO	483	SS =	2.2	SI =	2.2
		SS =	2.4	SI =	2.4
GUSCIO	484	SS =	2.3	SI =	2.3
		SS =	1.8	SI =	1.8
GUSCIO	485	SS =	2.4	SI =	2.4
		SS =	2.7	SI =	2.7
GUSCIO	486	SS =	2.0	SI =	2.0
		SS =	2.4	SI =	2.4
GUSCIO	487	SS =	3.9	SI =	3.9
		SS =	2.8	SI =	2.8
GUSCIO	488	SS =	0.9	SI =	0.9
		SS =	0.7	SI =	0.7
GUSCIO	489	SS =	3.0	SI =	3.0
		SS =	2.6	SI =	2.6
GUSCIO	490	SS =	9.7	SI =	9.7
		SS =	8.6	SI =	8.6
GUSCIO	491	SS =	8.2	SI =	8.2
		SS =	8.4	SI =	8.4
GUSCIO	492	SS =	2.4	SI =	2.4
		SS =	2.4	SI =	2.4
GUSCIO	493	SS =	2.7	SI =	2.7
		SS =	3.9	SI =	3.9

GUSCIO	494	SS =	0.7	SI =	0.7
		SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.9	SI =	2.9
		SS =	2.3	SI =	2.3
GUSCIO	496	SS =	8.7	SI =	8.7
		SS =	6.7	SI =	6.7
GUSCIO	497	SS =	4.8	SI =	4.8
		SS =	6.2	SI =	6.2
GUSCIO	498	SS =	1.3	SI =	1.3
		SS =	1.3	SI =	1.3
GUSCIO	499	SS =	2.4	SI =	2.4
		SS =	2.6	SI =	2.6
tensione max =		9.7	guscio =	490	

SOLLECITAZIONE GUSCI RETTANGOLARI
 CASO DI CARICO : 14 Quasi Perm
 N. 3 CONDIZIONE ANALISI STATICA
 1 Peso proprio + 1.00
 2 Permanente + 1.00
 3 Azioni abilitazione + 0.30
 1) +1.00*0.01 +1.00*0.02 +0.30*0.03
 unità di misura: SI,SS [dav/cm2]

GUSCIO	415	SS =	1.1	SI =	1.1
GUSCIO	416	SS =	0.8	SI =	0.8
GUSCIO	417	SS =	3.0	SI =	3.0
GUSCIO	418	SS =	3.0	SI =	3.0
GUSCIO	419	SS =	7.1	SI =	7.1
GUSCIO	420	SS =	5.8	SI =	5.8
GUSCIO	421	SS =	6.9	SI =	6.9
GUSCIO	422	SS =	5.7	SI =	5.7
GUSCIO	423	SS =	2.7	SI =	2.7
GUSCIO	424	SS =	2.8	SI =	2.8
GUSCIO	425	SS =	1.0	SI =	1.0
GUSCIO	426	SS =	0.6	SI =	0.6
GUSCIO	427	SS =	2.2	SI =	2.2
GUSCIO	428	SS =	2.6	SI =	2.6
GUSCIO	429	SS =	1.6	SI =	1.6
GUSCIO	430	SS =	3.6	SI =	3.6
GUSCIO	431	SS =	3.8	SI =	3.8
GUSCIO	432	SS =	3.2	SI =	3.2
GUSCIO	433	SS =	5.1	SI =	5.1
GUSCIO	434	SS =	5.1	SI =	5.1
GUSCIO	435	SS =	6.9	SI =	6.9
GUSCIO	436	SS =	4.8	SI =	4.8
GUSCIO	437	SS =	4.9	SI =	4.9
GUSCIO	438	SS =	6.6	SI =	6.6
GUSCIO	439	SS =	3.0	SI =	3.0
GUSCIO	440	SS =	3.7	SI =	3.7
GUSCIO	441	SS =	3.3	SI =	3.3
GUSCIO	442	SS =	2.2	SI =	2.2
GUSCIO	443	SS =	2.7	SI =	2.7
GUSCIO	444	SS =	1.7	SI =	1.7
GUSCIO	445	SS =	1.2	SI =	1.2
GUSCIO	446	SS =	1.7	SI =	1.7
GUSCIO	447	SS =	1.0	SI =	1.0
GUSCIO	448	SS =	2.4	SI =	2.4
GUSCIO	449	SS =	2.9	SI =	2.9
GUSCIO	450	SS =	2.6	SI =	2.6
GUSCIO	451	SS =	4.8	SI =	4.8
GUSCIO	452	SS =	4.3	SI =	4.3
GUSCIO	453	SS =	5.2	SI =	5.2
GUSCIO	454	SS =	4.2	SI =	4.2
GUSCIO	455	SS =	4.1	SI =	4.1
GUSCIO	456	SS =	4.6	SI =	4.6
GUSCIO	457	SS =	1.7	SI =	1.7
GUSCIO	458	SS =	2.2	SI =	2.2
GUSCIO	459	SS =	1.8	SI =	1.8
GUSCIO	460	SS =	1.9	SI =	1.9
GUSCIO	461	SS =	1.4	SI =	1.4
GUSCIO	462	SS =	2.5	SI =	2.5
GUSCIO	463	SS =	2.3	SI =	2.3
GUSCIO	464	SS =	1.7	SI =	1.7

COMBINAZIONE

GUSCIO	465	SS =	1.9	SI =	1.9
GUSCIO	466	SS =	1.6	SI =	1.6
GUSCIO	467	SS =	1.6	SI =	1.6
GUSCIO	468	SS =	1.8	SI =	1.8
GUSCIO	469	SS =	1.9	SI =	1.9
GUSCIO	470	SS =	1.9	SI =	1.9
GUSCIO	471	SS =	1.6	SI =	1.6
GUSCIO	472	SS =	2.0	SI =	2.0
GUSCIO	473	SS =	1.9	SI =	1.9
GUSCIO	474	SS =	1.9	SI =	1.9
GUSCIO	475	SS =	1.2	SI =	1.2
GUSCIO	476	SS =	1.9	SI =	1.9
GUSCIO	477	SS =	1.4	SI =	1.4
GUSCIO	478	SS =	1.3	SI =	1.3
GUSCIO	479	SS =	0.5	SI =	0.5
GUSCIO	480	SS =	1.4	SI =	1.4
GUSCIO	481	SS =	0.6	SI =	0.6
GUSCIO	482	SS =	2.4	SI =	2.4
GUSCIO	483	SS =	1.9	SI =	1.9
GUSCIO	484	SS =	1.9	SI =	1.9
GUSCIO	485	SS =	2.2	SI =	2.2
GUSCIO	486	SS =	1.9	SI =	1.9
GUSCIO	487	SS =	2.9	SI =	2.9
GUSCIO	488	SS =	0.6	SI =	0.6
GUSCIO	489	SS =	2.2	SI =	2.2
GUSCIO	490	SS =	7.3	SI =	7.3
GUSCIO	491	SS =	6.6	SI =	6.6
GUSCIO	492	SS =	1.9	SI =	1.9
GUSCIO	493	SS =	2.7	SI =	2.7
GUSCIO	494	SS =	0.5	SI =	0.5
GUSCIO	495	SS =	2.1	SI =	2.1
GUSCIO	496	SS =	6.3	SI =	6.3
GUSCIO	497	SS =	4.7	SI =	4.7
GUSCIO	498	SS =	1.2	SI =	1.2
GUSCIO	499	SS =	2.2	SI =	2.2
tensione max =		7.3	guscio =	490	

VERIFICA GUSCI IN C.A.:

MACROSCOPICO FONDAZ

VERIFICA ARMATURE EFFETTIVE (EFFETTO MEMBRANA + PIASTRA)

CASI DI CARICO:

Nome Descrizione
1 su VENT0
2 su VENT0
3 su VENT0
4 su su SIEWM
5 su su SIEWM
6 su su SIEWM
7 su su SIEWM

DATI:

tensione di snervamento acciaio (fyk): 4500 daN/cm2
coefficiente sicurezza acciaio: 1.15
deformazione ultima ultls: 1.97 per mille
deformazione ultima cls: 3.5 per mille
rapporto rottura/snervamento (k): 1.5
resistenza cilindrica cls (fck): 249 daN/cm2
coefficiente sicurezza cls: 1.5
coefficiente riduttivo (alfa): 0.85
copriferro inferiore (asse amatura): 3 cm
copriferro superiore (asse amatura): 3 cm
moltiplicatore sollecitazioni: 1

LEGENDA:

spess = spessore guscio, verfica effettuata su sezione Bm, con B-I cm e H="spess" cm
AF = area disposta al lembo teso, in cm2 al metro
Afc = area disposta al lembo compresso, in cm2 al metro
Mem = momento flettente (daN/cm)
Nor = sforzo normale [daN]
ecc = deformazione cls [per mille]
wfk = deformazione acciaio [per mille]

L'armatura è sufficiente se le deformazioni dei materiali sono ovunque minori delle corrispondenti deformazioni ultime.

INFERIORE ORIZZONTALE										INFERIORE VERTICALE									
GUSCI	spess	AF	Afc	Mem	Nor	ecc	of	wfk	spess	AF	Afc	Mem	Nor	ecc	of	wfk	spess	AF	Afc
415	35	4.21	4.21	1344	0	0.10	0.51	4.16	4.36	447	0	0	0	0.04	0.17				
416	35	4.21	4.21	497	0	0.04	0.19	4.16	4.36	278	0	0	0	0.02	0.11				
417	35	4.21	4.21	1815	0	0.14	0.68	4.16	4.36	1760	0	0	0	0.14	0.66				
418	35	4.21	4.21	511	0	0.04	0.19	4.16	4.36	1621	0	0	0	0.13	0.62				
419	35	4.21	4.21	2157	0	0.17	0.83	4.16	4.36	1465	0	0	0	0.17	0.83				
420	35	4.21	4.21	431	0	0.03	0.16	4.16	4.36	4386	0	0	0	0.36	1.75				
421	35	4.21	4.21	2447	0	0.17	0.85	4.16	4.36	4618	0	0	0	0.36	1.76				
422	35	4.21	4.21	347	0	0.03	0.13	4.16	4.36	4813	0	0	0	0.38	1.83				
423	35	4.21	4.21	1876	0	0.15	0.71	4.16	4.36	1819	0	0	0	0.14	0.69				
424	35	4.21	4.21	1815	0	0.03	0.05	4.16	4.36	1592	0	0	0	0.02	0.12				
425	35	4.21	4.21	1239	0	0.10	0.47	4.16	4.36	489	0	0	0	0.04	0.19				
426	35	4.21	4.21	451	0	0.04	0.17	4.16	4.36	307	0	0	0	0.02	0.12				
427	35	4.21	4.21	138	0	0.03	0.05	4.16	4.36	194	0	0	0	0.02	0.12				
428	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	319	0	0	0	0.02	0.12				
429	35	4.21	4.21	136	0	0.12	0.56	4.16	4.36	1761	0	0	0	0.14	0.67				
430	35	4.21	4.21	93	0	0.01	0.03	4.16	4.36	1073	0	0	0	0.08	0.41				
431	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	1157	0	0	0	0.09	0.44				
432	35	4.21	4.21	1530	0	0.12	0.58	4.16	4.36	2970	0	0	0	0.13	0.65				
433	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	2970	0	0	0	0.23	1.13				
434	35	4.21	4.21	303	0	0.02	0.09	4.16	4.36	618	0	0	0	0.05	0.24				
435	35	4.21	4.21	1527	0	0.12	0.57	4.16	4.36	3766	0	0	0	0.29	1.43				
436	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	324	0	0	0	0.05	0.24				
437	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	2377	0	0	0	0.19	0.90				
438	35	4.21	4.21	1307	0	0.12	0.57	4.16	4.36	3870	0	0	0	0.30	1.47				
439	35	4.21	4.21	0	0	0.02	0.11	4.16	4.36	91	0	0	0	0.01	0.03				
440	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	1074	0	0	0	0.08	0.41				
441	35	4.21	4.21	1276	0	0.10	0.48	4.16	4.36	617	0	0	0	0.05	0.23				
442	35	4.21	4.21	303	0	0.02	0.11	4.16	4.36	91	0	0	0	0.01	0.03				
443	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	321	0	0	0	0.03	0.12				
444	35	4.21	4.21	0	0	0.02	0.09	4.16	4.36	617	0	0	0	0.05	0.24				
445	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
446	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
447	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
448	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
449	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
450	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
451	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
452	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
453	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
454	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
455	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
456	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
457	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
458	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
459	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
460	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
461	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
462	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
463	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
464	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
465	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
466	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
467	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
468	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
469	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
470	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
471	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
472	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
473	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
474	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
475	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
476	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
477	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
478	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
479	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
480	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
481	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
482	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
483	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
484	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
485	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
486	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
487	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
488	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
489	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
490	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
491	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
492	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
493	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
494	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
495	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
496	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
497	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.02	0.12				
498	35	4.21	4.21	0	0	0.00	0.00	4.16	4.36	299	0	0	0	0.0					

340	30	2.61	2.61	330.	1.	0.03	0.25	2.61	2.61	1240.	-3.	-0.16	0.87	278	30	2.61	6.81	18.	1.	0.00	0.02	2.61	6.61	0.	-1.	0.00	0.00	102.	0.014	433	0.	7.69	630.	0.087	233	0.	4.14	339.	0.047	135	0.	2.40	281	[6.90	2.69]	1096	0.	13.06	640.	0.036]	588	0.	7.01	343.	0.019]	245	0.	2.91							
341	30	2.61	2.61	89.	1.	0.00	0.08	2.61	2.61	975.	-2.	-0.13	0.69	279	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	103	0.0271	434	0.	0.00	0.00	0.00	135	0.	1.24	278	[6.90	2.69]	1099	1.	16.66	820.	0.046]	759	0.	9.04	445.	0.025]	476	0.	5.67												
342	30	2.61	2.61	352	1.	0.00	0.00	2.61	2.61	877.	-3.	-0.00	0.03	280	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	104	0.0001	435	0.	0.00	0.00	0.00	136	0.	1.24	278	[6.90	2.69]	1100	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78												
343	30	2.61	2.61	1526.	-1.	-0.20	0.19	2.61	2.61	0.	3.	0.00	0.03	281	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	105	0.0001	436	0.	0.00	0.00	0.00	137	0.	0.12	10.	0.0031	11	0.	0.00	0.00	0.00	138	[6.90	2.69]	1101	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
344	30	2.61	2.61	2830.	-1.	-0.23	0.29	2.61	2.61	0.	3.	0.00	0.03	282	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	106	0.0001	437	0.	0.00	0.00	0.00	138	0.	0.00	0.00	0.00	139	0.	0.00	0.00	0.00	139	0.	0.00	0.00	0.00	140	[6.90	2.69]	1102	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78
345	30	2.61	2.61	1139.	-1.	-0.16	0.89	2.61	2.61	0.	8.	0.00	0.07	283	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	107	0.0001	438	0.	0.00	0.00	0.00	139	0.	0.00	0.00	0.00	140	0.	0.00	0.00	0.00	141	[6.90	2.69]	1103	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
346	30	2.61	2.61	1252.	-1.	-0.16	0.89	2.61	2.61	0.	8.	0.00	0.07	284	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	108	0.0001	439	0.	0.00	0.00	0.00	140	0.	0.00	0.00	0.00	141	0.	0.00	0.00	0.00	142	[6.90	2.69]	1104	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
347	30	2.61	2.61	401.	-2.	-0.16	0.87	2.61	2.61	604.	-12.	-0.08	0.41	285	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	109	0.0001	440	0.	0.00	0.00	0.00	141	0.	0.00	0.00	0.00	142	0.	0.00	0.00	0.00	143	[6.90	2.69]	1105	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
348	30	2.61	2.61	968.	-1.	-0.12	0.69	2.61	2.61	0.	8.	0.00	0.07	286	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	110	0.0001	441	0.	0.00	0.00	0.00	142	0.	0.00	0.00	0.00	143	0.	0.00	0.00	0.00	144	[6.90	2.69]	1106	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
349	30	2.61	2.61	441.	4.	0.02	0.35	2.61	2.61	0.	5.	0.00	0.05	287	30	2.69	6.90	17.	1.	0.00	0.02	2.66	6.65	0.	-1.	0.00	0.01	111	0.0001	442	0.	0.00	0.00	0.00	143	0.	0.00	0.00	0.00	144	0.	0.00	0.00	0.00	145	[6.90	2.69]	1107	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
350	30	2.61	2.61	262.	6.	0.02	0.29	2.61	2.61	0.	5.	0.00	0.05	288	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	112	0.0001	443	0.	0.00	0.00	0.00	144	0.	0.00	0.00	0.00	145	0.	0.00	0.00	0.00	146	[6.90	2.69]	1108	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
351	30	2.61	2.61	293.	3.	0.01	0.24	2.61	2.61	0.	3.	0.00	0.03	289	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	113	0.0001	444	0.	0.00	0.00	0.00	145	0.	0.00	0.00	0.00	146	0.	0.00	0.00	0.00	147	[6.90	2.69]	1109	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
352	30	2.61	2.61	1139.	-2.	-0.16	0.89	2.61	2.61	0.	8.	0.00	0.07	290	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	114	0.0001	445	0.	0.00	0.00	0.00	146	0.	0.00	0.00	0.00	147	0.	0.00	0.00	0.00	148	[6.90	2.69]	1110	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
353	30	2.61	2.61	650.	3.	0.06	0.49	2.61	2.61	0.	2.	0.00	0.02	291	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	115	0.0001	446	0.	0.00	0.00	0.00	147	0.	0.00	0.00	0.00	148	0.	0.00	0.00	0.00	149	[6.90	2.69]	1111	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
354	30	2.61	2.61	476.	16.	0.01	0.42	2.61	2.61	1732.	8.	0.20	1.31	292	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	116	0.0001	447	0.	0.00	0.00	0.00	148	0.	0.00	0.00	0.00	149	0.	0.00	0.00	0.00	150	[6.90	2.69]	1112	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
355	30	2.61	2.61	376.	16.	0.01	0.42	2.61	2.61	1732.	8.	0.20	1.31	293	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	117	0.0001	448	0.	0.00	0.00	0.00	149	0.	0.00	0.00	0.00	150	0.	0.00	0.00	0.00	151	[6.90	2.69]	1113	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
356	30	2.61	2.61	371.	10.	0.05	0.27	2.61	2.61	911.	7.	0.08	0.71	294	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	118	0.0001	449	0.	0.00	0.00	0.00	150	0.	0.00	0.00	0.00	151	0.	0.00	0.00	0.00	152	[6.90	2.69]	1114	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
357	30	2.61	2.61	296.	6.	0.00	0.20	2.61	2.61	565.	-8.	-0.07	0.39	295	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	119	0.0001	450	0.	0.00	0.00	0.00	151	0.	0.00	0.00	0.00	152	0.	0.00	0.00	0.00	153	[6.90	2.69]	1115	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
358	30	2.61	2.61	378.	22.	0.00	0.47	2.61	2.61	137.	20.	0.00	0.39	296	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	120	0.0001	451	0.	0.00	0.00	0.00	152	0.	0.00	0.00	0.00	153	0.	0.00	0.00	0.00	154	[6.90	2.69]	1116	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
359	30	2.61	2.61	131.	0.	0.00	0.04	2.61	2.61	1526.	-4.	-0.11	0.46	297	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	121	0.0001	452	0.	0.00	0.00	0.00	153	0.	0.00	0.00	0.00	154	0.	0.00	0.00	0.00	155	[6.90	2.69]	1117	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
360	30	2.61	2.61	146.	13.	0.00	0.22	2.61	2.61	441.	-7.	-0.06	0.32	298	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	122	0.0001	453	0.	0.00	0.00	0.00	154	0.	0.00	0.00	0.00	155	0.	0.00	0.00	0.00	156	[6.90	2.69]	1118	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
361	30	2.61	2.61	382.	14.	0.00	0.21	2.61	2.61	179.	15.	0.00	0.29	299	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	123	0.0001	454	0.	0.00	0.00	0.00	155	0.	0.00	0.00	0.00	156	0.	0.00	0.00	0.00	157	[6.90	2.69]	1119	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
362	30	2.61	2.61	246.	4.	0.00	0.21	2.61	2.61	187.	7.	0.16	1.13	300	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	124	0.0001	455	0.	0.00	0.00	0.00	156	0.	0.00	0.00	0.00	157	0.	0.00	0.00	0.00	158	[6.90	2.69]	1120	0.	12.11	593.	0.033]	547	0.	6.52	319.	0.018]	233	0.	2.78					
363	30	2.61	2.61	265.	-1.	-0.03	0.19	2.61	2.61	823.	6.	0.07	0.64	301	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	125	0.0001	456	0.	0.00	0.00	0.00	157	0.	0.00	0.00	0.00	158	0.	0.00	0.00	0.00	159	[6.90	2.69]	1121	0.	16.56	515.	0.046]	740	0.	8.81	434.	0.024]	392	0.	4.67					
364	30	2.61	2.61	265.	7.	0.00	0.09	2.61	2.61	1200.	6.	0.12	0.90	302	30	2.69	6.90	0.	0.	0.00	0.00	2.66	6.65	0.	-1.	0.00	0.01	126	0.0001	457	0.	0.00	0.00	0.00																															

[illegible]

107/136

[illegible]

TAGLIO Z:										1 C 13-1 -2791.1 -37501.2 -61264.1 -6.4 81.1 SI					
Asta	Caso	Ned	Ved ger.	Ved	Vrsd	Vrcl	Asw	% rctg VE							
1	7- 2	254.4		814.1	52756.6	52756.6	53413.1	1.51 11.1							
1 C	7- 2	254.4		814.1	52756.6	52756.6	53536.5	1.51 11.1	2.35 SI						
1 S	7- 2	254.4		814.1	52756.6	52756.6	53300.1	1.51 11.1	2.35 SI	1 C 13-1 -2416.1 -29240.2 -31515.2 -3.8 31.7 SI					
										1 S 13-1 -2041.1 -20979.2 -1766.4 -1.6 1 SI					
QUANT. PERMANENTI:															
Asta	Caso	Ned		Meyd	Mzsd	oc	cc	cf							
1	14-1	-2546.8		-26959.2	-5642.5	-5.2	-5.2	63.6 SI							
1 C	14-1	-2546.8		-16649.2	-28796.9	-2.8	-18.1	63.6 SI							
1 S	14-1	-1796.8		-8339.3	-1151.3	-1.1	-4.6	SI							

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:

Asta	Caso		NEd		MEyd		MEzd		oc		of		VE
1 I	10- 1		-3521.5		-63522.6		39583.6		-6.5		68.2		SI
1 C	10- 1		-3146.5		-80845.6		10961.8		-5.9		79.3		SI
1 S	10- 1		-2771.5		-96168.7		-17660.		-7.6		135.8		SI

FREQUENTI:

Asta	Caso		NEd		MEyd		MEzd		oc		of		VE
1 I	13- 1		-2928.6		-26409.2		33187.6		-3.7		22.3		SI
1 C	13- 1		-2552.6		-20002.7		11496.7		-2.7		11.		SI
1 S	13- 1		-2178.6		-34976.2		-10274.2		-2.8		20.4		SI

QUASI PERMANENTI:

Asta	Caso		NEd		MEyd		MEzd		oc		of		VE
1 I	14- 1		-2664.6		-16951.		30223.6		-2.9		13.8		SI
1 C	14- 1		-2289.6		-17365.8		11197.5		-1.9		2.7		SI
1 S	14- 1		-1914.6		-17780.5		-7828.6		-1.7		3.4		SI

VERIFICA PILASTRO IN CEMENTO ARMATO

Nome pilastro : P03c (ID=6)
Asse : 175
Metodo di verifica : stati limite - NTC08 (q=3.2)
Dati/Vita : basca con gerarchia.
Unita' di misura : cm; dAv; dAv/cm; dAvcm; dAv/cm2; deform. %; 1/r ðe'(permille)
Unita' particolari : fessure (m|mm - ferri|mm e cm2 - sezioni|cm e derivate.
Coeff.ferri (ass): : longitudo|mm 3.5 ; stat|Fie 2.5
Imperfezioni : M minimo = N * eð ; M aggiunto = N * ei
Instabilita' : rigidizza nominale [ðc2 5.8.7]; Fief=3

MATERIALI

CLS : C25/30; Rcs=300; fcd=240; fctd=17.91; fctm=25.58; Ecm=314472;
gs=1.5; fctd14=1; ftd=26.86; fctd11.94; Ecu=8.39;
ACCIAIO: B450C; fts=5175; fyk=4500; E=2100000;
gs=1.5; fyð=3913; ftd=4500; ftd=4439.8; Eud=6.79%

TENSIONI MASSIME IN ESERCIZIO

GRUPPO : ordinario.
CLS : oc (rara)=149.4; oc (quasi permanente)=112; ftd(esercizio)=26.86
ACCIAIO: of (rara)=3600; Coeff.Omgel=15

SEZIONE UTILIZZATE

1) Rettangolare: base=50; alt.=50; Acls=2500; iy=14.43; iz=14.43

DESCRIZIONE ASTE E ARMATURA LONGITUDINALE

As Seleð |eð |eiz |eiz |eiy |Lassi Lnet Lcr.I Lcr.S| Af % am
1| 1|2.5 | 2.5 | 4 | 4 | 120. |120. | 0. | 0. | 26.52|1.06|1126|14+40|16 |

CASI DI CARICO

Nome	Descrizione	Tipo	Ses
1	SLU	SLU (statico)	1
2	SLU VENTOK	SLU (statico)	1
3	SLU VENTOK	SLU (statico)	2
6	SLU con STEMAX	SLU (statico)	4
7	SLU con STEMAX	SLU (statico)	4
8	Rara	RARA	1
9	Rara Ventok	RARA	1
10	Rara Ventok	RARA	2
11	Frequente	FREQUENTE	1
12	Frequente Ventok	FREQUENTE	1
13	Frequente Ventok	FREQUENTE	2
14	Quasi Perm	QUASI PERMAN.	1

GERARCHIA DELLE RESISTENZE

MOMENTI ULTIME MINIME (CASI STATICI):

Asta		Caso		Mu+ min		Caso		Mu+ min		Caso		Mu+ min		Caso		Mu+ min		nu
1 I		6- 1		-2345700.		6- 1		2345700.		7- 2		-2339800.		7- 2		2339800.		
1 S		7- 4		-2341740.		7- 4		2327280.		7- 4		2327280.		7- 4		2327280.		

TAGLI GERARCHIA:

As	Lp		Caso		VEyd-		0.		Caso		VEyd+		Caso		VEzd-		Caso		VEzd+	
1	120.		6- 1		0.		7- 3		2053.5		7- 1		-889.8		7- 4		3.4			

VERIFICHE ALLO STATO LIMITE ULTIMO

PRESSO-FLESSIONE (inclusi imperfezioni e second'ordine):

Asta		Caso		NEd		MEyd		MEzd		E cls		oc		E acc		of		VE
> 1		3- 1		-4744.		-124117.1 02		-102697.1 02		-0.11		-14.9		0.11		233.		SI
1		3- 1		-4257.		-112810.1 1		-53314.1.		-0.08		-10.8		0.07		156.7		SI
1		3- 1		-3769.		-104910.1 01		-10936.1 88		-0.05		-7.5		0.05		109.2		SI

INSTABILITA' - RIGIDENZA NOMINALE Y [ðc2 5.8.7]:

Asta	Caso	NE	10	JN	Jc1s/JN	Mca1	MEd	MEd	nu
1 I	3- 1	-12524066	120.	58106.5	8.9634	-122172.	-124070.	-124117.	.013

INSTABILITA' - RIGIDENZA NOMINALE Z [ðc2 5.8.7]:

Asta	Caso	NE	10	in	Dc1s2m	NcA1	NEd	MEd	nu
1 I	3- 1	-12524066	120.	58106.5	8.9634	-100760.	-102658.	-102697.	.013

TAGLIO Y:

Asta	Caso	Ved	Ved ger.	Vrid	Vrsd	Vrcd	Asw	s	ctgt	VE
1 I	7- 3	641.7	2053.5	52909.9	53879.	52909.9	1.51	11.	2.4	SI
1 C	7- 3	641.7	2053.5	52854.2	53879.	52854.2	1.51	11.	2.4	SI
1 S	7- 3	641.7	2053.5	52798.5	53879.	52798.5	1.51	11.	2.4	SI

TAGLIO Z:

Asta	Caso	Ved	Ved ger.	Vrd	Vrsd	Vrcd	Asw	s	ctgt	VE
1 I	7- 1	-278.1	-889.8	52921.8	53879.	52921.8	1.51	11.	2.4	SI
1 C	7- 1	-278.1	-889.8	52866.1	53879.	52866.1	1.51	11.	2.4	SI
1 S	7- 1	-278.1	-889.8	52810.3	53879.	52810.3	1.51	11.	2.4	SI

VED LIMITE (Ned < Nmax ; Nmax=65% di Nc1s ; Nc1s=fcfd*Ac) [7.4.4.2.2.1]:

Asta		Caso		NEd		Nmax		Nc1s		% Nc1s VE
1		7- 1		-3434.		-229287.5		-352750.		.97 SI

VERIFICHE ALLO STATO LIMITE DI ESERCIZIO

RARE:

Asta	Caso		NEd		MEyd		MEzd		oc		of		VE
1 I	10- 1		-3334.6		-82947.2		-71000.1		-10.2		153.2		SI
1 C	10- 1		-2959.6		-76003.6		-37460.4		-7.4		104.3		SI
1 S	10- 1		-2504.6		-69060.		-3503.7		-4.7		65.7		SI

FREQUENTI:

Asta	Caso		NEd		MEyd		MEzd		oc		of		VE
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1 I		13- 1		-2791.1		-37501.2		-61264.1		-6.4		81.1		SI
1 C		13- 1		-2416.1		-20240.2		-31515.2		-3.8		31.7		SI
1 S		13- 1		-2041.1		-20979.2		-1766.4		-1.6		1.		SI

QUASI PERMANENTI:

Asta	Caso	NEd	MEyd	MEzd	oc	of	VE
1 I	14- 1	-2546.8	-24959.2	-56442.5	-5.2	63.6	SI
1 C	14- 1	-2171.8	-16649.2	-28796.9	-2.8	18.3	SI
1 S	14- 1	-1796.8	-8339.3	-1151.3	-1.	-4.6	SI

VERIFICA ASTE IN ACCIAIO:

VERIFICA ELEMENTI IN ACCIAIO

Numero = 15044.
Unità di misura:
Lunghezza: cm
Prop. sez.: cm
Rozze: daN
Momenti: daNm
Tensioni: daN/cm2
MATERIALE:
S235 (N 10025-2) Mod.EI = 210000000; $\rho_H = 1.050$;
fyk = 2350.0(2150.0 per sp=40 mm); fyd = 238.1(2047.6 per sp=40 mm).

CASI DI CARICO

N	Descrizione	Soll.
1	SU	1
2	SU VENTOS	1
3	SU VENTOS	2
4	SU con SISM	4
5	SU con SISM	4

CARATTERISTICHE GEOMETRICHE
P.LIN180.S001 (1)
A = 27.9857e+00 Ix = 1.3549e+03 Iy = 113.3579e+00 IxIy = 8.8711e+00
P.LIN180.S002 (2)
A = 78.2479e+00 Ix = 5.7065e+03 Iy = 2.0036e+03 IxIy = 47.0030e+00
P.LIN180.S003 (3)
A = 54.3071e+00 Ix = 2.4964e+03 Iy = 889.3628e+00 IxIy = 24.5209e+00
P.LIN180.S001 (1) stato limite ultimo - ASTA (466- 470) 2.

COLLETTAZIONE

Caso	MZ	MY	MT	N	TZ	TY
3-1	71104.7	117.6	-66.9	-777.7	-0.7	-1475.6
TENSIONI						
Caso	Ve	No	massimi			
3-1	1	1	1	1	1	1
3-2	1	1	1	1	1	1
3-3	1	1	1	1	1	1
3-4	1	1	1	1	1	1
3-5	1	1	1	1	1	1
3-6	1	1	1	1	1	1
3-7	1	1	1	1	1	1
3-8	1	1	1	1	1	1
3-9	1	1	1	1	1	1
3-10	1	1	1	1	1	1
3-11	1	1	1	1	1	1
3-12	1	1	1	1	1	1
3-13	1	1	1	1	1	1
3-14	1	1	1	1	1	1
3-15	1	1	1	1	1	1
3-16	1	1	1	1	1	1
3-17	1	1	1	1	1	1
3-18	1	1	1	1	1	1
3-19	1	1	1	1	1	1
3-20	1	1	1	1	1	1
3-21	1	1	1	1	1	1
3-22	1	1	1	1	1	1
3-23	1	1	1	1	1	1
3-24	1	1	1	1	1	1
3-25	1	1	1	1	1	1
3-26	1	1	1	1	1	1
3-27	1	1	1	1	1	1
3-28	1	1	1	1	1	1
3-29	1	1	1	1	1	1
3-30	1	1	1	1	1	1
3-31	1	1	1	1	1	1
3-32	1	1	1	1	1	1
3-33	1	1	1	1	1	1
3-34	1	1	1	1	1	1
3-35	1	1	1	1	1	1
3-36	1	1	1	1	1	1
3-37	1	1	1	1	1	1
3-38	1	1	1	1	1	1
3-39	1	1	1	1	1	1
3-40	1	1	1	1	1	1
3-41	1	1	1	1	1	1
3-42	1	1	1	1	1	1
3-43	1	1	1	1	1	1
3-44	1	1	1	1	1	1
3-45	1	1	1	1	1	1
3-46	1	1	1	1	1	1
3-47	1	1	1	1	1	1
3-48	1	1	1	1	1	1
3-49	1	1	1	1	1	1
3-50	1	1	1	1	1	1
3-51	1	1	1	1	1	1
3-52	1	1	1	1	1	1
3-53	1	1	1	1	1	1
3-54	1	1	1	1	1	1
3-55	1	1	1	1	1	1
3-56	1	1	1	1	1	1
3-57	1	1	1	1	1	1
3-58	1	1	1	1	1	1
3-59	1	1	1	1	1	1
3-60	1	1	1	1	1	1
3-61	1	1	1	1	1	1
3-62	1	1	1	1	1	1
3-63	1	1	1	1	1	1
3-64	1	1	1	1	1	1
3-65	1	1	1	1	1	1
3-66	1	1	1	1	1	1
3-67	1	1	1	1	1	1
3-68	1	1	1	1	1	1
3-69	1	1	1	1	1	1
3-70	1	1	1	1	1	1
3-71	1	1	1	1	1	1
3-72	1	1	1	1	1	1
3-73	1	1	1	1	1	1
3-74	1	1	1	1	1	1
3-75	1	1	1	1	1	1
3-76	1	1	1	1	1	1
3-77	1	1	1	1	1	1
3-78	1	1	1	1	1	1
3-79	1	1	1	1	1	1
3-80	1	1	1	1	1	1
3-81	1	1	1	1	1	1
3-82	1	1	1	1	1	1
3-83	1	1	1	1	1	1
3-84	1	1	1	1	1	1
3-85	1	1	1	1	1	1
3-86	1	1	1	1	1	1
3-87	1	1	1	1	1	1
3-88	1	1	1	1	1	1
3-89	1	1	1	1	1	1
3-90	1	1	1	1	1	1
3-91	1	1	1	1	1	1
3-92	1	1	1	1	1	1
3-93	1	1	1	1	1	1
3-94	1	1	1	1	1	1
3-95	1	1	1	1	1	1
3-96	1	1	1	1	1	1
3-97	1	1	1	1	1	1
3-98	1	1	1	1	1	1
3-99	1	1	1	1	1	1
3-100	1	1	1	1	1	1
3-101	1	1	1	1	1	1
3-102	1	1	1	1	1	1
3-103	1	1	1	1	1	1
3-104	1	1	1	1	1	1
3-105	1	1	1	1	1	1
3-106	1	1	1	1	1	1
3-107	1	1	1	1	1	1
3-108	1	1	1	1	1	1
3-109	1	1	1	1	1	1
3-110	1	1	1	1	1	1
3-111	1	1	1	1	1	1
3-112	1	1	1	1	1	1
3-113	1	1	1	1	1	1
3-114	1	1	1	1	1	1
3-115	1	1	1	1	1	1
3-116	1	1	1	1	1	1
3-117	1	1	1	1	1	1
3-118	1	1	1	1	1	1
3-119	1	1	1	1	1	1
3-120	1	1	1	1	1	1
3-121	1	1	1	1	1	1
3-122	1	1	1	1	1	1
3-123	1	1	1	1	1	1
3-124	1	1	1	1	1	1
3-125	1	1	1	1	1	1
3-126	1	1	1	1	1	1
3-127	1	1	1	1	1	1
3-128	1	1	1	1	1	1
3-129	1	1	1	1	1	1
3-130	1	1	1	1	1	1
3-131	1	1	1	1	1	1
3-132	1	1	1	1	1	1
3-133	1	1	1	1	1	1
3-134	1	1	1	1	1	1
3-135	1	1	1	1	1	1
3-136	1	1	1	1	1	1
3-137	1	1	1	1	1	1
3-138	1	1	1	1	1	1
3-139	1	1	1	1	1	1
3-140	1	1	1	1	1	1
3-141	1	1	1	1	1	1
3-142	1	1	1	1	1	1
3-143	1	1	1	1	1	1
3-144	1	1	1	1	1	1
3-145	1	1	1	1	1	1
3-146	1	1	1	1	1	1
3-147	1	1	1	1	1	1
3-148	1	1	1	1	1	1
3-149	1	1	1	1	1	1
3-150	1	1	1	1	1	1
3-151	1	1	1	1	1	1
3-152	1	1	1	1	1	1
3-153	1	1	1	1	1	1
3-154	1	1	1	1	1	1
3-155	1	1	1	1	1	1
3-156	1	1	1	1	1	1
3-157	1	1	1	1	1	1
3-158	1	1	1	1	1	1
3-159	1	1	1	1	1	1
3-160	1	1	1	1	1	1
3-161	1	1	1	1	1	1
3-162	1	1	1	1	1	1
3-163	1	1	1	1	1	1
3-164	1	1	1	1	1	1
3-165	1	1	1	1	1	1
3-166	1	1	1	1	1	1
3-167	1	1	1	1	1	1
3-168	1	1	1	1	1	1
3-169	1	1	1	1	1	1
3-170	1	1	1	1	1	1
3-171	1	1	1	1	1	1
3-172	1	1	1	1	1	1
3-173	1	1	1	1	1	1
3-174	1	1	1	1	1	1
3-175	1	1	1	1	1	1
3-176	1	1	1	1	1	1
3-177	1	1	1	1	1	1
3-178	1	1	1	1	1	1
3-179	1	1	1	1	1	1
3-180	1	1	1	1	1	1
3-181	1	1	1	1	1	1
3-182	1	1	1	1	1	1
3-183	1	1	1	1	1	1
3-184	1	1	1	1	1	1
3-185	1	1	1	1	1	1
3-186	1	1	1	1	1	1
3-187	1	1	1	1	1	1
3-188	1	1	1	1	1	1
3-189	1	1	1	1	1	1
3-190	1	1	1	1	1	1
3-191	1	1	1	1	1	1
3-192	1	1	1	1	1	1
3-193	1	1	1	1	1	1
3-194	1	1	1	1	1	1
3-195	1	1	1	1	1	1
3-196	1	1	1	1	1	1
3-197	1	1	1	1	1	1
3-198	1	1	1	1	1	1
3-199	1	1	1	1	1	1
3-200	1	1	1	1	1	1
3-201	1	1	1	1	1	1
3-202	1	1	1	1	1	1
3-203	1	1	1	1	1	1
3-204	1	1	1	1	1	1
3-205	1	1	1	1	1	1
3-206	1	1	1	1	1	1
3-207	1	1	1	1	1	1
3-208	1	1	1	1	1	1
3-209	1	1	1	1	1	1
3-210	1	1	1	1	1	1
3-211	1	1	1	1	1	1
3-212	1	1	1	1	1	1
3-213	1	1	1	1	1	1
3-214	1	1	1	1	1	1
3-215	1	1	1	1	1	1
3-216	1	1	1	1	1	1
3-217	1	1	1	1	1	1
3-218	1	1	1	1	1	1
3-219	1	1	1	1	1	1
3-220	1	1	1	1	1	1
3-221	1	1	1	1	1	1
3-222	1	1	1	1	1	1
3-223	1	1	1	1	1	1
3-224	1	1	1	1	1	1
3-225	1	1	1	1	1	1
3-226	1	1	1	1	1	1
3-227	1	1	1	1	1	1
3-228	1	1	1	1	1	1
3-229	1	1	1	1	1	1
3-230	1	1	1	1	1	1

3-1	24388.9	7010.8	-323.2	-372.3	-22.2	45.7
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	506.3	0.0	0.0	506.3	
3-1	3-1	-175.3	-48.0	0.0	194.0	
3-1	3-1	60.9	-34.2	0.0	60.9	
SOLLECAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	18332.4	7412.7	201.8	6.5	12.0
3-1	3-1	18486.1	-591.9	-591.9	3.0	-329.0
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	480.6	0.0	0.0	480.6	
3-1	3-1	-143.6	53.8	0.0	171.2	
3-1	3-1	104.8	0.0	56.4	143.3	
SOLLECAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-200.0	6755.3	-323.2	N	28.3
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	-7.3	65.8	0.0	114.1	
3-1	3-1	85.8	0.0	87.4		
SOLLECAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-40699.6	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	233.5	77.8	0.0	209.6	
3-1	3-1	48.8	0.0	118.4	210.7	
SOLLECAZIONE						
Caso	MZ	MY	MT	N	TZ	TY
3-1	3-1	-93882.6	5038.5	-323.2	N	53.5
TENSIONE						
Caso	Ve No massimi	Sx	Tz	Ty	Si	
3-1	3-1	-1650.8	101.8	0.0	1043.9	
3-1	3-1	79.3	0.0	180.3	322.2	

VERIFICA STABILITA' :
 Z (Lc = 336, Ro = 6.96)Im = 48.3Ncr= 248509.61aIa(c)=-0.4900(ki=0.8349)
 Y (Lc = 336, Ro = 2.01)Im = 167.0Ncr= 20791.81aIa(c)=-0.4900(ki=0.2392)
 Caso 3-1 - Nodo 3 - Asse Y
 Ned = -1470.4Mreq = -122106.7Mreq = 5964.0Ss = -1322.8 (0.591)

P.LIN180_S001 (1)	stato limite ultimo	-ASTA (340- 729)	15	0
SOLLECAZIONE				
Caso	MZ	MY	MT	N
3-1	3-1	-162809.0	-1520.6	516.7
TENSIONE				
Caso	Ve No massimi	Sx	Tz	Ty
3-1	3-1	1137.3	0.0	0.0
3-1	3-1	1009.2	-221.7	0.0
3-1	3-1	-38.1	0.0	-200.6
SOLLECAZIONE				
Caso	MZ	MY	MT	N
3-1	3-1	-129702.0	-1454.4	516.7
TENSIONE				
Caso	Ve No massimi	Sx	Tz	Ty
3-1	3-1	906.0	0.0	0.0
3-1	3-1	849.4	-116.6	0.0
3-1	3-1	-33.8	0.0	-184.6
SOLLECAZIONE				
Caso	MZ	MY	MT	N
3-1	3-1	-100655.2	-1008.2	516.7
TENSIONE				
Caso	Ve No massimi	Sx	Tz	Ty
3-1	3-1	698.9	0.0	0.0
3-1	3-1	653.7	-113.5	0.0
3-1	3-1	-29.4	0.0	-168.5
3-1	3-1	-678.3	109.2	0.0
SOLLECAZIONE				
Caso	MZ	MY	MT	N
3-1	3-1	-74444.3	-752.0	516.7
TENSIONE				
Caso	Ve No massimi	Sx	Tz	Ty
3-1	3-1	519.6	0.0	0.0
3-1	3-1	482.2	-10.4	0.0
3-1	3-1	-55.1	0.0	-152.5
3-1	3-1	-506.8	104.1	0.0
SOLLECAZIONE				
Caso	MZ	MY	MT	N
3-1	3-1	-52256.7	-495.9	516.7
TENSIONE				
Caso	Ve No massimi	Sx	Tz	Ty
3-1	3-1	334.8	0.0	0.0
3-1	3-1	291.7	-10.4	0.0
3-1	3-1	-359.4	99.0	0.0
SOLLECAZIONE				
Caso	MZ	MY	MT	N
3-1	3-1	-33700.7	-239.7	516.7
TENSIONE				
Caso	Ve No massimi	Sx	Tz	Ty
3-1	3-1	211.6	-96.3	0.0
3-1	3-1	181.3	0.0	-120.5
3-1	3-1	-236.2	93.9	0.0
SOLLECAZIONE				
Caso	MZ	MY	MT	N
3-1	3-1	-18782.5	-16.5	516.7
TENSIONE				
Caso	Ve No massimi	Sx	Tz	Ty
3-1	3-1	137.8	0.0	0.0
3-1	3-1	112.5	-91.2	0.0
3-1	3-1	-137.0	88.9	0.0
SOLLECAZIONE				
Caso	MZ	MY	MT	N
3-1	3-1	-2476.9	1829.9	78.5
3-1	3-1	-7495.9	272.7	78.5

Caso	Ve No massimi	Sx	Tz	Ty	Si
6-3	3-1	-116.0	0.0	0.0	116.0
3-1	3-1	-27.5	0.0	0.0	153.8
3-1	3-1	-7.6	0.0	-88.4	153.3
3-1	3-1	-62.1	83.8	0.0	157.8
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
6-3	3-1	2231.6	78.5	-367.6	-16.1
3-1	3-1	157.1	516.7	-343.8	-13.7
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
6-3	3-1	-113.4	0.0	0.0	113.4
3-1	3-1	-13.3	-81.1	0.0	141.0
3-1	3-1	-3.3	0.0	-72.4	125.4
VERIFICA STABILITA' :					
Z (Lc = 150, Ro = 6.96) Im = 21.6 Ncr= 1248070.31aIa(c) = -0.4900(ki=0.8650)					
Y (Lc = 150, Ro = 2.01) Im = 74.5 Ncr= 104421.11aIa(c) = -0.4900(ki=0.6662)					
Caso 3-1 - Nodo 4 - Asse Y					
Ned = -343.8 Mreq = -122106.7 Mreq = -1140.5 Ss = -849.2 (0.379)					
P.LIN180_S001 (1) stato limite ultimo -ASTA (471- 732) 16 0					
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
3-1	3-1	-150401.5	-1497.0	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
3-1	3-1	1078.9	0.0	0.0	1078.9
3-1	3-1	1011.9	-117.7	0.0	1003.2
3-1	3-1	-12.6	0.0	-192.9	334.3
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
3-1	3-1	-118865.0	-1351.7	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
3-1	3-1	109.8	0.0	0.0	109.8
3-1	3-1	802.4	-112.6	0.0	825.8
3-1	3-1	-10.1	0.0	-176.9	366.3
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
3-1	3-1	-90062.1	-1073.2	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
3-1	3-1	671.1	0.0	0.0	671.1
3-1	3-1	617.0	-107.5	0.0	644.6
3-1	3-1	-7.7	0.0	-160.8	278.7
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
3-1	3-1	-66692.9	-1061.0	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
3-1	3-1	503.3	0.0	0.0	503.3
3-1	3-1	455.3	-102.5	0.0	489.2
3-1	3-1	-5.2	0.0	-144.8	250.9
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
3-1	3-1	-46057.3	-915.7	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
3-1	3-1	318.8	-97.4	0.0	318.8
3-1	3-1	-2.7	0.0	-128.8	223.1
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
3-1	3-1	-29055.4	-770.4	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
3-1	3-1	240.3	0.0	0.0	240.3
3-1	3-1	205.8	-92.3	0.0	260.6
3-1	3-1	-0.2	0.0	-112.8	159.3
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
6-2	3-1	-5795.1	-2894.9	44.9	24.9
3-1	3-1	-15687.2	-625.0	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
6-2	3-1	198.4	0.0	0.0	198.4
3-1	3-1	117.0	-87.2	0.0	191.1
3-1	3-1	2.2	0.0	-96.7	131.0
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
6-2	3-1	-2295.6	-3361.1	44.9	24.9
3-1	3-1	-5952.6	-479.7	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
6-2	3-1	196.0	0.0	0.0	196.0
3-1	3-1	52.4	-82.1	0.0	134.0
3-1	3-1	4.7	0.0	-80.7	139.9
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
6-2	3-1	54.3	-3827.3	44.9	24.9
3-1	3-1	146.3	-334.4	507.1	-7.8
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
6-2	3-1	146.3	0.0	0.0	146.3
3-1	3-1	11.9	-77.0	0.0	134.0
3-1	3-1	7.2	0.0	-64.7	112.3
VERIFICA STABILITA' :					
Z (Lc = 150, Ro = 6.96) Im = 21.6 Ncr= 1248070.31aIa(c) = -0.4900(ki=0.8650)					
Y (Lc = 150, Ro = 2.01) Im = 74.5 Ncr= 104421.11aIa(c) = -0.4900(ki=0.6662)					
Caso 6-3 - Nodo 3 - Asse Y					
Ned = -535.1 Mreq = -36188.7 Mreq = 2601.3 Ss = -386.2 (0.173)					
P.LIN180_S001 (1) stato limite ultimo -ASTA (19- 472) 17 0					
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
6-2	3-1	1362.0	59.0	18.2	-0.1
3-2	3-1	4658.8	-545.5	98.8	-3.2
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si
6-2	3-1	-94.6	0.0	0.0	94.6
3-2	3-1	17.0	-40.7	0.0	72.5
3-2	3-1	-23.3	0.0	93.2	163.1
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
3-1	3-1	-30556.8	363.6	60.1	-7.8
3-2	3-1	-30304.5	-411.9	98.8	-3.2

Caso	Ve No massimi	Sx	Tz	Ty	Si
3-1	3-1	-246.4	0.0	0.0	246.4
3-1	3-1	-246.4	-24.9	0.0	214.2
3-1	3-1	-13.1	0.0	62.2	108.6
SOLLECAZIONE					
Caso	MZ	MY	MT	N	TZ
3-1	3-1	-4978.2	368.0	60.1	-0.1
3-2	3-1	-49524.4	-278.3	98.8	47.7
TENSIONE					
Caso	Ve No massimi	Sx	Tz	Ty	Si</

VERIFICA STABILITA' :										
Z Lc = 150, Ro = 6.96 m = 21.6 ncr= 1248070.3 a fa(c) >= 0.4900 ki=0.9850 Y Lc = 150, Ro = 2.01 m = 74.5 ncr= 104421.1 a fa(c) >= 0.4900 ki=0.6662 Caso 3-1 - Noddo 2 - Assse Y Ned = -269.1 Mseq = 121618.6 Mreq = 320.4 Ss = -836.8 (0.374)										
P.LPNR80_S001 (1) stato limite ultimo - ASTA (472- 731) 24										
PROGR. 19.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	165767.7	501.4	-179.4	N	303.9	TZ	-1.4	TY	-1881.7	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-2	1	4	Sx	SI	1120.5	0.0	0.0	1120.5		
3-2	1	9	Tz	SI	112.0	-74.1	0.0	113.9		
3-2	1	5	TY		19.4	0.0	171.8	298.2		
PROGR. 38.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	13203.3	528.4	-179.4	N	303.9	TZ	-1.4	TY	-1687.9	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-2	1	4	Sx	SI	898.7	0.0	0.0	898.7		
3-2	1	9	Tz	SI	889.7	-69.3	0.0	897.8		
3-2	1	5	TY		19.8	0.0	155.8	270.5		
PROGR. 75.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	102472.5	555.4	-179.4	N	303.9	TZ	-1.4	TY	-1494.1	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-2	1	4	Sx	SI	701.0	0.0	0.0	701.0		
3-2	1	9	Tz	SI	691.5	-64.2	0.0	700.4		
3-2	1	5	TY		20.3	0.0	139.7	267.7		
PROGR. 56.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	75230.7	523.0	-147.5	N	60.1	TZ	-5.0	TY	-1289.3	
3-2	76275.3	580.5	-179.4	N	303.9	TZ	-1.4	TY	-1300.3	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-2	1	4	Sx	SI	-531.0	0.0	0.0	531.0		
3-2	1	9	Tz	SI	517.5	-59.1	0.0	527.6		
3-2	1	5	TY		20.8	0.0	123.7	215.3		
PROGR. 94.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	52873.4	743.2	-147.5	N	60.1	TZ	-5.0	TY	-1095.5	
3-2	53711.8	699.5	-179.4	N	303.9	TZ	-1.4	TY	-1106.5	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-2	1	4	Sx	SI	-386.6	0.0	0.0	386.6		
3-2	1	9	Tz	SI	367.6	-54.0	0.0	379.4		
3-2	1	5	TY		21.2	0.0	107.7	207.7		
PROGR. 112.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	34949.7	836.4	-147.5	N	60.1	TZ	-5.0	TY	-980.7	
3-2	34782.0	686.5	-179.4	N	303.9	TZ	-1.4	TY	-912.7	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-2	1	4	Sx	SI	-266.4	0.0	0.0	266.4		
3-2	1	9	Tz	SI	252.9	-46.9	0.0	267.8		
3-2	1	5	TY		21.7	0.0	91.7	160.3		
PROGR. 131.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
6-2	6524.1	2939.7	-38.3	N	828.8	TZ	-2.2	TY	-229.8	
3-2	19485.9	663.5	-179.4	N	303.9	TZ	-1.4	TY	-718.9	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
6-2	1	3	Sx	SI	-205.2	0.0	0.0	205.2		
6-2	1	9	Tz	SI	140.3	-43.9	0.0	159.9		
6-2	1	5	TY		22.1	0.0	75.6	132.9		
PROGR. 150.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
6-2	2701.9	3412.8	-38.3	N	828.8	TZ	-2.2	TY	-128.5	
3-2	7823.4	690.6	-179.4	N	303.9	TZ	-1.4	TY	-525.1	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
6-2	1	3	Sx	SI	-200.3	0.0	0.0	200.3		
6-2	1	9	Tz	SI	62.8	-38.8	0.0	92.0		
6-2	1	5	TY		22.6	0.0	59.6	105.7		
PROGR. 150.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	-70.8	3885.9	-38.3	N	828.8	TZ	-2.2	TY	-117.2	
3-2	-205.5	717.6	-179.4	N	303.9	TZ	-1.4	TY	-331.3	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-2	1	3	Sx	SI	-204.0	0.0	0.0	204.0		
3-2	1	9	Tz	SI	9.5	-33.7	0.0	29.2		
3-2	1	5	TY		9.3	0.0	43.6	79.0		

VERIFICA STABILITA' :										
Z Lc = 150, Ro = 6.96 m = 21.6 ncr= 1248070.3 a fa(c) >= 0.4900 ki=0.9850 Y Lc = 150, Ro = 2.01 m = 74.5 ncr= 104421.1 a fa(c) >= 0.4900 ki=0.6662 Caso 3-1 - Noddo 2 - Assse Y Ned = -60.1 Mseq = 123078.5 Mreq = 966.2 Ss = -864.1 (0.380)										
P.LPNR80_S001 (1) stato limite ultimo - ASTA (28- 473) 25										
PROGR. 0.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	0.0	0.0	0.0	N	-1775.5	TZ	99.4	TY	1267.1	
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-2	1	3	Sx	SI	43.4	0.0	0.0	63.4		
3-2	1	9	Tz	SI	47.0	41.8	0.0	96.3		
3-2	1	5	TY		63.4	0.0	-104.8	192.2		
PROGR. 42.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	45104.1	3377.7	0.0	-430.4	TZ	51.4	886.1			
3-2	45370.4	-3647.5	0.0	-1335.9	TZ	74.2	882.4			
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-1	1	3	Sx	SI	-475.1	0.0	0.0	475.1		
3-1	1	9	Tz	SI	245.8	29.8	0.0	251.1		
3-1	1	5	TY		-117.6	0.0	-73.8	173.3		
PROGR. 84.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	74464.9	6096.0	0.0	-210.8	TZ	47.3	511.4			
3-2	74697.4	-6235.7	0.0	-1335.9	TZ	74.2	517.7			
TENSIONE :										
Caso	Ve	No	massimi	Sx	Tz	TY				
3-1	1	3	Sx	SI	-775.0	0.0	0.0	775.0		
3-1	1	9	Tz	SI	450.4	17.8	0.0	451.5		
3-1	1	5	TY		-153.7	0.0	-42.8	170.7		

PROGR. 126.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	88802.2	7555.0	0.0	8.8	-22.1	136.7				
3-2	88880.9	-7764.5	0.0	-1115.6	23.8					
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-1	1	2	Sx	Sz	0.0	0.0	302.9			
3-1	1	8	Tz	0.0	5.8	0.0	550.6			
3-2	1	5	Ty	-17.1	0.0	-11.8	17.3			
PROGR. 168.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	85956.1	7954.6	0.0	228.5	3.1	-237.9				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-1	1	2	Sx	Sz	0.0	0.0	318.8			
3-1	1	8	Tz	-56.2	6.5	0.0	562.9			
3-2	1	5	Ty	34.3	0.0	19.7	34.7			
PROGR. 210.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	69417.8	-7643.9	0.0	-677.4	-26.6	-606.3				
3-1	86806.6	-7704.8	0.0	-148.1	-28.3	-612.3				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-2	1	2	Sx	Sz	0.0	0.0	779.0			
3-1	1	8	Tz	-436.3	18.5	0.0	437.4			
3-2	1	5	Ty	340.0	0.0	50.7	365.7			
PROGR. 252.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	3360.2	-5994.6	0.0	-2.7	-51.9	9.0				
3-1	34473.6	5575.6	0.0	667.7	53.5	-987.3				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-2	1	2	Sx	Sz	0.0	0.0	491.5			
3-1	1	8	Tz	-205.3	10.4	0.0	213.8			
3-2	1	5	Ty	118.6	0.0	81.6	184.6			
PROGR. 294.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	1297.9	-2585.6	0.0	-12.8	-77.1	-1255.6				
3-1	-14882.7	7797.1	0.0	887.4	78.7	-1361.9				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-2	1	2	Sx	Sz	0.0	0.0	225.0			
3-1	1	8	Tz	130.6	62.5	0.0	62.8			
3-1	1	5	Ty	79.2	0.0	112.6	210.5			
3-2	1	5	Ty	132.5	0.0	97.3	227.3			
PROGR. 336.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	-79982.4	-1040.8	0.0	1107.0	103.9	-1736.6				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-1	1	2	Sx	Sz	0.0	0.0	60.4			
3-1	1	8	Tz	570.8	54.5	0.0	578.6			
3-2	1	5	Ty	21.9	0.0	143.6	249.8			
VERIFICA STABILITA' :										
Z L = 336										
L = 336; Ro = 6.96; ln = 48.3; Ncr= 248520.61a1fa(c - 0.40000; k= 0.8349)										
N = 630.136; Ro = 2.01; ln = 36.1; Ncr= 20791.81a1fa(c - 0.40000; k= 0.2382)										
Nel = -690.136w = 66061.61wq = 6668.515 = -845.1 (0.3392)										
P_LINFORM_5001 (1) stato limite ultimo - ASTA (469- 342) 27.0										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	330.9	-330.9	0.0	-13.8	99.6	1570.5				
3-1	-95679.4	-577.6	338.6	-444.7	-98.0	1559.4				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-2	1	2	Sx	Sz	0.0	0.0	732.3			
3-1	1	8	Tz	620.7	0.0	0.0	662.8			
3-1	1	5	Ty	-24.6	0.0	-139.5	277.4			
PROGR. 42.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	-3805.0	3009.2	338.6	135.1	-72.8	8.7				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-1	1	2	Sx	Sz	0.0	0.0	394.2			
3-1	1	8	Tz	245.6	-84.3	0.0	265.8			
3-2	1	5	Ty	44.2	0.0	-128.5	227.0			
PROGR. 84.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	3884.0	5536.6	338.6	24.5	-47.5	1.0				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-1	1	2	Sx	Sz	0.0	0.0	272.7			
3-1	1	8	Tz	-24.9	-72.3	0.0	127.8			
3-2	1	5	Ty	95.0	0.0	-97.6	395.8			
PROGR. 126.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	30050.6	7004.6	338.6	244.2	-22.3	45.4				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-1	1	2	Sx	Sz	0.0	0.0	504.4			
3-1	1	8	Tz	330.9	0.0	0.0	217.6			
3-2	1	5	Ty	127.8	0.0	-66.6	172.1			
PROGR. 168.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-1	4040.3	-7930.0	-193.4	-699.7	-1.3	61.8				
3-2	38767.3	7413.3	338.6	463.8	2.9	70.7				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-2	1	2	Sx	Sz	0.0	0.0	385.6			
3-1	1	8	Tz	285.4	48.8	0.0	297.7			
3-2	1	5	Ty	142.6	0.0	-55.6	155.3			
PROGR. 210.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	3353.3	-7346.5	-193.4	-680.0	-26.5	-302.8				
3-1	33617.5	6762.5	338.6	483.4	28.1	-313.9				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-1	1	2	Sx	Sz	0.0	0.0	535.6			
3-1	1	8	Tz	-209.1	57.7	0.0	231.7			
3-2	1	5	Ty	139.4	0.0	56.5	170.3			
PROGR. 252.										
COLLETTAZIONE :										
Caso	MZ	MY	MT	N	TZ	TY				
3-2	13041.0	-5703.7	-139.4	-240.4	-51.7	-677.5				
3-1	33533.3	6762.5	338.6	483.4	28.1	-313.9				
TENSIONI :										
Caso	Vel	Nel	max	Sx	Sz	Ty	Si			
3-2	1	2	Sx	Sz	0.0	0.0	332.6			
3-1	1	8	Tz	-312.3	69.7	0.0	155.3			
3-2	1	5	Ty	139.4	0.0	56.5	170.3			

PUNTO		Caso		Vel	Nel	messini	Sx	Tz	0,0	0,0	Ty	Sz	416,0			
3 - 1		1	1	1	1	1	416,0	0,0	0,0	0,0	0,0	416,0				
3 - 1		1	1	1	1	1	38,8	37,6	0,0	0,0	0,0	394,3				
3 - 1		1	1	1	1	1	166,0	0,0	0,0	117,9	0,0	204,8				
VERIFICA STABILITA' : asta tesa per tutti i casi di carico.																
P_LINPUNO_5001 (- 1)																
stato limite ultimo - ASTA (750 - 460)																
PROGR. 134																
0.																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	-563,6	Tz	-0,5	Ty	-958,2		
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	20,1	0,0	0,0	0,0	0,0	0,0	48,0			
3 - 1		1	1	1	1	1	-20,1	-25,2	0,0	0,0	0,0	0,0	138,7			
3 - 1		1	1	1	1	1	Ty	Sz	1	0,0	0,0	0,0	17,3	29.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-2327,4	M	15,4	0,0	N	-563,6	Tz	-0,5	Ty	-661,1
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	-175,5	0,0	0,0	0,0	0,0	0,0	175,5			
3 - 1		1	1	1	1	1	-174,8	-37,4	0,0	0,0	0,0	0,0	17,3			
3 - 1		1	1	1	1	1	Ty	Sz	1	-19,9	0,0	0,0	54,7	58.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-3801,6	M	30,8	0,0	N	-563,6	Tz	-0,5	Ty	-363,9
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	-274,0	0,0	0,0	0,0	0,0	0,0	274,0			
3 - 1		1	1	1	1	1	-272,6	-9,6	0,0	0,0	0,0	0,0	23,1			
3 - 1		1	1	1	1	1	Ty	Sz	1	-19,6	0,0	0,0	30,1	86.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-44202,8	M	46,2	0,0	N	-563,6	Tz	-0,5	Ty	-66,8
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	-31,8	0,0	0,0	0,0	0,0	0,0	31,8			
3 - 1		1	1	1	1	1	-313,8	-1,8	0,0	0,0	0,0	0,0	313,8			
3 - 1		1	1	1	1	1	Ty	Sz	1	-19,4	0,0	0,0	5,5	115.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-41859,7	M	61,6	0,0	N	-563,6	Tz	-0,5	Ty	230,4
3 - 1		1	1	1	1	1	-408,8	64,8	0,0	0,0	0,0	0,0	131,6			
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	-300,9	0,0	0,0	0,0	0,0	0,0	300,9			
3 - 1		1	1	1	1	1	-267,4	-6,3	0,0	0,0	0,0	0,0	267,6			
3 - 1		1	1	1	1	1	Ty	Sz	1	-19,7	0,0	0,0	5,6	144.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-39846,9	M	77,0	0,0	N	-563,6	Tz	-0,5	Ty	824,7
3 - 2		1	1	1	1	1	-20949,6	81,0	0,0	-131,6	-0,6	-0,6	535,3			
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	-229,2	0,0	0,0	0,0	0,0	0,0	229,2			
3 - 1		1	1	1	1	1	-189,6	-4,4	0,0	0,0	0,0	0,0	189,1			
3 - 1		1	1	1	1	1	Ty	Sz	1	-44,3	0,0	0,0	76,7	172.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-11517,3	M	92,4	0,0	N	-563,6	Tz	-0,5	Ty	832,4
3 - 2		1	1	1	1	1	-10186,9	97,2	0,0	-131,6	-0,6	-0,6	832,4			
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	-300,8	0,0	0,0	0,0	0,0	0,0	300,8			
3 - 1		1	1	1	1	1	-63,0	0,0	0,0	0,0	0,0	0,0	73,5			
3 - 1		1	1	1	1	1	Ty	Sz	1	-68,8	0,0	0,0	119,3			
3 - 2		1	1	1	1	1	-3,1	0,0	0,0	-54,7	0,0	0,0	32,0	201.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-16654,1	M	107,8	0,0	N	-563,6	Tz	-0,5	Ty	1121,8
3 - 2		1	1	1	1	1	-182,6	113,4	0,0	-131,6	-0,6	-0,6	1129,6			
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	-134,3	0,0	0,0	0,0	0,0	0,0	134,3			
3 - 1		1	1	1	1	1	-124,4	-29,7	0,0	0,0	0,0	0,0	124,6			
3 - 1		1	1	1	1	1	Ty	Sz	1	-93,4	0,0	0,0	161,8			
3 - 1		1	1	1	1	1	-99,3	0,0	0,0	0,0	0,0	0,0	162,7	230.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-52988,7	M	123,2	0,0	N	-563,6	Tz	-0,5	Ty	1419,0
3 - 2		1	1	1	1	1	-54762,6	129,6	0,0	-131,6	-0,6	-0,6	1426,7			
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	-377,6	0,0	0,0	0,0	0,0	0,0	377,6			
3 - 1		1	1	1	1	1	-368,5	-37,5	0,0	0,0	0,0	0,0	374,1			
3 - 1		1	1	1	1	1	-35,5	0,0	0,0	0,0	0,0	0,0	204,4			
3 - 1		1	1	1	1	1	Ty	Sz	1	-39,3	0,0	0,0	37,7			
VERIFICA STABILITA' :																
I = 230,0 ; Z = 6,961 ; N = 33,31N/m ; 53842,71n/mcf ; 90,40000(kN)0,0024																
LC = 230,0 ; Nb = 2,001 ; Np = 414,33N/m ; 53842,71n/mcf ; 90,40000(kN)0,0024																
Caso 3 - 1 - Nod 2 - Asse y																
Np = 414,33 ; Np2 = 39741,5My/m ; 92,4155 ; -315,8 (0,136)																
P_LINPUNO_5001 (- 1)																
stato limite ultimo - ASTA (749 - 460)																
PROGR. 0																
136																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	690,6	Tz	2,9	Ty	772,6		
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	24,7	0,0	0,0	0,0	0,0	0,0	24,7			
3 - 1		1	1	1	1	1	-24,7	-20,5	0,0	0,0	0,0	0,0	43,3			
3 - 1		1	1	1	1	1	Ty	Sz	1	-63,9	0,0	0,0	113,4	29.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-17941,1	M	83,7	0,0	N	690,6	Tz	2,9	Ty	475,5
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	147,6	0,0	0,0	0,0	0,0	0,0	147,6			
3 - 1		1	1	1	1	1	143,9	0,0	0,0	0,0	0,0	0,0	146,5			
3 - 1		1	1	1	1	1	Ty	Sz	1	-39,3	0,0	0,0	72,0	58.		
SOLLECITAZIONE																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	-27339,0	M	167,4	0,0	N	690,6	Tz	2,9	Ty	178,3
TENSIONI																
Caso		Vel		N		M		T		S		Z				
3 - 1		1	1	1	1	1	0,0	0,0	0,0	0,0	Ty	Sz	1			
3 - 1		1	1	1	1	1	213,8	0,0	0,0	0,0	0,0	0,0	213,8			
3 - 1		1	1	1	1	1	206,3	0,0	0,0	0,0	0,0	0,0	206,6			
3 - 1		1	1	1	1	1	Ty	Sz	1	-14,7	0,0	0,0	33,6			

3-1	11	21	Sx	Si	-27.71	0.01	0.0	271.5	
3-2	91	91	Tz		-78.7	-33.5	0.0	97.8	
3-1	91	61	Ty		16.8	0.0	58.7	103.1	
PROGR. 201.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-1133.8	2032.4	-17.21	-18.3	-337.1	-258.4		
3-1	91	-1394.6	1014.6	-13.8	-13.4	-309.1	-964.3		
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	166.9	0.0	0.0	0.0	166.9			
3-1	91	-71.9	-48.0	0.0	0.0	112.6			
3-1	61	Ty			85.4	123.5			
PROGR. 230.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 231.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 232.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 233.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 234.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 235.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 236.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 237.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 238.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 239.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 240.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 241.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 242.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 243.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 244.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 245.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 246.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 247.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 248.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 249.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty			112.1	206.2			
PROGR. 250.									
COLLECTAZIONE									
Caso	3-1	MZ	MY	MT	N	Tz	Ty		
3-1	11	-433.2	98.5	-12.2	-18.3	-314.7	-1225.5		
3-1	91	-4941.7	-8608.0	-15.8	-13.4	302.9			
TENSIONE									
Caso	3-1	Si	Sx	Tz	Ty				
3-1	11	-733.3	0.0	0.0	0.0	733.3			
3-1	91	-287.6	-27.5	0.0	0.0	100.3			
3-1	61	Ty							

3-1	2,6	-155,8	0,0	-46,4	-0,7	-1188,6
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	4	6,3	0,0	6,3		
3-1	8	3,6	31,2	0,0	44,2	
3-1	5	4,3	0,0	96,3	170,3	
3-2	5	6,3	0,0	96,3	170,4	29.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29898,7	136,5	0,0	101,7	0,7
3-1	-29898,7	-136,3	0,0	-46,4	-0,7	-891,5
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	344,1	0,0	0,0	206,6	
3-1	8	202,2	23,4	0,0	206,3	
3-1	5	-4,0	0,0	73,7	127,7	58.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51256,9	117,0	0,0	101,7	0,7
3-1	-51256,9	-116,8	0,0	-46,4	-0,7	-594,3
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	344,1	0,0	0,0	345,2	
3-1	8	344,1	15,6	0,0	345,2	
3-1	5	-3,6	0,0	49,1	85,2	86.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64071,9	97,5	0,0	101,7	0,7
3-1	-64071,9	-97,4	0,0	-46,4	-0,7	-297,2
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	430,9	0,0	0,0	430,9	
3-1	8	429,2	7,9	0,0	429,5	
3-1	5	-3,3	0,0	24,6	42,7	115.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-68343,8	78,0	0,0	101,7	0,7
3-1	-68343,8	-78,0	0,0	-46,4	-0,7	-297,2
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	458,9	0,0	0,0	458,9	
3-1	8	457,6	0,1	0,0	457,6	
3-1	6	341,3	0,0	0,1	341,3	144.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64072,6	58,5	0,0	101,7	0,7
3-1	-64072,6	-58,5	0,0	-46,4	-0,7	-297,2
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	430,2	0,0	0,0	430,2	
3-1	8	422,0	0,9	0,0	422,2	
3-2	5	4,6	0,0	-24,6	42,8	172.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	344,8	0,0	0,0	344,8	
3-1	8	-336,9	15,6	0,0	337,9	
3-2	5	4,3	0,0	-49,1	85,2	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29900,7	19,5	0,0	101,7	0,7
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	-891,5
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	202,6	0,0	0,0	202,6	
3-1	8	-195,0	23,4	0,0	199,2	
3-2	5	4,0	0,0	-73,7	127,7	172.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	344,1	0,0	0,0	345,2	
3-1	8	344,1	15,6	0,0	345,2	
3-1	5	-3,6	0,0	49,1	85,2	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29900,7	19,5	0,0	101,7	0,7
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	-891,5
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	202,6	0,0	0,0	202,6	
3-1	8	-195,0	23,4	0,0	199,2	
3-2	5	4,0	0,0	-73,7	127,7	172.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,2	39,0	0,0	101,7	0,7
3-1	-51258,2	-39,0	0,0	-46,4	-0,7	-594,3
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	344,1	0,0	0,0	345,2	
3-1	8	344,1	15,6	0,0	345,2	
3-1	5	-3,6	0,0	49,1	85,2	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29900,7	19,5	0,0	101,7	0,7
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	-891,5
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	202,6	0,0	0,0	202,6	
3-1	8	-195,0	23,4	0,0	199,2	
3-2	5	4,0	0,0	-73,7	127,7	172.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29900,7	19,5	0,0	101,7	0,7
3-1	-29900,7	-19,5	0,0	-46,4	-0,7	-891,5
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	202,6	0,0	0,0	202,6	
3-1	8	-195,0	23,4	0,0	199,2	
3-2	5	4,0	0,0	-73,7	127,7	172.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,8	0,0	0,0	13,8	0,0
3-1	-51258,8	0,0	0,0	5,0	0,0	-594,3
3-1	-51258,8	0,0	0,0	5,0	0,0	-594,3
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	340,7	15,6	0,0	341,7	
3-1	5	0,3	0,0	49,1	85,1	86.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64073,5	0,0	0,0	13,8	0,0
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	340,7	15,6	0,0	341,7	
3-1	5	0,3	0,0	49,1	85,1	86.

TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	425,8	7,8	0,0	426,1	
3-1	8	425,8	7,8	0,0	426,1	
3-1	5	0,3	0,0	24,6	42,6	115.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64073,5	0,0	0,0	13,8	0,0
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	425,8	7,8	0,0	426,1	
3-1	8	425,8	7,8	0,0	426,1	
3-1	5	0,3	0,0	24,6	42,6	115.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-64073,5	0,0	0,0	13,8	0,0
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
3-1	-64073,5	0,0	0,0	5,0	0,0	-297,2
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	425,8	7,8	0,0	426,1	
3-1	8	425,8	7,8	0,0	426,1	
3-1	5	0,3	0,0	24,6	42,6	115.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-51258,8	0,0	0,0	13,8	0,0
3-1	-51258,8	0,0	0,0	9,4	0,0	594,3
3-1	-51258,8	0,0	0,0	9,4	0,0	594,3
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	341,0	0,0	0,0	341,0	
3-1	8	340,7	15,6	0,0	341,7	
3-1	5	0,3	0,0	49,1	85,1	201.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-29901,0	0,0	0,0	13,8	0,0
3-1	-29901,0	0,0	0,0	9,4	0,0	891,5
3-1	-29901,0	0,0	0,0	9,4	0,0	891,5
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	199,1	0,0	0,0	199,1	
3-1	8	-198,3	23,4	0,0	198,6	
3-1	5	0,3	0,0	-73,7	127,7	230.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-18131,5	13,8	0,0	-46,1	-0,5
3-1	-18131,5	-13,8	0,0	-46,1	-0,5	-482,1
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	122,7	0,0	0,0	122,7	
3-1	8	-122,1	-12,7	0,0	122,7	
3-1	5	-1,4	0,0	39,9	69,1	58.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-27720,0	27,6	0,0	-46,1	-0,5
3-1	-27720,0	-27,6	0,0	-46,1	-0,5	-184,9
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	187,0	0,0	0,0	187,0	
3-1	8	-187,0	-4,9	0,0	186,0	
3-1	5	-1,7	0,0	15,3	26,3	86.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-28765,2	41,4	0,0	-46,1	-0,5
3-1	-28765,2	-41,4	0,0	-46,1	-0,5	-122,2
3-1	-28765,2	-41,4	0,0	-46,1	-0,5	-122,2
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	194,6	0,0	0,0	194,6	
3-1	8	-194,6	-4,9	0,0	194,6	
3-1	5	-1,7	0,0	15,3	26,3	86.

SOLLECITAZIONE	MZ	MY	MT	N	TZ	TY
Caso	3-2	-21267,4	61,2	0,0	-9,1	-0,5
3-1	-21267,4	-61,2	0,0	-9,1	-0,5	-444,9
TENSIONI						
Caso Ve\No\massimi	Sx	Tz	Ty	Si		
3-2	1	145,4	0,0	0,0	145,4	
3-1	8	-145,4	-11,7	0,0	145,4	
3-1	5	0,7	0,0	-36,8	63,7	144.

3-2		2342,6		49,9	0,0	26,8	-1,7	666,1
TENSIONI :								
Caso	Ve	No	Smax	Sx	Tz	Ty	Sz	
3-1	51	8	1	-163,9	0	0,0	163,9	
3-1	51	8	1	148,0	17,7	0,0	331,2	
3-2	51	5	1	1,8	0,0	-55,1	95,4	
3-1	51	8	1	-162,5	-17,2	0,0	165,2	
								PROGR.
								58.
SOLLECITAZIONE :								
	MT	MY		MT	N	TZ	TY	

SOLLECITAZIONE :												
Caso		MZ		My		MT		N		TZ		TY
3- 1		-25130.2		41.5		-19.9		-10893.1		-10.8		-17.9
3- 2		16187.1		-478.7		13.5		-10088.7		-1.6		336.1
TENSIONE :												
Caso	Ve	No	massimi		Sx		Tz		Ty		Si	
3- 1	1	1	Sx	Si	-182.9		0.0		0.0		182.9	
3- 2	1	6	Tz	Si	-156.8		-4.7		0.0		157.0	
3- 2	1	9	Ty	Si	-129.0		0.0		-21.3		134.2	

PROGR. 255.

SOLLECITAZIONE :							
Caso	MZ	MY	MT	N	TZ	TY	
3- 1	-25980.4	488.5	-19.9	-10619.2	-10.8	17.9	
3- 2	30472.7	-412.4	13.5	-10054.8	-1.6	336.1	
TENSIONE :							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3- 1	1	1	Sx	Si	-186.1	0.0	186.1
3- 2	1	6	Tz	Si	-181.4	-4.7	181.6
3- 2	1	9	Ty	Si	-128.6	0.0	133.8

PROGR. 298.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 2	44758.3	-946.0	MT	13.5	N	-10020.9	-1.6	TZ	336.1
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-208.2	0.0	0.0	208.2	
3- 2	1	6	Tz	SI	-206.1	-4.7	0.0	170.9	
3- 2	1	9	TY	SI	-128.1	0.0	-21.3	133.4	

PROGR. 340.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 2	59043.8	-279.7	MT	13.5	N	-9987.1	-1.6	TZ	336.1
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-208.2	0.0	0.0	208.2	
3- 2	1	6	Tz	SI	-206.1	-4.7	0.0	170.9	
3- 2	1	9	TY	SI	-127.7	0.0	-21.3	132.9	

VERIFICA STABILITA' :
 [L0 = 340. ;
 Z [Lc = 340. ;Ro = 8.54]m = 39.8]Ncr= 1023125.51aIa(b >=0.3400)k(i=0.9165)
 Y [Lc = 340. ;Ro = 5.06]m = 66.2]Ncr= 359233.91aIa(c >=0.4900)k(i=0.7151)
 Caso 3- 1 - NodD 2 - Asse Y
 Ned = -11022.5]Mreq = -24978.2]Mreq = -897.3]Ss = -245.9 (0.110)
 P.HER002_5002 (2) stato limite ultimo - ASTA (-748 - 4) 35
 PROGR. 0.

P_JER200_S002 (2)		stato limite ultimo - ASTA (978- 41) 35					0.
SOLLECITAZIONI :		-----					PROGR.
Caso	MZ	MY	MT	N	TZ	TY	
3- 1	90763.4	-5006.5	0.0	-2840.4	-56.4	-218.8	
3- 2	-60905.4	-9669.8	0.0	-2848.5	-91.3	585.5	
TENSIONI :							
Caso	Ve	No	massimi	Sx	Tz	TY	SI
3- 2	1	1	Sx	SI	-547.9	0.0	0.0
3- 2	1	6	Tz	SI	-546.4	-9.5	0.0
3- 2	1	9	TY	SI	-366.2	0.0	-36.7

PROGR. 21.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	86251.5	-3844.0	MT	0.0	N	-2843.5	-56.4	TZ	218.8
3- 2	-48829.4	-7785.8	MT	0.0	N	-2846.0	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-534.0	0.0	0.0	534.0	
3- 2	1	6	Tz	SI	-529.5	-9.5	0.0	270.0	
3- 2	1	9	TY	SI	-365.5	0.0	-36.7	371.0	

PROGR. 41.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	81739.7	-2681.5	MT	0.0	N	-2843.7	-56.4	TZ	218.8
3- 2	-36753.3	-5901.8	MT	0.0	N	-2844.6	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-520.1	0.0	0.0	520.1	
3- 2	1	6	Tz	SI	-520.5	-9.5	0.0	293.0	
3- 2	1	9	TY	SI	-364.9	0.0	-36.7	371.0	

PROGR. 62.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	77227.9	-1519.0	MT	0.0	N	-2842.1	-56.4	TZ	218.8
3- 2	-24677.3	-4017.8	MT	0.0	N	-2843.1	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-506.1	0.0	0.0	506.1	
3- 2	1	6	Tz	SI	-515.6	-9.5	0.0	316.0	
3- 2	1	9	TY	SI	-364.3	0.0	-36.7	369.8	

PROGR. 82.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	77216.0	-1519.0	MT	0.0	N	-2842.1	-56.4	TZ	218.8
3- 2	-24677.3	-4017.8	MT	0.0	N	-2843.1	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-506.1	0.0	0.0	506.1	
3- 2	1	6	Tz	SI	-515.6	-9.5	0.0	316.0	
3- 2	1	9	TY	SI	-364.3	0.0	-36.7	369.8	

PROGR. 103.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	77216.0	-1519.0	MT	0.0	N	-2842.1	-56.4	TZ	218.8
3- 2	-24677.3	-4017.8	MT	0.0	N	-2843.1	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-492.2	0.0	0.0	492.2	
3- 2	1	6	Tz	SI	-492.7	-9.5	0.0	339.1	
3- 2	1	9	TY	SI	-363.6	0.0	-36.7	369.8	

PROGR. 124.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	68204.2	806.1	MT	0.0	N	-2838.2	-56.4	TZ	218.8
3- 2	3092.7	-525.2	MT	0.0	N	-2840.3	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-486.3	0.0	0.0	486.3	
3- 2	1	6	Tz	SI	-486.8	-9.5	0.0	362.1	
3- 2	1	9	TY	SI	-363.0	0.0	-36.7	369.8	

PROGR. 144.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	63692.4	1266.6	MT	0.0	N	-2837.7	-56.4	TZ	218.8
3- 2	11550.9	1634.1	MT	0.0	N	-28383.8	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-484.0	0.0	0.0	484.0	
3- 2	1	6	Tz	SI	-484.9	-9.5	0.0	364.8	
3- 2	1	9	TY	SI	-362.4	0.0	-36.7	367.9	

PROGR. 165.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	56668.7	4203.7	MT	0.0	N	-2838.9	-56.4	TZ	218.8
3- 2	35703.0	5402.1	MT	0.0	N	-28350.9	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-479.4	0.0	0.0	479.4	
3- 2	1	6	Tz	SI	-481.0	-9.5	0.0	451.3	

PROGR. 289.

SOLLECITAZIONE :									
Caso	MZ	MY	MT	N	TZ	TY			
3- 1	54668.7	4203.7	MT	0.0	N	-2838.9	-56.4	TZ	218.8
3- 2	35703.0	5402.1	MT	0.0	N	-28350.9	-91.3	TZ	585.5
TENSIONE :									
Caso	Ve	No	massimi	Sx	Tz	TY	SI		
3- 2	1	1	Sx	SI	-479.4	0.0	0.0	479.4	
3- 2	1	6	Tz	SI	-481.0	-9.5	0.0	451.3	

PROGR. 330.

3- 1	54668.7	4203.7	MT	0.0	N	-2838.9	-56.4	TZ	218.8
3- 2	35703.0	5402.1	MT	0.0	N	-28350.9	-91.3	TZ	585.5
TENSIONE :									

SOLLECITAZIONE :				PROG. :			
Caso	MZ	MY	MT	N	TZ	TY	
3-2	-419700.9	-6020.3	-199.0	-63.6	-39.8	-6962.1	
6-3	-127743.4	528.0	2475.6	52.9	501.5	-2668.4	
TENSIONE :							
Caso	Ve	No	massim	Sx	Tz	Ty	Si
3-2	Si	4	Sx	-1400.3	0.0	0.0	1400.3
6-3	Si	4	Sx	402.2	196.3	0.0	0.0
3-2	Si	9	Ty	-3.9	0.0	624.7	1082.0

```

VERIFICA STATISTICA :
Y      |L0 = 10. |
Z      |LC = 10. |Ro = 6.78 |Im = 1.5 |Ncr=517408865.8|alfa(b) =0.3400|ki=1.0000|
Y      |LC = 10. |Ro = 4.04 |Im = 2.5 |Ncr=184330846.8|alfa(c) =0.4900|ki=1.0000|
Caso 3 - 2 - Nodo 4 - Asse Y
Ned = -63.6 |Meqz = -463224.8 |Myeq = -6169.5 |ss = -1541.1 ( 0.689)

```

3-1	Si	4	Sx	-1377.1	0.0	0.0	1377.1
6-3	Si	5	Tz	395.4	211.1	0.0	538.5
3-1	Si	9	Tv	-7.2	0.0	-626.2	1084.7

VERIFICA STABILITA' :

Z	L0 = 10.1								
Y	Lc = 10.1	R0 = 6.78	Im = 1.5	Ncr = 517408865.8	a fa(b) = 0.3400	ki = 1.0000			
Z	Lc = 10.1	R0 = 4.04	Im = 2.5	Ncr = 184330846.8	a fa(c) = 0.4900	ki = 1.0000			
Caseo	3- 1 + Nod0	4 - Ass0	Y						
Ned =	-384.4	Mreq = -479557.5	Mreq =	-256.9	Ss =	-1546.2	(0.691)		

TENSIONI				Sx	Tz	Ty	Sy
Caso	Ve	No	massimi	-13.0	0.0	0.0	13.0
3-	1	1	Sx	0.1	-464.2	111.3	11.0
3-	1	1	Tz	-7.0	0.0	-278.0	481.6
3-	1	1	Ty				

VERIFICA STABILITA' :

$|L_0| = 130.$

3-2	1	5	4	5x	-290.5	0.0	0.0	290.5
3-2	1	5	9	Tz	175.9	-172.3	0.0	346.5
3-1	1	5	9	Tys	-12.3	0.0	509.9	883.2

SOLLECITAZIONE

Caso	MZ	MY	MT	N	TZ	TY
3-2	-93355.6	-374.3	201.7	-565.1	-9.1	-5637.0
3-1	-65446.1	-442.6	-1485.2	-656.8	-3.2	-5195.8

TENSIONI

3-1	16690.4	4183.4	-502.7	-373.3	-32.3	1529.1
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	4	Si	104.7	0.0	104.7
3-1	151	6	Tz	-69.3	-55.3	0.0
3-1	151	9	Ty	-5.0	0.0	118.2
3-1	151	10	Si	-8.7	0.0	263.8
PROGR.						
SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	41464.6	4709.0	-502.7	-373.3	TZ	1520.1
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	2	Si	-182.1	0.0	182.1
3-1	151	6	Tz	-149.8	0.0	177.1
3-1	151	9	Ty	-4.7	0.0	262.3
3-1	151	12	Si	-95.4	0.0	265.7

VERIFICA STABILITA' :
 Z Lc = 130. lRo = 6.78 lIm = 19.2 lncr= 3061590.9 lalfa(b) >= 0.3400 (k=0.9929)
 Y Lc = 130. lRo = 4.04 lIm = 32.1 lncr= 1090715.1 lalfa(c) >= 0.4900 (k=0.9275)
 Caso 3-1 - Nodo 3 - Asse Y
 Ned = -373.3 lMeq = -120620.0 lMeq = 3531.8 lSs = -425.8 (0.190)

P.JHERLO_5003 (3) stato limite ultimo - ASTA (748- 737) 122						
PROGR.						
SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	40256.3	4709.0	190.8	-131.6	TZ	746.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	2	Si	-172.8	0.0	173.8
3-1	151	5	Tz	-121.4	27.1	0.0
3-1	151	9	Ty	-0.3	0.0	125.5
PROGR.						
SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	51963.6	2847.9	190.8	-131.6	TZ	592.0
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	5	Si	-194.6	0.0	194.6
3-1	151	5	Tz	-162.9	24.4	0.0
3-1	151	9	Ty	-1.1	0.0	101.9

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	60974.7	986.7	190.8	-131.6	TZ	437.9
3-1	29464.3	2878.3	-179.3	115.0	TZ	-459.5
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	5	Si	-206.7	0.0	206.7
3-1	151	5	Tz	-195.7	21.6	0.0
3-1	151	9	Ty	3.4	0.0	80.9

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	67289.5	874.4	190.8	-131.6	TZ	283.8
3-1	20074.9	3866.7	-179.3	115.0	TZ	-613.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	5	Si	-225.9	0.0	225.9
3-1	151	5	Tz	-54.0	-22.5	0.0
3-1	151	9	Ty	3.9	0.0	60.3

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	70908.0	-2735.6	190.8	-131.6	TZ	129.7
3-1	7989.2	4855.0	-179.3	115.0	TZ	-767.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	5	Si	-13.1	-25.2	0.0
3-1	151	5	Tz	-54.0	-22.5	0.0
3-1	151	9	Ty	3.9	0.0	60.3

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	70908.0	-2735.6	190.8	-131.6	TZ	129.7
3-1	7989.2	4855.0	-179.3	115.0	TZ	-767.6
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	5	Si	-13.1	-25.2	0.0
3-1	151	5	Tz	-54.0	-22.5	0.0
3-1	151	9	Ty	3.9	0.0	60.3

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	71830.3	-6596.8	190.8	-131.6	TZ	-24.2
3-1	6702.8	5843.4	-179.3	115.0	TZ	-921.7
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	5	Si	-274.0	0.0	274.0
3-1	151	5	Tz	-36.4	-28.0	0.0
3-1	151	9	Ty	4.7	0.0	87.7

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	70956.3	-6457.9	190.8	-131.6	TZ	-178.8
3-1	24071.0	6831.7	-179.3	115.0	TZ	-1075.8
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	5	Si	-285.0	0.0	285.0
3-1	151	5	Tz	94.5	-30.8	0.0
3-1	151	9	Ty	5.2	0.0	101.4

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	65986.0	-5319.1	190.8	-131.6	TZ	-332.5
3-1	44445.5	7820.1	-179.3	115.0	TZ	-1229.9
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	5	Si	-287.4	0.0	287.4
3-1	151	5	Tz	-171.3	12.5	0.0
3-1	151	9	Ty	5.6	0.0	115.1

SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	67316.2	8808.4	-179.3	115.0	TZ	-56.5
3-1	297.1	237.1	0.0	0.0	297.1	0.0
3-1	236.7	-36.3	0.0	0.0	244.9	0.0
3-1	6.1	0.0	0.0	128.9	223.1	0.0

VERIFICA STABILITA' :
 Z Lc = 140. lRo = 6.78 lIm = 20.7 lncr= 2638841.2 lalfa(b) >= 0.3400 (k=0.9929)
 Y Lc = 140. lRo = 4.04 lIm = 34.6 lncr= 940463.5 lalfa(c) >= 0.4900 (k=0.9138)
 Caso 3-1 - Nodo 1 - Asse Y
 Ned = -131.6 lMeq = 71830.3 lMeq = -7635.2 lSs = -301.5 (0.123)

P.JHERLO_5003 (3) stato limite ultimo - ASTA (746- 735) 123						
PROGR.						
SOLLECITAZIONE :						
Caso	MZ	MY	MT	N	TZ	TY
3-1	-119083.9	-60.5	2173.9	14.8	-45.2	-1916.6
3-1	-115811.4	-569.4	2433.9	-155.2	13.7	-1898.8
TENSIONI						
Caso	Ve	No	massimi	Sx	Tz	Si
3-1	151	2	Sx	382.4	0.0	382.4
3-1	151	6	Tz	369.5	163.9	466.0
3-1	151	9	Ty	-3.1	0.0	429.8
3-1	151	8	Si	-244.3	0.0	237.9

SOLLECITAZIONE :							
Caso	MZ	MY	MT	N	TZ	TY	
3-1	-176835.7	422.7	2315.3	-15.6	-13.0	TZ	2562.8
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Si	
3-1	151	3	Si	-570.8	0.0	570.8	
3-1	151	6	Tz	-565.1	-169.5	0.0	

SOLLECITAZIONE :						PROGR.		1.
Caso		MZ	MY	MT	N	TZ	TY	
3-1		-127480.1	-4.0	2173.9	14.8	-45.2	-1917.3	
3-1		-118185.1	-586.5	2433.9	-155.2	13.7	-1899.5	
TENSIONI								
Caso	Ve	No	massimi	Sx	Tz	Ty	Si	
3-1	151	2	Sx	389.6	0.0	0.0	389.6	
3-1	151	6	Tz	377.1	163.9	0.0	0.0	
3-1	151	9	Ty	-3.1	0.0	248.2	429.9	

3	-	2	1	21	13		Si	-249.3	0.0	237.9	481.6																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																													
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3-2	25	9	TY	-3.1	0.0	248.3	430.0
3-2	25	13	SI	-254.3	0.0	238.0	484.3
SOLLECITAZIONE :							PROGR. 4.
Caso	MZ	MY	MT	N	TZ	TY	
3-1	-126275.0	109.0	2173.9	14.8	-45.2	-1918.7	
3-1	-122955.8	-620.6	2433.9	-155.2	13.7	-1900.9	
TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Si	
3-1	151	3	SI	405.9	0.0	405.9	
3-1	151	6	TZ	-392.4	164.0	0.0	
3-1	151	9	TY	-3.1	0.0	248.3	
3-1	151	13	SI	-398.1	164.0	0.0	

3-1	2	Si	9	Tz	392.4	164.0	0.0	484.4
3-1	2	Si	6	Ty	0.0	-3.1	248.3	430.2
3-1	2	Si	7	Si	-398.1	164.0	0.0	489.0

SOLLECITAZIONE :								PROGR.	5.
Caso		MZ		MY	MT	N	TZ	TY	
3-1		-128673.7		165.5	2173.9	14.8	-45.2	-1919.3	
3-1		-125312.4		-637.7	2433.9	-155.2	13.7	-1901.6	

TENSIONI							
Caso	Ve	No	massimi	Sx	Tz	Ty	Si
3-1	151	3	Si	-414.1	0.0	0.0	414.1
3-1	151	6	Tz	-414.1	164.0	0.0	0.0
3-1	151	9	Ty	-3.1	0.0	248.3	0.0
3-1	151	13	Si	-405.8	164.0	0.0	0.0

3-1	Si	6	Sx	400.1	164.0	0.0	490.6
3-2	Si	7	Ty	-3.1	0.0	248.4	430.3
3-2	Si	7	Si	-405.8	164.0	0.0	495.3

SOLLECITAZIONE :							PROGR.	6.
Caso	MZ	MY	MT	N	TZ	TY		
3-1	-131073.3	222.0	2173.9	14.8	-45.2	-1920.0		
3-2	-127689.8	-654.8	2433.9	-155.2	13.7	-1902.3		
TENSIONI								
Caso	Ve	No	massimi	Sx	Tz	Si		
3-1	151	3	Si	-422.3	0.0	422.3		
3-1	151	6	Tz	-407.7	164.0	0.0		
3-1	151	9	Ty	-3.1	0.0	248.4		
3-1	151	13	Si	-413.5	164.0	0.0		

Case		MZ	MY	MT	N	TZ	TY
3-2	1	-5172.6	-202.4	15.6	-28.3	3.1	-816.7
3-2	1	-6955.1	-801.6	69.4	-13.5	13.9	-781.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-160.4	0.0	0.0	168.3	
3-2	1	4	160.4	18.2	0.0	163.5	
3-2	1	9	Tz	-0.6	0.0	73.0	
3-2	1	7	Si	-166.9	15.6	0.0	169.0
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-6518.9	-233.0	15.6	-28.3	3.1	-827.7
3-2	1	-6230.1	-1127.0	69.4	-13.5	13.9	-790.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-211.5	0.0	0.0	211.5	
3-2	1	4	211.5	0.0	0.0	204.3	
3-2	1	9	Tz	-0.6	0.0	73.8	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-7867.6	-303.7	15.6	-28.3	3.1	-894.7
3-2	1	-8806.6	-1572.8	69.4	-13.5	13.9	-879.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-253.2	0.0	0.0	255.2	
3-2	1	4	253.2	18.5	0.0	245.8	
3-2	1	9	Tz	-0.7	0.0	74.6	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-8224.4	-354.3	15.6	-28.3	3.1	-943.7
3-2	1	-9080.6	-1577.8	69.4	-13.5	13.9	-917.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-299.3	0.0	0.0	299.3	
3-2	1	4	299.3	18.7	0.0	289.3	
3-2	1	9	Tz	-0.7	0.0	75.4	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-10419.1	-1803.2	69.4	-13.5	13.9	-1017.1
TENSION							
Case	Vel	non-si	Sx	Tz	Ty	Si	
3-2	1	4	-343.9	0.0	0.0	343.9	
3-2	1	4	343.9	18.8	0.0	330.4	
3-2	1	9	Tz	-0.7	0.0	76.2	
3-2	1	7	Si	-209.7	15.8	0.0	212.5
PROGR.							
SOLLECAZIONE							
Case	MZ	MY	MT	N	TZ	TY	
3-2	1	-10016.8	-404.9	15.6	-28.3	3.1	-1027.7
3-2	1	-104					

Case	MZ	My	MT	N	Tz	Ty
3-1	-1507.7	75.4	-4608.1	N -2.3	Tz 41.6	Ty 1522.9
Case	W	no	miss			Si
3-1	5	Sx	-49.0	0.0	Ty	49.0
3-1	5	Tz	48.4	273.7	0.0	476.5
3-1	5	Ty	0.0	0.0	-285.9	495.2
3-1	5	Ty	-0.1	0.0	-285.9	495.2
PROGR.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-15174.6	23.4	-4608.1	N -2.3	Tz 41.6	Ty 1522.9
Case	W	no	miss			Si
3-1	5	Sx	-42.5	0.0	Ty	42.5
3-1	5	Tz	42.2	273.7	0.0	475.9
3-1	5	Ty	0.0	0.0	-285.8	495.1
3-1	5	Ty	-0.1	0.0	-285.8	495.1
PROGR.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-1127.1	-28.5	-4608.1	N -2.3	Tz 41.6	Ty 1522.9
Case	W	no	miss			Si
3-1	5	Sx	-36.4	0.0	Ty	36.4
3-1	5	Tz	36.0	273.7	0.0	475.3
3-1	5	Ty	-0.1	0.0	-285.8	495.0
PROGR.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-9369.0	-80.5	-4608.1	N -2.3	Tz 41.6	Ty 1521.6
Case	W	no	miss			Si
3-1	5	Sx	-30.8	0.0	Ty	30.8
3-1	5	Tz	29.8	273.6	0.0	474.9
3-1	5	Ty	-0.1	0.0	-285.7	494.9
PROGR.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-7467.5	-132.5	-4608.1	N -2.3	Tz 41.6	Ty 1520.9
Case	W	no	miss			Si
3-1	5	Sx	-25.2	0.0	Ty	25.2
3-1	5	Tz	23.6	273.6	0.0	474.5
3-1	5	Ty	-0.1	0.0	-285.7	494.8
PROGR.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-5566.9	-184.4	-4608.1	N -2.3	Tz 41.6	Ty 1520.2
Case	W	no	miss			Si
3-1	5	Sx	-19.5	0.0	Ty	19.5
3-1	5	Tz	17.4	273.6	0.0	474.2
3-1	5	Ty	-0.1	0.0	-285.6	494.7
PROGR.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-3667.1	-236.4	-4608.1	N -2.3	Tz 41.6	Ty 1519.5
Case	W	no	miss			Si
3-1	5	Sx	-13.9	0.0	Ty	13.9
3-1	5	Tz	11.2	273.6	0.0	474.0
3-1	5	Ty	-0.1	0.0	-285.5	494.6
PROGR.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-1768.2	-288.4	-4608.1	N -2.3	Tz 41.6	Ty 1518.8
Case	W	no	miss			Si
3-1	5	Sx	-8.3	0.0	Ty	8.3
3-1	5	Tz	5.0	273.6	0.0	473.9
3-1	5	Ty	-0.2	0.0	-285.5	494.5
PROGR.						
SOLICITAZIONE						
Case	MZ	My	MT	N	Tz	Ty
3-1	-315.6	-340.3	-4608.1	N -2.3	Tz 41.6	Ty 1518.1
Case	W	no	miss			Si
3-1	5	Sx	-5.1	0.0	Ty	5.1
3-1	5	Tz	-1.2	273.6	0.0	473.8
3-1	5	Ty	-0.2	0.0	-285.4	494.3
PROGR.						
VERIFICA STABILITA'						
Z	I(0 = 30.1)					
Z	I(2 = 10, I(0 = 6.78) Im = 1.5)Ncr=51740885.8IaI(0 = 30.40)k=1.0000					
Z	I(2 = 10, I(0 = 6.04) Im = 2.5)Ncr=184330846.8IaI(0 = 30.40)k=1.0000					
Case	3-1	Node	4	Node	5	
Nid =	-2.31	M2eq = -11309.0	M1eq = -255.2	Iss = -38.6	(0.007)	

VERIFICA NODI IN ACCIAIO:

VERIFICA TENSIONALE NODI: 40 - METODO DEGLI STATI LIMITE (NTC 2008)

UNITA' DI MISURA: [daN] ; [daNcm] ; [daN/cm2] ; [mm]

GEOMETRIA NODO

Profili utilizzati

Tipi prof.:
HERDO

Piastra e fazzoletti		h		b		e		r	
Num	Lz	Y	Sp	1	2	3	4	5	6
1	400	100	5	10	10	10	10	10	10
2(Y)	400	100	5						
3(2C)	95	100	5						

Tirafond (n° 4)		h		b		e		r	
Num	X	Y	F	Area	Num	X	Y	F	Area
1	350	50	14	115	3	350	350	14	115
2	50	50	14	115	4	50	350	14	115

Dimensioni			
1	1ft	11	r
300.	100.	250.	50.

SALDATURE (n° 40)		h		b		e		r	
Nome	Lung	Lato	Nome	Lung	Lato				
S1	134	6	S21	100	6				
S2	77.5	6	S22	100	6				
S3	100	6	S23	100	6				
S4	77.5	6	S24	100	6				
S5	124	6	S25	95	6				
S6	124	6	S26	95	6				
S7	200	6	S27	95	6				
S8	77.5	6	S28	100	6				
S9	190	6	S29	120	6				
S10	100	6	S30	100	6				
S11	100	6	S31	100	6				
S12	100	6	S32	100	6				
S13	100	6	S33	100	6				
S14	100	6	S34	100	6				
S15	95	6	S35	100	6				
S16	95	6	S36	100	6				
S17	95	6	S37	100	6				
S18	95	6	S38	100	6				
S19	190	6	S39	100	6				
S20	100	6	S40	100	6				

MATERIALI		Calcestruzzo C25/30	
Acciaio S 235 (re 360)			
fd=40mm	fd=40mm=80mm		
223.1	140		
Acciaio tirafond S 235 (re 360)			
1880			

SOLLECITAZIONE AGENTI E STATO TENSIONALE

Combinazione di sollecitazioni agenti Caso 6 As. 35 Nd. 40

N: -8630.7 Ty: 53.1 Tz: 33.9
Mc: 0 Mx: 8847 My: -4118

Verifica tirafond

Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)										
Co-3: Ft,Ed / Td,Rd										
Num	Fv,Ed	Fv,Rd	Fb,Rd	Ft,Ed	Ft,Rd	Bp,Rd	Td,Rd	Co-1	Co-2	Co-3/Ver
1	14.2	1987.2	8842.1	-14.3	1980.8	11400.2	3023.8	.01	0	.01 ST
2	14.2	1987.2	8842.1	-23.3	1980.8	11400.2	3023.8	.01	.01	.01 ST
3	14.2	1987.2	8842.1	-10.2	1980.8	11400.2	3023.8	.01	0	.01 ST
4	14.2	1987.2	8842.1	-19.1	1980.8	11400.2	3023.8	.01	.01	.01 ST

Verifica saldature

Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)		Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome	S_prip	Talpa	Talpa	Seq-1	Seq-2	Seq-1	Seq-2	Seq-1	Seq-2	Seq-1	Seq-2
S1	31.3	31.3	31.3	1997.5	2350.1						
S2	30.8	30.8	30.8	1997.5	2350.1						
S3	38.9	38.9	38.9	1997.5	2350.1						
S4	38.4	38.4	38.4	1997.5	2350.1						
S5	41.6	41.6	41.6	1997.5	2350.1						
S6	33.6	33.6	33.6	1997.5	2350.1						
S7	33.1	33.1	33.1	1997.5	2350.1						
S8	26	26	26	1997.5	2350.1						
S9	39.2	39.2	39.2	1997.5	2350.1						
S10	39.2	39.2	39.2	1997.5	2350.1						
S11	41.6	41.6	41.6	1997.5	2350.1						
S12	42.2	42.2	42.2	1997.5	2350.1						
S13	33	33	33	1997.5	2350.1						
S14	33.6	33.6	33.6	1997.5	2350.1						
S15	44.9	44.9	44.9	1997.5	2350.1						
S16	45.1	45.1	45.1	1997.5	2350.1						
S17	39.5	39.5	39.5	1997.5	2350.1						
S18	39.3	39.3	39.3	1997.5	2350.1						
S19	25.9	25.9	25.9	1997.5	2350.1						
S20	29.5	29.5	29.5	1997.5	2350.1						
S21	29.5	29.5	29.5	1997.5	2350.1						
S22	28.9	28.9	28.9	1997.5	2350.1						
S23	20.9	20.9	20.9	1997.5	2350.1						
S24	20.3	20.3	20.3	1997.5	2350.1						
S25	26	26	26	1997.5	2350.1						
S26	26.3	26.3	26.3	1997.5	2350.1						
S27	20.6	20.6	20.6	1997.5	2350.1						
S28	20.4	20.4	20.4	1997.5	2350.1						
S29	60.3	60.3	60.3	1997.5	2350.1						
S30	56.1	56.1	56.1	1997.5	2350.1						
S31	60.3	60.3	60.3	1997.5	2350.1						
S32	96.3	96.3	96.3	1997.5	2350.1						
S33	96.3	96.3	96.3	1997.5	2350.1						
S34	96.3	96.3	96.3	1997.5	2350.1						
S35	96.3	96.3	96.3	1997.5	2350.1						
S36	96.3	96.3	96.3	1997.5	2350.1						
S37	96.3	96.3	96.3	1997.5	2350.1						
S38	96.3	96.3	96.3	1997.5	2350.1						
S39	96.3	96.3	96.3	1997.5	2350.1						
S40	56.1	56.1	56.1	1997.5	2350.1						

Verifica tirafond

S3	32.1	.9	0.	32.1	32.1	1997.5	2350.	S1'
S6	33.6	.9	0.	33.6	33.6	1997.5	2350.	S1'
S7	33.1	.9	0.	33.1	33.1	1997.5	2350.	S1'
S8	26.	.9	0.	26.1	26.	1997.5	2350.	S1'
S10	39.2	.3	0.	39.2	39.2	1997.5	2350.	S1'
S11	41.6	.3	0.	41.6	41.6	1997.5	2350.	S1'
S12	42.2	.3	0.	42.2	42.2	1997.5	2350.	S1'
S13	22.	.3	0.	22.	22.	1997.5	2350.	S1'

Verifica saldature

S16	45.1	.9	0.	45.1	45.1	1997.5	2350.	SI'																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										</
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Verifica tirafond

\$24	20.3	.3	0.	20.3	20.3	1997.5	2350.	\$2'
\$25	26.	.9	0.	26.	26.	1997.5	2350.	\$2'
\$26	26.3	.9	0.	26.3	26.3	1997.5	2350.	\$2'
\$27	20.6	.9	0.	20.7	20.6	1997.5	2350.	\$2'
\$28	20.4	.9	0.	20.4	20.4	1997.5	2350.	\$2'
\$29	0.	135.6	60.3	148.4	60.3	1997.5	2350.	\$2'
\$30	56.1	62.1	60.3	103.1	116.3	1997.5	2350.	\$2'

S7	200.	7.	S27	144.	7.
S8	78.8	7.	S28	144.	7.
S9	124.6	7.	S29	150.	7.
S10	178.	7.	S30	150.	7.
S11	150.	7.	S31	150.	7.
S12	150.	7.	S32	150.	7.
S13	150.	7.	S33	150.	7.
S14	150.	7.	S34	150.	7.
S15	144.	7.	S35	150.	7.
S16	144.	7.	S36	150.	7.
S17	144.	7.	S37	150.	7.
S18	144.	7.	S38	150.	7.
S19	150.	7.	S39	150.	7.
S20	178.	7.	S40	150.	7.

MATERIALI				
Acciaio S 235 (R 360)				
f _{td} 40mmx50mm				
2238.1				
Acciaio tirafond S 275 (R 430)				
2200.				

SOLLECITAZIONE AGENTI E STATO TENSIONALE

Combinazione di sollecitazioni agenti Caso 6 As. 35. Nd. 978

N: -6527.5 Ty: 23.5 Tz: 60.1

Mt: 0 My: 9575 Mz: 10090

Verifica tirafond

Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)

Co-3: F _{t,Ed} / T _{ad,Ed}												
Num	P _{v,Ed}	P _{v,Rd}	F _{b,Rd}	F _{t,Ed}	F _{t,Rd}	F _{b,Rd}	T _{ad,Ed}	Co-1	Co-2	Co-3	Ver	
1	16.1	3240.5	13714.3	-38.1	4860.7	19543.2	3564.	0	0	.01	.01	.01
2	16.1	3240.5	13714.3	-26.7	4860.7	19543.2	3564.	0	.01	.01	.01	.01
3	16.1	3240.5	13714.3	-26.7	4860.7	19543.2	3564.	0	.01	.01	.01	.01
4	16.1	3240.5	13714.3	-34.	4860.7	19543.2	3564.	0	.01	.01	.01	.01

Verifica saldature

Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.78)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)												
Nome	S _{imp}	T _{alpa}	T _{alpe}	Seq-1	Seq-2	Seq-1	Seq-2	Ver				
S2	31.9	7.	31.9	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S3	35.4	7.	35.4	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S4	35.9	7.	35.9	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S5	38.4	7.	38.4	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S6	42.2	7.	42.2	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S7	42.7	7.	42.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S8	38.1	7.	38.1	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S9	42.7	7.	42.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S10	42.7	7.	42.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S11	35.4	7.	35.4	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S12	35.8	7.	35.8	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S13	48.2	7.	48.2	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S14	48.6	7.	48.6	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S15	40.8	7.	40.8	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S16	40.4	7.	40.4	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S17	47.3	7.	47.3	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S18	47.7	7.	47.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S20	35.7	7.	35.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S21	28.9	7.	28.9	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S22	28.5	7.	28.5	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S23	41.7	7.	41.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S24	41.4	7.	41.4	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S25	28.9	7.	28.9	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S26	28.5	7.	28.5	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S27	35.7	7.	35.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S28	35.9	7.	35.9	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S29	0.	119.9	58.6	131.4	58.6	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S30	81.7	68.7	131.8	140.4	140.4	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S31	0.	185.1	58.6	194.1	58.6	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S32	104.5	84.6	58.6	146.7	163.1	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S33	104.5	84.6	134.4	104.5	1997.5	2350.	1997.5	1997.5	2350.	1997.5	2350.	1997.5
S34	104.5	84.6	134.4	104.5	1997.5	2350.	1997.5	1997.5	2350.	1997.5	2350.	1997.5
S35	104.5	84.6	134.4	104.5	1997.5	2350.	1997.5	1997.5	2350.	1997.5	2350.	1997.5
S36	0.	252.5	80.1	264.9	80.1	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S37	81.7	78.3	80.1	137.7	161.8	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S38	0.	187.3	80.1	203.7	80.1	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S39	81.7	68.7	0.	106.8	81.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S40	81.7	68.7	0.	106.8	81.7	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5

Verifica piastra				
Smax f _{td} Ver				
72.7 2238.11St				

Verifica nervature				
Posizione Smax f _{td} Ver				
Z 312. 2238.11St				
Y 285.5 2238.11St				

Verifica pressione sul calcestruzzo				
Smax f _{td} Ver				
3.6 141.11St				

NOO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONE AGENTI Caso 6 As. 35. Nd. 978

Combinazione di sollecitazioni agenti Caso 3 As. 35. Nd. 978

N: -28482.5 Ty: 585.5 Tz: -91.3

Mt: 0 My: -9670 Mz: -60905

Verifica tirafond

Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)

Co-3: F _{t,Ed} / T _{ad,Ed}												
Num	P _{v,Ed}	P _{v,Rd}	F _{b,Rd}	F _{t,Ed}	F _{t,Rd}	F _{b,Rd}	T _{ad,Ed}	Co-1	Co-2	Co-3	Ver	
1	148.1	3240.5	13714.3	-142.8	4860.7	19543.2	3564.	.05	.03	.04	.01	.01
2	148.1	3240.5	13714.3	-135.4	4860.7	19543.2	3564.	.05	.03	.04	.01	.01
3	148.1	3240.5	13714.3	-95.3	4860.7	19543.2	3564.	.01	.02	.03	.01	.01
4	148.1	3240.5	13714.3	-87.9	4860.7	19543.2	3564.	.05	.02	.01	.02	.01

Verifica saldature

Seq-1, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.78)

Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)												
Nome	S _{imp}	T _{alpa}	T _{alpe}	Seq-1	Seq-2	Seq-1	Seq-2	Ver				
S1	171.1	6.5	171.1	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S2	178.1	1.	178.1	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S3	181.5	1.	181.5	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S4	174.	1.	174.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S5	171.	1.	171.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S6	136.4	1.	136.4	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S7	127.	1.	127.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S8	140.5	1.	140.5	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S10	172.5	6.5	172.5	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S11	168.4	6.5	168.4	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S12	208.1	6.5	208.1	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5	2350.	1997.5
S13	131.	6.5	131.1	131.	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S14	130.6	6.5	130.8	130.6	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S15	172.	1.	172.	172.	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S16	174.5	1.	174.5	174.5	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S17	132.6	1.	132.6	132.6	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S18	130.1	1.	130.1	130.1	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S20	179.8	6.5	179.9	179.8	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S21	215.	1.	215.1	215.	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S22	215.4	6.5	215.5	215.4	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5
S23	137.9	6.5	137.7	137.9	1997.5	2350.	2350.	1997.5	2350.	1997.5	2350.	1997.5

127/136

Verifica piastra			
Smax		fdlVer	
377.5	2238.1	St'	
Verifica nervature			
Smax		fdlVer	
502		2238.1	
Z		St'	
Y		437.8	
		2238.1	St'
Verifica pressione sul calcestruzzo			
Smax		fdlVer	
6,3		141,1	
		St'	

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 112 Nd. 734									
Combinazione di sollecitazioni agenti Caso 1 As. 112 Nd. 734									

N:	-8956.7	Ty:	30.2	Tz:	22.5				
Mt:	0	My:	5003	Mz:	20095				

Verifica tirafond									
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)									
Co-3: Ft,Ed / T ad,Rd									
Nome	Fv,Rd	Fv,Rd	Rb,Rd	Ft,Ed	Ft,Ed	Rb,Rd	T ad,Rd	Co-1 Co-2 Co-3 Ver	
1	9.4	3240.5	13734.3	-26.5	4860.7	19543.2	3564.	0., 0., 01.	01 St'
2	9.4	3240.5	13734.3	-30.4	4860.7	19543.2	3564.	0., 01.	01 St'
3	9.4	3240.5	13734.3	-42.2	4860.7	19543.2	3564.	0., 01.	01 St'
4	9.4	3240.5	13734.3	-46.	4860.7	19543.2	3564.	0., 01.	01 St'

Verifica saldature									
Seq-1, Seq-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)									
Seq-2, Seq-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)									
Nome	S,grp1	Tau,pel	Tau,pel	Seq-1	Seq-2	Seq-1	Seq-1	Seq-1	Seq-1
S1	52.	5.4	0.	32.5	32.	1997.5	2350.	157.	2350.
S2	29.3	8.	0.	29.3	29.3	1997.5	2350.	157.	2350.
S3	40.4	-8.	0.	40.4	40.4	1997.5	2350.	157.	2350.
S4	34.2	8.	0.	34.2	34.2	1997.5	2350.	157.	2350.
S5	54.	5.4	0.	32.	32	1997.5	2350.	157.	2350.
S6	37.4	-8.	0.	37.4	37.4	1997.5	2350.	157.	2350.
S7	48.5	-8.	0.	48.5	48.5	1997.5	2350.	157.	2350.
S8	42.3	-8.	0.	42.3	42.3	1997.5	2350.	157.	2350.
S9	37.2	5.4	0.	37.6	37.2	1997.5	2350.	157.	2350.
S10	37.2	5.4	0.	37.6	37.2	1997.5	2350.	157.	2350.
S11	57.	5.4	0.	101.5	101.4	1997.5	2350.	157.	2350.
S12	101.8	-5.4	0.	102.	101.8	1997.5	2350.	157.	2350.
S13	101.6	5.4	0.	101.7	101.6	1997.5	2350.	157.	2350.
S14	101.1	5.4	0.	101.3	101.1	1997.5	2350.	157.	2350.
S15	42.9	-8.	0.	42.9	42.9	1997.5	2350.	157.	2350.
S16	46.4	-8.	0.	46.4	46.4	1997.5	2350.	157.	2350.
S17	35.6	-8.	0.	35.6	35.6	1997.5	2350.	157.	2350.
S18	40.1	5.4	0.	40.1	40.1	1997.5	2350.	157.	2350.
S19	46.1	5.4	0.	46.1	46.1	1997.5	2350.	157.	2350.
S20	45.3	5.4	0.	45.6	45.3	1997.5	2350.	157.	2350.
S21	95.1	5.4	0.	95.1	95.1	1997.5	2350.	157.	2350.
S22	93.	5.4	0.	93.2	93.	1997.5	2350.	157.	2350.
S23	109.5	5.4	0.	109.6	109.5	1997.5	2350.	157.	2350.
S24	109.5	5.4	0.	109.5	109.5	1997.5	2350.	157.	2350.
S25	27.5	-8.	0.	27.5	27.5	1997.5	2350.	157.	2350.
S26	40.	-8.	0.	40.	40.	1997.5	2350.	157.	2350.
S27	50.	-8.	0.	50.	50.	1997.5	2350.	157.	2350.
S28	54.5	-8.	0.	54.5	54.5	1997.5	2350.	157.	2350.
S29	9.7	0.	0.	9.7	9.7	1997.5	2350.	157.	2350.
S30	14.9	201.2	97.7	224.2	112.6	1997.5	2350.	157.	2350.
S31	68.1	97.7	0.	68.1	68.1	1997.5	2350.	157.	2350.
S32	43.6	175.7	97.7	205.7	141.3	1997.5	2350.	157.	2350.
S33	43.6	175.7	0.	181.	43.6	1997.5	2350.	157.	2350.
S34	43.6	175.7	0.	181.	43.6	1997.5	2350.	157.	2350.
S35	43.6	175.7	0.	181.	43.6	1997.5	2350.	157.	2350.
S36	139.3	192.3	174.	401.3	186.3	1997.5	2350.	157.	2350.
S37	14.9	201.2	174.	244.8	186.3	1997.5	2350.	157.	2350.
S38	115.7	444.	174.	371.4	174.5	1997.5	2350.	157.	2350.
S39	14.9	201.2	0.	201.8	14.9	1997.5	2350.	157.	2350.
S40	14.9	201.2	0.	201.8	14.9	1997.5	2350.	157.	2350.

Verifica piastra			
	Smx	fdlVer	
138.3	2238.1	st'	

Verifica nervature			
Posizione	Smx	fdlVer	
Z	434.3	2238.1	st'
Y	379.8	2238.1	st'

Verifica pressione sul calcestruzzo									
Smex					fdlVer				
4.8 141.1 St'									

NODO VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 1 As. 112 Nd. 734									
Verifica tensione NODO: 742 - METODO DEGLI STATI LIMITE (NTC 2008)									

UNITA' DI MISURA: [daN] ; [daNm] ; [daNm/cm] ; [mm]									
GEOMETRIA NODO									
Profili utilizzati									
Tip prof.	h	b	a	e	r				
HEA100	190.	100.	6.5	10.	18.				

Piastra e fazzoletti									
Num	Lz	Lyl	Sp						
1	500.	480.	150.	6.					
2	300.	140.	150.	6.					

TIRAFONDI									
Tirafond (N° 4)									
Num	X	Y	F	Areal	Nm	F	Areal		
1	450.	50.	157.	1	450.	440.	16.	157.	
2	50.	50.	16.	157.	4	50.	440.	16.	157.

Dimensioni					
1	h	T	l1	r1	
1	400.	100.	50.	20.	
SALDATURE (n° 40)					
Nome	Lung	Lato	Nome	Lung	Lato
S1	134.	7.	S21	150.	7.
S2	78.8	7.	S22	150.	7.
S3	200	7.	S23	150.	7.
S4	78.8	7.	S24	150.	7.
S5	134.	7.	S25	144.	7.
S6	78.8	7.	S26	144.	7.
S7	200.	7.	S27	144.	7.
S8	78.8	7.	S28	144.	7.
S9			S29	150.	7.
S10	178.	7.	S30	150.	7.
S11	150.	7.	S31	150.	7.
S12	150.	7.	S32	150.	7.
S13	150.	7.	S33	150.	7.
S14	150.	7.	S34	150.	7.
S15	144.	7.	S35	150.	7.
S16	144.	7.	S36	150.	7.
S17	144.	7.	S37	150.	7.
S18	144.	7.	S38	150.	7.
S19			S39	150.	7.

S20	178.	7.	S40	150.	7.				
MATERIE									
Acciaio S 235 (Fe 360)					Calcestruzzo C25/30				
fcd s=40mm					fcd				
2238.1					141.1				
2238.1					12047.6				
Acciaio tirafondi S 275 (Fe 430)									
fcd									
2200.									

S51	29.61	12.51	0.	32.11	29.61	1997.51	2350.151*
S56	46.31	3.21	0.	46.41	46.31	1997.51	2350.151*
S71	46.21	3.21	0.	46.31	46.21	1997.51	2350.151*
S58	24.31	3.21	0.	24.61	24.31	1997.51	2350.151*
S10	48.31	12.51	0.	48.81	48.31	1997.51	2350.151*
S11	46.71	12.51	0.	48.31	46.71	1997.51	2350.151*
S12	48.71	12.51	0.	50.31	48.71	1997.51	2350.151*
S13	45.81	12.51	0.	48.71	45.81	1997.51	2350.151*
S14	47.81	12.51	0.	49.41	47.81	1997.51	2350.151*
S15	73.81	3.21	0.	73.91	73.81	1997.51	2350.151*
S16	73.91	3.21	0.	73.91	73.91	1997.51	2350.151*
S17	73.41	3.21	0.	73.41	73.41	1997.51	2350.151*
S18	73.41	3.21	0.	73.41	73.41	1997.51	2350.151*
S20	9.11	12.51	0.	15.41	9.11	1997.51	2350.151*
S131	11.41	8.51	0.	11.41	11.41	1997.51	2350.151*
S22	9.41	12.51	0.	15.71	9.41	1997.51	2350.151*
S23	10.51	12.51	0.	16.31	10.51	1997.51	2350.151*
S24	8.51	12.51	0.	15.11	8.51	1997.51	2350.151*
S25	16.61	3.21	0.	16.91	16.61	1997.51	2350.151*
S26	16.61	3.21	0.	16.91	16.61	1997.51	2350.151*
S27	17.11	3.21	0.	17.31	17.11	1997.51	2350.151*
S28	17.11	3.21	0.	17.41	17.11	1997.51	2350.151*
S29	0.1	26.41	0.	52.21	0.1	1997.51	2350.151*
S30	17.51	54.61	53.1	78.11	70.51	1997.51	2350.151*
S31	0.1	32.71	53.1	33.21	33.1	1997.51	2350.151*
S32	143.71	95.51	53.1	180.51	196.71	1997.51	2350.151*
S33	143.71	95.51	0.1	172.51	143.71	1997.51	2350.151*
S34	143.71	95.51	54.61	181.1	181.1	1997.51	2350.151*
S35	143.71	95.51	0.1	172.51	143.71	1997.51	2350.151*
S36	0.1	32.21	54.61	32.51	54.61	1997.51	2350.151*
S37	17.51	53.31	54.61	78.31	72.21	1997.51	2350.151*
S38	0.1	32.21	54.61	62.91	54.61	1997.51	2350.151*
S39	17.51	8.61	0.1	19.51	17.51	1997.51	2350.151*
S40	17.51	8.61	0.1	19.51	17.51	1997.51	2350.151*

Verifica piastra
Smax | fd|ver|
361.71 2238.1151*

Verifica nervature
Posizione | Smax | fd|ver|
Z | 361.71 2238.1151*
Y | 355.31 2238.1151*

Verifica pressione sul calcestruzzo
Smax | fd|ver|
4.61 141.1151*

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 175 Nd. 0

Combinazione di sollecitazioni agenti Caso 7 As. 175 Nd. 0

N: -2604 Ty: -641.7 Tz: -240.2
Mt: 0 Mt: 65881 Mt: 2735

Verifica tirafond
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)
Co-3: Ft,Ed / Tadm |
Num | Pv,Ed | Pv,Rd | Fb,Rd | Ft,Ed | Ft,Rd | Bp,Rd | Tadm,Rd | Co-1 | Co-2 | Co-3 | Ver|
1 | 171.31 3240.51 13714.31 | 171.11 4860.71 19543.21 | 3564.1 | .08 | .04 | .05151*
2 | 171.31 3240.51 13714.31 | -49.31 4860.71 19543.21 | 3564.1 | .05 | .01 | .01151*
3 | 171.31 3240.51 13714.31 | 164.41 4860.71 19543.21 | 3564.1 | .08 | .03 | .05151*
4 | 171.31 3240.51 13714.31 | -56.11 4860.71 19543.21 | 3564.1 | .05 | .01 | .02151*

Verifica saldature
Seq-1, SLim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)
Seq-2, SLim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)
Nome | S_pmp | Tadm | Tadm | Seq-1 | Seq-2 | SLim-1 | SLim-2 | Ver|
S1 | 13.61 1.71 | 0.1 | 15.41 | 13.61 | 1997.51 | 2350.151*
S2 | 9.51 2.61 | 0.1 | 9.81 | 9.51 | 1997.51 | 2350.151*
S3 | 36.21 2.61 | 0.1 | 36.31 | 36.21 | 1997.51 | 2350.151*
S4 | 36.31 2.61 | 0.1 | 36.41 | 36.31 | 1997.51 | 2350.151*
S5 | 16.21 2.11 | 0.1 | 17.71 | 16.21 | 1997.51 | 2350.151*
S6 | 38.11 2.61 | 0.1 | 38.11 | 38.11 | 1997.51 | 2350.151*
S7 | 38.21 2.61 | 0.1 | 38.21 | 38.21 | 1997.51 | 2350.151*
S8 | 10.21 2.61 | 0.1 | 10.61 | 10.21 | 1997.51 | 2350.151*
S10 | 40.11 7.11 | 0.1 | 40.61 | 40.11 | 1997.51 | 2350.151*
S11 | 35.61 3.51 | 0.1 | 35.61 | 35.61 | 1997.51 | 2350.151*
S12 | 38.11 7.11 | 0.1 | 38.81 | 38.11 | 1997.51 | 2350.151*
S13 | 39.11 7.11 | 0.1 | 39.71 | 39.11 | 1997.51 | 2350.151*
S14 | 41.61 7.11 | 0.1 | 41.61 | 41.61 | 1997.51 | 2350.151*
S15 | 70.61 2.61 | 0.1 | 70.71 | 70.61 | 1997.51 | 2350.151*
S16 | 70.51 2.61 | 0.1 | 70.61 | 70.51 | 1997.51 | 2350.151*
S17 | 72.41 2.61 | 0.1 | 72.41 | 72.41 | 1997.51 | 2350.151*
S18 | 72.51 2.61 | 0.1 | 72.61 | 72.51 | 1997.51 | 2350.151*
S20 | 11.51 7.11 | 0.1 | 11.51 | 11.51 | 1997.51 | 2350.151*
S21 | 10.61 7.11 | 0.1 | 12.81 | 10.61 | 1997.51 | 2350.151*
S22 | 13.11 7.11 | 0.1 | 14.91 | 13.11 | 1997.51 | 2350.151*
S23 | 7.11 7.11 | 0.1 | 10.11 | 7.11 | 1997.51 | 2350.151*
S24 | 9.61 7.11 | 0.1 | 12.11 | 9.61 | 1997.51 | 2350.151*
S25 | 43.91 2.61 | 0.1 | 44.11 | 43.91 | 1997.51 | 2350.151*
S26 | 44.11 2.61 | 0.1 | 44.11 | 44.11 | 1997.51 | 2350.151*
S27 | 42.11 2.61 | 0.1 | 42.21 | 42.11 | 1997.51 | 2350.151*
S28 | 42.11 2.61 | 0.1 | 42.11 | 42.11 | 1997.51 | 2350.151*
S29 | 0.1 35.31 | 21.1 | 35.31 | 21.1 | 1997.51 | 2350.151*
S30 | 21.1 22.91 | 21.1 | 37.41 | 21.1 | 1997.51 | 2350.151*
S31 | 0.1 306.21 | 21.1 | 306.91 | 21.1 | 1997.51 | 2350.151*
S32 | 186.41 109.91 | 21.1 | 217.41 | 207.41 | 1997.51 | 2350.151*
S33 | 186.41 109.91 | 0.1 | 216.41 | 186.41 | 1997.51 | 2350.151*
S34 | 186.41 109.91 | 16.11 | 217.11 | 207.51 | 1997.51 | 2350.151*
S35 | 186.41 109.91 | 0.1 | 216.41 | 186.41 | 1997.51 | 2350.151*
S36 | 0.1 326.91 | 16.11 | 327.31 | 16.11 | 1997.51 | 2350.151*
S37 | 21.1 27.61 | 37.11 | 37.11 | 27.61 | 1997.51 | 2350.151*
S38 | 0.1 132.81 | 16.11 | 133.81 | 16.11 | 1997.51 | 2350.151*
S39 | 21.1 11.91 | 0.1 | 21.11 | 21.11 | 1997.51 | 2350.151*
S40 | 21.1 11.91 | 0.1 | 24.11 | 21.11 | 1997.51 | 2350.151*

Verifica piastra
Smax | fd|ver|
460.1 2238.1151*

Verifica nervature
Posizione | Smax | fd|ver|
Z | 460.1 2238.1151*
Y | 425.91 2238.1151*

Verifica pressione sul calcestruzzo
Smax | fd|ver|
8.41 141.1151*

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 7 As. 175 Nd. 0

Combinazione di sollecitazioni agenti Caso 3 As. 175 Nd. 0

N: -3769.4 Ty: -791.1 Tz: -156.8
Mt: 0 Mt: -103362 Mt: -5829

Verifica tirafond
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)
Co-3: Ft,Ed / Tadm |
Num | Pv,Ed | Pv,Rd | Fb,Rd | Ft,Ed | Ft,Rd | Bp,Rd | Tadm,Rd | Co-1 | Co-2 | Co-3 | Ver|
1 | 201.61 3240.51 13714.31 | 201.71 4860.71 19543.21 | 3564.1 | .08 | .01 | .03151*
2 | 201.61 3240.51 13714.31 | 310.71 4860.71 19543.21 | 3564.1 | .11 | .06 | .09151*
3 | 201.61 3240.51 13714.31 | 74.91 4860.71 19543.21 | 3564.1 | .06 | .01 | .02151*
4 | 201.61 3240.51 13714.31 | 326.71 4860.71 19543.21 | 3564.1 | .11 | .07 | .09151*

Verifica saldature
Co-3: Ft,Ed / Tadm |

Seq-1, SLim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)
Seq-2, SLim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)
Nome | S_pmp | Tadm | Tadm | Seq-1 | Seq-2 | SLim-1 | SLim-2 | Ver|
S1 | 24.11 8.81 | 0.1 | 25.71 | 24.11 | 1997.51 | 2350.151*
S2 | 58.41 1.71 | 0.1 | 58.41 | 58.41 | 1997.51 | 2350.151*
S3 | 58.71 1.71 | 0.1 | 58.71 | 58.71 | 1997.51 | 2350.151*
S4 | 14.81 1.71 | 0.1 | 14.91 | 14.81 | 1997.51 | 2350.151*
S5 | 20.11 8.81 | 0.1 | 21.91 | 20.11 | 1997.51 | 2350.151*
S6 | 17.11 1.71 | 0.1 | 17.21 | 17.11 | 1997.51 | 2350.151*
S7 | 54.41 1.71 | 0.1 | 54.51 | 54.41 | 1997.51 | 2350.151*
S8 | 54.81 1.71 | 0.1 | 54.81 | 54.81 | 1997.51 | 2350.151*
S10 | 20.31 8.81 | 0.1 | 22.11 | 20.31 | 1997.51 | 2350.151*
S11 | 12.31 8.81 | 0.1 | 15.11 | 12.31 | 1997.51 | 2350.151*
S12 | 16.31 8.81 | 0.1 | 18.51 | 16.31 | 1997.51 | 2350.151*
S13 | 19.81 8.81 | 0.1 | 21.61 | 19.81 | 1997.51 | 2350.151*
S14 | 23.71 8.81 | 0.1 | 25.31 | 23.71 | 1997.51 | 2350.151*
S15 | 67.31 1.71 | 0.1 | 67.31 | 67.31 | 1997.51 | 2350.151*
S16 | 67.11 1.71 | 0.1 | 67.11 | 67.11 | 1997.51 | 2350.151*
S17 | 71.11 1.71 | 0.1 | 71.11 | 71.11 | 1997.51 | 2350.151*
S18 | 71.31 1.71 | 0.1 | 71.31 | 71.31 | 1997.51 | 2350.151*
S20 | 61.61 8.81 | 0.1 | 62.21 | 61.61 | 1997.51 | 2350.151*
S21 | 61.11 8.81 | 0.1 | 61.61 | 61.11 | 1997.51 | 2350.151*
S22 | 65.11 8.81 | 0.1 | 65.31 | 65.11 | 1997.51 | 2350.151*
S23 | 53.61 8.81 | 0.1 | 54.31 | 53.61 | 1997.51 | 2350.151*
S24 | 57.51 8.81 | 0.1 | 58.21 | 57.51 | 1997.51 | 2350.151*
S25 | 112.41 1.71 | 0.1 | 112.41 | 112.41 | 1997.51 | 2350.151*
S26 | 112.61 1.71 | 0.1 | 112.61 | 112.61 | 1997.51 | 2350.151*
S27 | 106.61 1.71 | 0.1 | 106.61 | 106.61 | 1997.51 | 2350.151*
S28 | 108.31 1.71 | 0.1 | 108.41 | 108.31 | 1997.51 | 2350.151*
S29 | 0.1 507.51 | 36.11 | 508.81 | 36.11 | 1997.51 | 2350.151*
S30 | 134.21 172.11 | 36.11 | 221.21 | 170.31 | 1997.51 | 2350.151*
S31 | 0.1 213.81 | 36.11 | 216.81 | 36.11 | 1997.51 | 2350.151*
S32 | 39.91 40.71 | 36.11 | 67.51 | 39.91 | 1997.51 | 2350.151*
S33 | 39.91 22.81 | 0.1 | 45.91 | 39.91 | 1997.51 | 2350.151*
S34 | 39.91 30.51 | 4.31 | 50.41 | 44.11 | 1997.51 | 2350.151*
S35 | 39.91 22.81 | 0.1 | 45.91 | 39.91 | 1997.51 | 2350.151*
S36 | 0.1 253.71 | 4.31 | 253.71 | 4.31 | 1997.51 | 2350.151*
S37 | 134.21 172.11 | 4.31 | 218.31 | 138.51 | 1997.51 | 2350.151*
S38 | 0.1 467.71 | 4.31 | 467.71 | 4.31 | 1997.51 | 2350.151*
S39 | 134.21 172.11 | 0.1 | 218.21 | 134.21 | 1997.51 | 2350.151*
S40 | 134.21 172.11 | 0.1 | 218.21 | 134.21 | 1997.51 | 2350.151*

Verifica piastra
Smax | fd|ver|
826.41 2238.1151*

Verifica nervature
Posizione | Smax | fd|ver|
Y | 826.41 2238.1151*
Z | 519.91 2238.1151*

Verifica pressione sul calcestruzzo
Smax | fd|ver|
14.21 141.1151*

NDD VERIFICATO IN BASE ALLA COMB. DI SOLLECITAZIONI AGENTI Caso 3 As. 175 Nd. 0

Combinazione di sollecitazioni agenti Caso 7 As. 116 Nd. 741

N: -4200.4 Ty: -381.3 Tz: 2.6
Mt: 0 Mt: -5829 Mt: 10362

Verifica tirafond
Co-1, Co-2: NTC 2008, 4.2.8.1.1 formula (4.2.65)
Co-3: Ft,Ed / Tadm |
Num | Pv,Ed | Pv,Rd | Fb,Rd | Ft,Ed | Ft,Rd | Bp,Rd | Tadm,Rd | Co-1 | Co-2 | Co-3 | Ver|
1 | 95.31 3240.51 13714.31 | 256.71 4860.71 19543.21 | 3564.1 | .07 | .05 | .07151*
2 | 95.31 3240.51 13714.31 | 271.11 4860.71 19543.21 | 3564.1 | .07 | .06 | .08151*
3 | 95.31 3240.51 13714.31 | -90.71 4860.71 19543.21 | 3564.1 | .03 | .01 | .03151*
4 | 95.31 3240.51 13714.31 | -76.41 4860.71 19543.21 | 3564.1 | .03 | .02 | .02151*

Verifica saldature
Seq-1, SLim-1: NTC 2008, 4.2.8.2.4 formula (4.2.78)
Seq-2, SLim-2: NTC 2008, 4.2.8.2.4 formula (4.2.79)
Nome | S_pmp | Tadm | Tadm | Seq-1 | Seq-2 | SLim-1 | SLim-2 | Ver|
S1 | 69.11 4.21 | 0.1 | 69.11 | 69.11 | 1997.51 | 2350.151*
S2 | 8.51 0.1 | 0.1 | 8.51 | 8.51 | 1997.51 | 2350.151*
S3 | 16.71 0.1 | 0.1 | 16.71 | 16.71 | 1997.51 | 2350.151*
S4 | 10.91 0.1 | 0.1 | 10.91 | 10.91 | 1997.51 | 2350.151*
S5 | 48.81 4.21 | 0.1 | 49.11 | 48.81 | 1997.51 | 2350.151*
S6 | 54.51 0.1 | 0.1 | 54.51 | 54.51 | 1997.51 | 2350.151*
S7 | 62.71 0.1 | 0.1 | 62.71 | 62.71 | 1997.51 | 2350.151*
S8 | 56.91 0.1 | 0.1 | 56.91 | 56.91 | 1997.51 | 2350.151*
S10 | 55.21 4.21 | 0.1 | 55.41 | 55.21 | 1997.51 | 2350.151*
S11 | 75.71 4.21 | 0.1 | 73.81 | 73.71 | 1997.51 | 2350.151*
S12 | 75.91 4.21 | 0.1 | 74.11 | 73.91 | 1997.51 | 2350.151*
S13 | 115.71 4.21 | 0.1 | 115.81 | 115.71 | 1997.51 | 2350.151*
S14 | 115.51 4.21 | 0.1 | 115.61 | 115.51 | 1997.51 | 2350.151*
S15 | 15.51 0.1 | 0.1 | 15.51 | 15.51 | 1997.51 | 2350.151*
S16 | 19.81 0.1 | 0.1 | 19.81 | 19.81 | 1997.51 | 2350.151*
S17 | 54.31 0.1 | 0.1 | 54.31 | 54.31 | 1997.51 | 2350.151*
S18 | 58.51 0.1 | 0.1 | 58.51 | 58.51 | 1997.51 | 2350.151*
S19 | 59.61 4.21 | 0.1 | 59.81 | 59.61 | 1997.51 | 2350.151*
S21 | 69.81 4.21 | 0.1 | 69.91 | 69.81 | 1997.51 | 2350.151*
S22 | 69.51 4.21 | 0.1 | 69.71 | 69.51 | 1997.51 | 2350.151*
S23 | 119.71 4.21 | 0.1 | 119.81 | 119.71 | 1997.51 | 2350.151*
S24 | 119.91 4.21 | 0.1 | 120.11 | 119.91 | 1997.51 | 2350.151*
S25 | 12.31 0.1 | 0.1 | 12.31 | 12.31 | 1997.51 | 2350.151*
S26 | 12.61 0.1 | 0.1 | 12.61 | 12.61 | 1997.51 | 2350.151*
S27 | 61.51 0.1 | 0.1 | 61.51 | 61.51 | 1997.51 | 2350.151*
S28 | 65.71 0.1 | 0.1 | 65.71 | 65.71 | 1997.51 | 2350.151*
S29 | 0.1 101.61 | 22.91 | 102.21 | 22.91 | 1997.51 | 2350.151*
S30 | 57.41 232.41 | 22.91 | 57.41 | 232.41 | 1997.51 | 2350.151*
S31 | 0.1 232.21 | 22.91 | 233.41 | 22.91 | 1997.51 | 2350.151*
S32 | 43.41 163.51 | 0.1 | 43.41 | 163.51 | 1997.51 | 2350.151*
S33 | 43.41 163.51 | 0.1 | 43.41 | 163.51 | 1997.51 | 2350.151*
S34 | 43.41 163.51 | 220.41 | 227.91 | 263.81 | 1997.51 | 2350.151*
S35 | 43.41 163.51 | 0.1 | 43.41 | 163.51 | 1997.51 | 2350.151*
S36 | 0.1 474.41 | 220.41 | 523.11 | 220.41 | 1997.51 | 2350.151*
S37 | 57.41 102.41 | 220.41 | 277.91 | 108.21 | 1997.51 | 2350.151*
S38 | 0.1 515.11 | 220.41 | 560.31 | 220.41 | 1997.51 |

3.2 Report Grafico

